

MEMORANDUM

P L A N N I N G D E P A R T M E N T T O W N O F C U M B E R L A N D , M A I N E

Date: August 15, 2018

To: Cumberland Planning Board From: Carla Nixon, Town Planner

Subject: OceanView at Cumberland Major Subdivision Final Review

The applicants were hopeful that the MDEP permits would be issued by the meeting date, however that is not looking likely. There are still some outstanding engineering issues that need to be addressed so it will be likely that following the presentation and public hearing, the Board will need to table this until the September 18th meeting.

Date August 15, 2018

To Town of Cumberland Planning Board

From Carla Nixon, Town Planner

Subject Major 52 Unit Major Subdivision, Final Review: OceanView at Cumberland –

277 Tuttle Road

I. REQUEST/OVERVIEW:

The applicant is Oceanview at Cumberland, LLC. The applicant is requesting Final Subdivision Review of a proposed major subdivision; there will be 52 single family "cottage" homes and 1 community center. The project access point will be at 277 Tuttle Road, approximately 250' south of Town Hall. The project will be served by public water and sewer and natural gas. The parcels are shown on Tax Assessor Map R 04, lots 4E, 4B, 4D & 5 in the Rural Residential 1 (RR 1) zoning district. Frederic Licht, P.E. of Licht Environmental Design, LLC is the Applicant's representative. Jeffrey Read, P.E. of Sevee and Maher Engineers reviewed the plans for the Town of Cumberland.

II. PROJECT HISTORY:

Sketch Plan Review: 10/17/17

Site Walk: 11/3/17 (did not include the Allen property)

<u>February 20, 2018:</u> Preliminary Subdivision Review. Tabled by Board.

March 20, 2018: Preliminary Subdivision Review approved by Planning Board.

III. DESCRIPTION:

Parcel size: 36.56 acres

Net Residential Density: Not required for developments in the SHC Overlay district.

Proposed # of units: 52, plus a community center.

Zoning: Rural Residential 1 with a Senior Housing Community Overlay

Development Type: Clustered Subdivision Design

Right, Title or Interest: Applicant has closed on the 3 subject parcels and deeds have been submitted.

Min. Lot Size: RR 1 requires a 4 acre minimum lot size; the SHC Overlay requires a 5 acres minimum

total parcel lot size. The proposed project site is 36.83 acres.

Setbacks: 20' between structures; 25' from edge of roads;

Parking: 2 spaces per unit required;

Buffering: 50' undisturbed buffer along entire perimeter of site.

Water & Sewer: Portland Water District

Electricity: Central Maine Power

Natural Gas: Summit Gas

Open Space: 20% required, 78% provided.

Wetlands: 12,700' of wetland fill (including stream crossings)

Trails: Shown on plans and reviewed by Lands & Cons. Comm.

Utilities: Underground electric, telephone, cable, gas, water and sewer from Tuttle Road.

Street Lighting: For street intersections and along roadways at "key locations".

Road: 22' wide paved main road (Little Acres Drive) will extend approximately 1500' from

Tuttle Rd; with a 5'esplanade and 5'sidewalk on right side.

Road will be constructed to municipal standards for a Residential Sub-collector Road.

25 mph speed limit posted.

Homeowners Association: Draft homeowners' documents are required for final submission.

Floodplain Map Classification: Zone C – area of minimal flooding; Map # 230005C0536F

Fire Protection: Public water. 4 hydrant locations. Units to have sprinklers

Waiver Granted (2/21/18): To show trees over 10" in diameter.

Outside Agency Approvals Required:

Agency	Type of Permit	Status
MDEP	Site Location of Dev.	
	Permit (SLODA)	
MDEP	NRPA Tier 1 permit	
US Army Corp of Engineers	(wetlands) permit	
MDOT	Traffic Movement Permit	
MDOT	Entrance Permit	On file, dated 3/16/18
Maine Natural Areas Program	Rare Botanical Data	Letter dated 5/25/17
Maine Historic Preservation	Historic Properties	Letter dated 6/27/17
Commission	_	
Maine Dept. Inland Fisheries &	Habitat Data	Letter dated 6/14/17
Wildlife		

IV. REVIEW COMMENTS:

DEPARTMENT HEAD REVIEWS:

William Longley, CEO: No comments

Police Chief Charles Rumsey: No comments

Fire Chief Small: The proposed automatic fire protection sprinkler systems must conform to the code requirements of the State of Maine Fire Marshal's Office. It is recommended, *but not required*, to have monitored fire alarm systems in each residence. It is recommended, *but not required*, to have fire department approved key boxes on each residence.

CUMBERLAND LANDS & CONSERVATION COMMITTEE: All comments have been addressed.

TOWN PLANNER COMMENTS DATED AUGUST 13, 2018

Carla:

See responses below in blue. Please let us know if you have any additional comments.

Best Rick

From: Carla Nixon [mailto:cnixon@cumberlandmaine.com]

Sent: Monday, August 13, 2018 2:24 PM

To: rick licht Cc: Jeffrey Read

Subject: Planner's Comments for Ocean View

Hi Rick,

A few items to respond to please.

Thanks. Carla

TOWN PLANNER'S REVIEW: 8-13-18:

- 1. Photometric plan missing. Light fixture locations are shown on plans and appear to be excessive with overhead street lights, front lawn pole lights and wall mounted lights at each unit door entrance. Night Sky concerns? Carla: We omitted Plan ES-1 Photometric Plan as an oversight. It was included in the Prelim Plan Set. See copy attached. The focus is indeed on Dark Sky ideals. The Beacon Full-Cut off Street Fixtures with LED lights meet the IDA cut off standards. The Individual driveway lights while not cut off are low wattage and provide ambient night lighting without creating a large "glare". The residents of OceanVIew Falmouth have found these to be pleasing. The wall mounts at the front entry are typical for any home and are recessed into the ceiling so there is no spillover and the other light fixture matching the post light is mounted at the garage. Again very subtle. The unit lights do not create spillover beyond the unit itself.
 - We will add the Photometric Plan Es-1 to the Town Link for the Final Plan Submission.
- 2. Typos noticed in the following locations: Note 16 on S-4 ("does includes"); Sheets C33 and 34 (Portland Water District"). We will fix typos for the final Mylar. Thanks for picking up.
- 3. DOT Entrance Permit and Traffic Movement Permit: Status? Required? Attached. Submitted on March 16th. Copy Attached for ease of accessing.
- 4. On Sheet C1 there are small green circles shown with no legend reference. Meaning? These are simply surveyed pine trees (Along Tuttle Road and the beginning of Little Acres Drive) as a file layer. Not important to the Phasing plan.
- 5. On Sheet C 2, what do orange dashes depict? The orange dashes are the 6-8 foot Trail Type C shown on the Trail and Walk Masterplan C-12. Also the Green Dash refers graphically to the Snowmobile/multi use trail type F on the Trails plan C-12.
- 6. Note 11 on S-4 does not include all the roads in the subdivision as requiring access and utility easements. Why? The note references the streets which have utility easements for the various utility companies (Summit NG, CMP, TWCTV, Fairpoint and PWD) Each street is noted with the width of the easement and noted that PWD does NOT require easements on Ivy, Azalea, Honeysuckle and Lilac). **Perhaps we should remove the word "Access" and just leave as "Utility" easements and reference the access easement over the 490 ft +/- of the Allen Front lot separately as there are no real access easements over the roads as the internal roads and drives are private and under the ownership of OV at Cumberland LLC and residents have full use of all of the underlying land.

TOWN ENGINEER'S REVIEW: Jeffrey Read, P.E., Sevee & Maher Engineers. 8-15-18:

As requested, Sevee & Maher Engineers, Inc. (SME) has completed a review of the comment responses submitted for the final application for a Major Subdivision and Site Plan for the proposed OceanView at Cumberland senior living community located off Tuttle Road. This submission is identified by the applicant as Revised Final Subdivision Plan Submittal. The application materials received by SME were prepared by LICHT Environmental Design, LLC (LICHT), and consist of the following:

- Cover letter report by Frederic Licht, P.E., L.S.E, dated July 31, 2018;
- Major Subdivision Final Plan Review Checklist;
- MEDEP and US ACOE emails:
- Exhibits 1 through 8 prepared by LICHT outlining the Tax Map Locus; Conveyance Plan; Right, Title & Interest; Snowmobile Trail License Draft; Utility Letters; Stormwater Maintenance Agreement; lighting cut sheets; and response to SME comments from March 12, 2018;
- Final Subdivision Plans, Revision 6, dated July 31st, 2018;
- Stormwater Management Report dated March 1, 2018;
- Pre-Development Drainage Plan dated May 4, 2018; and
- Post-Development Drainage Plan dated June 15, 2018.

PROJECT DESCRIPTION

The Applicant received Preliminary Major Subdivision approval on March 20, 2018 for a 52-unit senior living facility on a combined 36.83-acre parcel currently owned by Richard Doane and Laurence Allen. The parcel is located off Tuttle Road in Cumberland, across the street from the Town of Cumberland (Town) Municipal Office. The development will be accessed by a proposed private roadway constructed in accordance with Town residential sub-collector roadway standards as outlined in Article VI and Table 2 of Chapter 250, Subdivision of Land, of the Cumberland Code. The subdivision will be served with public utilities, including water, sewer, natural gas, electric, telephone, and cable.

PEER REVIEW COMMENTS DATED MARCH 12, 2018

The project was reviewed as a Major Subdivision as outlined in Chapter 250 - Subdivision of Land of the Town of Cumberland Ordinances, most recently amended and adopted on January 12, 2011, and Chapter 229 - Site Plan Review, most recently amended and adopted on March 26, 2012. The comments and responses below relate to the appropriate Ordinance Sections.

Chapter 250: Subdivision of Land

SME has reviewed comment responses provided by the Applicant and applicable sections of Chapter 250 and has provided comments for those sections not found to be addressed by the Application. The remaining sections have been reviewed and found to comply with Chapter 250 requirements.

Section 250-1(P) – River, stream or brook

1. There are two stream crossings associated with the proposed development. Please submit additional detail regarding the proposed construction, including any State or Federal Permit approvals, for review prior to final approval.

The Applicant intends to provide vendor supplied design details for wall construction prior to installation. Permit applications are currently under review by MEDEP. The USACOE permit was received on August 14, 2018.

Section 250-19 – Review and approval by other agencies

- 2. SME understands the following permit applications are underway for the project and applications will be filed with appropriate agencies following submittal of the preliminary subdivision and site plan application:
 - Maine Department of Environmental Protection (MEDEP) Site Location of Development Act (SLODA) permit,
 - MEDEP Natural Resources Protection Act (NRPA) Tier 1 permit for proposed wetland impacts,
 - Cumberland County Soil and Water Conservation District (CCS&WCD) stormwater and erosion control review, and

Where review and approval of any subdivision or site plan by any other governmental agency is required, approvals shall be submitted to the Planning Board in writing prior to the submission of the final plan.

MEDEP SLODA and MEDEP NRPA permit applications are currently under review by MEDEP.

Section 250-27 - Utilities

 Design details for utility pipes and conduits are not included in the project plan set. SME recommends sizes of all utilities pipes and additional design information be provided with the final plan application.

There are some overlapping tables on sheet C-13A. Please verify the Pipe Table is complete and not missing any information.

Chapter 229: Site Plan Review

SME has reviewed the application for conformance with the applicable sections of Chapter 229 and has no further comment.

General Comments

- 4. Erosion Control Notes C16 SME recommends the applicant update the Construction Plan Notes to reflect the current project.
- 5. SME recommends the applicant update the Construction Plan Notes to reflect the current project schedule.
- 6. Misc. Details C19 SME recommends the applicant update the Trench Repair Detail to reflect current Town pavement sections.
- 7. SME recommends the trench repair and pavement butt joint details be adjusted to reflect Town standards.
- 8. Stormwater Management Report, Page 4, Focal Point Proprietary System This section references 500 feet of gutter line flow. Section 250-40, B(4) outlines 300 feet as the maximum length for stormwater in a street gutter prior to intake at a catch basin. SME recommends the Applicant adjust the length of flow or request a waiver prior to final approval.

- 9. Gutter line between CB-2A and CB-3 exceeds 300 feet. SME Recommends the Applicant address this item prior to final approval.
- 10. Stormwater Management Report, Page 4, Forested Buffer Please verify that wetland buffers outlined on the plan qualify as stormwater treatment based on length, grade and soil type. If approved for treatment by MEDEP, SME recommends adding required sign details and boundary information to the plan set.
- 11. It is not clear if the DEP Forested Buffers outlined on the Subdivision Plat qualify as stormwater treatment based on length, grade and soil type. We anticipate MEDEP will require this prior to issuance of the SLODA permit.
- 12. Stormwater Management Report, Page 5, Arctic Fox Wet Pond Design Criteria Please verify above pool and below pool treatment volume calculations.
- 13. SME Recommends the Applicant address this item prior to final approval.
- 14. Stormwater Management Report, Page 6, Mallard Way Wet Pond Design Criteria Please verify above pool and below pool treatment volume and provided storage calculations.
- 15. SME Recommends the Applicant address this item prior to final approval.
- 16. Stormwater Management Report, Page 7, Post Area Summary and General Standard Calculation Please verify total area calculations. The sum of component areas does not appear to match the total area.
- 17. SME Recommends the Applicant address this item prior to final approval.
- 18. Exhibit 3 Please update site footprint to reflect inclusion of the Allen Property.
- 19. SME recommends the Applicant address this item prior to final approval.
- 20. Pre-Development Drainage Plan SME recommends the plan be updated to include the full drainage area and subcatchment boundaries, soil boundaries, and topography outside the project area. Labels for 18R and 55R are missing from the plan sheet.
- 21. SME Recommends the Applicant address this item prior to final approval.
- 22. Post Development Drainage Plan SME recommends the plan be updated to include the full drainage area and subcatchment boundaries, soil boundaries, and topography outside the project area. Labels for 15S, 51S, and 51P are missing from the plan sheet.
- 23. SME recommends the Applicant address this item prior to final approval.
- 24. The gravel trench outlets for Mallard Way and Arctic Fox Drive wet ponds are not modeled. SME will complete a more thorough review with the final plan submission.
- 25. SME Recommends the Applicant address this item prior to final approval.

- 26. The elevations for the Cultec separator row are not consistent with the stormwater model. SME will complete a more thorough review with the final plan submission.
- 27. SME Recommends the Applicant address this item prior to final approval.

New Comments

- 28. On sheet S-1 and throughout the plan set, the proposed multi use trail is shown passing through the DEP Meadow buffer for stormwater treatment. According to MEDEP standards, buffers should not be traversed by all-terrain vehicles or other vehicles. Activities within buffers should be conducted so as not to damage vegetation, disturb any organic duff layer, or expose soil.
- 29. On sheet C-8, Little Acres Drive profile section at STA 38+75 appears to have some information overlaid onto the profile section that makes that portion of the plan difficult to interpret. Please clarify.
- 30. On sheet C-9, Low Station and Low Elevation information are missing at STA 51+84.47 and STA 58+09.32.
- 31. On sheet C-10, Low Station and Low Elevation information are missing at STA 43+45.6.
- 32. Sheet C-9 does not include a plan view for Azalea Lane.
- 33. Sheet C-13, Road Construction Note 4, SME recommends the Applicant provide additional information for fabric under road base when clay is encountered.
- 34. Sheet C-13, Verizon Notes should be coordinated with utility providers outlined on Sheet C-0.
- 35. Sheet C-13, the bituminous concrete walk detail does not conform to Town performance standards outlined in Section 250, Attachment 2, Table 3. Please update the pavement materials and thicknesses to reflect current Town standards.
- 36. Sheet C-13A, the bottom of the Pipe Table appears to be cut off. Please verify there is no information missing.
- 37. Sheet C-14, SME recommends the Typical Stormwater Buffer Sign identify the area as a stormwater buffer and include a note to outline size and spacing requirements per MEDEP standards.
- 38. Erosion Control Notes C16 SME recommends the applicant update the Construction Plan Notes to reflect the current project schedule.
- 39. Sheet C-28, R-Tank dimensional data for FP-2 is incomplete.
- 40. The plan set submitted to the Town should be updated to include copies of plan sheets C-28, C-29, and C-30 signed and sealed by a registered professional engineer.
- 41. Throughout the plan set, a significant amount of information is overlaid on top of other information, making it difficult to interpret stationing, utility information, site layout, etc. SME recommends revising the plans to provide clear, consistent information.

Please call me with any questions, or if you would like, I could meet with you to discuss our comments.

Sincerely, SEVEE & MAHER ENGINEERS, INC.

Jeffrey T. Read, P.E. Civil Engineer/Project Manager

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V. SUBDIVISION REVIEW:

PROPOSED FINDINGS OF FACT - Chapter 250 - Subdivision of Land

The purpose of these standards shall be to assure the comfort, convenience, safety, health and welfare of the people, to protect the environment and to promote the development of an economically sound and stable community. To this end, in approving subdivisions within the Town of Cumberland, Maine, the Board shall consider the following criteria and before granting approval shall determine that the proposed subdivision:

- 1. <u>Pollution</u>. The proposed subdivision will not result in undue water or air pollution. In making this determination, it shall at least consider:
 - A. The elevation of the land above sea level and its relation to the flood plains;
 - B. The nature of soils and subsoil and their ability to adequately support waste disposal;
 - C. The slope of the land and its effect on effluents;
 - D. The availability of streams for disposal of effluents; and
 - E. The applicable state and local health and water resource rules and regulations;

The parcel is above sea level and not within a floodplain. The project will use public water and sewer. A groundwater impact assessment was provided by the applicant and reviewed and approved by the Town Engineer.

Based on the information provided, the standards of this section have been met.

2. <u>Sufficient Water</u>. The proposed subdivision has sufficient water available for the reasonable foreseeable needs of the subdivision;

The subdivision will be served by public water. There is a letter on file, dated July 31, 2018, from the Portland Water District stating the District's ability to serve the proposed project.

Based on the information provided, the standards of this section have been met.

3. <u>Municipal Water Supply</u>. The proposed subdivision will not cause an unreasonable burden on an existing water supply, if one is to be used;

The subdivision will utilize a municipal water source. There is a letter on file, dated July 31, 2018, from the Portland Water District stating the District's ability to serve the proposed project.

Based on the information provided, the standards of this section have been met for preliminary plan approval.

4. <u>Erosion</u>. The proposed subdivision will not cause unreasonable soil erosion or a reduction in the land's capacity to hold water so that a dangerous or unhealthy condition results;

The applicant has submitted an erosion and sedimentation control plan that is consistent with the current Maine Erosion and Sediment Control Best Management Practices. This plan has been reviewed and approved by the Town Engineer.

Based on the information provided, the standards of this section have been met.

5. <u>Traffic</u>. The proposed subdivision will not cause unreasonable highway or public road congestion or unsafe conditions with respect to the use of the highways or public roads existing or proposed;

A traffic study was performed by Maine Traffic Resources and reviewed and approved by the Town Engineer. An MDOT Entrance permit is required for final plan submission.

Based on the information provided, the standards of this section have been met for preliminary plan approval.

6. <u>Sewage disposal</u>. The proposed subdivision will provide for adequate sewage waste disposal and will not cause an unreasonable burden on municipal services, if they are utilized;

The project will utilize public sewer. A letter indicating there is sufficient capacity is on file from both the Portland Water District and the Town of Falmouth. There is a letter dated 5/22/18 from Town Manager Bill Shane stating that the Town agrees to accept the sewer design flow from the project. A charge of \$500 for each of the units will be charged to the applicant.

Based on the information provided, the standards of this section have been met for preliminary plan approval.

7. <u>Municipal solid waste disposal</u>. The proposed subdivision will not cause an unreasonable burden on the municipality's ability to dispose of solid waste, if municipal services are to be utilized;

Cumberland provides curbside trash collection and recycling through a contracted waste hauler. Based on a conversation with the Director of Public Services, the addition of 52 new homes will not cause a burden on the municipality's ability to dispose of solid waste.

Based on the information provided, the standards of this section have been met.

8. <u>Aesthetic, cultural and natural values</u>. The proposed subdivision will not have an undue adverse effect on the scenic or natural beauty of the area, aesthetics, historic sites, significant wildlife habitat identified by the Department of inland Fisheries and Wildlife or the municipality, or rare and irreplaceable natural areas or any public rights for physical or visual access to the shoreline;

Letters are on file from the relevant state agencies stating that the subdivision will not have an undue adverse effect on the scenic or natural beauty of the area, aesthetics, historic sites, significant wildlife habitat or rare and irreplaceable natural areas.

Based on the information provided, the standards of this section have been met.

9. <u>Conformity with local ordinances and plans.</u> The proposed subdivision conforms to a duly adopted subdivision regulation or ordinance, comprehensive plan, development plan or land use plan, if any. In making this determination, the municipal reviewing authority may interpret these ordinances and plans;

The plans have been reviewed by the town planner, the town engineer and town department heads. There are outstanding issues that have been raises by the Town Planner and Town Engineer.

Based on the information provided, the standards of this section have not yet been met.

10. <u>Financial and technical capacity</u>. The subdivider has adequate financial and technical capacity to meet the standards of this section;

Technical capacity is evidenced by the use of the following experts: a professional engineer, a licensed land surveyor, a traffic engineer and a licensed soils scientist.

Evidence of financial capacity is evidenced by a letter dated 12/20/17 from SIS Bank stating that developer has solid financial capacity and that the bank has approved financing for the acquisition, infrastructure development, and home construction for the project.

Based on the information provided, the standards of this section have been met for preliminary plan approval.

11. Surface waters; outstanding river segments. Whenever situated entirely or partially within the watershed of any pond or lake or within 250 feet of any wetland, great pond or river as defined in Title 38 chapter 3, subchapter I, article 2-B, the proposed subdivision will not adversely affect the quality of that body of water or unreasonably affect the shoreline of the body of water;

The proposed subdivision will not adversely affect the quality of the mapped wetlands or unreasonably affect the shoreline of the stream on the parcel. Plans include a MEDEP 75' stream setback to protect the resource.

Based on the information provided, the standards of this section have been met.

<u>12.</u> <u>Ground water.</u> The proposed subdivision will not alone, or in conjunction with, existing activities, adversely affect the quality or quantity of ground water;

The project will not utilize any groundwater from wells. Infiltration of stormwater is limited to the installation of BMP's along the access road which meet all DEP standards for treatment of stormwater prior to discharge of groundwater.

Based on the information provided, the standards of this section have been met.

13. Flood areas. Based on the Federal Emergency Management Agency's Flood Boundary and Floodway Maps and Flood Insurance Rate Maps, and information presented by the applicant whether the subdivision is in a flood-prone area. If the subdivision, or any part of it, is in such an area, the subdivider shall determine the 100-year flood elevation and flood hazard boundaries within the subdivision. The proposed subdivision plan must include a condition of plan approval requiring that principal structures in the subdivision will be constructed with their lowest floor, including the basement, at least one foot above the 100-year flood elevation;

The parcel is shown on FEMA floodplain maps as being in Zone C (area of minimal flooding). Based on the information provided, the standards of this section have been met.

14. Storm water. The proposed subdivision will provide for adequate storm water management;

A stormwater management plan was submitted as part of the application packet and has been reviewed and approved by the Town Engineer for conformance with Chapter 250-38 of the Cumberland Subdivision Ordinance. The stormwater plan is being reviewed by the MDEP. Based on the information provided, the standards of this section have not yet been met.

15. <u>Freshwater wetlands</u>. All potential freshwater wetlands, as defined in 30-A M.R.S.A. §4401 (2-A), within the proposed subdivision have been identified on any maps submitted as part of the application, regardless of the size of these wetlands. Any mapping of freshwater wetlands may be done with the help of the local soil and water conservation district.

All wetlands within the proposed subdivision have been delineated and mapped by Mark Hampton Associate, Inc. and shown on the project plans. A DEP Tier 1 permit has been requested for the disturbance to the wetlands.

Based on the information provided, the standards of this section have not yet been met.

16. <u>River, stream or brook...</u> Any river, stream, or brook within or abutting the proposed subdivision has been identified on any map submitted as a part of the application. For purposes of this section, "river, stream or brook" has the same meaning as in Title 38, Section 480-B, Subsection 9. [Amended; Effective. 11/27/89]

There is a stream on the property which is depicted on the plans. Based on the information provided, the standards of this section have been met.

X. STANDARD CONDITIONS OF APPROVAL:

This approval is dependent upon and limited to the proposals and plans contained in the application and supporting documents submitted by the applicant. Any variation from the plans, proposals and supporting documents, except deminimus changes as so determined by the Town Planner which do not affect approval standards, is subject to review and approval of the Planning Board prior to implementation.

XI. LIMITATION OF APPROVAL:

Construction of the improvements covered by any site plan approval must be substantially commenced within twelve (12) months of the date upon which the approval was granted. If construction has not been substantially commenced and substantially completed within the specified period, the approval shall be null and void. The applicant may request an extension of the approval deadline prior to expiration of the period. Such request must be in writing and must be made to the Planning Board. The Planning Board may grant up to two (2) 1 year extensions to the periods if the approved plan conforms to the ordinances in effect at the time the extension is granted and any and all federal and state approvals and permits are current.



July 31, 2018 (Via Delivery & Email) J16.084

Carla Nixon, Town Planner Town of Cumberland 290 Tuttle Road Cumberland, Maine 04021

OceanView at Cumberland, Tuttle Road, Cumberland FINAL SUBDIVISION PLAN SUBMISSION (Map R04 Parcels 4B, 4E and 5)

Dear Carla:

On behalf of OceanView at Cumberland LLC, we are pleased to present for staff and Planning Board review, a *Final Subdivision Application and Plans dated July 31st, 2018* for the development of the "OceanView at Cumberland" active senior community located at 277 Tuttle Road across from the Town Hall and Town Forest property.

This submission includes the following materials; (3 hard copies and PDF Copies)

- Cover Letter Report
- Major Subdivision -Final Plan Review Checklist Appendix I
- DEP and Corps of Engineers Emails re: Permitting
- Exhibit-1 Tax Map Locus-Project Parcels
- Exhibit -2 Conveyance Plan (Reduced Copy)
- Exhibit -3 Right, Title & Interest Deeds
- Exhibit -4 Snowmobile Trail License Draft
- Exhibit -5 Utility Serviceability Letters
- Exhibit -6 Stormwater Maintenance Agreement
- Exhibit -7 Lighting Cuts
- Exhibit -8 Responses to Sevee and Maher Comments
- Final Subdivision Plans, OceanView at Cumberland, Tuttle Road, Cumberland, Maine prepared by Belanger Engineering and Licht Environmental Design, LLC Revised 07-31-18.

1. BACKGROUND:

The project received Preliminary Major Subdivision approval on March 20, 2018 for a 52-unit senior community with a community center. No waivers were requested nor granted for Preliminary Approval. In the interim months since Preliminary Approval the project has undergone a number of refinements to satisfy Final Major Subdivision submission. Each of the project updates are described below and in the accompanying Exhibits, however a general summary of updates are as follows:

(Note- within this document use of the terms "OceanView at Cumberland, LLC " and "OceanView" shall have the same meaning as OceanView at Cumberland, LLC.)



- 1. Right, title and Interest OceanView at Cumberland, LLC has executed the prior Purchase and Sale Options and closed on the three subject parcels or portions of parcels and properties included within the project scope. The overall project acreage and areas are described in detail below to update the Planning Board. Refer to Exhibit 3 for deeds.
- 2. Plan Design Changes The design team has spent the interim period following Preliminary Approval working closely with the DEP and Corps of Engineers through their respective permitting processes. The accompanying plans provide several key project detailed refinements as described below. However the overall plan design and program has not changed. (Refer to items 7 and 9 below for further information.)
- 3. DEP and U.S. Army Corps of Engineers (Corps) Permitting The DEP and Corps of Engineers are completing permit reviews and all comments to date have been addressed by the applicant's team. We have submitted, attached to this cover letter, copies of emails from both agencies indicating that the applications are under review however final drafting of permits has not yet been completed. We understand that the Town of Cumberland will not provide final plan approval without receipt of final agency permits. To that end we are working closely with the agencies to have permits issued as soon as possible so that final plan approval can be granted.

The project will be subject to the MDIF&W and Corps "window" for stream culvert installation – requiring installation of culvert #1 on Little Acres Drive to be installed by October 1st. The applicant's team is working closely with the DEP and the site contractor to plan for a potentially tight window of time to install the culvert once final permits are issued to provide access to Phase 1 of the project for the 2018-19 construction season.

4. Utility Extensions and Serviceability- The project team has been working closely with the various utility companies to complete final utility designs and secure letters of serviceability. Final utility information is included herein.

2. RIGHT TITLE & INTEREST – AMENDMENTS TO ORIGINAL APPLICATION:

The applicants have worked closely with Richard Doane (Map R04 Portions of Parcels 4B 4D and 4E) and Laurence and Beverly Allen (Map R04 Parcel 5) to satisfy conditions of the purchase and sales agreements provided to the Town with the Preliminary Submission. The final plans and Exhibit 1 Tax Map Locus and Exhibit 2 -Conveyance Plan reflects the following minor adjustments to the project area. Exhibit 3 contains copies of the executed property deeds. Refer also to the Subdivision Plats Sheets S1-S4 for detailed information.

- a. The main development parcel (portion of Map R04 Parcel 4E) has been acquired from Richard W. Doane and recorded in the CCRD Book 24876 Page 194 in June, 2018. The acreage of this parcel is 30.99 acres.
- b. Negotiations with Richard Doane resulted in the slight re-alignment of the Little Acres Drive such that the prior full length 50-foot access and utility easement over the former Maine Central Railroad bed has been reduced to require only the conveyance of a small (0.22 acre) portion of said railroad ROW to OceanView at Cumberland. That conveyance was recorded



in a deed from Richard and Hillary Doane to OceanView at Cumberland, LLC and recorded in the CCRD Book 34876 Page 192.

- c. The division of the Allen Lot (Map R04-05) has been executed and the deed from Laurence Allen to OceanView at Cumberland, LLC recorded in Book 34876 page 184. The Allen's conveyed 5.35 acres in the rear of their 8.64 acre lot to OceanView and retained a 3.29 acre lot fronting on Tuttle Road and Little Acres Drive. The plan to provide a 50-foot by 450 foot right of way from Tuttle Road as a part of the OceanView property has been revised to a 50 foot access and utility easement over the new front Allen Lot. Review with the Codes Enforcement Officer determined that a right of way would have created a corner lot for the Allen lot and there would be less than the required 200 feet of frontage on Tuttle Road with the dedication of a 50 foot right of way to OceanView. The final plans, deed and Exhibit 2 provide an easement granted from Allen to Oceanview over the 3.29 acre front Allen lot.
- d. The applicant has reserved within the 50 foot access and utility easement the rights for Richard Doane to access the adjacent lot R04-4D with a single driveway for future potential single family residences on lots 4D and/or 4B. (Refer to Subdivision Plat Sheet S1).
- e. The plans have removed reference to any formal landscaping buffers on the Doane properties (Map R04 Parcels 4B and 4D). Instead, the applicants and Richard Doane have provided separate agreements to provide infill landscaping and buffering to be field located during construction. (These areas on the west side of Little Acres Drive are already wooded - the additional plantings have been negotiated as additional buffering.)
- f. The project no longer includes any portion of Map R04 Parcel 4D (Richard W. Doane)

The revised project acreage is as follows:

	Total Project Area (fee and easement)	37.09 acres
•	50 foot access and utility easement over Allen	0.53 acres
	Total acreage (fee)	36.56 acres
•	Allen lot parcel 5 to OceanView	5.35 acres
•	Right of Way Doane parcel 04B to OceanView	0.22 acres
•	Doane rear parcel 04E	30.99 acres

3. SNOWMOBILE TRAIL LICENSE:

The applicants have worked closely with the Town Manager, Lands and Recreation Committee and Snow Skimmers Snowmobile Club to provide a snowmobile/multi-use path connection along the southeastern property line. A license agreement (Exhibit 4) has been drafted and reviewed with the Town Manager and will be executed following project approvals.

The license provides for reasonable use of this section of trail by the public and for provisions to resolve conflicts or uses resulting in adverse impacts to OceanView residents. OceanView has agreed to fund the construction of this section of trail for up to \$10,000 and work with the Town on construction and maintenance. The project will also provide additional buffer planting along sections of this trail to provide additional privacy to the adjacent cottages as shown on Plan C12 – Landscaping Plan.



Refer also to the Trail and Walkway Masterplan, plan sheet C12 and the Landscaping Plan, sheet C11A for the trail location and proposed buffer plantings along the trail.

4. PROJECT PHASING:

The project phasing plan, Sheet C1 provides a six (6) phased project for purposes of marketing of units. However, the infrastructure is expected to be installed over a three (3) year period in either two (2) or three (3) phases commencing in the fall of 2018, following permit approvals. The general infrastructure phasing is planned as follows:

Phase 1A - Install water main tap Tuttle Road and Little Acres Drive (Completed June 2018)

Phase 1 –Little Acres Drive (Station 10+00 to 28+50, Periwinkle Drive Ivy Lane and Honeysuckle Way, Wet Pond 1, Stream Crossing 1 and associated infrastructure. Units 1-20. Phase 1 will utilize the existing Allen residence and provide temporary power as Little Acres Drive is constructed and the Allen's complete construction of their new home on the front Allen 3.29 acre lot over the summer and late fall of 2018. The existing Allen residence may be used as a temporary sales and construction office or removed as the project progresses to provide for Units 50-52 construction. (2018-2019.)

Phase 2 – Little Acres Drive Station 28+50 to 29+43, Mallard Way and Lilac Way, Wet Pond 2 and associated infrastructure. Units 21-35. (2019-2020.)

Phase 3 - Mallard Way and Azalea Lane and associated infrastructure. Units 36-49 and 50-52. (2020-2021.)

Trail construction phasing will be coordinated based on project infrastructure phasing and occupation of units and completion of the various neighborhoods.

5. UTILTY SERVICEABILITY:

Final letters of serviceability from the Portland Water District (PWD), Central Maine Power Company (CMP), Summit Natural Gas and the Town of Cumberland are included in Exhibit 5.

Easements have been shown on the Subdivision Plat and engineering plans over the private roadways for the respective utilities. The water distribution system will be constructed in phases conveyed to PWD as a public utility through a Portland Water District Main Extension Agreement and Easement.

The CMP design plan for the project has been included at the end of the plan set and final transformer locations shown on plan sheets C3-C10.



6. STORMWATER AGREEMENT MS-4:

A draft copy of the Town Stormwater Agreement is attached in *Exhibit 6*. The applicant intends to contract with a third party, Ross Cudlitz, PE for annual inspections and reporting. The stormwater system including two wet ponds will be private and maintained by OceanView at Cumberland, LLC.

7. UNIT DRIVEWAY POST -LIGHITNG CUTS:

Site lighting has been shown on the previous Photometric Plan ES-1. The standard cut-off-LED Beacon® site fixtures provided in the Preliminary Submission are attached for convenience in *Exhibit 7 – Lighting Cuts*. Additionally each unit will have a decorative driveway light similar to the Falmouth project mounted on a granite or similar post and also building mounted on the front of each unit. The lighting cuts for these fixtures have been added in *Exhibit 7* as well. These are small decorative lights and while not formally cut-off style, are low wattage and very attractive. The residents of OceanVlew Falmouth have found these to fit well within their neighborhoods.

8. SEVEE & MAHER FEBRUARY 12, 2018 PEER REVIEW COMMENTS:

The majority of the Sevee and Maher comments were addressed at the Preliminary Plan approval submission. Outstanding items for Final Plan review are addressed in *Exhibit 8*.

9. PLAN REVISIONS:

The Final Subdivision plans dated July 31, 2018 include an additional level of detail commensurate with final plan submission to comply with the Town of Cumberland Appendix I Final Plan Checklist and Chapter 250-7.D Final Plan and Article IV Design Improvement requirements. A summary of overall plan changes including responses to agency review comments follows:

- a. Little Acres Road Alignment (Stations 15+00 to 28+00) the road was shifted 5-10 feet to the east at the Culvert #1 crossing and approach stations to save specific trees requested by Richard Doane resulting also in a reconfiguration of the curve and alignment from Station 22+00 to 28+00. In response to DEP Comments the road "sag" at culvert 1 was also revised to shift the location of the Focal Point stormwater treatment systems to be further away from the stream. The system was reconfigured and located on the right side of the road only. Refer to plan sheets C6, C7 and C27.
- b. Culvert Designs- After evaluation of constructability with the site contractor the two stream crossing culverts (#1 and #2) were changed from open pipe arches to pre-cast box culverts buried with 2 feet of substrate in the bottom in accordance with Corps of Engineers requirements. Refer to plan sheets C20 and C21.
- c. Utility Designs The plans have undergone final utility design with the respective utility companies. The water main on Little Acres Drive has been increased from an 8 to a 12 inch main and the main on Mallard Way reduced to a 4 inch main per PWD recommendations. Additional valving and details have been added to the plans together with CMP transformer and pull box locations.
- d. Stormwater Management– The plans reflect minor modifications to the two wet ponds in response to DEP comments. A level spreader and DEP meadow buffer have been added



- behind Unit 52 to treat stormwater from a portion of Little Acres Drive and Units 50-52. The Focal Point treatment system was revised as noted above and a culvert added at the project entrance.
- e. Buffers the plans have been updated to clearly label several key buffers—the 100 foot MDIFW stream Buffer, the DEP Forested Stormwater Buffer Areas and a DEP Meadow Buffer located with a level lip spreader behind Unit 52. Additionally tree lines and limits of cutting have been further refined.
- f. Trails Plan C12 Trail and Walkway Masterplan, has been updated to reflect the location of the snowmobile trail and adjustments to several hiking trails near wetlands.
- g. Crosswalk at Tuttle Road Plan C3 indicates a crosswalk and ADA ramps on either side of Tuttle Road at the project entrance. The Town sidewalk project has incorporated the ADA ramp on the south side of Tuttle Road this summer. The project will complete the crosswalk and signage during Phase 1 or 2 of the project. We understand through communication with the MDOT that this crosswalk can be approved by the Town of Cumberland.
- h. Road Names Road names have been approved and added to the plans.

10. SUMMARY:

We believe that the submitted materials address the Town of Cumberland requirements for final plan review and approval. Should you have any further comments please do not hesitate to contact me. On behalf of our entire project team we look forward to meeting with the Planning Board at the August 21st meeting to present the project in further detail.

Sincerely,

Frederic (Rick) Licht, PE, LSE

Principal

Encl: As Noted

Cc: Matt Teare; OceanView at Cumberland LLC

Chris Wasileski: OceanView at Cumberland LLC Christian Haynes; OceanView at Cumberland LLC David Haynes; SeaCoast Management Company

Chris Belanger; Belanger Engineering Rex Croteau; Titcomb Associates Scott Anderson; Verrill-Dana

SUBDIVISION OF LAND

Appendix I Application Checklist Major Subdivision – Final Plan Review

Pro	posed subdivision name OCFANIA	NAT CLIME	SEALUD	
Ap	plicant name OCEANUEW AT	competers	so, ue	
Ow	ner name OCEANUEW AT	cumpte	MP. LLC	
	3	Check When S		Indicate Date When Satisfactory Planning Bd.
1.	19 copies of final plan and accompanying materials SPPFFIE			
2.	Title			
3.	Scale			
4.	North arrow	~		
5.	Date of plan			
6.	Name, address and signature of owner			
7.	Name, address and signature of subdivider			
8.	Name, address and signature of licensed engineer, land surveyor, architect or planner	~		
9.	Names of adjoining property owners or subdivisions	<i>V</i>		
10.	Check for conformity with preliminary plan			
11.	Dimensions and bearings of property being subdivided	~		
12.	Location, names and widths of existing and proposed streets	_		
13.	Location and names of existing and proposed parks, playgrounds and other public areas	/		

CUMBERLAND CODE

14.	Lot lines and accurate dimensions and bearings or angles			
15.	Lot areas			
16.	Building setback lines			
17.	Curve data			
18.	Location, description and size of all monuments	_ V		
19.		PEHDING vel DEPKorpsema	ide)	
20.	Destrictive covenants	percovenal is		
21.	Street plans and profiles			
22.	Typical cross sections of street pavements, including curbs and gutters, sidewalks, manholes and catch basins			
23.	Landscaping	_		
24.	Plan and profiles showing location, size and invert elevations of existing and proposed sanitary sewers and storm sewers	_/		
25.	Plan and profiles showing location and size of all waterlines, gas lines, and other underground utilities and structures	V		

To the Applicant:

If you are requesting a waiver from a particular requirement or you do not feel that the requirement is applicable to your proposed project, please place an asterisk (*) in the space and explain your reasons in the space below or on attached sheets.

From: Bergeron, Mark
To: Carla Nixon

Cc: rlicht@securespeed.net; Stebbins, Mark N; Sirois, Alison; Woodruff, Christine

Subject: OceanView project

Date: Tuesday, July 31, 2018 12:01:12 PM

Hi Carla-

It's nice to see a familiar name again. I hope all is well with you.

The applicant has requested that we provide an update of where DEP's review stands for the application review of the OceanView project. The Department received a Site Location of Development application and a Natural Resources Protection Act application on February 18, 2018 for the OceanView project in Cumberland. The Department accepted these applications as complete for processing on March 3, 2018, making the statutory deadline September 10, 2018 as to when the Department needs to make a decision. This email confirms that the Department is diligently reviewing these applications, but due to our very heavy workloads, we are not able to issue a decision before our statutory deadline of September 10.

Please contact me if you have any questions.

Thank you.

Mark Bergeron, P.E.
Director, Bureau of Land Resources
Maine Department of Environmental Protection
(207) 215-4397
www.maine.gov/dep

From: <u>Clement, Jay L CIV USARMY CENAE (US)</u>

To: rick licht

Subject: RE: [Non-DoD Source] OceanView at Cumberland DEP and Corps Permits

Date: Wednesday, July 25, 2018 4:17:44 AM

Not this week Rick, too many in front of it and too much field time this week. Perhaps next week.

Jay

----Original Message----

From: rick licht [mailto:rlicht@securespeed.net]

Sent: Monday, July 23, 2018 12:03 PM

To: Clement, Jay L CIV USARMY CENAE (US) < Jay.L.Clement@usace.army.mil> Subject: FW: [Non-DoD Source] OceanView at Cumberland DEP and Corps Permits

Hi Jay:

Was out last week and just checking in to see if permit may be issued this week? Thanks for any updates you can provide.

Best

Rick Licht

Frederic (Rick) Licht, PE, LSE Licht Environmental Design, LLC 35 Fran Circle Gray, Maine 04039 (v) 207.749.4924 lichtenvironmentaldesign.com

----Original Message-----

From: rick licht [mailto:rlicht@securespeed.net]

Sent: Friday, July 13, 2018 7:52 AM

To: 'Clement, Jay L CIV USARMY CENAE (US)'

Subject: RE: [Non-DoD Source] OceanView at Cumberland DEP and Corps Permits

Great thanks Jay

Rick

Frederic (Rick) Licht, PE, LSE Licht Environmental Design, LLC 35 Fran Circle Gray, Maine 04039 (v) 207.749.4924 lichtenvironmentaldesign.com ----Original Message----From: Clement, Jay L CIV USARMY CENAE (US) [mailto:Jay.L.Clement@usace.army.mil] Sent: Friday, July 13, 2018 7:37 AM To: rick licht; 'Woodruff, Christine' Subject: RE: [Non-DoD Source] OceanView at Cumberland DEP and Corps Permits Think I have what I need for now Rick. Jay ----Original Message----From: rick licht [mailto:rlicht@securespeed.net] Sent: Wednesday, July 11, 2018 7:37 AM To: 'Woodruff, Christine' < Christine. Woodruff@maine.gov>; Clement, Jay L CIV USARMY CENAE (US) < Jay.L.Clement@usace.army.mil> Subject: [Non-DoD Source] OceanView at Cumberland DEP and Corps Permits Good Morning Christine & Jay: I just wanted to reach out to see if there were any lingering comments which need addressing in the final processing of the SLODA/NRPA and Corps permits for the Cumberland Project. We are expecting to submit final plans to the Town of Cumberland on or about July 30th so that we can get a late August approval and follow up with Performance Guarantees, etc. and start construction towards Culvert 1 in Early September if all goes well. Again per email of July 10th we are withdrawing request for an extension of the July - Oct 1 Culvert installation window. Please advise if you see any issues with final permits by the end of July as they are required for Final Plan submittal to the Town. **Best** Rick Licht Frederic (Rick) Licht, PE, LSE Licht Environmental Design, LLC

Gray, Maine 04039

35 Fran Circle

(v) 207.749.4924

lichtenvironmentaldesign.com



DEPARTMENT OF THE ARMY NEW ENGLAND DISTRICT, CORPS OF ENGINEERS 696 VIRGINIA ROAD CONCORD, MASSACHUSETTS 01742-2751

MAINE GENERAL PERMIT (GP) <u>AUTHORIZATION LETTER</u> AND SCREENING SUMMARY

OCEANVIEW AT CUMBERLAND, LLC			OODDO DEDINE	NAE 2019 00515	
20 BLUEBERRY LANE			CORPS PERMIT # CORPS GP ID#	NAE-2018-00545 18-155	
FALMOUTH, MAINE 04105		,	STATE ID#	NRPA	
DESCRIPTION OF WORK:					
Place temporary and permanent fill b	elow the ordin	arv high water	line of unnamed st	reams and in adiac	cent
freshwater wetlands at Cumberland, I					
will result in approximately 70 s.f. of					
s.f. of permanent wetland fill. An add					
This work is shown on the attached p Road, Cumberland, Maine" in 17 shee			umberiand, Semor	Community, Tutti	<u>E</u>
LAT/LONG COORDINATES : 43.792043		-70 242084°	W USGS QUA	D: CUMBERLAND C	TR, ME
I. CORPS DETERMINATION:					
Based on our review of the information you provided	d, we have determi	ned that your project	will have only minimal in	dividual and cumulative	impacts on
waters and wetlands of the United States. Your wo Permit, the Maine General Permit (GP). Accordin	ork is therefore au	thorized by the U.S	. Army Corps of Engine		
You must perform the activity authorized herein in c	ompliance with all	the terms and conditi	ions of the GP [including	any attached Additional	Conditions
and any conditions placed on the State 401 Water 0	Quality Certification	including any require	<u>ed mitigation]</u> . Please rev	riew the enclosed GP ca	refully,
including the GP conditions beginning on page 5, to requirements; therefore you should be certain that v					
conditions of this authorization with your contractor					
If you change the plans or construction methods for authorization. This office must approve any change			tact us immediately to dis	cuss modification of this	;
Condition 20 of the OD (new 46) movides and year					L
Condition 38 of the GP (page 16) provides one year of the GP on October 13, 2020. You will need to ap	pply for reauthorizat	ion for any work with	in Corps jurisdiction that	is not completed by Oct	ober 13,
<u> 2021.</u>		-			
This authorization presumes the work shown on you submit a request for an approved jurisdictional dete			U.S. Should you desire	o appeal our jurisdiction	, please
No work may be started unless and until all other re	equired local. State	and Federal license	s and permits have been	obtained This include	es hut is no
limited to a Flood Hazard Development Permit is			o and pomino nato book		
II. STATE ACTIONS: PENDING [], ISSU	ED[X], DEN	IED[] DATE_	·····		
APPLICATION TYPE: PBR:, TIER 1:	TIER 2 <u>: X</u>	TIER 3: L	URC: DMR LEA	ASE: NA:	_
III. FEDERAL ACTIONS:					
JOINT PROCESSING MEETING: 3/15/18	LEVEL OI	REVIEW: CATE	GORY 1: CAT	EGORY 2: X	·
AUTHORITY (Based on a review of plans and/or s	State/Federal appli	cations): SEC 10	, 404X10)/404, 103	_
EXCLUSIONS: The exclusionary criteria identified	d in the general per	mit do not apply to th	nis project.	· · · · · · · · · · · · · · · · · · ·	
FEDERAL RESOURCE AGENCY OBJECTION	ONS: EPA <u>NO</u> ,	USF&WS <u>NO</u> , NN	MFS_NO		
If you have any questions on this matter, please cor you, we would appreciate your completing our Cust	ntact my staff at 20 omer Service Surve	7-623-8367 at our Au ey located at <u>http://co</u>	ıgusta, Maine Project Off preşmapu.usace.army.mi	ice. In order for us to be l/cm_apex/f?p=136;4;0	etter serve
Taul (Ocasion +	!	Auch (De la como	+ shule	

JAY L. CLEMENT SENIOR PROJECT MANAGER MAINE PROJECT OFFICE

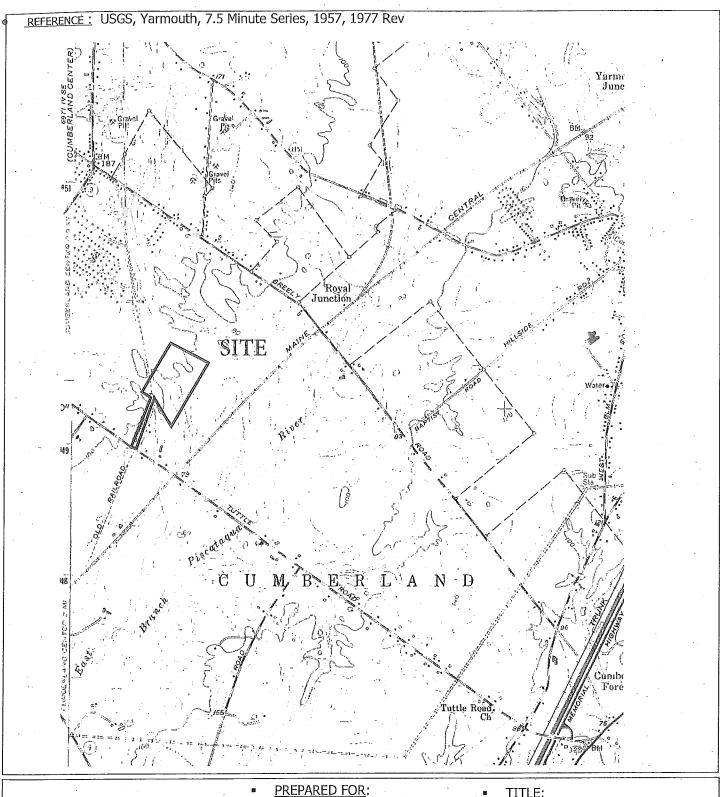
FORFRANK J. DEL GIUDICE DAT CHIEF, PERMITS & ENFORCEMENT BRANCH

REGULATORY DIVISION



PLEASE NOTE THE FOLLOWING CONDITIONS FOR DEPARTMENT OF THE ARMY GENERAL PERMIT NO. NAE-2018-01631

- 1. This authorization requires you to 1) notify us before beginning work so we may inspect the project, and 2) submit a Compliance Certification Form. You must complete and return the enclosed Work Start Notification Form(s) to this office at least two weeks before the anticipated starting date. You must complete and return the enclosed Compliance Certification Form within one month following the completion of the authorized work and any required mitigation (but not mitigation monitoring, which requires separate submittals).
- 2. The permittee shall assure that a copy of this permit is at the work site whenever work is being performed and that all personnel performing work at the site of the work authorized by this permit are fully aware of the terms and conditions of the permit. This permit, including its drawings and any appendices and other attachments, shall be made a part of any and all contracts and sub-contracts for work which affects areas of Corps of Engineers' jurisdiction at the site of the work authorized by this permit. This shall be done by including the entire permit in the specifications for the work. If the permit is issued after construction specifications but before receipt of bids or quotes, the entire permit shall be included as an addendum to the specifications. The term "entire permit" includes permit amendments. Although the permittee may assign various aspects of the work to different contractors or sub-contractors, all contractors and sub-contractors shall be obligated by contract to comply with all environmental protection provisions of the entire permit, and no contract or sub-contract shall require or allow unauthorized work in areas of Corps of Engineers jurisdiction.
- 3. Adequate sedimentation and erosion control devices, such as geotextile silt fences or other devices capable of filtering the fines involved, shall be installed and properly maintained to minimize impacts during construction. These devices must be removed upon completion of work and stabilization of disturbed areas. The sediment collected by these devices must also be removed and placed upland, in a manner that will prevent its later erosion and transport to a waterway or wetland.
- 4. All exposed soils resulting from the construction will be promptly seeded and mulched in order to achieve vegetative stabilization.
- 5. All areas of temporary fill shall be removed and the areas restored to original contours and character upon completion of the construction.
- 6. The permittee must still obtain any other Federal, State, or local permits as required by law before beginning work. This includes but is not limited to a Flood Hazard Development Permit issued by the town if necessary.
- 7. No additional filling of waters of the United States (wetlands or waterways) for additional lot development is authorized without written approval from the Corps.
- 8. In water work shall be conducted between July 15 and September 30 in order to minimize potential impact to aquatic organisms and local water quality.
- 9. All tree cutting shall occur between October 16 and April 19 of any year to the maximum extent practicable and no tree cutting shall occur between June 1 and July 31 of any year in order to minimize potential impacts to federally listed northern long-eared hats



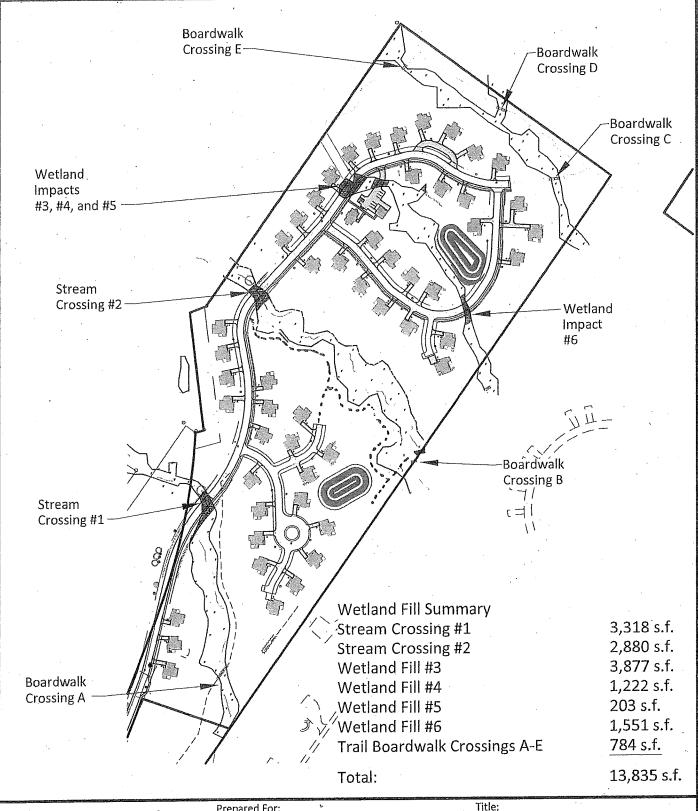


Oceanview @ Cumberland Senior Community Tuttle Road, Cumberland, Maine TITLE:

USGS Locus Map

SCALE: 1"=1000^{to} DATE: 12.2017ª JOB NO: 16.084

Exhibit 3







Oceanview @ Cumberland **Senior Community** Tuttle Road, Cumberland, Maine

Overall Plan Wetland Impacts

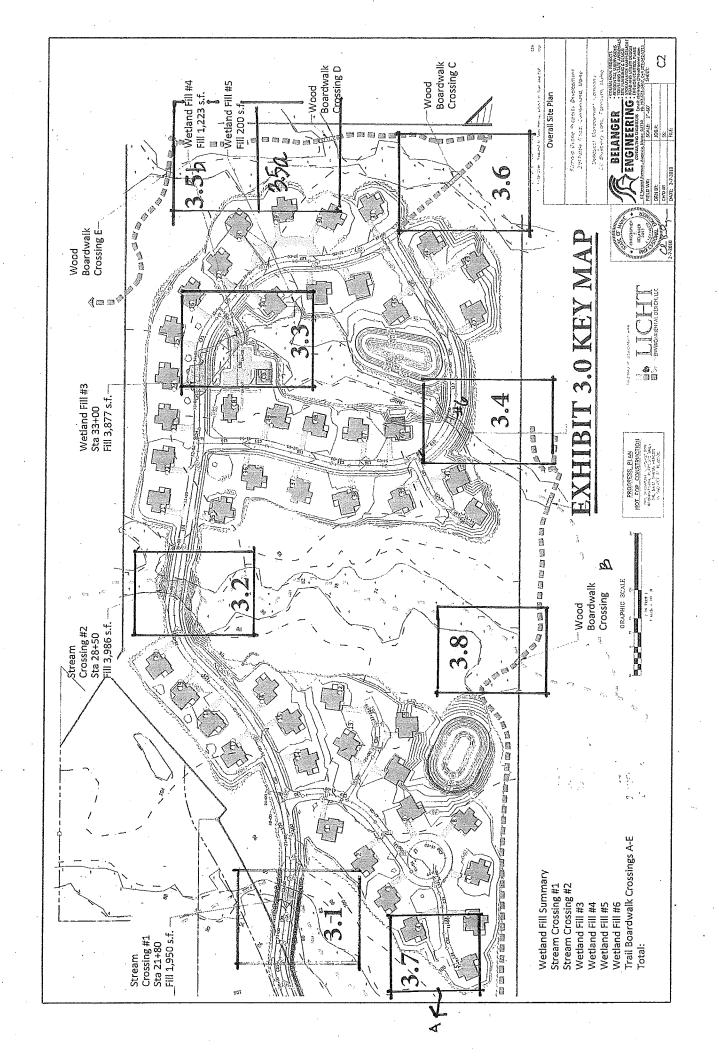
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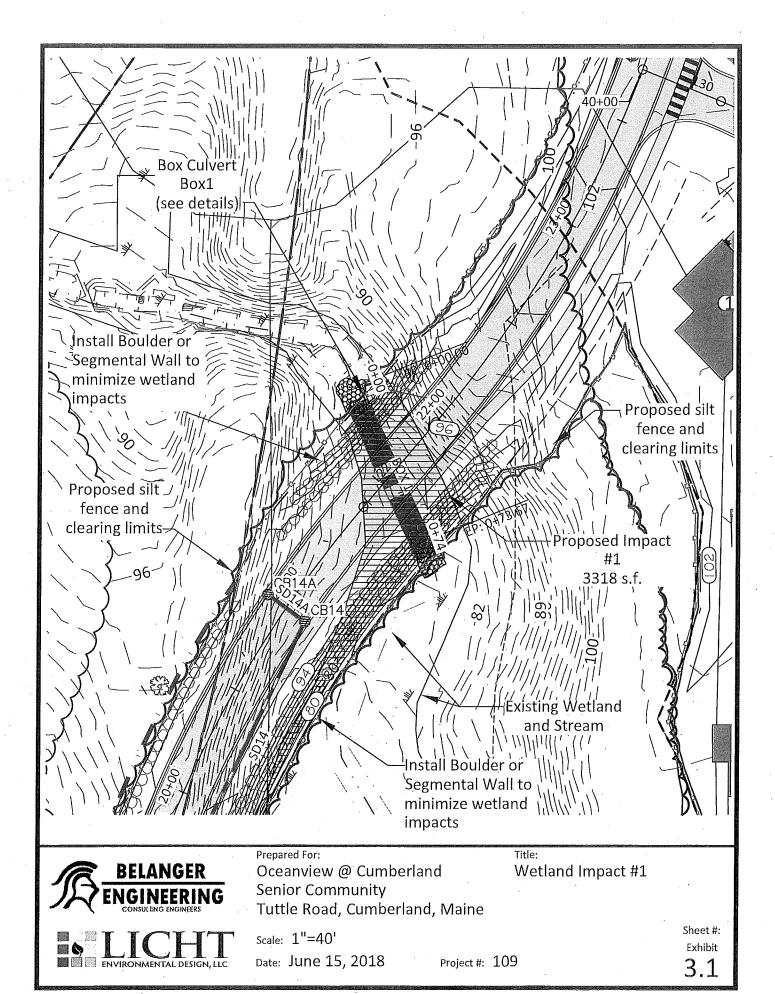
Date: May 4, 2018

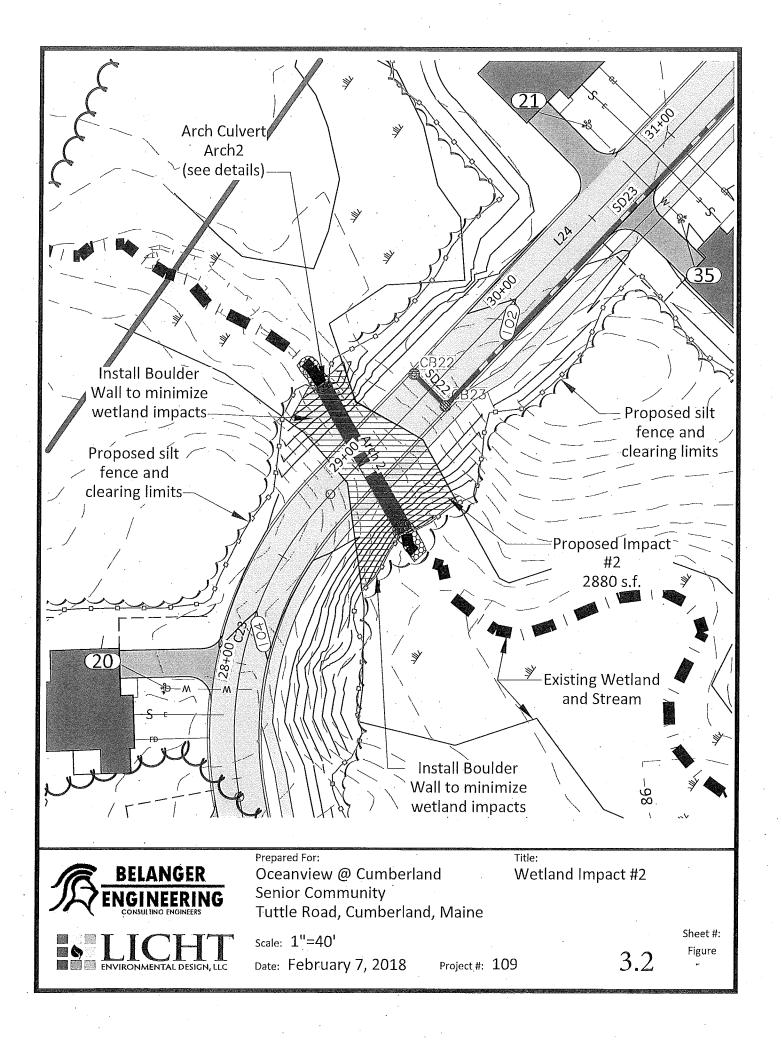
Project #: 109

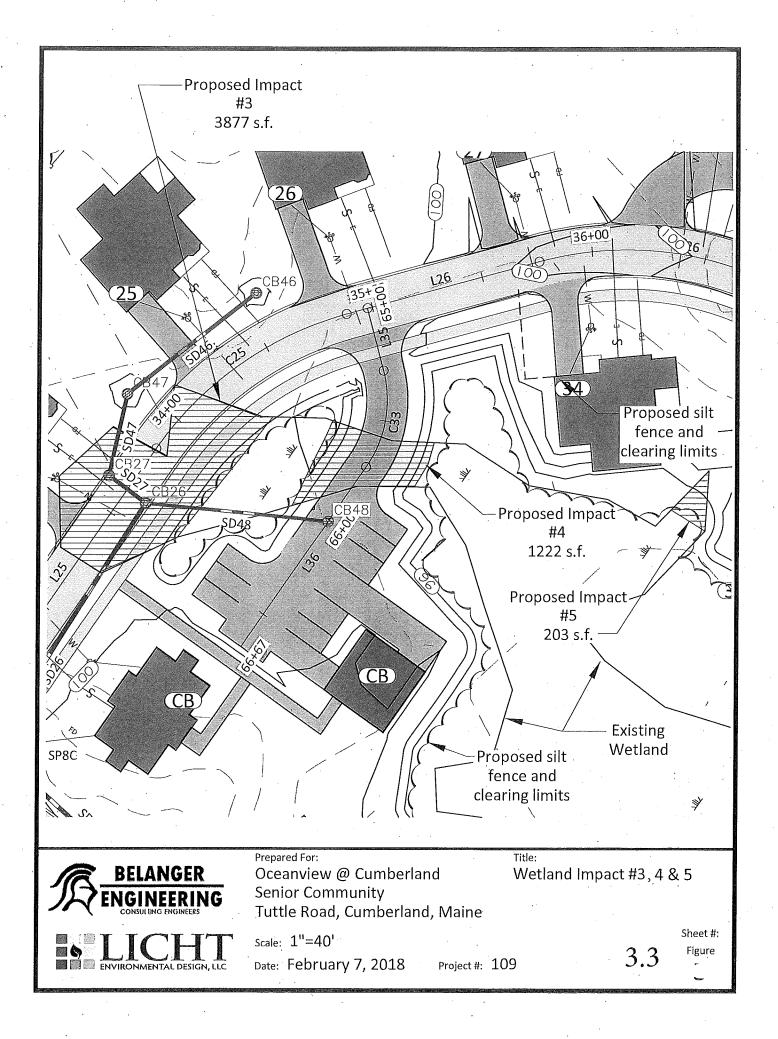
Sheet #: Figure

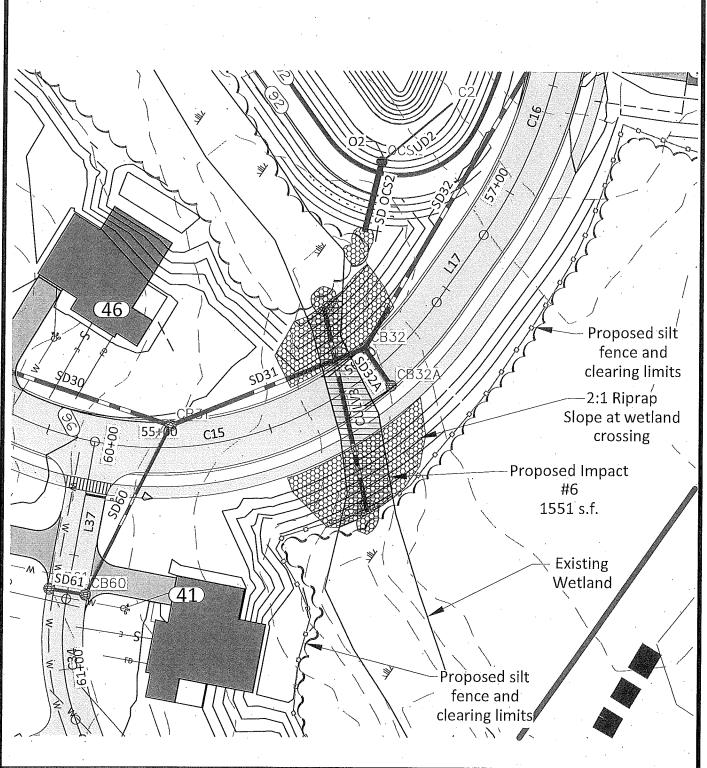
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ENVIRONMENTAL DESIGN, LLC

Prepared For:

Oceanview @ Cumberland Senior Community Tuttle Road, Cumberland, Maine

Scale: 1"=40'

Date: February 7, 2018

Title:

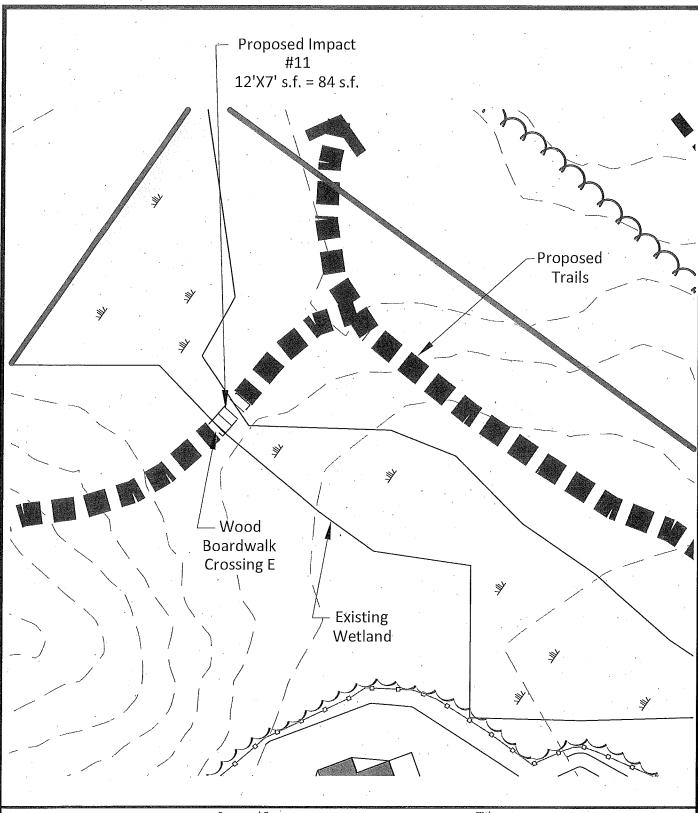
Wetland Impact #6

Sheet #:

Figure

Project #: 109

3.4







Oceanview @ Cumberland Senior Community Tuttle Road, Cumberland, Maine

Scale: 1"=40'

Date: February 7, 2018

Title:

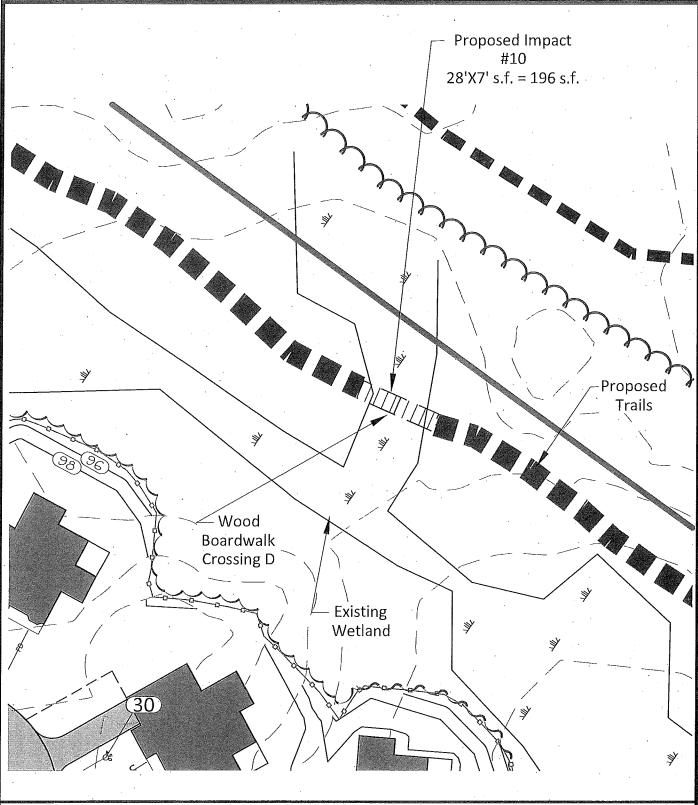
Project #: 109

Boardwalk Crossing E Wetland Impact #11

Sheet #:

Figure

3.5a







Oceanview @ Cumberland **Senior Community** Tuttle Road, Cumberland, Maine

Scale: 1"=40'

Date: February 7, 2018

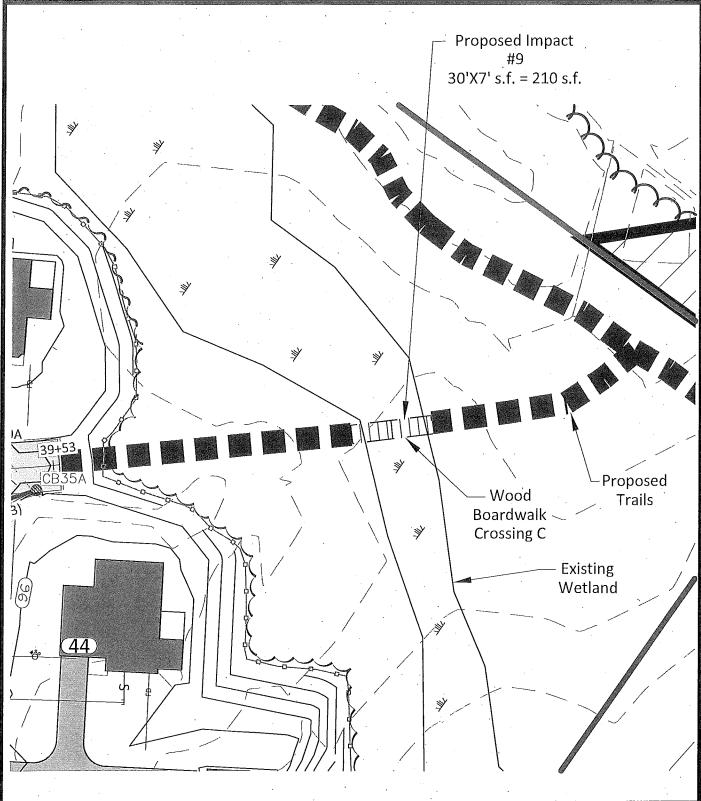
Title:

Project #: 109

Boardwalk Crossing D Wetland Impact #10

> Sheet #: Figure

3.5b







Oceanview @ Cumberland Senior Community Tuttle Road, Cumberland, Maine

Scale: 1"=40'

Date: February 7, 2018

Title:

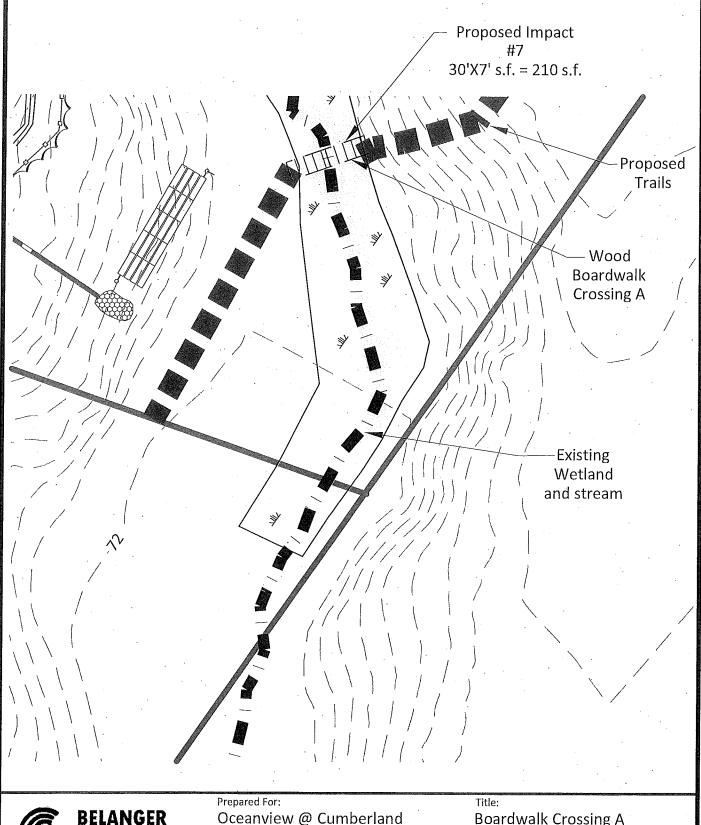
Project #: 109

Boardwalk Crossing C Wetland Impact #9

Sheet #:

Figure

3.6







Oceanview @ Cumberland Senior Community Tuttle Road, Cumberland, Maine

Project #: 109

Scale: 1"=40'

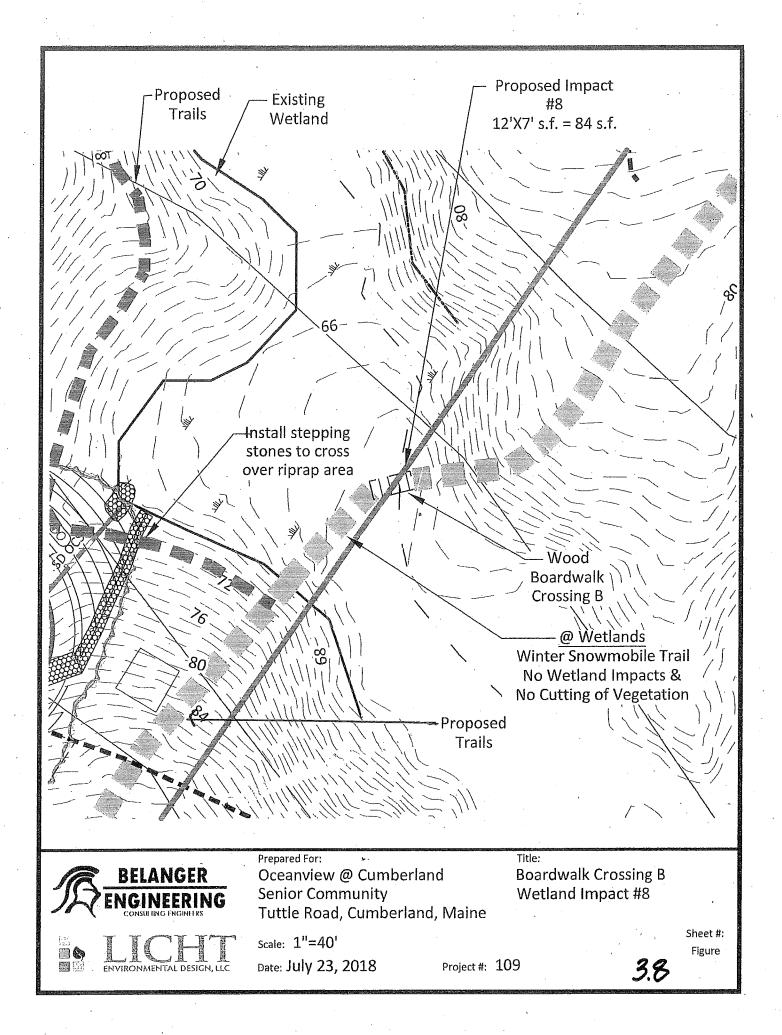
Date: February 7, 2018

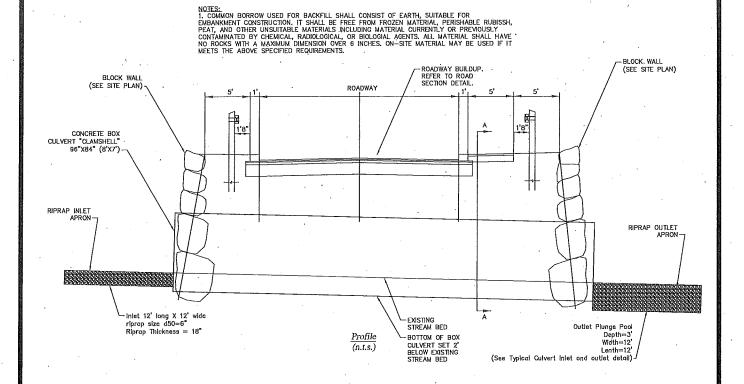
Boardwalk Crossing A Wetland Impact #7

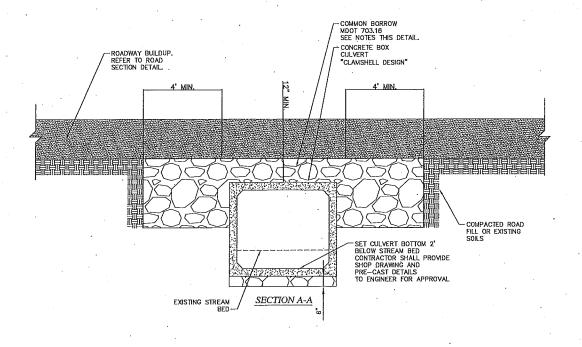
Sheet #:

Figure

3.7











Prepared For:

Oceanview @ Cumberland Senior Community Tuttle Road, Cumberland, Maine

Scale: N.T.S.

Date: May 4, 2018

Title:

Project #: 109

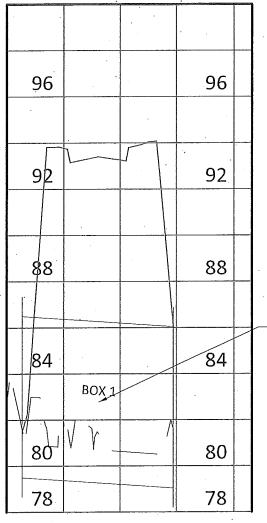
Box Culvert #1 Section

Sheet #:

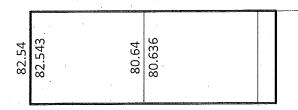
Figure

3.9

Box Culvert 1 PROFILE



-L=73.28',S=0.68%, 96"



0+00

0+50

1+00 1+07.86



S LICHT ENVIRONMENTAL DESIGN, LLC Prepared For:

Oceanview @ Cumberland Senior Community Tuttle Road, Cumberland, Maine Title:

Box Culvert 1 Section

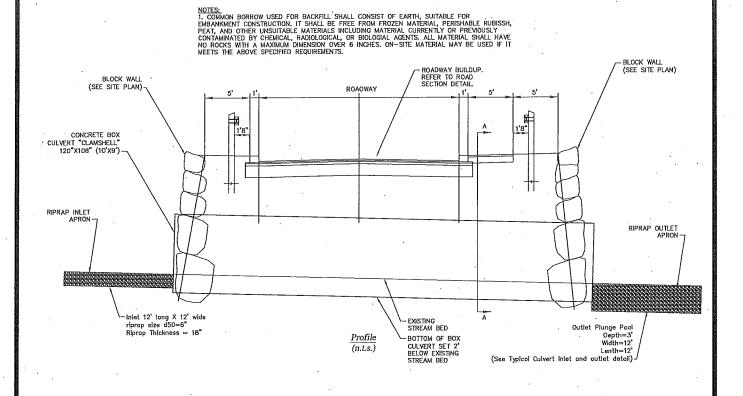
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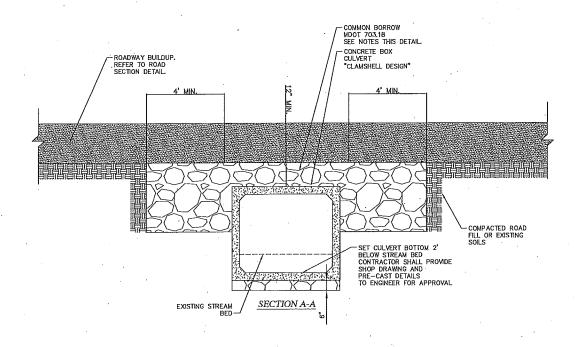
Date: May 4, 2018

Project #: 109

Sheet #: Figure

3.9A









Prepared For:

Oceanview @ Cumberland Senior Community Tuttle Road, Cumberland, Maine Title:

Box Culvert #2 Section

Scale: N.T.S.

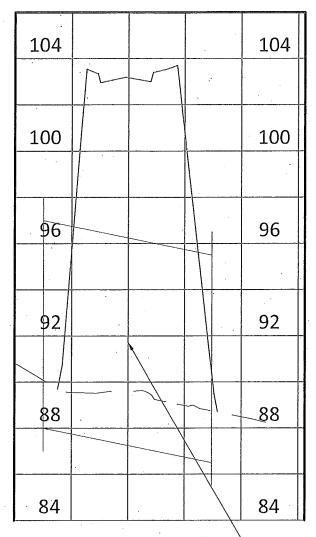
Date: May 4, 2018

Project #: 109

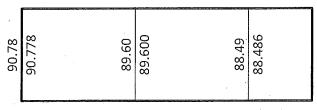
Sheet #: Figure

3.10

Box Culvert 2 PROFILE



-L=73.61',S=2.04%, 120"



0+00

0+50

1+00

1+27.92





Prepared For:

Oceanview @ Cumberland Senior Community Tuttle Road, Cumberland, Maine Title:

Box Culvert #2 Section

Scale: 1"=40'H-4'V

Date: May 4, 2018

Project #: 109

Sheet #: Figure

3.10A

REFERENCE:

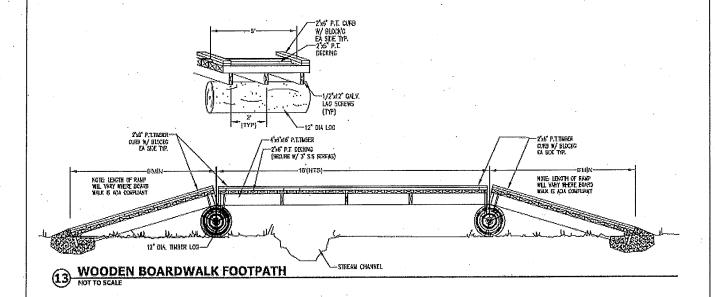


EXHIBIT 3.11





PREPARED FOR:

Oceanview @ Cumberland Senior Community Tuttle Road, Cumberland, Maine

TRAIL
BOARDWALK
CROSSING

- SCALE: FILL IN
- <u>DATE:</u> 01-30-18
- <u>JOB NO:</u> 16.084



(Minimum Notice: Permittee must sign and return notification within one month of the completion of work.)

COMPLIANCE CERTIFICATION FORM

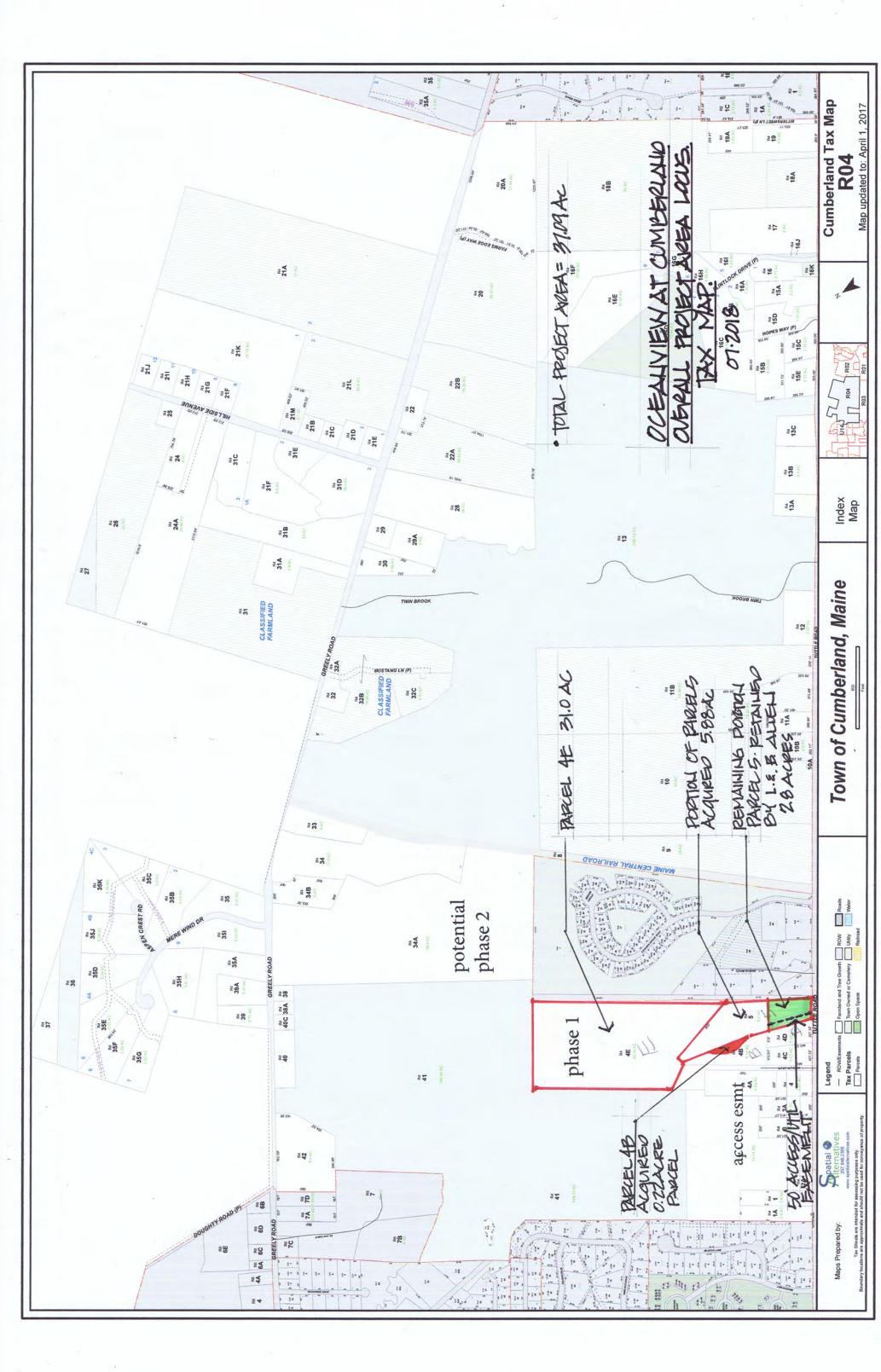
Permit Number: NAE-2018-00545	
Project Manager Clement	
Name of Permittee: Oceanview at Cumberland,	LLC
Permit Issuance Date:	
Please sign this certification and return it to the fol and any mitigation required by the permit. You m but not the mitigation monitoring, which requires s	ust submit this after the mitigation is complete,
***********	***********
* MAIL TO: U.S. Army Corps of Engineers,	New England District *
* Permits and Enforcement Branc	eh C *
* Regulatory Division	*
* 696 Virginia Road	2751 *
* Concord, Massachusetts 01742-	-2/31 ***************
Corps of Engineers representative. If you fail to copermit suspension, modification, or revocation. I hereby certify that the work authorized by the accordance with the terms and conditions of the mitigation was completed in accordance with the	e above referenced permit was completed in e above referenced permit, and any required
Signature of Permittee	Date
Printed Name	Date of Work Completion
	()
Telephone Number	Telephone Number

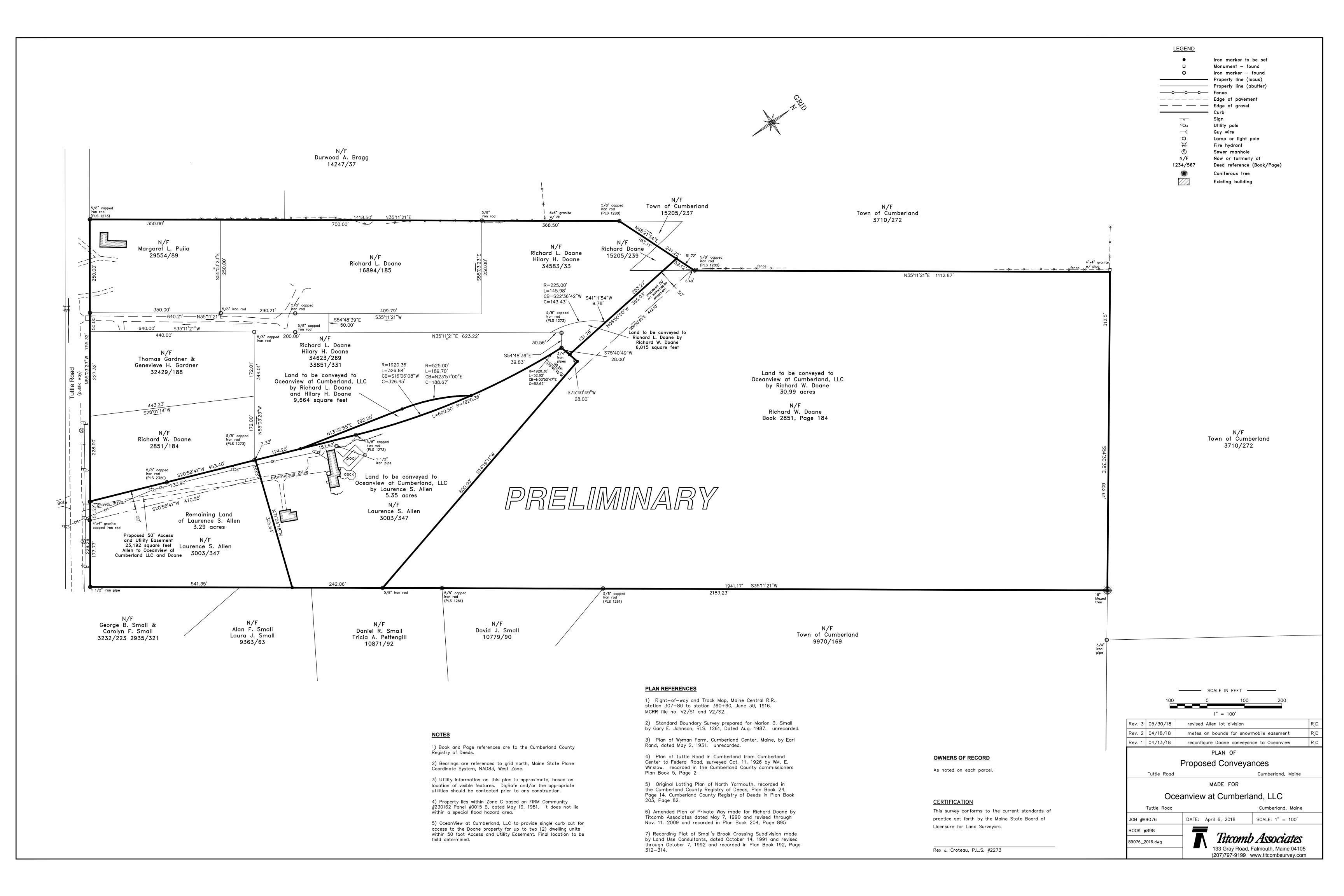


GENERAL PERMIT WORK-START NOTIFICATION FORM

(Minimum Notice: Two weeks before work begins)

* MAIL TO: U.S. Army Corps of Engineers	
* Permits and Enforcement Bran	nch *
* Regulatory Division * 696 Virginia Road	*
* 696 Virginia Road* Concord, Massachusetts 01742	2 2751 *
**************************************	~~~/JI *****************
Cumberland, Maine. The permit authorized the pin order to develop a 52 unit senior community. 70 s.f. of temporary and 1,386 s.f. of permanent swetland fill. An additional 784 s.f. of wetland with The people (e.g., contractor) listed below will do	in unnamed streams and in adjacent wetlands at permittee to place temporary and permanent fill. The development will result in approximately stream bed impact, and 12,449 s.f. of permanent ill be spanned by elevated timber boardwalk.
conditions and limitations.	
PLEASE PRINT OR TYPE	
Name of Person/Firm:	
Business Address:	
Telephone Numbers: ()	<u>(</u>)
Proposed Work Dates: Start:	Finish:
Permittee/Agent Signature:	Date:
Printed Name:	Title:
Date Permit Issued: ***********************************	**************
FOR USE BY THE CO	DRPS OF ENGINEERS
PM: Clement Sub	omittals Required: No
Inspection Recommendation: Inspect as c	convenient





DLN: 1001840027971

WARRANTY DEED

KNOW ALL PERSONS BY THESE PRESENTS, that Laurence S. Allen, Jr., in consideration of One Dollar and other valuable considerations paid by Ocean View at Cumberland, LLC, a Maine limited liability company, whose mailing address is 20 Blueberry Lane, Falmouth, Maine, the receipt whereof is hereby acknowledged, do hereby GIVE, GRANT, BARGAIN, SELL AND CONVEY unto the said Ocean View at Cumberland, LLC, its successors and assigns forever, the following described real estate:

Property Conveyed by Grantor to Grantee: A certain lot or parcel of land located on the northeasterly side of Tuttle Road in the Town of Cumberland, County of Cumberland, State of Maine, bounded and described as follows: Beginning at a point on the northeasterly side of Tuttle Road at the southerly corner of land now or formerly of Richard W. Doane as described in a deed recorded in the Cumberland County Registry of Deeds in Book 2851, Page 184; thence N 20°58'41" E by said land of Doane and land now or formerly of Richard L. Doane and Hilary H. Doane as described in deeds recorded in said Registry in Book 34623, Page 269 and Book 33851, Page 331 a distance of Seven Hundred Thirty-Three and 90/100 (733.90) feet to a point of curvature; thence Northerly by said land of Richard L. Doane and Hilary H. Doane, following a curve to the left having a radius of One Thousand Nine Hundred Twenty and 36/100 (1920.36) feet, an arc distance of Six Hundred and 50/100 (600.50) feet to a 3/4" iron pipe at a separate portion of the land now or formerly of Richard W. Doane as described in a deed recorded in said Registry in Book 2851, Page 184; thence N 75°40'49" E by said land of Richard W. Doane a distance of Fifty-Six and 00/100 (56.00) feet to a point; thence S 14°19'11" E by said land of Richard W. Doane a distance of Eight Hundred and 00/100 (800.00) feet to a point on the northwesterly line of land now or formerly of Daniel R. Small and Tricia A. Pettengill as described in a deed recorded in said Registry in Book 10871, Page 92; thence S 35°11'21" W by said land of Small and Pettegill and land now or formerly of Alan F. Small and Laura J. Small as described in a deed recorded in said Registry in Book 9363, Page 63 a distance of Two Hundred Forty-Two and 06/100 (242.06) feet to a point; thence N 71°04'18" W through the "Retained Allen Land" of the Grantor described below a distance of Three Hundred Five and 61/100 (305.61) feet to a point; thence S20°58'41" W through said land of the Grantor a distance of Four Hundred Seventy and 95/100 (470.95) feet to a point on the northwesterly side of said Tuttle Road; thence N 55°03'23" W by said Tuttle Road a distance of Fifty-One and 52/100 (51.52) feet to the point of beginning.

Bearings are referenced to grid north, Maine State Plane Coordinate System, NAD83, West Zone.

The above described parcel contains 5.9 acres, more or less, and being a portion of land now or formerly of Grantor, Laurence S. Allen, Jr. as described in the deed from Leroy W. Beal and Lois E. Beal, dated July 14, 1967 and recorded in the Cumberland County Registry of Deeds in Book 3003, Page 347.

Road Access Area Excepting and reserving to Grantor, his heirs and assigns and not hereby conveying the following described portion of the above described parcel: Beginning at a point on the northeasterly side of Tuttle Road at the southerly corner of Richard W. Doane as described in a deed recorded in the Cumberland County Registry of Deeds in Book 2851, Page 184; thence N 20°58'41" E by said land of Doane and land now or formerly of Richard L. Doane and Hilary H. Doane as described in deeds recorded in said Registry in Book 34623, Page 269 and Book 33851, Page 331 a distance of Four Hundred Fifty-Six and 73/100 (456.73) feet to a point; thence S 71°04'18" E a distance of Fifty and 03/100 (50.03) feet to a point at the northwesterly corner of said remaining land of Laurence S. Allen, Jr.; thence S20°58'41" W by said remaining land of Laurence S. Allen, Jr. a distance of Four Hundred Seventy and 95/100 (470.95) feet to a point on the northwesterly side of said Tuttle Road; thence N 55°03'23" W by said Tuttle Road a distance of Fifty-One and 52/100 (51.52) feet to the point of beginning. The Road Access Area described in this paragraph contains 23,192 square feet, more or less. Grantor grants to Grantee, its successors and assigns, for the benefit of the property conveyed to Grantee by this deed and for the benefit of any other property hereafter acquired by Grantee, its successors and assigns, perpetual easements for access and utilities, including the right and obligation to construct, use and maintain the road access and utilities in the area described in this paragraph to provide access and utilities to and from Tuttle Road in common with Grantor and Grantee and their respective heirs, successors and assigns and others. Grantee, its successors and assigns agree to be solely responsible for construction and maintenance of the road to be constructed in said 23,192 square foot area and agree to indemnify, defend and hold Grantor, his heirs and assigns from any liability arising in connection with such area and shall name Grantor, his heirs and assigns as additional insureds on all applicable property liability policies. The parties agree that the Road Access Area described in this paragraph shall be conveyed to Grantee upon the substantial completion of the road area abutting the Retained Allen Land described below and upon the Town of Cumberland's approval of the conveyance as in compliance with any applicable zoning requirements. Grantee shall be responsible for all costs and fees associated with obtaining zoning approval.

The remaining land of Grantor Laurence S. Allen, Jr. not conveyed to Grantee in this deed (hereinafter called the "Retained Allen Land") consists of the parcel described in the prior paragraph hereof and the following parcel that is bounded and described as follows: A certain lot or parcel of land located on the northeasterly side of Tuttle Road in the Town of Cumberland, County of Cumberland, State of Maine, bounded and described as follows: Beginning at a 1-1/2" iron pipe at the westerly corner of land now or formerly of George B. Small and Carolyn F. Small as described in deeds recorded in the Cumberland County Registry of Deeds in Book 3232, Page 223 and Book 2935, Page 321 and the northwesterly side of Tuttle Road; thence N 55°03'23" W by Tuttle Road a distance of One Hundred Seventy-Seven and 77/100 (177.77) feet to a point; thence N 20°58'41" E a distance of Four Hundred Seventy and 95/100 (470.95) feet to a point; thence S 71°04'18" E a distance of Three Hundred Five and 61/100 (305.61) feet to a point on the northwesterly line of land now or formerly of Alan F. Small and Laura J. Small as described in a deed recorded in said Registry in Book 9363, Page 63; thence S 35°11'21" W by said land of Alan F. Small and Laura J. Small, and said land of George B. Small and Carolyn F. Small a distance of Five Hundred Forty-One and 35/100 (541.35) feet to the point of beginning. Bearings are referenced to grid north, Maine State Plane Coordinate System, NAD83, West Zone. The above described Retained Allen Land parcel contains the 2.8 acres, more or less,

described in this paragraph and the 23,192 square foot parcel described in the prior paragraph and being a portion of land of Grantor Laurence S. Allen Jr. as described in a deed recorded in the Cumberland County Registry of Deeds in Book 3003, Page 347.

Covenants of Grantor and Grantee Affecting Retained Allen Land: Grantor, his heirs and assigns, shall not sell or convey or lease the Retained Allen Land or any interest in the Retained Allen Land to any person or entity, except that notwithstanding the foregoing, Grantor, his heirs or assigns may convey the Retained Allen Land, subject to the covenants set forth herein, to his wife, Beverly J. Allen, or any of their children, who may live on the Retained Allen Land subject to the foregoing restrictions, provided, however at such time as either of the Grantor or Beverly J. Allen or any of their children no longer live on the Retained Allen Land, the Retained Allen Land shall be sold to Grantee, its successors and assigns, in accordance with the terms hereof. Grantor or Beverly J. Allen, or their child or children as applicable shall notify Grantee when the applicable person(s) no longer reside on the Retained Allen Land.

References to Grantor below shall mean Grantor, his heirs and assigns, and the references to Grantee below, shall mean Grantee, its successors and assigns:

(i) Appraisal and Price: As soon as reasonably feasible after Grantor or his spouse or children move out of the Retained Allen Land, the Retained Allen Land shall be appraised as described herein. The total Purchase Price payable by Grantee to Grantor for the Retained Allen Land shall be the "Appraised Value", as hereafter defined, adjusted as provided herein (the "Purchase Price"), with payment to be made by wire transfer, or by bank, law firm or title company check, or by certified check. Retained Allen Land taxes shall be prorated at Closing. Appraised Value of shall mean the Fair Market Value of the Retained Allen Land herein conveyed together with all buildings and improvements located thereon at the time of Closing, determined as provided herein. The parties shall instruct a licensed appraiser (the "Appraiser") to determine the fair market value of the Retained Allen Land and the improvements then located thereon, taking into consideration such factors as ordinarily considered by the Appraiser in determining the fair market value of property. The Appraiser shall provide Grantee and Grantor a written appraisal as soon as reasonably possible, setting forth its determination of the Fair Market Value of the Retained Allen Land. The cost of the appraisal shall be split equally by Grantee and Grantor. If either Grantee or Grantor are dissatisfied with the fair market value of the Retained Allen Land, as determined by the Appraiser, such party may commission a second appraisal (the "Second Appraisal) to be performed by a "Qualified Appraiser", provided that notice is given by the requesting party to the other party within ten (10) days after receipt of the First Appraisal. The second appraiser shall be instructed to complete the Second Appraisal within forty-five (45) days. If the Second Appraisal is within five percent (5%) of the value as determined by the first Appraisal, the value determined by the first Appraisal shall be deemed to be the Fair Market Value and the party requesting the Second Appraisal shall be solely responsible for the cost thereof. If the Second Appraisal varies by more than 5% from the value as determined by the first Appraisal, the parties shall designate a third Qualified Appraiser who shall be instructed to select either the First Appraisal or the Second Appraisal as the one he/she believes most accurately represents the fair market value of the Retained Allen Land. If the third appraiser selects the First Appraisal, the party requesting the Second Appraisal shall be solely responsible for the cost of the second and third appraisal. If the third appraiser selects the Second Appraisal,

the parties shall split the cost of all three appraisers. A "Qualified Appraiser" is a Maine licensed appraiser with at least five (5) years of experience appraising residential properties.

(ii) Closing: The Closing shall occur on the date that is 45 days after completion of such appraisal process. Grantor shall deliver to Grantee at Closing: (i) a Real Estate Transfer Tax Declaration of Value and any other documents as are reasonably necessary to convey the Retained Allen Land; (ii) an owners/seller's affidavit for the title insurance company issuing the title insurance policy to Grantee to allow the title company to omit from such policy all exceptions for unfiled mechanic's, materialmen's or similar liens arising from any action of Grantor and for parties in possession; (iii) a written notice, in form and substance reasonably satisfactory to Grantee, which written notice shall certify either: (A) that to the best of the Grantor's knowledge, there is no underground oil storage facilities located on the Retained Allen Land, or (B) pursuant to 38 M.R.S.A. § 563(6), if there are any such facilities on the Retained Allen Land, that the facilities exist and shall disclose its registration number or numbers, the exact location of the facilities, whether or not it has been abandoned in place, and that the facilities are subject to regulation by the Maine Board of Environmental Protection.

(iii) Title and Deed. At the Closing, Grantor shall execute and deliver to Grantee or its nominee a good and sufficient Warranty Deed, conveying the Retained Allen Land. It is condition to Grantee's obligations hereunder that Grantor convey the Retained Allen Land in fee simple, with good and marketable title thereto, free and clear of all liens and encumbrances, except for the following ("Permitted Exceptions"): (i) real estate taxes which are not yet due or payable; (ii) any encumbrances existing as of the date hereof, or that may be created or consented to by Grantee hereafter; (iii) zoning and land use regulations; and (iii) customary public utility easements serving the Retained Allen Land.

(iv) Possession; Condition of Retained Allen Land; Casualty Loss. Full possession of the Retained Allen Land will be transferred to Grantee at the Closing in substantially the same condition as the Retained Allen Land is in as of the date of the completion of construction of improvements on the Retained Allen Land, except for: 1) reasonable wear and tear; 2) any non-structural, cosmetic improvements or alterations that do not significantly impact the general character or quality of the Retained Allen Land or significantly diminish the Retained Allen Land exterior's conformity with the general character of Grantee's property in the Town of Cumberland; and 3) any other material improvements or alterations made to the Retained Allen Land by Grantor, its successors or assigns, after notice to Grantee with no objection made by Grantee within 30 days of receipt of such notice, to which Grantee shall make no unreasonable objection. Prior to Closing, the Grantor shall remove all of its personal property, waste and debris from the Retained Allen Land, and shall leave the Retained Allen Land in a clean and orderly condition.

Grantor shall bear the risk of loss to the Retained Allen Land, excepting the Road Access Area described above, prior to the Closing. Grantor agrees to maintain fire and casualty insurance on the Retained Allen Land for the full replacement cost thereof, and to provide evidence of such coverage upon request by Grantee from time to time Notwithstanding anything to the contrary set forth in this Agreement, if, prior to Closing, Two Hundred Thousand Dollars (\$200,000.00) or more of damage, as determined by Grantor's insurance company, is caused to the Retained

Allen Land by fire, casualty or otherwise, and such damage is not repaired and restored by Grantor within 180 days after the date of such fire or casualty and in any event prior to Closing, then Grantee may elect to terminate this Agreement by giving written notice to Grantor of its election to terminate this Agreement on or before the date that is ten (10) days after (i) the end of such 180-day period or (ii) the date that Grantor gives notice that it does not intend to repair, as applicable, to terminate this Agreement. If Grantor elects to repair any such damage or destruction, the Closing shall be extended, if necessary, to the date that is fifteen (15) business days after the expiration of such 180 day period; provided, however, that if such destruction or damage is repaired before the end of such 180 day period, Grantor shall have the right to close earlier by giving Grantee written notice setting a Closing Date for the Closing not sooner than twenty one (21) days after such notice, but in any event not sooner than the Closing Date specified above.

If Grantee does not give (or has no right to give) notice of termination within such period specified above: (i) this transaction shall close at Closing, (ii) Grantee shall pay the full applicable Purchase Price (subject to clause (iv) below), (iii) Grantor shall assign to Grantee the proceeds of any insurance policies payable to Grantor (or shall assign the right or claim to receive such proceeds after such Closing), and (iv) the amount of any deductible or self-insured or uninsured amount shall be a credit against the applicable Purchase Price. If Grantee timely delivers a notice of termination pursuant to this section, such that this Agreement is terminated prior to the Closing, the Grantor and Grantee shall have no further obligations or liabilities hereunder.

(v) Default. In the event Grantor or Grantee fails to perform any of its obligations as described herein and such default continues for a period of 15 days after written notice of default, the non-defaulting party may elect either: (a) to waive the default and continue the purchase and sale as if there had been no default; or (b) to terminate this Agreement; or (c) to employ all legal and equitable remedies, including, without limitation, the right of specific performance.

(vi) Benefits. Grantee covenants and agrees that Grantor, his wife and children shall have the right to use, without charge for as long as Grantor, his wife or children reside on the Retained Allen Land, all common facilities and amenities such as walking trails and wellness, educational and entertainment programs (but any meals and/or use of its assisted living and memory care programs and facilities shall be at the cost of Grantor at the ordinary charges therefor by Grantee) and events provided by Grantee to residents of its facilities in Falmouth, Maine and its facilities to be constructed in Cumberland, Maine. The provisions of this paragraph shall benefit Grantor and his family but not any unrelated future buyer of the Retained Allen Land. Grantee covenants and agrees that any restrictions, restrictive covenants or restrictions on use of Grantee's adjoining and nearby property shall not apply to the Retained Allen Land or the residence on the Retained Allen Land.

TO HAVE AND TO HOLD the aforegranted and bargained premises with all the privileges and appurtenances thereof to the said Ocean View at Cumberland, LLC, its successors and assigns and to them and their use and behoof forever.

AND the undersigned do COVENANT with the said Grantee, its successors and assigns forever, that the undersigned are lawfully seized in fee of the premises; that they are free of all encumbrances; that the undersigned have good right to sell and convey the same to the said Grantees to hold as aforesaid; and that the undersigned and our heirs and assigns shall and will WARRANT and DEFEND the same to the said Grantee, its successors and assigns forever, against the lawful claims and demands of all persons.

IN WITNESS WHEREOF, the said Laurence S. Allen, Jr. has hereunto set his hand and seal, this 31 day of May, 2018.

WITNESS:	\circ	ı
AX -	Jana Dana do Si	PM IL
Ryan C. Almy	Laurence S. Allen, Jr.	skent

The undersigned Ocean View at Cumberland, LLC, a Maine limited liability company, and Ocean View Retirement Community Limited Partnership for themselves and their successors and assigns hereby agree to the covenants and restrictions set forth in the foregoing deed.

Witness:

Ocan View & Camberland, LLC

John B. Wasileski, Its Manager

Ocean View Retirement Community Limited Partnership
By Ocean View Management Company, its General Partner

(as Gyarantor)

John B. Wasileski, Its President

STATE OF MAINE COUNTY OF CUMBERLAND, ss.

<u>5/3/</u>,2018

Then personally appeared the above-named Laurence S. Allen, Jr., and acknowledged the foregoing instrument to be his free act and deed, before me,

Attorney at Law Hotary Public

WARRANTY DEED

KNOW ALL PERSONS BY THESE PRESENTS, that Richard L. Doane and Hilary H. Doane, in consideration of One Dollar and other valuable considerations paid by Ocean View at Cumberland, LLC, a Maine limited liability company, whose mailing address is 20 Blueberry Lane, Falmouth, Maine, the receipt whereof is hereby acknowledged, do hereby GIVE, GRANT, BARGAIN, SELL AND CONVEY unto the said Ocean View at Cumberland, LLC, its successors and assigns forever, the following described real estate:

A certain lot or parcel of land located northeasterly of, but not adjacent to, Tuttle Road in the Town of Cumberland, County of Cumberland, State of Maine, bounded and described as follows:

Beginning at a 5/8" capped iron rod ("PLS 1273") on the northwesterly line of land now or formerly of Laurence S. Allen as described in a deed recorded in the Cumberland County Registry of Deeds in Book 3003, Page 347, said point of beginning being located N 20°58'41" E by said land of Allen a distance of Seven Hundred Thirty-Three and 90/100 (733.90) feet from the northeasterly sideline of Tuttle Road. Thence:

- 1. S 20°58'41" W by said land of Allen a distance of One Hundred Fifty-Two and 92/100 (152.92) feet to a point;
- 2. N 13°35'55" E through land of the Grantor a distance of Two Hundred Ninety-Two and 20/100 (292.20) feet to a point of curvature;
- 3. Northerly through said land of the Grantor, following a curve to the right having a radius of Five Hundred Twenty-Five and 00/100 (525.00) feet, an arc distance of One Hundred Eighty-Nine and 70/100 (189.70) feet to a point at said land of Allen, said point being located N 23°57'00" E a distance of One Hundred Eighty-Eight and 67/100 (188.67) feet from the last described point of curvature;
- 4. Southerly by said land of Allen, following a non-tangent curve to the right having a radius of One Thousand Nine Hundred Twenty and 36/100 (1920.36) feet, an arc distance of Three Hundred Twenty-Six and 84/100 (326.84) feet to the point of beginning, said point of beginning being located S 16°06'08" W a distance of Three Hundred Twenty-Six and 45/100 (326.45) feet from the last described point.

Bearings are referenced to grid north, Maine State Plane Coordinate System, NAD83, West Zone.

The above described parcel contains 9,664 square feet, more or less, being a portion of land now or formerly of Richard L. Doane and Hilary H. Doane as described in a deeds recorded in the Cumberland County Registry of Deeds in Book 34623, Page 269 and Book 33851, Page 331, Page 184.

TO HAVE AND TO HOLD the aforegranted and bargained premises with all the privileges and appurtenances thereof to the said Ocean View at Cumberland, LLC, its successors and assigns and to them and their use and behoof forever.

AND the undersigned do COVENANT with the said Grantee, its successors and assigns forever, that the undersigned are lawfully seized in fee of the premises; that they are free of all encumbrances; that the undersigned have good right to sell and convey the same to the said Grantees to hold as aforesaid; and

that the undersigned and our heirs and assigns shall and will WARRANT and DEFEND the same to the said Grantee, its successors and assigns forever, against the lawful claims and demands of all persons.

IN WITNESS WHEREOF, the said Richard L. Doane and Hilary H. Doane have hereunto set their hands and seals, this 2018.

WITNESS:

Zeek

Richard L. Doane

为公武

Hilary H. Doane

STATE OF MAINE COUNTY OF CUMBERLAND, ss.

uy 3/, 2018

Then personally appeared the above-named Richard L. Doane, and acknowledged the foregoing instrument to be his free act and deed, before me,

Attomey at Law Notary Public Rand H.C.

DLN: 1001840027973

WARRANTY DEED

KNOW ALL PERSONS BY THESE PRESENTS, that Richard W. Doane, in consideration of One Dollar and other valuable considerations paid by Ocean View at Cumberland, LLC, a Maine limited liability company, whose mailing address is 20 Blueberry Lane, Falmouth, Maine, the receipt whereof is hereby acknowledged, do hereby GIVE, GRANT, BARGAIN, SELL AND CONVEY unto the said Ocean View at Cumberland, LLC, its successors and assigns forever, the following described real estate:

A certain lot or parcel of land located northeasterly of, but not adjacent to, Tuttle Road in the Town of Cumberland, County of Cumberland, State of Maine, bounded and described as follows:

Beginning at a point on at the southeasterly line of land now or formerly of the Town of Cumberland as described in a deed recorded in the Cumberland County Registry of Deeds in Book 3710, Page 272, and the northwesterly corner of other land of the Town of Cumberland as described in a deed recorded in said Registry in Book 9970, Page 169; thence:

- 1. S 35°11'21" W by said other land of the Town of Cumberland, land now or formerly of David J. Small as described in a deed recorded in said Registry in Book 10779, Page 90, and land now or formerly of Daniel R. Small and Tricia A. Pettengill as described in a deed recorded in said Registry in Book 10871, Page 92 a distance of One Thousand Nine Hundred Forty-One and 17/100 (1941.17) feet to a 5/8" iron rod at land now or formerly of Laurence S. Allen, Jr. as described in a deed recorded in said Registry in Book 3003, Page 347;
- 2. N 14°19'11" W by said land of Allen a distance of Eight Hundred and 00/100 (800.00) feet to a point:
- 3. S 75°40'49" W by said land of Allen a distance of Twenty Eight and 00/100 (28.00) feet to a point;
- 4. N 06°50'50" W along land now or formerly of Richard L. Doane et al. a distance of Three Hundred Eighty-Five and 03/100 (385.03) feet to a point at land now or formerly of the Town of Cumberland as described in a deed recorded in said Registry in Book 15205, Page 237;
- 5. N 68°21'54" E by said land of the Town of Cumberland a distance of Fifty-Eight and 12/100 (58.12) feet to a 5/8" capped iron rod ("PLS 1280");
- 6. N 35°11'21" E by said land of the Town of Cumberland a distance of One Thousand One Hundred Twelve and 87/100 (1112.87) feet to a point:

7. S 54°30'35" E by said land of the Town of Cumberland a distance of Eight Hundred Fifty-Two and 61/100 (852.61) feet to the point of beginning.

Bearings are referenced to grid north, Maine State Plane Coordinate System, NAD83, West Zone.

The above described parcel contains 31.0 acres, more or less, being a portion of land now or formerly of Richard W. Doane as described in a deed recorded in the Cumberland County registry of Deeds in Book 2851, Page 184 and a portion of land now or formerly of land of Richard Doane as described in a deed recorded in said Registry in Book 15205, Page 239.

Grantee, its successors and assigns covenant and agree that no more than 50 single family residential dwelling units (and related amenities and common facilities, including a common community or activity building, and also including parking, utilities, drainage, detention and other site improvements) will be constructed on the above described property (this restriction shall not apply to any dwelling units or other improvements to be constructed by Grantee, its successors and assigns on any other adjoining property that Grantee, its successors and assigns may elect to acquire). The restrictions set forth in this paragraph shall be in effect for only as long as Richard L. Doane or Hilary H. Doane or any of their children or any of their grandchildren own the property described in the deed recorded in said Registry, Book 16894, Page 185 or the property described in the deed recorded in said Registry, Book 22850, Page 251.

Grantee, its successors and assigns further covenant and agree that they shall not grant any easements or create any trails of any kind including for snowmobiles, ATVs, bikes or pedestrians in the following described area: Beginning at a point on a line of land now or formerly of the Town of Cumberland as described in a deed recorded in the Cumberland County Registry of Deeds in Book 3710, Page 272, said point of beginning being located S 68°21'54" W a distance of Six and 40/100 (6.40) feet from a capped 5/8" iron rod "PLS 1280" at the easterly corner of land now or formerly of Richard Doane as described in a deed recorded in said Registry in Book 15205, Page 239; thence S 06°50'50" E a distance of Four Hundred Forty-Two and 10/100 (442.10) feet to a point; thence S 75°40'49" W a distance of Eighty-Eight and 28/100 (88.28) feet to a point and land now or formerly of Richard L. Doane and Hilary H. Doane as described in deeds recorded in said Registry in Book 34623, Page 269 and Book 33851, Page 331; thence Northerly by said land of Richard L. Doane and Hilary H. Doane, following a non-tangent curve to the left having a radius of One Thousand Nine Hundred Twenty and 36/100 (1920.36) feet, an arc distance of Fifty-Two and 62/100 (52.62) feet to a 3/4" iron pipe and said land of Richard Doane, said iron pipe being located N 03°50'47" E a distance of Fifty-Two and 62/100 (52.62) feet from the last described point; thence N 75°40'49" E a distance of Twenty-Eight and 00/100 (28.00) feet to a point; thence N 06°50'50" W by said land of Richard W. Doane, by land of Richard L. Doane and Hilary H. Doane as described in a deed recorded in said Registry in Book 34583, Page 33, a distance of Three Hundred Eighty-Five and 03/100 (385.03) feet to a point and said land of the Town of Cumberland; thence N 68°21'54" E by said land of the Town of Cumberland a distance of Fifty-One and 72/100 (51.72) feet to the point of beginning. Bearings are referenced to grid north, Maine State Plane Coordinate System, NAD83, West Zone. The above described no snowmobile or trail area contains 23,579 square feet, more or less, lying over a portion of land now or formerly of Richard Doane as described in a deed

recorded in the Cumberland County Registry of Deeds in Book 15205, Page 239, a portion of land now or formerly of Richard W. Doane as described in a deed recorded in said Registry in Book 2851, Page 184, and a portion of land now or formerly of Laurence S. Allen as described in a deed recorded in said Registry in Book 3003, Page 347.

Grantee, its successors and assigns agree to develop the sidewalk of Little Acres Drive substantially as shown on the preliminary subdivision plan submitted to the Town of Cumberland Planning Board.

TO HAVE AND TO HOLD the aforegranted and bargained premises with all the privileges and appurtenances thereof to the said Ocean View at Cumberland, LLC, its successors and assigns and to them and their use and behoof forever.

AND the undersigned do COVENANT with the said Grantee, its successors and assigns forever, that the undersigned are lawfully seized in fee of the premises; that they are free of all encumbrances; that the undersigned have good right to sell and convey the same to the said Grantees to hold as aforesaid; and that the undersigned and our heirs and assigns shall and will WARRANT and DEFEND the same to the said Grantee, its successors and assigns forever, against the lawful claims and demands of all persons.

IN WITNESS WHEREOF, the said Richard W. Doane, by Jeffrey W. Doane, attorney in fact under a Power of Attorney dated September 9, 2011 and recorded in the Cumberland County Registry of Deeds, Book 31294, Page 185, has hereunto set his hand and seal, this <u>25</u> day of May, 2018.

WITNESS:

STATE OF MAINE COUNTY OF CUMBERLAND, ss.

May 25th, 2018

Richard W. Doane by Jeffrey W. Doane, attorney in

fact under a Power of Attorney dated September 9.

Then personally appeared the above-named Jeffrey W. Doane, attorney in fact for Richard W. Doane, and acknowledged the foregoing instrument to be his free act and deed in said capacity, before me,

2011

Shela Nodine
Sheila Nodine

MY COMMISSION EXPIRES
JUNE 5, 2025

License Agreement

This license agreement ("Agreement") is effective as of ____, 2018, between OceanView at Cumberland, LLC ("OceanView") and the Town of Cumberland (the "Town") to permit the use of a portion of property owned by OceanView in Cumberland, Maine, (the "Property") for recreational use by the residents of Cumberland and surrounding towns.

WHEREAS, OceanView proposes to develop a portion of the Property for residential development; and

WHEREAS, OceanView wishes to make a portion of the Property available to the Town for recreational use compatible with OceanView's proposed development and believes that such use may occur in a manner that is compatible with the proposed development; and

WHEREAS, the Town wishes to use a portion of the Property for recreational use.

NOW THEREFORE, OceanView and the Town (the "Parties") agree as follows:

- 1. OceanView shall make available a multi-use trail across the Property, located as shown generally on the attached Exhibit "A" (the "Multi-Use Trail"), for recreational use for residents of Cumberland and surrounding towns during all seasons.
- 2. The Multi-Use Trail may be used by snowmobiles, as well as for pedestrian, bicycle, cross country skiing and other similar non-motorized recreational uses. The Multi-Use Trail may also be used by dogs, when leashed and accompanied by their owners.
- 3. OceanView shall contribute all funds necessary to construct and improve the Multi-Use Trail and shall also contribute all funds necessary to improve any portion of the connector trail shown on the attached Exhibit "A" on property owned by the Town (the "Town Trail"), in an amount not to exceed \$10,000.
- 4. The Town agrees to use reasonable efforts to maintain the Multi-Use Trail free of debris and trash, and to maintain the Multi-Use Trail such that it can be safely used for the permitted uses as note herein. OceanView shall be responsible for all repairs necessary for the continued use of the Multi-Use Trail and the Town shall maintain the Town Trail.
- 5. OceanView shall be responsible for obtaining any permits required from any local, state, or federal board, commission, or agency, necessary for the construction and operation of the Multi-Use Trail and the Town shall be responsible for obtaining any permits required for any required improvements to the Town Trail.
- 6. Use of the Multi-Use Trail shall be subject to reasonable rules set by OceanView, which may be revised or amended from time to time. The Multi-Use Trail may be used during daylight hours between 7 am and 7 pm daily, and snowmobiles shall not exceed a posted limit of 10 miles per hour. The Multi-Use Trail is a connector trail, and no user shall stop for any significant period for picnicking or other similar activities.

- 7. In the event OceanView determines that the continued use of the Multi-Use Trail for any particular form of recreation is resulting in unreasonable adverse impacts to the adjacent residential uses, OceanView shall contact the Town to discuss its concerns. The Parties shall work in good faith to address any such concerns, including identifying any modifications to the terms and conditions of the use of the Multi-Use Trail deemed necessary by the Parties. OceanView commits to using best efforts working with the Town to ensure the continued use of the Multi-Use Trail for all recreational uses cited herein.
- 8. If, notwithstanding the efforts of the Parties, concerns about the compatibility of the use of the Multi-Use Trail with adjacent residential uses cannot be resolved, OceanView retains the right, in the exercise of its sole discretion, to terminate this Agreement and discontinue the use of the Multi-Use Trail for any use(s).
- 9. The rights granted herein are contingent on OceanView obtaining all local, state, and federal permits and approvals necessary to acquire and develop the Property as planned, and to construct and improve the Multi-Use Trail.
- 10. Subject to the provisions in Section 7, the Town agrees that the rights granted herein are revocable by OceanView, and no rights granted herein are deemed to provide the Town with any permanent right to use or occupy any portion of the Property, including the Multi-Use Trail.

SEEN AND AGREED TO:		
, 2018		
OceanView at Cumberland, LLC		Town of Cumberland
By:	By:	
Its:	Its:	



July 31, 2018

Frederic (Rick) Licht, PE, LSE Licht Environmental Design, LLC 35 Fran Circle Gray, Maine 04039

Re: Oceanview at Cumberland, CU

Ability to Serve with PWD Water

Dear Mr. Licht:

The Portland Water District has received your request for an Ability to Serve Determination for the noted site submitted on June 7, 2017. Based on the information provided per plans dated July 31, 2018, we can confirm that the District will be able to serve the proposed project as further described in this letter. Please note that this letter constitutes approval of the water system as currently designed. Any changes affecting the approved water system will require further review and approval by PWD.

Conditions of Service

The following conditions of service apply:

- The District can confirm that the existing water and sewer systems in Tuttle Road have the capacity to serve the additional single family house lots within the Oceanview at Cumberland Subdivision in Cumberland. A 12-inch ductile iron water main extension will be required from the end of the Phase 1 water main extension to at least the center of the last lot to be served within the subdivision.
- New 1.5-inch domestic water services may be installed from the 12-inch water main extension within the subdivision.
- It is the District's understanding that all single family homes within the subdivision will require an NFPA 13D life safety sprinkler system. A single service line may be used to serve both domestic and fire protection needs. The split for the sprinkler service must be located after the water meter and must include a non-testable backflow prevention device.
- Our records show that the site is currently served with a 12-inch ductile iron water main installed during Phase 1 in 2018.

Prior to construction, the owner or contractor will need to complete the Main Extension Initiation form and pay all necessary fees. PWD will guide the applicant through the new development process.

Existing Site Service

According to District records, the project site does currently have existing water service. A 12-inch diameter ductile iron water main installed in Phase 1 provides water service to the site. Please refer to the "Conditions of Service" section of this letter for requirements related to the use of this service.

Water System Characteristics

According to District records, there is an 12-inch diameter cast iron water main in Tuttle Road and a public fire hydrant located approximately 500 feet from the site. Recent flow data is not available in this area. The most recent static pressure reading was 101 psi.

Public Fire Protection

The installation of new public hydrants to be accepted into the District water system will most likely be required. It is your responsibility to contact the Town of Cumberland Fire Department to ensure that this project is adequately served by existing and/or proposed hydrants.

Domestic Water Needs

The data noted above indicates there should be adequate pressure and volume of water to serve the domestic water needs of your proposed project. Based on the high water pressure in this area, we recommend that you consider the installation of pressure reducing devices that comply with state plumbing codes.

Private Fire Protection Water Needs

You have indicated that this project will require water service to provide private fire protection to the site. Please note that the District does not guarantee any quantity of water or pressure through a fire protection service. Please share these results with your sprinkler system designer so that they can design the fire protection system to best fit the noted conditions. If the data is out of date or insufficient for their needs, please contact MEANS to request a hydrant flow test and we will work with you to get more complete data.

Should you disagree with this determination, you may request a review by the District's Internal Review Team. Your request for review must be in writing and state the reason for your disagreement with the determination. The request must be sent to MEANS@PWD.org or mailed to 225 Douglass Street, Portland Maine, 04104 c/o MEANS. The Internal Review Team will undertake review as requested within 2 weeks of receipt of a request for review.

If the District can be of further assistance in this matter, please let us know.

Sincerely, Portland Water District

Robert A. Bartels, P.E. Senior Project Engineer

BUSISHS



TOWN OF CUMBERLAND, MAINE 290 TUTTLE ROAD

CUMBERLAND, MAINE 04021

TEL: 207-829-2205 FAX: 829-2224

May 22, 2018

Rick Licht, PE, LSE Licht Environmental Design, LLC 35 Fran Circle Gray, Maine 04039

Re: OceanView at Cumberland

Cumberland, Maine

Dear Rick:

The Town of Cumberland agrees to accept the sewer design flow from your project on Tuttle Road. The Town has the capacity to handle the requested flow amounts. Each unit will be required to have its own account and each permit will be \$500. Monthly bills will be assessed upon occupancy through the Portland Water District.

Cumberland is a relatively new sewer system (less than 30 years in age) and we have been fortunate to have limited inflow and infiltration in our system. We presently own 30% of the Falmouth Treatment Plant. This new flow would be pumped via our Route One distribution system.

Please let me know if you have any additional questions regarding this request.

Sincerely,

William R. Shane, P.E.

Town Manager

cc: Carla Nixon, Director of Planning

Bill Longley, Code Enforcement Officer

Town of Falmouth

Wastewater Treatment Facilities ~ 271 Falmouth Road ~ Falmouth, Maine 04105 (207) 781-4462 ~ (Fax 781-2052)

December 19,2017

Mr. Rick Licht, PE Licht Environmental Design, LLC 35 Fran Circle Gray, Maine 04039

Regarding: Oceanview satellite community, Cumberland - Capacity to Serve

Dear Mr. Licht;

In response to your inquiry related to the planned 50 to 100 housing unit development proposed in Cumberland, the Town of Cumberland current utilizes approximately one-half of their daily capacity allotment of 468,000 gallons per day. Sewage collection and treatment facilities that are in Falmouth and are shared with Cumberland through the Town's contractual agreements with the Portland Water District, have adequate capacity to accommodate the 9000 to 18,500 gallons per day of sewage flow the development is projected to contribute.

If you require additional information or I can be of any other assistance, please feel free to contact me.

Sincerely:

Robert Clark Superintendent

cc: Chris Wasileski. Matt Teare 2 DeLorme Drive • Yarmouth, ME 04096 • Phone: (207) 621-8000 • www.SummitNaturalGasMaine.com

May 4, 2018

Via Hand Delivery

OceanView Retirement Community, LP Tuttle Rd Cumberland, ME

Re: Natural Gas Service

Dear Rick.

Thank you for your interest in receiving natural gas service from Summit Natural Gas of Maine, Inc. We are excited that you are considering developing a senior living community on Tuttle Road, Cumberland, Maine, that will be capable of using natural gas as an energy source. We understand that the Phase 1 development plan includes construction of 52 residential cottages, and that an additional 50 cottages may be constructed as part of the Phase 2 development plan.

If the community is engineered and constructed to receive natural gas service, we anticipate being able to provide natural gas service to the community by installing approximately 5100 linear feet of natural gas main line. After further discussion, we should be able to provide you a projected timeframe for completing installation and commencing service.

Any natural gas service will be provided in accordance with our Terms and Conditions of Service currently on file with Maine Public Utilities Commission. For a copy of the Terms and Conditions of Service, please visit http://summitnaturalgasmaine.com/rates-tariff.

Thank you for your interest in Summit as your natural gas provider. We look forward to speaking with you soon.

Sincerely Wash ton

Arthur Woolverton

Director of Sales and Marketing



7/30/2018

Frederic Licth Licht Environmental Design, LLC 35 Fran Circle Gray, Maine 04039

Sent via email

RE: Ability to Serve Letter for Oceanview at Cumberland in Cumberland, ME

Dear Mr. Licth:

CMP has the ability to serve your proposed project located on Tuttle Road in Cumberland, Maine, in accordance with our CMP Handbook (web link below). We can provide you the desired pole or pad mounted transformers per your request and city approval, in accordance with our CMP Standards Handbook. If you have any questions on the process, or need help in completion of the documents, please feel free to contact me. Should this project be single phase with all self-contained metering, then you will be dealing directly with the Portland Service Center. If you require a polyphase service a line extension would have to be completed.

New Service Milestones

- Call 1-800-565-3181 to establish a new account and an SAP work order. Please provide both of these
 to me.
- Submit Load information. Please complete this CMP spreadsheet using load information
- Submit the easement information worksheet. Please complete this CMP form and either email or fax back to us.
- Submit any electronic drawings (PDF (preferred) or DWG files) of the site layout and proposed electrical connections if you have them.
- Preliminary meetings with CMP Advisor and Engineer to determine details of job (I will need to schedule with your electrician/contractor-please let me know who this is)
- Field planner design appointment to cost out job and develop CMP Invoice.
- Submit invoice for payment.
- Easements signed and payment received.
- Job scheduled for completion after the electrical inspection has been received.

This process can take several months, depending upon several factors including transformer delivery, potential substation upgrades, return of completed paperwork, and other jobs in the system that may be ahead of yours. In addition, contact with the other utilities, including telephone and cable, should be commenced as soon as practical. They may have additional work or charges in addition to the CMP work required to bring your project on line.





Please complete the attached forms (specific instructions are on each form) and email them back to me at your earliest convenience.

For your convenience, here is a link to the CMP Website which contains our Handbook with details on most service requirements:

CMP Handbook of Standard Requirements

(http://www.cmpco.com/MediaLibrary/3/6/Content%20Management/YourAccount/PDFs%20and%20Docs/handbook.pdf)

If you have any questions, please contact me.

Regards.

Supervisor-Energy Services Central Maine Power Company

CENTRAL MAINE POWER

www.cmpco.com
An equal opportunity employer

URBAN SERIES

URBAN LUMINAIRE

Cat.# URBCAP-26/36NB-80/4K/UNV/T3/PEC-208/GENI-XX/NRNW/BBT

Job

OceanView at Cumberland

Type

SA



Approvals

SPECIFICATIONS

Intended Use:

The Beacon Urban luminaire is available with a choice of different LED wattage configurations, shapes, sizes and optical distributions designed to replace HID lighting up to 400W MH or HPS.

Construction:

- The drivers shall be located in the top cast housing and shall be accessible without tools by hinging the lower shade assembly. The driver and all electrical components shall be on a tray.
- The lower shade shall be made from a onepiece aluminum spinning.
- The housing is designed for LED thermal management without the use of metallic screens, cages, or fans. The top casting shall be able to be pendent mounted in place with a stainless steel safety pin and then permanently held in place with four stainless steel bolts.

Electrical:

- 100V through 277V, 50 Hz to 60 Hz (UNV), or 347V or 480V input.
- Power factor is ≥0.90 at full load.
- Dimming drivers are standard with connections for external dimming equipment available upon request.
- Component-to-component wiring within the luminaire may carry no more than 80% of rated load and is listed by UL for use at 600VAC at 50°C or higher.
- · Plug disconnects are listed by UL for use at 600 VAC, 13A or higher. 13A rating applies to primary (AC) side only.
- Fixture electrical compartment shall contain all LED driver components.
- Button photocell available.
- Ambient operating temperature -40°C to 40°C
- Surge protection 20KA.
- Lifeshield™ Circuit protects luminaire from excessive temperature. The device shall activate at a specific, factory-preset temperature, and progressively reduce power over a finite temperature range. A luminaire equipped with the device may be reliably operated in any ambient temperature up to 55°C (131°F). Operation shall be smooth and undetectable to the eye. Thermal circuit is designed to "fail on", allowing the luminaire to revert to full power in the event of an interruption of its power supply, or faulty wiring connection to the drivers. The device shall be able to co-exist with other 0-10V control devices (occupancy sensors, external dimmers, etc.).

Controls/Options:

- · Available with Energeni for optional set dimming, timed dimming with simple delay, or timed dimming based on time of night
- www.beaconproducts.com/products/energeni
- Urban can be specified with SiteSync™ wireless control system for reduction in energy and maintenance cost while optimizing light quality 24/7. See ordering information or visit: www.hubbelllighting.com/products/sitesync/ for more details

Finish:

- IFS polyester powder-coat electrostatically applied and thermocured.
- IFS finish consists of a five stage pretreatment regimen with a polymer primer sealer and top coated with a thermoset super TGIC polyester powder coat finish.
- The finish meets the AAMA 605.2 performance specification which includes passing a 3000 hour salt spray test for corrosion resistance and resists cracking or loss of adhesion per ASTM D522 and resists surface impacts of up to 160 inch-pounds.

Certifications:

- DesignLights Consortium (DLC) qualified, consult DLC website for more details: http:// www.designlights.org/QPL
- NRTL Certified, UL8750, UL 1598 and CSA22.2#250. 13-14 for wet locations
- IDA approved
- This product is approved by the Florida Fish and Wildlife Conservation Commission. Separate spec available at
- http://www.beaconproducts.com/products/urban

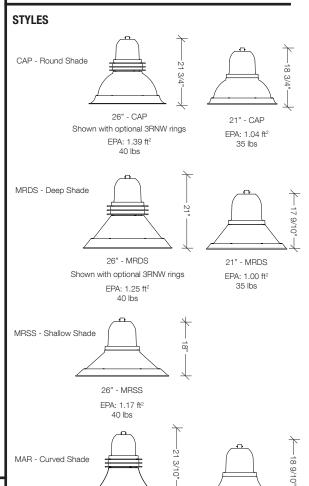
Warranty:

Five year limited warranty for more information visit:

www.hubbelllighting.com/resources/warranty

PRODUCT IMAGE(S)





26" - MAF

Shown with optional 3RNW rings

EPA: 1.25 ft²

CERTIFICATIONS/LISTINGS







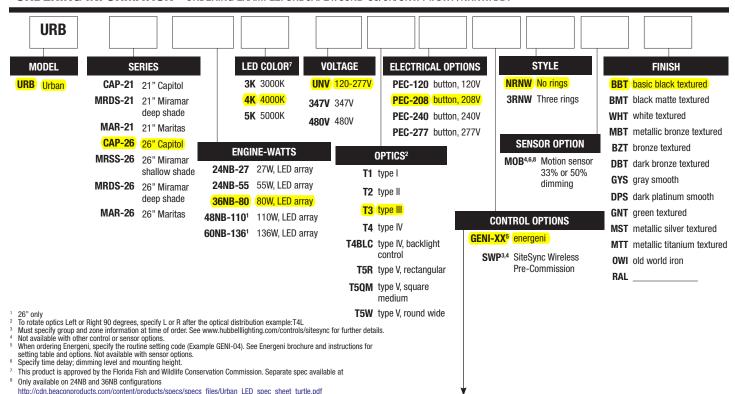


21" - MAR

EPA: 1.00 ft²

35 lbs

ORDERING INFORMATION ORDERING EXAMPLE: URBCAP21/36NB-80/5K/UNV/T4/SWP/NRNW/BBT



PRECOMMISSIONED SITESYNC ORDERING INFORMATION: When ordering a fixture with the SiteSync lighting control option, additional information will be required to complete the order. The SiteSync Commissioning Form or alternate schedule information must be completed. This form includes Project location, Group information, and Operating schedules. For more detailed information please visit https://www.hubbelllighting.com/products/sitesync/ or contact Hubbell Lighting tech support at (800) 345-4928.

SiteSync fixtures with Motion control (SWPM) require the mounting height of the fixture for selection of the lens.

Examples: URB/CAP-26/60NB-136/3K/UNV/T5QM/SWP/NRNW/BBT SiteSync only URB/CAP-26/60NB-136/3K/UNV/T5QM/SWPM-20F/NRNW/BBT SiteSync with Motion Control



SiteSync Lighting Control is available from our most popular brands in a broad range of award-winning product families.

Accessories and Services (Ordered Separately)

Accessories and Services (Ordered Separately)						
Catalog Number Description						
SWUSB*^	SiteSync interface software loaded on USB flash drive for use with owner supplied PC (Windows based only). Includes SiteSync license, software and USB radio bridge node.					
SWTAB*^	Windows tablet and SiteSync interface software. Includes tablet with preloaded software, SiteSync license and USB radio bridge node.					
SWBRG+	SiteSync USB radio bridge node only. Order if a replacement is required or if an extra bridge node is requested.					

 $^{^{\}star}$ When ordering SiteSync at least one of these two interface options must be ordered per project.

ELECTRICAL DATA

LLLUIIIIO	IL DAIA				
# OF LEDS	NUMBER OF DRIVERS	DRIVE CURRENT (mA)	INPUT VOLTAGE (V)	SYSTEM POWER (w)	CURRENT (Amps)
			120	· í	0.2
0.4		0504	277	07	0.1
24	1	350mA	347	27	0.1
			480		0.1
			120		0.5
24	2	700 mA	277	55	0.2
24	4	700 IIIA	347	33	0.2
			480		0.1
			120		0.7
36	1	700 mA	277	80	0.3
30	'	700 mA	347	00	0.2
			480		0.2
			120		0.9
48	1	700 mA	277	110	0.4
40	'	700 IIIA	347	110	0.3
			480		0.2
			120		1.1
60	1	700 mA	277	136	0.5
bU	'	700 IIIA	347	130	0.4
			480		0.3

PROJECTED LUMEN MAINTENANCE

AMBIENT TEMP.	0	25 000	50,000	¹TM-21-11 60.000	100.000	Calculated L70 (HOURS)
TEIVII.		20,000	00,000	00,000	100,000	(Hoono)
25°C / 77°C	1.00	0.97	0.95	0.95	0.92	>470,000

¹ Projected per IESNA TM-21-11

Data references the extrapolated performance projections for the base model in a 40° C ambient, based on 10,000 hours of LED testing per IESNA LM-80-08.

AMBIENT TEMP	ERATURE	LUMEN MULTIPLIER
0°C	32°F	1.02
10°C	50°F	1.01
20°C	68°F	1.00
25°C	77°F	1.00
30°C	86°F	0.98
40°C	104°F	0.98

Use these factors to determine relative lumen output for average ambient temperatures from 0-40°C (32-104°F).





au If needed, an additional Bridge Node can be ordered.

PHOTOMETRICS

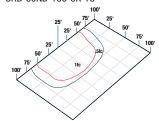
Type II URB-60NB-136-5K-T2



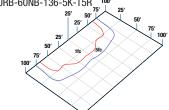
Type V Square Medium URB-60NB-136-5K-T5QM



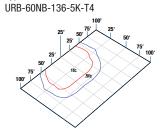
Type III URB-60NB-136-5K-T3



Type V Rectangular URB-60NB-136-5K-T5R



Type IV





PERFORMANCE DATA			5K			4K					3K							
				(5000	K nomina	I, 70	CRI)		(4000K	nomina	il, 70	CRI)		(3000K	nomina	ıl, 70	CRI)	
# LED'S	DRIVE CURRENT (MILLIAMPS)	SYSTEM WATTS (120- 277V)	DISTRIBUTION Type	LUMENS	LPW ¹	В	U	G	LUMENS	LPW ¹	В	U	G	LUMENS	LPW ¹	В	U	G
			T2	2833	105	1	0	1	2805	104	1	0	1	2408	89	1	0	1
			T3	2805	104	1	0	1	2777	103	1	0	1	2392	89	1	0	1
24	350 mA	27 W	T4	3086	114	1	0	1	3055	113	1	0	1	2623	97	1	0	1
24	330 IIIA	27 VV	T5QM	3085	114	2	0	0	3055	113	2	0	0	2623	97	1	0	0
			T5R	3142	115	2	0	2	3111	115	2	0	2	2670	99	2	0	2
			T5W	3044	113	2	0	1	3014	112	2	0	1	2600	96	2	0	1
			T2	5666	102	2	0	2	5610	101	2	0	2	4816	86	1	0	2
			T3	5610	101	1	0	2	5554	100	1	0	2	4784	86	1	0	2
24	700 mA	55 W	T4	6171	111	1	0	2	6110	109	1	0	2	5245	94	1	0	2
24	700111A	33 W	T5QM	6171	111	3	0	1	6110	109	3	0	1	5245	94	2	0	1
			T5R	6283	113	3	0	3	6221	111	3	0	3	5341	96	3	0	3
			T5W	6087	109	3	0	1	6027	108	3	0	1	5201	93	3	0	1
			T2	8505	101	2	0	3	8415	100	2	0	3	7224	87	2	0	2
		80 W	T3	8415	100	2	0	2	8331	99	2	0	2	7175	86	2	0	2
36	700 mA		T4	9256	110	1	0	3	9164	109	1	0	3	7868	94	1	0	3
	700 1111		T5QM	9257	110	3	0	1	9164	109	3	0	1	7868	94	3	0	1
			T5R	9425	112	3	0	3	9331	111	3	0	3	8011	96	3	0	3
			T5W	9131	109	3	0	2	9040	108	3	0	2	7801	93	3	0	2
			T2	11332	102	3	0	3	11220	101	3	0	3	9633	87	2	0	3
			T3	11220	101	2	0	3	11108	100	2	0	3	9567	86	2	0	3
48*	700 mA	110 W	T4	12342	111	2	0	3	12219	110	2	0	3	10491	95	2	0	3
			T5QM	12342	111	3	0	2	12219	111	3	0	2	10491	95	3	0	2
			T5R	12567	113	4	0	4	12441	112	4	0	4	10682	96	3	0	3
			T5W	12175	110	4	0	2	12053	109	4	0	2	10402	94	4	0	2
	60° 700 mA		T2	14165	103	3	0	3	14025	102	3	0	3	12041	88	3	0	3
		136 W	T3	14025	102	3	0	3	13885	101	3	0	3	11959	87	3	0	3
60 [*]			T4	15427	113	2	0	3	15274	111	2	0	3	13114	96	2	0	3
			T5QM	15427	113	4	0	2	15274	111	4	0	2	13314	96	3	0	2
			T5R	15708	115	4	0	4	15259	111	4	0	4	13352	97	4	0	4
			T5W	15218	111	4	0	2	15551	114	4	0	2	13002	95	4	0	2

Lumen values are from photometric tests performed in accordance with IESNA LM-79-08. Data is considered to be representative of the configurations shown. Actual performance may differ as a result of end-user environment and application.

'AVAILABLE IN THE 26" URBAN ONLY





ELECTRICAL DATA

# OF LEDS	NUMBER OF Drivers	DRIVE CURRENT (mA)	INPUT VOLTAGE (V)	SYSTEM POWER (w)	CURRENT (Amps)
24	1	350mA	120 277 347 480	27	0.2 0.1 0.1 0.1
24	2	700 mA	120 277 347 480	55	0.5 0.2 0.2 0.1
36	1	700 mA	120 277 347 480	80	0.7 0.3 0.2 0.2
48	1	700 mA	120 277 347 480	110	0.9 0.4 0.3 0.2
60	1	700 mA	120 277 347 480	136	1.1 0.5 0.4 0.3

PROJECTED LUMEN MAINTENANCE

AMBIENT				¹TM-21-11		Calculated L70
TEMP.	0	25,000	50,000	60,000	100,000	(HOURS)
25°C / 77°C	1.00	0.97	0.95	0.95	0.92	>470,000

¹ Projected per IESNA TM-21-11

Data references the extrapolated performance projections for the base model in a 40°C ambient, based on 10,000 hours of LED testing per IESNA LM-80-08.

AMBIENT TEMP	ERATURE	LUMEN MULTIPLIER
0°C	32°F	1.02
10°C	50°F	1.01
20°C	68°F	1.00
25°C	77°F	1.00
30°C	86°F	0.98
40°C	104°F	0.98

Use these factors to determine relative lumen output for average ambient temperatures from 0-40°C (32-104°F).





URBAN SERIES

URBAN LUMINAIRE

Cat.#URBCAP-26/36NB-80/4K/UNV/T5W/PEC-208/GENI-XX/NRNW/BBT

Job

OceanView at Cumberland

Type

SB



Approvals

SPECIFICATIONS

Intended Use:

The Beacon Urban luminaire is available with a choice of different LED wattage configurations, shapes, sizes and optical distributions designed to replace HID lighting up to 400W MH or HPS.

Construction:

- The drivers shall be located in the top cast housing and shall be accessible without tools by hinging the lower shade assembly. The driver and all electrical components shall be on a tray.
- The lower shade shall be made from a onepiece aluminum spinning.
- The housing is designed for LED thermal management without the use of metallic screens, cages, or fans. The top casting shall be able to be pendent mounted in place with a stainless steel safety pin and then permanently held in place with four stainless steel bolts.

Electrical:

- 100V through 277V, 50 Hz to 60 Hz (UNV), or 347V or 480V input.
- Power factor is ≥0.90 at full load.
- Dimming drivers are standard with connections for external dimming equipment available upon request.
- Component-to-component wiring within the luminaire may carry no more than 80% of rated load and is listed by UL for use at 600VAC at 50°C or higher.
- · Plug disconnects are listed by UL for use at 600 VAC, 13A or higher. 13A rating applies to primary (AC) side only.
- Fixture electrical compartment shall contain all LED driver components.
- Button photocell available.
- Ambient operating temperature -40°C to 40°C
- Surge protection 20KA.
- Lifeshield™ Circuit protects luminaire from excessive temperature. The device shall activate at a specific, factory-preset temperature, and progressively reduce power over a finite temperature range. A luminaire equipped with the device may be reliably operated in any ambient temperature up to 55°C (131°F). Operation shall be smooth and undetectable to the eye. Thermal circuit is designed to "fail on", allowing the luminaire to revert to full power in the event of an interruption of its power supply, or faulty wiring connection to the drivers. The device shall be able to co-exist with other 0-10V control devices (occupancy sensors, external dimmers, etc.).

Controls/Options:

- · Available with Energeni for optional set dimming, timed dimming with simple delay, or timed dimming based on time of night
- www.beaconproducts.com/products/energeni
- Urban can be specified with SiteSync™ wireless control system for reduction in energy and maintenance cost while optimizing light quality 24/7. See ordering information or visit: www.hubbelllighting.com/products/sitesync/ for more details

Finish:

- IFS polyester powder-coat electrostatically applied and thermocured.
- IFS finish consists of a five stage pretreatment regimen with a polymer primer sealer and top coated with a thermoset super TGIC polyester powder coat finish.
- The finish meets the AAMA 605.2 performance specification which includes passing a 3000 hour salt spray test for corrosion resistance and resists cracking or loss of adhesion per ASTM D522 and resists surface impacts of up to 160 inch-pounds.

- DesignLights Consortium (DLC) qualified, consult DLC website for more details: http:// www.designlights.org/QPL
- NRTL Certified, UL8750, UL 1598 and CSA22.2#250. 13-14 for wet locations
- IDA approved
- This product is approved by the Florida Fish and Wildlife Conservation Commission. Separate spec available at
- http://www.beaconproducts.com/products/urban

Warranty:

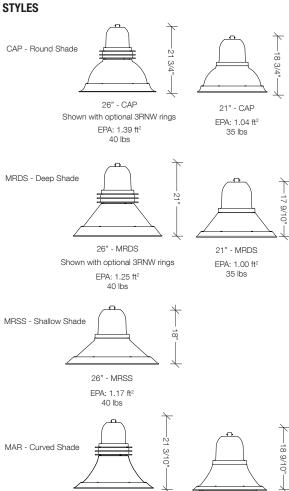
Five year limited warranty for more information visit:

www.hubbelllighting.com/resources/warranty

PRODUCT IMAGE(S)



Shown with SiteSync™



CERTIFICATIONS/LISTINGS









21" - MAR

EPA: 1.00 ft²

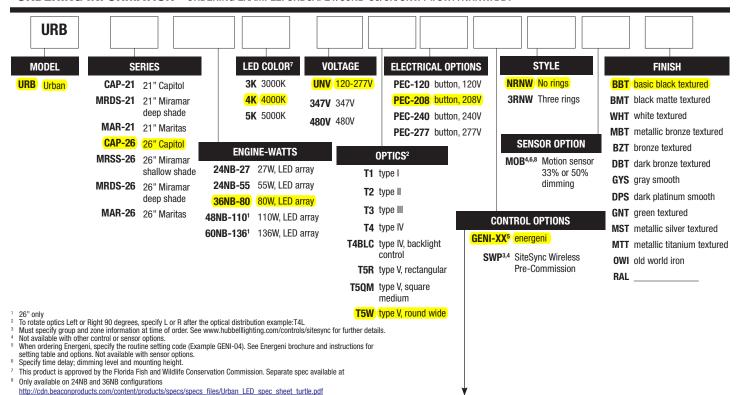
35 lbs

26" - MAR

Shown with optional 3RNW rings

EPA: 1.25 ft²

ORDERING INFORMATION ORDERING EXAMPLE: URBCAP21/36NB-80/5K/UNV/T4/SWP/NRNW/BBT



PRECOMMISSIONED SITESYNC ORDERING INFORMATION: When ordering a fixture with the SiteSync lighting control option, additional information will be required to complete the order. The SiteSync Commissioning Form or alternate schedule information must be completed. This form includes Project location, Group information, and Operating schedules. For more detailed information please visit https://www.hubbelllighting.com/products/sitesync/ or contact Hubbell Lighting tech support at (800) 345-4928.

SiteSync fixtures with Motion control (SWPM) require the mounting height of the fixture for selection of the lens.

Examples: URB/CAP-26/60NB-136/3K/UNV/T5QM/SWP/NRNW/BBT SiteSync only URB/CAP-26/60NB-136/3K/UNV/T5QM/SWPM-20F/NRNW/BBT SiteSync with Motion Control



SiteSync Lighting Control is available from our most popular brands in a broad range of award-winning product families.

Accessories and Services (Ordered Separately)

Accessories and Services (Ordered Separately)						
Catalog Number	Description					
SWUSB*^	SiteSync interface software loaded on USB flash drive for use with owner supplied PC (Windows based only). Includes SiteSync license, software and USB radio bridge node.					
SWTAB*^	Windows tablet and SiteSync interface software. Includes tablet with preloaded software, SiteSync license and USB radio bridge node.					
SWBRG+	SiteSync USB radio bridge node only. Order if a replacement is required or if an extra bridge node is requested.					

 $^{{}^{\}star}\text{When ordering SiteSync at least one of these two interface options must be ordered per project.}$

ELECTRICAL DATA

LLLUIIIIU	IL DAIA				
" OF 1 FDO	NUMBER OF	DRIVE CURRENT	INPUT VOLTAGE		CURRENT
# OF LEDS	DRIVERS	(mA)	(V)	(w)	(Amps)
			120		0.2
24	1	350mA	277	27	0.1
24	'	SSUIIA	347	21	0.1
			480		0.1
			120		0.5
24	2	700 mA	277	55	0.2
24	4	700 mA	347	33	0.2
			480		0.1
			120		0.7
36	1	700 4	277	80	0.3
30	'	700 mA	347		0.2
			480		0.2
			120		0.9
40	1	700 4	277	110	0.4
48	'	700 mA	347	110	0.3
			480		0.2
			120		1.1
60	4	700 m 4	277	100	0.5
60	1	700 mA	347	136	0.4
			480	1	0.3

PROJECTED LUMEN MAINTENANCE

AMBIENT				¹TM-21-11		Calculated L70
TEMP.	0	25,000	50,000	60,000	100,000	(HOURS)
25°C / 77°C	1.00	0.97	0.95	0.95	0.92	>470,000

¹ Projected per IESNA TM-21-11

Data references the extrapolated performance projections for the base model in a 40°C ambient, based on 10,000 hours of LED testing per IESNA LM-80-08.

AMBIENT TEMP	ERATURE	LUMEN MULTIPLIER
0°C	32°F	1.02
10°C	50°F	1.01
20°C	68°F	1.00
25°C	77°F	1.00
30°C	86°F	0.98
40°C	104°F	0.98

Use these factors to determine relative lumen output for average ambient temperatures from 0-40°C (32-104°F).





au If needed, an additional Bridge Node can be ordered.



a compact control device that gives lighting owners a simple way to save on energy costs...









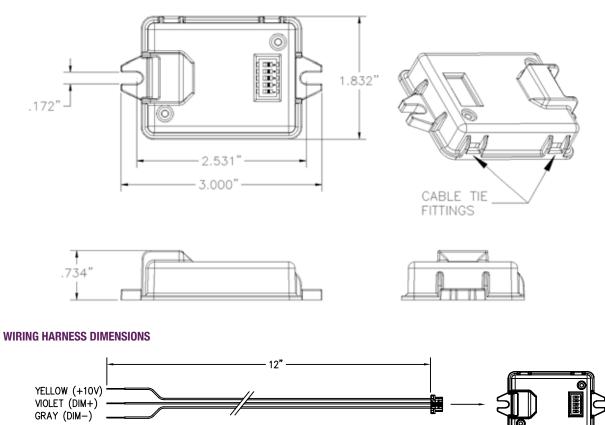


The **ENERGENI** lighting control system is a simple way for owners to save money by dimming the fixtures during unoccupied hours.



The **ENERGENI** has flexible setting options to work with fixtures activated by photocontrols or time clocks. The delay and dimming level options can be configured at the factory or re-configured at will in the field without the need for special cables or computers.

ENERGENI PRODUCT DIMENSIONS



Routine Setting Chart

32 Pre-programmed functional settings

SETTING OPTIONS

The ENERGENI has 32 pre-programmed functional settings that can be selected with its five DIP switches. The combination of switch settings allows for options of set dimming, timed diming with a simple delay or timed diming based on hours of operation or time at night.



	Switch Settings (0 = Down, 1 = Up)								
Routine Number	Switch 1	Switch 2	Switch 3	Switch 4	Switch 5	Brightness %	Energy Savings %	Simple Delay (Hrs.)	Variable Delay Estimated Time
01	0	0	0	0	0	100	0	0	
02	1	0	0	0	0	20	80	0	
03	0	1	0	0	0	20	80	3	
04	1	1	0	0	0	20	80	5	
05	0	0	1	0	0	20	80	7	
06	1	0	1	0	0	20	80	9	
07	0	1	1	0	0	40	60	0	
08	1	1	1	0	0	40	60	3	
09	0	0	0	1	0	40	60	5	
10	1	0	0	1	0	40	60	7	
11	0	1	0	1	0	40	60	9	
12	1	1	0	1	0	60	40	0	
13	0	0	1	1	0	60	40	3	
14	1	0	1	1	0	60	40	5	
15	0	1	1	1	0	60	40	7	
16	1	1	1	1	0	60	40	9	
17	0	0	0	0	1	20	80		6:00 pm
18	1	0	0	0	1	20	80		8:00 pm
19	0	1	0	0	1	20	80		10:00 pm
20	1	1	0	0	1	20	80		12:00 am
21	0	0	1	0	1	20	80		2:00 am
22	1	0	1	0	1	40	60		6:00 pm
23	0	1	1	0	1	40	60		8:00 pm
24	1	1	1	0	1	40	60		10:00 pm
25	0	0	0	1	1	40	60		12:00 am
26	1	0	0	1	1	40	60		2:00 am
27	0	1	0	1	1	40	60		4:00 am
28	1	1	0	1	1	60	40		6:00 pm
29	0	0	1	1	1	60	40		8:00 pm
30	1	0	1	1	1	60	40		10:00 pm
31	0	1	1	1	1	60	40		12:00 am
32	1	1	1	1	1	60	40		2:00 am

beacon products / design. performance. technology

RSA-B-SHO-S SERIES POLES ROUND STRAIGHT ALUMINUM

RSA-B-SHO-S-14-40-OT-BBT

Job

OceanView at Cumberland

Type



Approvals

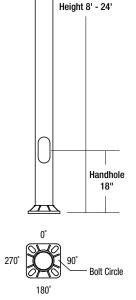
APPLICATIONS

· Lighting installations for side and top mounting of luminaires with effective projected area (EPA) not exceeding maximum allowable loading of the specified pole in its installed geographic location

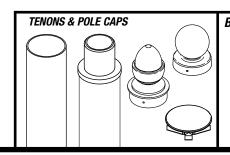
CONSTRUCTION

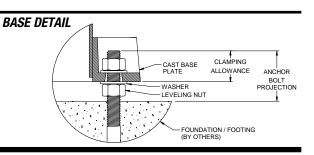
- SHAFT: One-piece straight aluminum with round cross section; Extruded shafts of 6061-T6 aluminum in 1/8", 3/16", or 1/4" thickness. Base plate of 356 cast aluminum.
- POLE CAP OR FINALS: Cap or decorative finials available for side mounted luminaires. Open top or tenons provided for post top mounted luminaires.
- HAND HOLE: Aluminum hand hole frame; Mounting provisions for grounding lug located behind cover
- ANCHOR BOLTS: Four galvanized anchor bolts provided per pole with minimum yield of 55,000 psi (ASTM F1554). Galvanized hardware with two washers and two nuts per bolt for leveling

- Durable thermoset polyester powder coat paint finish with nominal 3.0 mil thickness
- Powder paint finish coat available in twelve standard colors; Custom colors available; RAL number preferable.

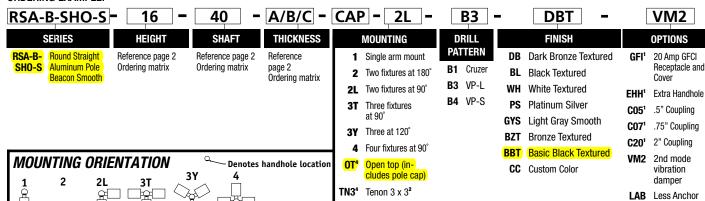


Overall





ORDERING EXAMPLE:



TN4⁴

TN5⁴

TN8⁴

ARC⁴

BAL⁴

ACCESSORIES - Order Separately

	• •
Catalog Number	Description
VM2SXX	2nd mode vibration damper

- Specify option location using logic found on page 2 (Option Orientation)
- TN3 and TN4 not available on 3" diameter poles
- TN5 and TN8 not available on 4" diameter poles
- Specify pole top





Bolts

Tenon 3 x 42

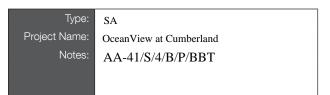
Tenon 4 x 5³

Tenon 4 x 83

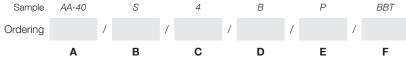
Acorn Finial

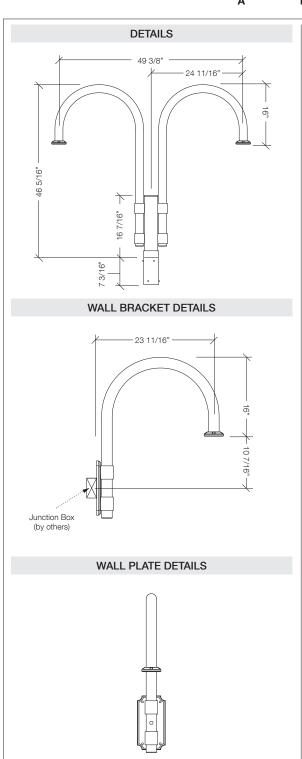
Ball Finial CAP⁴ Flat Cap





AA-41 RAILROAD STRAP





A. MODEL AA-41 Railroad Strap B. POST SHAFT PROFILE w wall mount S smooth F fluted C. POST SHAFT DIAMETER 5" 6" OTHER

D. ARRANGEMENT

see arrangement table below

E. LUMINAIRE MOUNTING

pendant

F. COLOR

BBT	basic black textured			
BMT	black matte textured			
WHT	white textured			
MBT	metallic bronze textured			
BZT	bronze textured			
GYS	gray smooth			
DPS	dark platinum smooth			
GNT	green textured			
MST	metallic silver textured			
MTT	metallic titanium textured			
OWI	old world iron			
RAL				

Fax: (941) 751-5535

Construction: All cast aluminum parts shall be low copper alloy A356. All extruded aluminum parts shall be alloy 6061-T6, 6063-T5 or equal.

EPA (effective projected area): EPA is de-fined as (projected surface area X drag factor) and measured in ft2. Allowable post, luminaire arm, luminaire and accessory EPAs are derived from the most current published AASHTO (American Association of State Highway and Transportation Officials) standard, currently AASHTO 2001 (50yr design life). Customer assumes all responsibility for selecting the ap-propriate post for installation (consult factory for assistance). Luminaire arm, luminaire and accessory EPA must be equal to or less than allowable EPA of post. Consult a professional engineer for compliance with local codes and standards.

Fasteners: All fasteners shall be Corrosion Resistant. When tamper resistant fasteners are required, spanner HD (snake eye) style shall be provided (special tool required, available at additional cost).

Finish: Finish shall be a Beacote V polyester powder-coat electro-statically applied and thermocured. Beacote V finish shall consist of a five stage iron phosphate chemical pretreatment regimen with a polymer primer sealer, oven dry off, and top coated with a thermoset super TGIC polyester pow-der coat finish. The finish shall meet the AAMA 605.2 performance specification which includes passing a 3000 hour salt spray test for corrosion resistance and resists cracking or loss of adhesion per ASTM D522 and resists surface impacts of up to 160 inch-pound.

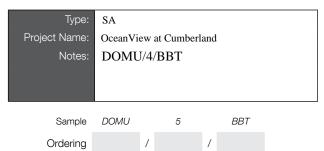
Limited Warranty: Beacon Products warrants its products, to the original purchaser, against defects in materials and workmanship for proper usage for a period of 5 years after date of production, when properly installed, maintained and appropriately specified. See Warranty Information on www.beaconproducts.com for complete details and exclusions.

	arrangement (EPA index ft² / weight (lbs)										
		H	-	•••	•••	٤.	٠.	٠.,	•••	+	÷
shaft Ø		А	В	С	D	E	F	G	Н	- 1	J
wall	weight	12	-	-	-	-	-	-	-	-	-
Ø4"	EPA	-	1.50	2.41	-	1.93	2.17	-	2.41	2.41	-
04	weight	-	15	23	-	23	32	-	32	41	-
Ø5"	EPA	-	1.52	2.49	-	2.00	2.24	-	2.49	2.49	-
W5	weight	-	16	25	-	25	34	-	34	43	-
Ø6"	EPA	-	1.71	2.62	-	2.10	2.36	-	2.62	2.62	-
, Ø6	weight	-	19	27	-	27	36	-	36	45	-

subject to change without notice.

Due to our continued efforts to improve our products, product specifications are





В

Domus

B. POST SHAFT DIAMETER

3"

С

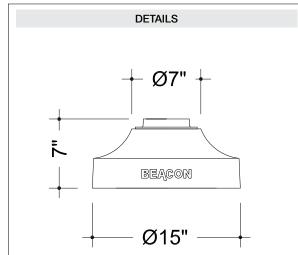
Α

A. MODEL

DOMU

3

rev. 02.20.2014 **DOMUS**Poles & Bases



4	4 "			
5	5"			
6	6"			
C. COLO	₹			
BBT	basic black textured			
BMT	black matte textured			
WHT	white textured			
MBT	metallic bronze textured			
BZT	bronze textured			
DBT	dark bronze textured			
GYS	gray smooth			
DPS	dark platinum smooth			
GNT	green textured			
MST	metallic silver textured			
MTT	metallic titanium textured			
OWI	old world iron			
RAL				

Construction: All cast aluminum parts shall be low copper alloy A356. All extruded aluminum parts shall be alloy 6061-T6, 6063-T5 or equal. Standard fluted shaft profile shall be 16-flat flutes for 3"OD and 12-flat flutes for 4", 5", & 6"OD.

Base Covers: require specification of smooth or fluted shafts of the size required to meet wind load requirements

Vibration Dampeners: Vibration dampener pads shall be provided when required by customer or deemed necessary by Beacon Products. Please consult factory for bridge mounted applications.

EPA (effective projected area): EPA is defined as (projected surface area X drag factor) and measured in ft2. Allowable post, luminaire arm, luminaire and accessory EPAs are derived from the most current published AASHTO (American Association of State Highway and Transportation Officials) standard, currently AASHTO 2001 (50yr design life). Customer assumes all responsibility for selecting the appropriate post for installation (consult factory for assistance). Luminaire arm, luminaire and accessory EPA must be equal to or less than allowable EPA of post. Consult a professional engineer for compliance with local codes and standards.

Anchor Bolt: Anchor bolts, sized as required, double hex nuts and flat washers shall be hot dipped galvanized steel. A bolt circle template shall be provided for installation.

Fasteners: All fasteners shall be Corrosion Resistant. When tamper resistant fasteners are required, spanner HD (snake eye) style shall be provided (special tool required, available at additional cost).

Finish: Finish shall be a Beacote V polyester powdercoat electrostatically applied and thermocured. Beacote V finish shall consist of a five stage iron phosphate chemical pretreatment regimen with a polymer primer sealer, oven dry off, and top coated with a thermoset super TGIC polyester powder coat finish. The finish shall meet the AAMA 605.2 performance specification which includes passing a 3000 hour salt spray test for corrosion resistance and resists cracking or loss of adhesion per ASTM D522 and resists surface impacts of up to 160 inch-pound.

Limited Warranty: Beacon Products warrants its products, to the original purchaser, against defects in materials and workmanship for proper usage for a period of 5 years after date of production, when properly installed, maintained and appropriately specified. See Warranty Information on www.beaconproducts.com for complete details and exclusions.

Due to our continued efforts to improve our products, product specifications are subject to change without notice.

Norwell

Cottage Building & Post lights

Cottage Onion

1323 1324 1321

OceanView at Cumberland

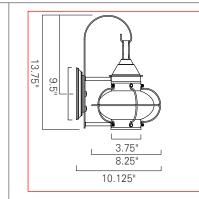
Fixture Type Quantity

Product Name

Model Number

Project Name





15.75" Cottage Onion Medium - 1324 Black (BL) Clear Glass (CL)

12.5" 3.0625

10.625

INC-10.625"

Cottage Post - 1321 Black (BL) Seedy Glass (SE) **Product Name / Model / Dimensions** Cottage Onion Small - 1323 Cottage Onion Medium - 1324 Cottage Onion Post - 1321 Height Width Projection 1323 13.75" 8.25" 10.125" 1324 15.75" 10.625" 12.5"

10.625"

14.625"

Backplate Sconce 6.25" Diameter

	Standard
	Black (B
	Bronze (
TTO	
9.5"	
10"	

Finish Options

Standard ack (BL) Clear (CL) onze (BR) Seedy (SE)

Cottage Post - 1321

Black (BL) Clear Glass (CL)

Glass

Standard Incandescent (1) 100 Watt Edison

Lamping Options

1 _ 2018



1321

COPY OF LETTER UPDATED WITH OCEANVIEW AT CUMBERLAND TEAM RESPONSES IN RED 07-31-18.

EXHIBIT 8 OF FINAL PLAN APPLICATION

March 12, 2018

Ms. Carla Nixon, Town Planner Town of Cumberland 290 Tuttle Road Cumberland, Maine 04021

Subject: Peer Review of OceanView At Cumberland

Major Subdivision and Site Plan Application – Addenda 1A

Preliminary Review Comment Responses

Tuttle Road, Cumberland, Maine

Dear Ms. Nixon:

As requested, Sevee & Maher Engineers, Inc. (SME) has completed a review of the comment responses submitted for the preliminary application for a Major Subdivision and Site Plan for the proposed OceanView at Cumberland senior living community located off Tuttle Road. This submission is identified by the applicant as Revised Preliminary Subdivision Plan Submittal – Addenda-1A. The application materials received by SME were prepared by LICHT Environmental Design, LLC (LICHT), and consist of the following:

- Cover letter by Frederic Licht, P.E., L.S.E, outlining responses to Planning Board, staff and peer review comments, dated March 2, 2018;
- Exhibits 1 through 4 prepared by LICHT outlining signage, lighting cut sheets, traffic updates, and cottage elevations, dated March 2, 2018;
- Project plan set, Revision 3, dated March 1, 2018;
- An updated stormwater management report prepared by Belanger Engineering, dated March 1, 2018; and
- Updated Pre- and Post-Development Stormwater Management Plans, dated March 1, 2018.

PROJECT DESCRIPTION

The Applicant proposes to develop a 52-unit senior living facility on a combined 36.83-acre parcel currently owned by Richard Doane and Laurence Allen. The parcel is located off Tuttle

Road in Cumberland, across the street from the Town of Cumberland (Town) Municipal Office. The development will be accessed by a proposed private roadway constructed in accordance with Town residential sub-collector roadway standards as outlined in Article VI and Table 2 of Chapter 250, Subdivision of Land, of the Cumberland Code. The subdivision will be served with public utilities, including water, sewer, natural gas, electric, telephone, and cable.

TOWN PLANNER COMMENTS DATED FEBRUARY 8, 2018

The applicant provided additional clarification to their previous response to comments on February 14, 2018. We anticipate the 26 comments listed have been reviewed with Carla Nixon, the Town Planner, and addressed to her satisfaction.

PEER REVIEW COMMENTS DATED FEBRUARY 12, 2018

The following comments were issued in our peer review letter for the Preliminary Major Subdivision and Site Plan Application, dated February 12, 2018. The project was reviewed as a Major Subdivision as outlined in Chapter 250 - Subdivision of Land of the Town of Cumberland Ordinances, most recently amended and adopted on January 12, 2011, and Chapter 229 - Site Plan Review, most recently amended and adopted on March 26, 2012. The comments and responses below relate to the appropriate Ordinance Sections.

Chapter 250: Subdivision of Land

SME has reviewed the applicable sections of Chapter 250 and has provided comments for those sections not found to be addressed by the Application. The remaining sections have been reviewed and found to comply with Chapter 250 requirements.

Section 250-1(C) – Municipal water supply

 SME understands that the applicant has contacted the Portland Water District regarding their capacity to serve the project. Please provide a verification letter from the District prior to final approval.

The Applicant intends to address this item in the final plan application. PWD letter attached Exhibit 5.

Section 250-1(E) - Traffic

 The Updated Traffic Impact Study included with this application prepared by Maine Traffic Resources and dated December 11, 2017 is based on a maximum of 50 residential units. SME recommends the study be updated to reflect the current planned development of 52 residential units.

Section 250-1(N) – Stormwater

3. The application SME reviewed did not include a Stormwater Management Exhibit. Please provide a stormwater report and stormwater management plan prior to preliminary approval.

This item has been addressed. Comment responses to our letter dated February 20, 2018 are included in the following section.

Section 250-1(O) – Freshwater Wetlands

4. The cover letter outlines 11,200 sf +/- of proposed wetland impacts. Plan sheet C2 outlined 12,700 sf of proposed wetland impacts. Please clarify.

This item has been addressed.

Section 250-1(P) - River, stream or brook

5. There are two stream crossings associated with the proposed development. Please submit additional detail regarding the proposed construction, including any State or Federal Permit approvals, for review prior to final approval.

The Applicant intends to address this item in the final plan application. Final concrete box culvert designs have been included with the final plans. Refer to Plan sheets C20-C21 and Plan and Profile Sheets. Final Wall shop submittals to be provided by wall vendor prior to construction under contract to the Site Contractor.

Section 250-19 – Review and approval by other agencies

- 6. SME understands the following permit applications are underway for the project and applications will be filed with appropriate agencies following submittal of the preliminary subdivision and site plan application:
 - Maine Department of Environmental Protection (MEDEP) Site Location of Development Act (SLODA) permit,
 - MEDEP Natural Resources Protection Act (NRPA) Tier 1 permit for proposed wetland impacts,
 - United States Army Corps of Engineers (USACOE) permit for proposed stream crossings and culvert replacements,
 - Cumberland County Soil and Water Conservation District (CCS&WCD) stormwater and erosion control review, and
 - Maine Department of Transportation (ME DOT) Driveway/Entrance Permit.

Where review and approval of any subdivision or site plan by any other governmental agency is required, approvals shall be submitted to the Planning Board in writing prior to the submission of the final plan.

The Applicant intends to address this item in the final plan application. See cover letter for agency emails re final permits in progress.

Section 250-22 – Retention of proposed public sites and open spaces

7. The application package outlines portions of the development, including pedestrian trails and walkways, will be available for public use. SME recommends that areas designated for recreation and/or reserved as public open space be outlined in the project plan set.

This item has been addressed.

Section 250-27 - Utilities

8. Design details for utility pipes and conduits are not included in the project plan set. SME recommends sizes of all utilities pipes and additional design information be provided with the final plan application.

This item has been addressed.

9. SME recommends Water Detail sheets be signed and stamped by a registered Professional Engineer prior to final approval.

This item has been addressed.

10. SME understands Summit Natural Gas has been contacted to provide natural gas for the development. SME recommends a capacity to serve letter be provided with the final plan application.

The Applicant intends to address this item in the final plan application. See Exhibit 5 for Summit NG Serviceability Letter.

11. SME understands Central Maine Power (CMP) has been contacted to provide electricity for the development. SME recommends the location of underground electric lines, transformers, and electrical easements be added to the plan. Please provide a capacity to serve letter with the final plan application.

The plans have been updated. The Applicant intends to submit a capacity to serve letter with the final plan application.

See Exhibit 5 for CMP Sereviceability Letter

Section 250-28 - Water Supply

12. SME understands that the applicant has contacted the Portland Water District regarding their capacity to serve the project. Please provide a verification letter from the District prior to final approval.

The Applicant intends to address this item in the final plan application. See Exhibit 5 for PWD Serviceability Letter.

Section 250-29 – Sewage disposal

13. The application includes a capacity to serve letter from the Town of Falmouth regarding their ability to accommodate the anticipated sewage flow from the development. In addition, SME recommends the applicant provide a letter from the Town of Cumberland and the Portland Water District to ensure capacity of the local system to accommodate additional loading.

The Applicant intends to address this item in the final plan application. See Exhibit 5 for a letter from Bill Shane indicating available capacity. An additional letter from the Falmouth Wastewater Facility is also included.

Section 250-32 – Design and construction standards

14. SME understands proposed streets will be constructed in accordance with Town residential sub-collector roadway standards as outlined in Article VI and Table 2 of Chapter 250, Subdivision of Land, of the Cumberland Code. Plans for Arctic Fox Drive do not include a sidewalk, which is listed in the Ordinance as a required improvement unless waived by the Board. SME recommends the applicant add a sidewalk to the final plans or request a waiver to address this item.

This item has been addressed.

Section 250-36 through 250-43 – Storm Drainage Design and Construction Standards

15. SME has not received an updated Stormwater Management Report for the revised plan set. As outlined previously in Comment 3, a stormwater report and stormwater management plan for the proposed development should be provided prior to preliminary approval.

This item has been addressed. Comment responses to our letter dated February 20, 2018 are included in the following section.

Section 250-44 – Fire Protection

16. SME understands the public water service will be used to sprinkle individual units in the proposed development. SME recommends the applicant provide

documentation to support the Water District's capacity to meet the fire protection needs of the development prior to final approval.

The Applicant intends to address this item in the final plan application. All units will be sprinklered under a NFPA 13D system. We have reviewed the project with PWD and 1.5 inch services and I inch meter shall be provided to each unit for domestic and fire sprinkler system designs as approved by PWD. A note has been added to the plans (PWD Service Connection Detail indicating services to be 1.5 inch.)

Section 250-49 – Waivers and modifications

17. The applicant has requested a waiver from the requirement to show street signs for preliminary approval only. SME recommends approval of the requested waiver and that signs be included on the final plan application.

This item has been addressed.

18. The applicant has requested a waiver from the requirement to provide capacity to serve letters from selected utility providers for preliminary approval only. SME recommends approval of the requested waiver and that capacity to serve letters be provided with the final plan application.

This item has been addressed.

 The applicant has requested a waiver from the requirement to locate 10-inch diameter or more trees on the property. SME recommends approval of this waiver.

This item has been addressed.

Chapter 229: Site Plan Review

SME has reviewed the applicable sections of Chapter 229 and has provided comments for those sections not found to be addressed by the Application. The remaining sections have been reviewed and found to comply with Chapter 229 requirements.

Section 229-10(H) – Exterior lighting

20. SME understands the Applicant is evaluating site lighting options for the project. SME recommends that a final lighting layout and photometrics plan be provided with the final plan application.

General Comments

21. Site Plan Application – Please update the project description to reflect the correct number of units in the proposed development.

This item has been addressed.

22. Application Exhibit 6 – Soils. The Soil Narrative Reports included in the exhibit should be signed and dated by Mark Hampton prior to final approval.

This item has been addressed.

23. Application Exhibit 10 – Traffic Impact Assessment. As previously outlined in Comment 2, SME recommends the Traffic Impact Study be updated to reflect the current planned development of 52 residential units.

This item has been addressed.

24. Plan Sheet C0 – Approvals Required Note 2 references a MEDEP SLODA permit *amendment*. Please update the plan to clarify the current project permitting status.

This item has been addressed.

25. Subdivision Plat S1 – The plan outlines overhead electric service from Tuttle Road to Units 51, 52 and 53. The application outlines underground utilities. Please clarify.

This item has been addressed.

26. Subdivision Plat S1-3 – Please add supplementary information to the drawings prior to final approval, including sight distances, stream setbacks, stormwater and grading easements, road layout information (alignment and intersection radii), and wetland impact areas, etc.

This item has been addressed.

27. Topographic Site Plan by Titcomb Associates (Sheet 1 of 1) is not included in the plan set. Please add an existing conditions plan to the drawing set.

28. Overall Plan Sheet C1 references a 50-foot buffer and golf cart trails not shown on the drawing.

This item has been addressed.

29. Site Development Plan Sheets C3 through C5 – Please include additional labeling and detail for utilities, easements, stormwater management, and natural features such as streams and wetlands. Please update clearing limits should be updated to reflect modifications to stormwater treatment systems. Please add grading easements to reflect work scheduled outside the property boundary and access easement limits. SME recommends this information be added to the plan to verify compliance with applicable Town standards.

This item has been addressed.

30. Plan and Profile Plan Sheets C6 through C10 do not outline utility information for force main, electric or communications wiring. SME recommends this information be added to the plan.

This item has been addressed.

31. Roadway design does not conform to minimum K factors for sag vertical curves at Little Acres Drive STA 21+50; Arctic Fox Drive STA 41+99.64 and STA 44+99.90; and Arctic Fox Spur STA 21+61.63. SME recommends the applicant review these areas and adjust to meet Town construction standards.

This item has been addressed.

32. Improvements were noted at several locations in the no-cut buffer along the property boundaries for site grading. SME recommends the applicant amend the plans to minimize disturbance in the 50 foot no-cut buffer.

This item has been addressed.

33. Roadway Sections and Details Sheet C13 –There are several references to Brunswick, Topsham, and SAD 75 in the notes on this plan sheet. SME recommends the notes be updated to reflect the current project.

34. Civil details C15 – The Town of Cumberland does not usually include ladder rungs in catch basin structures. SME recommends the applicant amend the plans to reflect Town construction standards.

This item has been addressed.

35. Erosion Control Notes C16 – SME Recommends Note 1 be updated to reflect the current Maine Erosion and Sediment Control Best Management Practices edition (October 2016).

This item has been addressed.

36. Erosion Control Notes C16 – SME recommends the applicant update the Construction Plan Notes to reflect the current project.

This item has been addressed.

37. Misc. Details C19 – SME recommends the applicant update the Trench Repair Detail to reflect current Town pavement sections.

SME recommends the base and subbase gravel materials be adjusted to reflect Town standards.

Detail has been updated.

38. Arch 1 Culvert Details – Profile does not include a sidewalk. SME recommends the applicant update the plan to reflect proposed construction.

The Applicant intends to address this item in the final plan application. The sidewalk has been added to the Culvert section/plan views.

39. Arch 2 Culvert Details C21 - Profile does not include a sidewalk. SME recommends the applicant update the plan to reflect proposed construction.

The Applicant intends to address this item in the final plan application. The sidewalk has been added to the section/plan views.

PEER REVIEW COMMENTS DATED FEBRUARY 20, 2018

The following comments were issued in our peer review letter for the Preliminary Stormwater Review for Major Subdivision and Site Plan Application, dated February 20, 2018.

Chapter 242: Stormwater Management

SME has reviewed the applicable sections of Chapter 242 and has provided comments for those sections not found to be addressed by the Application. The remaining sections have been reviewed and found to comply with Chapter 242 requirements.

Section 242-24(C)

1. SME understands the applicant intends to retain ownership of the stormwater management facilities shown in its post-construction stormwater management plan. Prior to final approval, SME recommends the applicant submit documentation that the applicant, its successors, heirs and assigns shall have the legal obligation and the resources available to operate, repair, maintain and replace the stormwater management facilities, as well as a maintenance agreement with the Town in conformance with this section of the Ordinance.

The Applicant intends to address this item in the final plan application. A Town of Cumberland Stormwater agreement (Draft) is included in Exhibit 6 to be completed and executed upon approvals. The applicant will maintain all facilities and will contract with Ross Cudlitz, PE to perform annual inspections under the MS-4 Program.

Section 242-1(D)

2. Stormwater management facilities not located in a public right-of-way and not offered to the Town for acceptance as public facilities may require access easements to the Town. SME recommends the Applicant clarify this item with the Town and add required easements, if necessary, prior to final approval.

The Applicant intends to address this item prior to final approval.

The Town will be named as a party in the Exhibit 6 Stormwater Agreement allowing access to facilities in the event they are not maintained.

General Comments

3. Stormwater Management Report, Page 1, Surface Water on or Abutting the Site – SME recommends the Applicant coordinate with the Town Engineer regarding runoff from the site and proposed improvements scheduled for Tuttle Road in the Summer of 2018.

This item has been addressed.

4. Stormwater Management Report, Page 2, Proposed Conditions – SME recommends the section be updated to reflect the 52 residential units.

This item has been addressed.

5. Stormwater Management Report, Page 3, Impervious Area Summary – The table references road sections not outlined in the plan detail sheets. SME recommends the Applicant update the plan set to include all applicable road section details.

This item has been addressed.

6. Stormwater Management Report, Page 4, Focal Point Proprietary System – This section references 500 feet of gutter line flow. Section 250-40, B(4) outlines 300 feet as the maximum length for stormwater in a street gutter prior to intake at a catch basin. SME recommends the Applicant adjust the length of flow or request a waiver prior to final approval.

The Applicant intends to address this item prior to final approval.

The focal point system has been revised along with the location due to a change in the road profile to move further away from the stream crossing. Refer to the plans.

7. Stormwater Management Report, Page 4, Forested Buffer – Please verify that wetland buffers outlined on the plan qualify as stormwater treatment based on length, grade and soil type. If approved for treatment by MEDEP, SME recommends adding required sign details and boundary information to the plan set.

The Applicant intends to address this item prior to final approval.

The Forested Stormwater Buffers and the one Meadow Buffer and level spreader behind unit 52 have been clarified and labeled. Notes on the Subdivision Plat sheet 4 and on the engineering plans indicate the Meadow Buffer to be pinned with buffer caps and 4 by 4 placards and survey pins with

caps to be placed at strategic locations along the residential sides of the Forested Buffers. A detail of the typical type of plackard is included on the plans.

8. Stormwater Management Report, Page 5, Arctic Fox Wet Pond Design Criteria – Please verify above pool and below pool treatment volume calculations.

SME Recommends the Applicant address this item prior to final approval. The Pond has been revised and also reflects final DEP review comments.

9. Stormwater Management Report, Page 5, Groundwater Impacts – Please show boring/test pit locations on the plan set.

This item has been addressed.

 Stormwater Management Report, Page 6, Mallard Way Wet Pond Design Criteria – Please verify above pool and below pool treatment volume and provided storage calculations.

SME Recommends the Applicant address this item prior to final approval. The Pond has been revised and also reflects final DEP review comments.

11. Stormwater Management Report, Page 6, Groundwater Impacts – Please show boring/test pit locations on the plan set.

This item has been addressed.

12. Stormwater Management Report, Page 7, Post Area Summary and General Standard Calculation – Please verify total area calculations. The sum of component areas does not appear to match the total area.

SME Recommends the Applicant address this item prior to final approval. The stormwater table has been updated.

13. Stormwater Management Report, Page 7, Flooding Standard – Please verify the top of the watershed area. A significant contributing drainage area exists above the middle school entrance.

14. Stormwater Management Report, Page 7, Flooding Standard – SME understands the site access was relocated from the former railroad bed to the Allen property. Please update the site entrance description.

This item has been addressed.

15. Property Maintenance Part 3, page 17 – Please update references to Loon Lane.

This item has been addressed.

 Permitting Authorization Letter – Please update authorizations to include OceanView at Cumberland

SME Recommends the Applicant address this item prior to final approval. (Applicant to review with SME for clarity on response to item.)

17. Exhibit 3 – Please update site footprint to reflect inclusion of the Allen Property.

SME Recommends the Applicant address this item prior to final approval. (Exhibit to be updated. The Allen acquisition includes 5.35 acres and the new Allen Lot is not part of the SLODA or stormwater application.

18. Pre-Development Drainage Plan – SME recommends the plan be updated to include the full drainage area and subcatchment boundaries, soil boundaries, and topography outside the project area. Labels for 18R and 55R are missing from the plan sheet.

SME Recommends the Applicant address this item prior to final approval. We believe the final plans address this comment and total areas.

19. Post Development Drainage Plan – SME recommends the plan be updated to include the full drainage area and subcatchment boundaries, soil boundaries, and topography outside the project area. Labels for 15S, 51S, and 51P are missing from the plan sheet.

SME Recommends the Applicant address this item prior to final approval. We believe the final plans address this comment and total areas.

New Comments

- 20. The gravel trench outlets for Mallard Way and Arctic Fox Drive wet ponds are not modeled. SME will complete a more thorough review with the final plan submission. We will await any further comments on the hydrocad model.
- 21. The elevations for the Cultec separator row are not consistent with the stormwater model. SME will complete a more thorough review with the final plan submission.

The Separator units have been revised in a new configuration and should be acceptable. We will await any further comments.

PLANNING BOARD ADDITIONAL COMMENTS

The applicant provided clarification for Planning Board comments from the Planning Board meeting held on February 20, 2018. We anticipate the comments listed have been addressed to the Board's satisfaction.

Please call me with any	questions, or if y	ou would like, I	could meet with	ı you to discuss our
comments.				

Sincerely,

SEVEE & MAHER ENGINEERS, INC.

Jeffrey T. Read, P.E. Civil Engineer/Project Manager

LEGEND: EXISTING PROPOSED OR 🌌 IRON PIPE OR MONUMENT O OR ⊡ BENCH MARK (SEE NOTES) TRAVERSE STATION TEST PIT CATCH BASIN SEWER MANHOLE FIRE HYDRANT WATER GATE VALVE WATER SHUT-OFF BLOW-OFF/CLEAN-OUT UTILITY POLE POLE W/SINGLE LIGHT POLE W/DOUBLE LIGHT SPOT LIGHT & WALL LIGHT BOLLARD LIGHT RESIDENTIAL SEWER PUMP STATION GAS VALVE HANDICAP SYMBOL PAVEMENT PAINT MARKINGS PARKING SPACE COUNT PROPERTY LINE EASEMENTS SETBACK/BUFFER SOILS BOUNDARY WETLAND BOUNDARY STREAM CULVERT CONCRETE SLIPFORM ======= ======= GRANITE CURB VERTICAL CONCRETE CURE ======= EDGE OF PAVEMENT ROAD CENTERLINE BUILDING STORM DRAIN(SEE PLAN FOR SIZE) SEWER LINE(SEE PLAN FOR SIZE) WATER LINE(SEE PLAN FOR SIZE) — w—— w—— w— ---- WC ---CHILLER LINES SPOT ELEVATION SPOT: CURB TOP & BOTTOM CONTOURS CATCH BASIN HAY BALE BARRIER CLEARING LIMIT TREE LINE SILT FENCE CHAIN LINK FENCE WOOD GUARD RAIL CONSTRUCTION ENTRANCE CONCRETE PAVEMENT PAVEMENT OVERLAY BUILDING EXISTING BUILDING NOT IN CONTRACT PROGRESS PLAN NOT FOR CONSTRUCTION THIS DOCUMENT IS ISSUED FOR INFORMATIONAL PURPOSES ONLY. THE DATA SHOWN HEREON IS SUBJECT TO REVISION. **PROJECT SCALES** GRAPHIC SCALE (IN FEET) 1 inch = 20 ft.

GRAPHIC SCALE

(IN FEET)

1 inch = 40 ft.

(IN FEET)

1 inch = 100 ft.

GRAPHIC SCALE

GENERAL NOTES:

TOPOGRAPHIC DATA IS BASED ON COMPILATIONS OF INFORMATION INCLUDING AERIAL INFORMATION, ON THE GROUND SURVEY, APPROVED DESIGN PLANS, AND FIELD OBSERVATIONS. ON THE GROUND SURVEYS HAVE BEEN COMPLETED BY TITCOMB ASSOCIATES IN 2017

- THE CONTRACTOR IS SPECIFICALLY CAUTIONED THAT THE LOCATION AND/OR THE ELEVATION OF THE EXISTING UTILITIES AS SHOWN ON THESE PLANS IS BASED ON RECORDS OF THE VARIOUS UTILITY COMPANIES AND WHERE POSSIBLE MEASUREMENTS TAKEN IN THE FIELD. THIS INFORMATION HAS NOT BEEN INDEPENDENTLY VERIFIED BY THE OWNER OR ITS REPRESENTATIVES AND IS NOT TO BE RELIED ON AS BEING EXACT OR COMPLETE. THE CONTRACTOR SHALL CALL THE APPROPRIATE UTILITY COMPANY AND DIG SAFE (1-800-DIG-SAFE) AT LEAST 72 HOURS PRIOR TO ANY EXCAVATION TO REQUEST EXACT FIELD LOCATION OF UTILITIES. IT SHALL BE THE RESPONSIBILITY OF THE CONTRACTOR TO RELOCATE ALL EXISTING UTILITIES WHICH CONFLICT WITH THE PROPOSED IMPROVEMENTS SHOWN ON THE PLANS.
- UNIT FOOTPRINTS AS SHOWN ARE FOR PLANNING PURPOSES ONLY. FINAL FOOTPRINTS MAY VARY. SEE ARCHITECTURAL DRAWINGS FOR EXACT BUILDING DIMENSIONS AND ALL DETAILS CONTIGUOUS TO THE BUILDING, INCLUDING SIDEWALKS, RAMPS, BUILDING ENTRANCES, STAIRWAYS, UTILITY PENETRATIONS, CONCRETE DOOR PADS, COMPACTOR PAD, LOADING DOCKS, BOLLARDS ETC.
- LAYOUT DIMENSIONS ARE FROM FACE OF BUILDING, RETAINING WALLS, CURBS OR BERMS.
- RIM ELEVATIONS OF PROPOSED DRAINAGE AND SANITARY SEWER MANHOLES AND ASSOCIATED STRUCTURES ARE APPROXIMATE. FINAL ELEVATIONS ARE TO BE SET FLUSH AND CONSISTENT WITH THE GRADING PLANS. ADJUST ALL OTHER RIM ELEVATIONS OF MANHOLES, WATER GATES, GAS GATES AND OTHER UTILITIES TO FINISH GRADE WITHIN LIMITS OF WORK.
- THE LOCATION, SIZE, DEPTH, AND SPECIFICATIONS FOR CONSTRUCTION OF PROPOSED PRIVATE UTILITY SERVICES SHALL BE INSTALLED ACCORDING TO THE REQUIREMENTS PROVIDED BY, AND APPROVED BY THE RESPECTIVE UTILITY COMPANY (GAS, TELEPHONE, ELECTRIC AND FIRE ALARM). FINAL DESIGN LOADS AND LOCATIONS TO BE COORDINATED WITH OWNER AND ARCHITECT.
- THE CONTRACTOR SHALL FIELD VERIFY THE LOCATION, SIZE, INVERTS AND TYPES OF EXISTING PIPES AT ALL PROPOSED POINTS OF CONNECTION PRIOR TO ORDERING MATERIALS. WHERE AN EXISTING UTILITY IS FOUND TO CONFLICT WITH THE PROPOSED WORK, THE LOCATIONS, ELEVATION, AND SIZE OF THE UTILITY SHALL BE ACCURATELY DETERMINED WITHOUT DELAY BY THE CONTRACTOR, AND THE INFORMATION FURNISHED IN WRITING TO THE OWNER'S REPRESENTATIVE FOR THE RESOLUTION OF THE CONFLICT.
- ALL AREAS OUTSIDE THE LIMIT OF WORK THAT ARE DISTURBED SHALL BE RESTORED BY THE CONTRACTOR TO THEIR ORIGINAL CONDITION AT THE CONTRACTOR'S EXPENSE. ALL AREAS DISTURBED DURING CONSTRUCTION NOT COVERED WITH BUILDINGS, STRUCTURES, OR PAVEMENT SHALL RECEIVE 6 INCHES OF LOAM AND SEED
- CONTRACTOR SHALL MAKE ALL ARRANGEMENTS AND SHALL BE RESPONSIBLE FOR PAYING ANY FEES FOR ANY POLE RELOCATION AND FOR THE ALTERATION OR ADJUSTMENT OF GAS, ELECTRIC, TELEPHONE, FIRE ALARM AND ANY OTHER PRIVATE UTILITIES BY THE UTILITY COMPANIES.
- UPON AWARD OF CONTRACT, CONTRACTOR SHALL MAKE ALL NECESSARY CONSTRUCTION NOTIFICATIONS AND APPLY FOR AND OBTAIN ALL NECESSARY PERMITS, PAY ALL FEES AND POST ALL BONDS ASSOCIATED WITH THE WORK INDICATED ON THE DRAWINGS.
- ALL PROPERTY MONUMENTATION DISTURBED DURING CONSTRUCTION SHALL BE RESET TO THEIR ORIGINAL LOCATION BY A MAINE REGISTERED PROFESSIONAL LAND SURVEYOR (PLS) AT THE CONTRACTOR'S EXPENSE
- THE CONTRACTOR SHALL PREPARE/PROVIDE AN AS-BUILT SURVEY SHOWING LOCATIONS OF ALL CONSTRUCTED SURFACE FEATURES AND SUBSURFACE UTILITY SYSTEMS INCLUDING THE GPS POINT LOCATION, TYPE, SIZE AND INVERTS. THE CONTRACTOR SHALL PROVIDE SURVEY POINTS AND DATA TO THE ENGINEER.
- CONTRACTOR SHALL INSTALL ALL EROSION CONTROL MEASURES PRIOR TO EARTHWORK OPERATION AND MAINTAIN ALL EROSION CONTROL MEASURES AND SEEDED EMBANKMENTS DURING CONSTRUCTION. EROSION CONTROL SHALL BE REMOVED ONLY UPON THE ESTABLISHMENT OF ALL LANDSCAPED AREAS. AL WORK SHALL BE IN COMPLIANCE WITH THE ENVIRONMENTAL QUALITY HANDBOOK FOR EROSION AND SEDIMENT CONTROL, LATEST EDITION, AS ADOPTED BY THE MAINE DEPARTMENT OF ENVIRONMENTAL PROTECTION
- CONTRACTOR SHALL BE SOLELY RESPONSIBLE FOR SITE SECURITY AND JOB SAFETY. ALL CONSTRUCTION ACTIVITY SHALL BE IN ACCORDANCE WITH OSHA STANDARDS AND LOCAL REQUIREMENTS
- ALL MATERIALS AND CONSTRUCTION METHODS USED WITHIN THE PUBLIC RIGHT-OF-WAY SHALL CONFORM TO ALL LOCAL MUNICIPAL STANDARDS AND MAINE DEPARTMENT OF TRANSPORTATION
- ALL HANDICAP ACCESSIBLE PARKING SPACES. RAMPS AND SIDEWALKS SHALL BE CONSTRUCTED IN CONFORMANCE WITH THE AMERICANS WITH DISABILITIES ACT (ADA).
- ALL SITE SIGNAGE AND PAVEMENT MARKINGS SHALL CONFORM TO THE MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES.

LAYOUT NOTES:

- ALL DIMENSIONING, UNLESS NOTED OTHERWISE, IS TO THE FACE OF CURB OR BUILDING.
- OFFSETS TO CATCH BASINS AND MANHOLES ARE TO THE CENTER OF THE FRAME.
- PIPE LENGTH EQUALS THE CENTER TO CENTER DISTANCES BETWEEN CATCH BASINS AND/OR MANHOLES MINUS ONE HALF THE DIAMETER OF EACH CATCH BASIN OR MANHOLE.
- BOUNDARY INFORMATION ON LAYOUT PLAN IS FOR REFERENCE ONLY, REFER TO SUBDIVISION PLAT AND ACTUAL SURVEY AND BOUNDARY SURVEY REFERENCES BY TITCOMB ASSOCIATES.

GRADING AND DRAINAGE NOTES:

UNLESS OTHERWISE NOTED, ALL STORM DRAIN PIPE SHALL BE IN ACCORDANCE WITH MDOT SPECIFICATIONS SECTION 603. PIPE CULVERTS AND STORM DRAINS, LATEST REVISION WITH THE EXCEPTION THAT THE ONLY ACCEPTABLE TYPES OF PIPE ARE AS FOLLOWS: REINFORCED CONCRETE PIPE POLYVINYL CHLORIDE PIPE (PVC)

SMOOTH BORE HDPE POLYETHYLENE PIPE

- TOPSOIL STRIPPED IN AREAS OF CONSTRUCTION THAT IS SUITABLE FOR REUSE AS LOAM SHALL BE STOCKPILED ON SITE AT A LOCATION TO BE DESIGNATED BY OWNER. UNSUITABLE SOIL SHALL BE SEPARATED, REMOVED AND DISPOSED OF AT AN APPROVED DISPOSAL LOCATION OFF SITE.
- THE CONTRACTOR SHALL ANTICIPATE THAT GROUNDWATER WILL BE ENCOUNTERED DURING CONSTRUCTION AND SHALL INCLUDE SUFFICIENT COSTS WITHIN THEIR BID TO PROVIDE DEWATERING AS NECESSARY NO SEPARATE PAYMENT SHALL BE MADE TO THE CONTRACTOR FOR DEWATERING.

EROSION CONTROL NOTES:

- LAND DISTURBING ACTIVITIES SHALL BE ACCOMPLISHED IN A MANNER AND SEQUENCE THAT CAUSES THE LEAST PRACTICAL DISTURBANCE OF THE SITE. SEE EROSION CONTROL PLAN FOR EROSION CONTROL SEQUENCING.
- ALL EROSION CONTROL METHODS IMPLEMENTED SHALL CONFORM TO THE "MAINE EROSION AND SEDIMENT CONTROL EST MANAGEMENT PRACTICES (BMP's) MANUAL" DATED OCTOBER 2016 BY THE DEPARTMENT OF ENVIRONMENTAL PROTECTION. http://www.maine.gov/dep/land/erosion/escbmps/esc_bmp_engineers.pdf
- PRIOR TO THE COMMENCEMENT OF CONSTRUCTION, THE CONTRACTOR SHALL PLACE THE EROSION CONTROL BMPS INCLUDING SILT FENCE, BERMS, EROSION CONTROL MIX, ETC.. THE CONTRACTOR SHALL INSPECT THE BARRIER AND OTHER PREVENTATIVE MEASURES BI-WEEKLY, BEFORE ANY PREDICTED RAIN EVENT, AND AFTER ANY RAIN EVENT. THE CONTRACTOR SHALL REMOVE ANY ACCUMULATED SILT AND/OR MAKE REPAIRS AS
- THE CONTRACTOR IS CAUTIONED THAT FAILURE TO COMPLY WITH THE SEQUENCE OF CONSTRUCTION, EROSION/SEDIMENT CONTROL PLAN, AND OTHER PERMIT REQUIREMENTS MAY RESULT IN MONETARY PENALTIES. THE CONTRACTOR SHALL BE ASSESSED ALL SUCH PENALTIES AT NO COST TO THE OWNER OR PERMITTEE.

APPROVALS REQUIRED:

- L. TOWN OF CUMBERLAND PLANNING BOARD 2. MAINE DEP SITE LOCATION OF DEVELOPMENT PERMIT.
- 3. MAINE DEP NRPA TIER 1 PERMIT.
- 4. MAINE DOT ENTRANCE PERMIT.
- U.S. ARMY CORPS OF ENGINEERS PERMIT.

OCEANVIEW @ CUMBERLAND Tuttle Road, Cumberland, Maine

SHEET INDEX:

COVER SHEET

C11A-C11B. LANDSCAPE PLANS 1"=60"

SUBDIVISION PLAT BY TITCOMB ASSOCIATES

OVERALL PHASING PLAN 1"=100'

PLAN & PROFILES *SCALE:* 1" = 40'

STRUCTURE NOTES AND TABLES

EROSION CONTROL NOTES AND DETAILS

LOW PRESSURE SEWER MAIN DETAILS

FORESTED BUFFER BEHIND UNITS 50-52

FOCALPOINT 10 SCALE PLAN VIEW

SITE DEVELOPMENT DETAILS

BOX CULVERT DETAILS

WET POND DETAILS

FOCALPOINT DETAILS

C33

7-31-2018

TOPOGRAPHIC SITE PLAN BY TITCOMB ASSOCIATES

OVERALL SITE DEVELOPMENT PLAN *SCALE:* 1" = 60"

OVERALL SITE DEVELOPMENT PLAN *SCALE:* 1" = 40"

OVERALL SITE DEVELOPMENT PLAN *SCALE:* 1" = 40'

OVERALL SITE DEVELOPMENT PLAN *SCALE:* 1" = 40"

TRAIL AND WALKWAY MASTER PLAN 1" = 100'

ROADWAY SECTIONS, EROSION DETAILS, AND GENERAL NOTES

ROOF DRIPLINE BMP, BOULDER WALL, AND MISC. DETAILS

PRETX CURB INLET DETAIL - STA 21+89.32 RIGHT SIDE

SH 1 PORTLAND WATER DISTRICT STANDARD DETAILS

SH 2 PORTLAND WATER DISTRICT STANDARD DETAILS

MANCINI ELECTRICAL PHOTOMETRIC PLAN

CLASS B HIGH INTENSITY SOIL SURVEY BY MARK HAMPTON

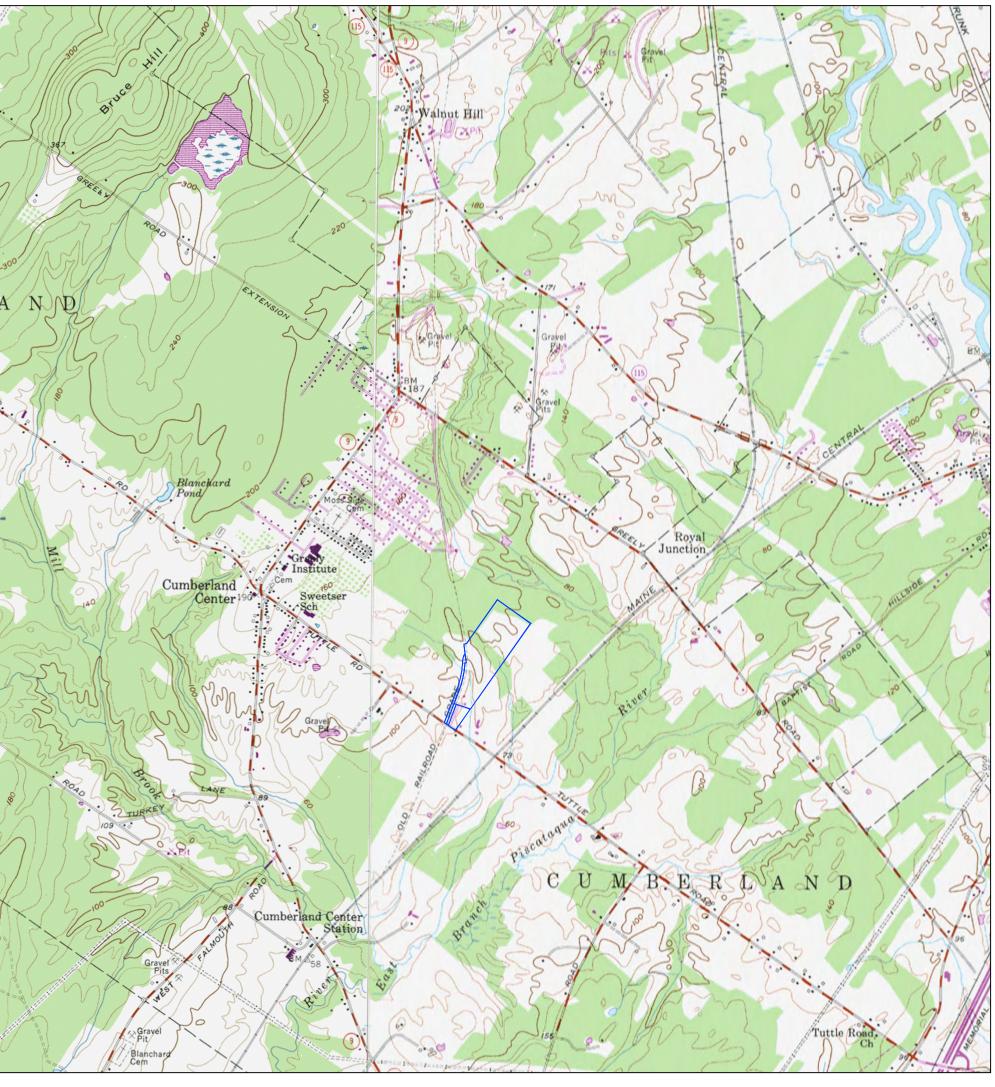
PRE DEVELOPMENT DRAINAGE PLAN - SUBMITTED SEPARATELY

POST DEVELOPMENT DRAINAGE PLAN - SUBMITTED SEPARATELY

RAIN GUARDIAN TURRET PRETREATMENT DETAIL - STA 21+89.32 LEFT SIDE

EXISTING CONDITIONS AND REMOVALS PLAN 1"=100"

July 31, 2018 Town Submission Set



LOCATION MAP 1"=2000'

UTILITY INFO & CONTACTS:

CONTACT: HERB STEVENS, 800.750.4000

SUMMIT NATURAL GAS: 12 INCH MAIN, W. SIDE TUTTLE RD. CONTACT: MICHAEL STINCHFIELD, PROJECT MANAGER 207.620.8000

WATER: PORTLAND WATER DISTRICT: 12 C.I.INCH MAIN, E. SIDE TUTTLE RD. CONTACT: ROBERT BARTELS, MEANS DEPT. 207.774.5961 X3199

SANITARY SEWER: PORTLAND WATER DISTRICT - 8 INCH GRAVITY SS, W. SIDE TUTTLE RD. CONTACT: ROBERT BARTELS, MEANS DEPT. 207.774.5961 X3199

ELECTRIC CENTRAL MAINE POWER: 3 PHASE OVERHEAD, W. SIDE TUTTLE RD.

COMMUNICATIONS/CTV: SPECTRUM COMMUNICATIONS, OVERHEAD, W. SIDE TUTTLE ROAD CONTACT: PETER DETESO, 207.318.6542

TELE; FAIRPOINT & CONSOLIDATED, OVERHEAD, W. SIDE TUTTLE ROAD CONTACT MATT FREE (CONSOLIDATED), 207.626.2007

STREET OPENING: TOWN OF CUMBERLAND URBAN COMPACT& (MDOT) CONTACT: MDOT SCARBOROGH, REGION 1, 207.885.7000 CONTACT: CUMBERLAND DPW: CHRIS BOLDUC, 207.829.2220

DESIGN CONSULTANTS:

BELANGER ENGINEERING *63 SECOND AVENUE*

AUGUSTA, ME 04330 (207) 622-0543

LICHT ENVIRONMENTAL DESIGN

35 FRAN CIRCLE GRAY, ME 04330 (207) 749-4924

DAVE HAYNES

MAINE REGISTERED LANDSCAPE ARCHITECT OCEAN VIEW RETIREMENT **COMMUNITY** 207-653-9427

TITCOMB ASSOCIATES 39 COURT STREET

BATH, ME 04530 (207) 443-9199

ANTHONY MANCINI, INC. *179 SHERIDAN STREET*

PORTLAND, MAINE 04101 (207) 774-5829

ARCHITECTS

207-883-6307

GAWRON / TURGEON

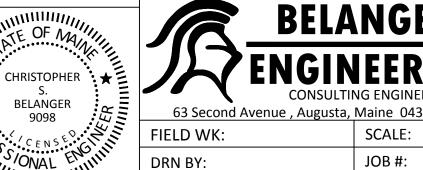
29 BLACK PT. ROAD SCARBOROUGH, MAINE 04074

6	6.	7-31-2018	Town Submission Set	CSB
5	5.	7-16-2018	Changes per PWD and CMP review	CSB
4	4.	5-4-2018	Change date, resubmit to DEP and ACOE	CSB
3	3.	3-1-2018	Respond to Town Memos, Re-submit to Town	CSB
2	2.	2-7-2018	Submit to Maine DEP	CSB
1	1.	1-31-2018	Respond to Town Memos, submit to Town	CSB

Cover Sheet and Notes

Oceanview at Cumberland LLC 277 Tuttle Road, Cumberland, Maine

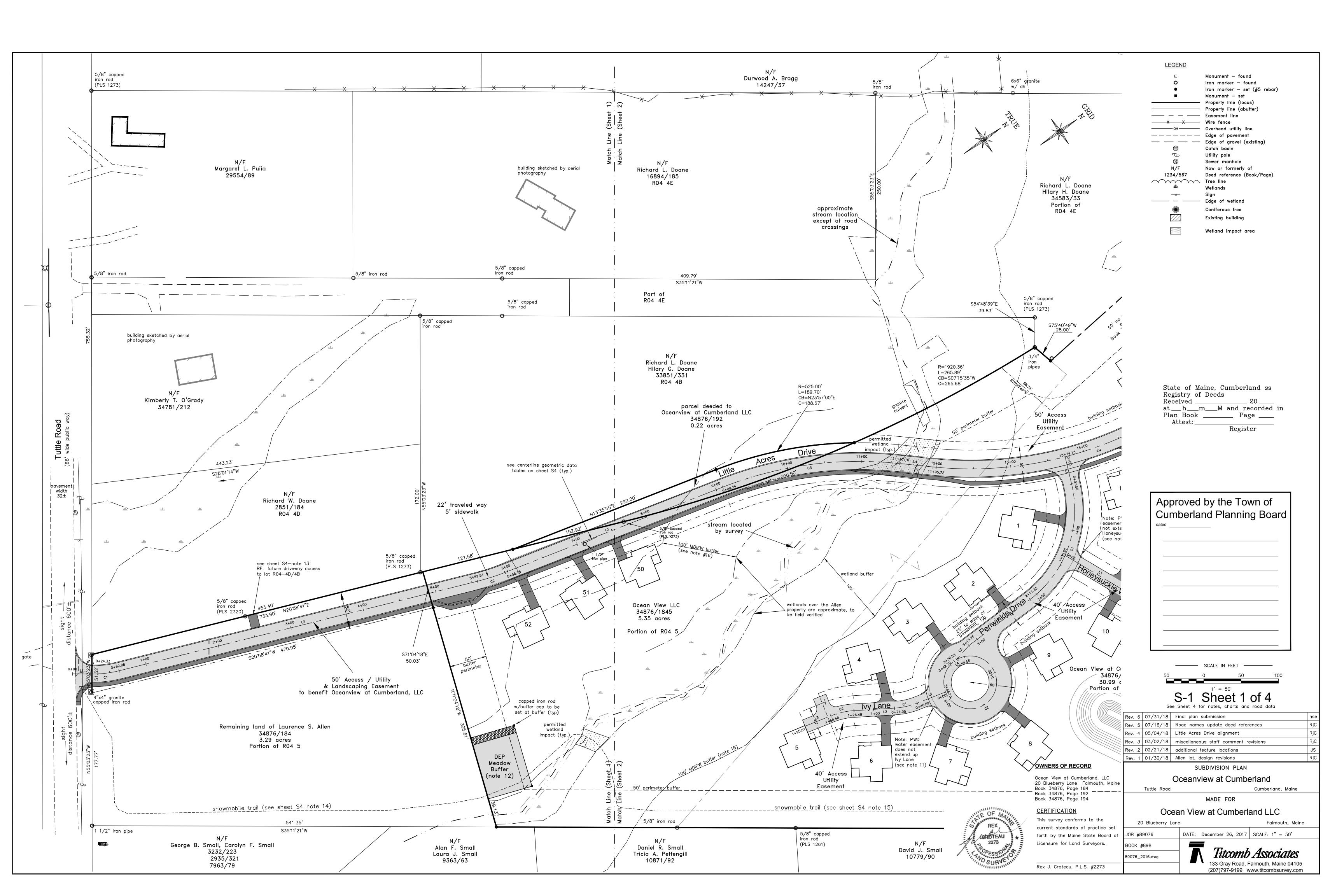
Seacoast Management Company 20 Blueberry Lane, Falmouth, Maine

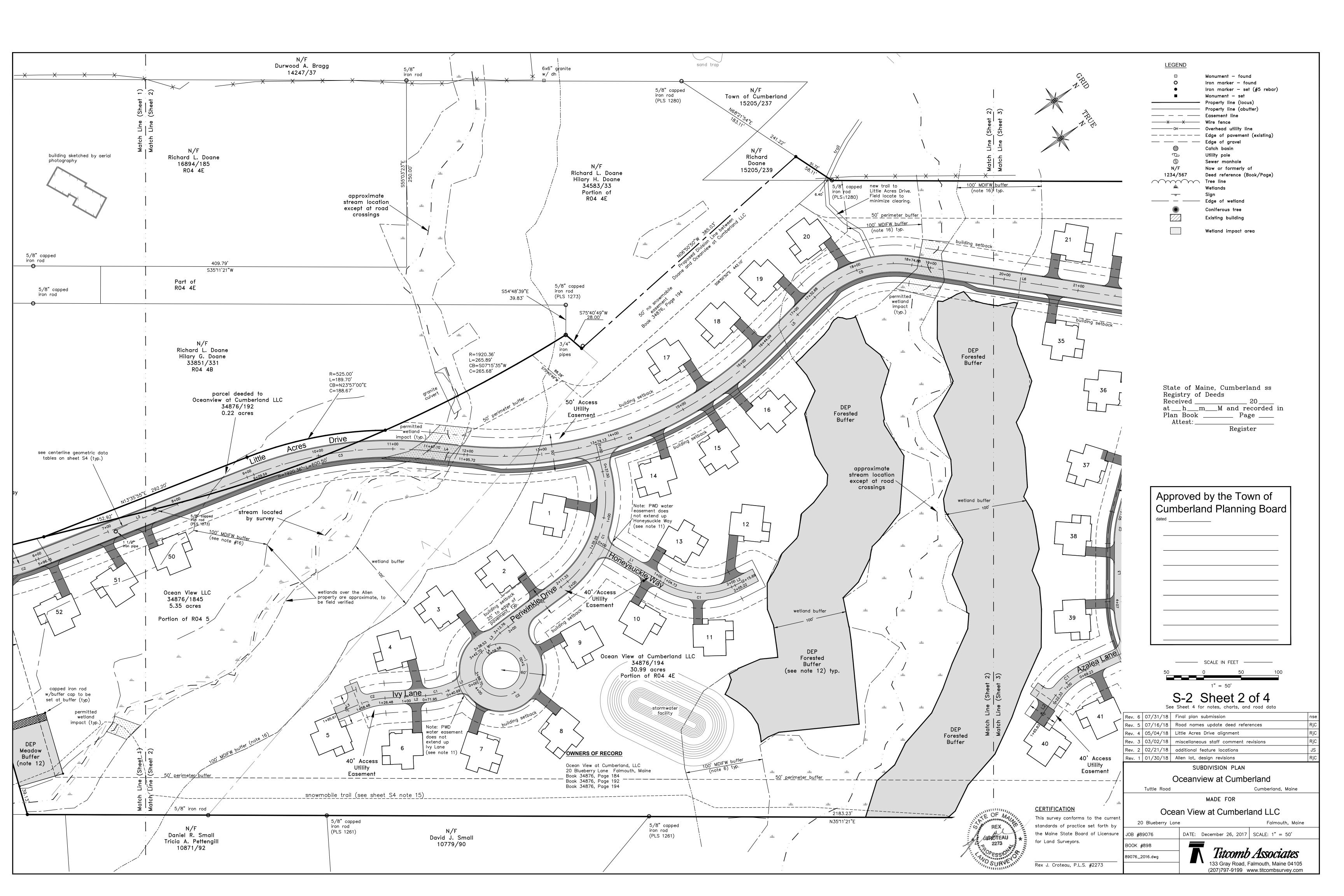


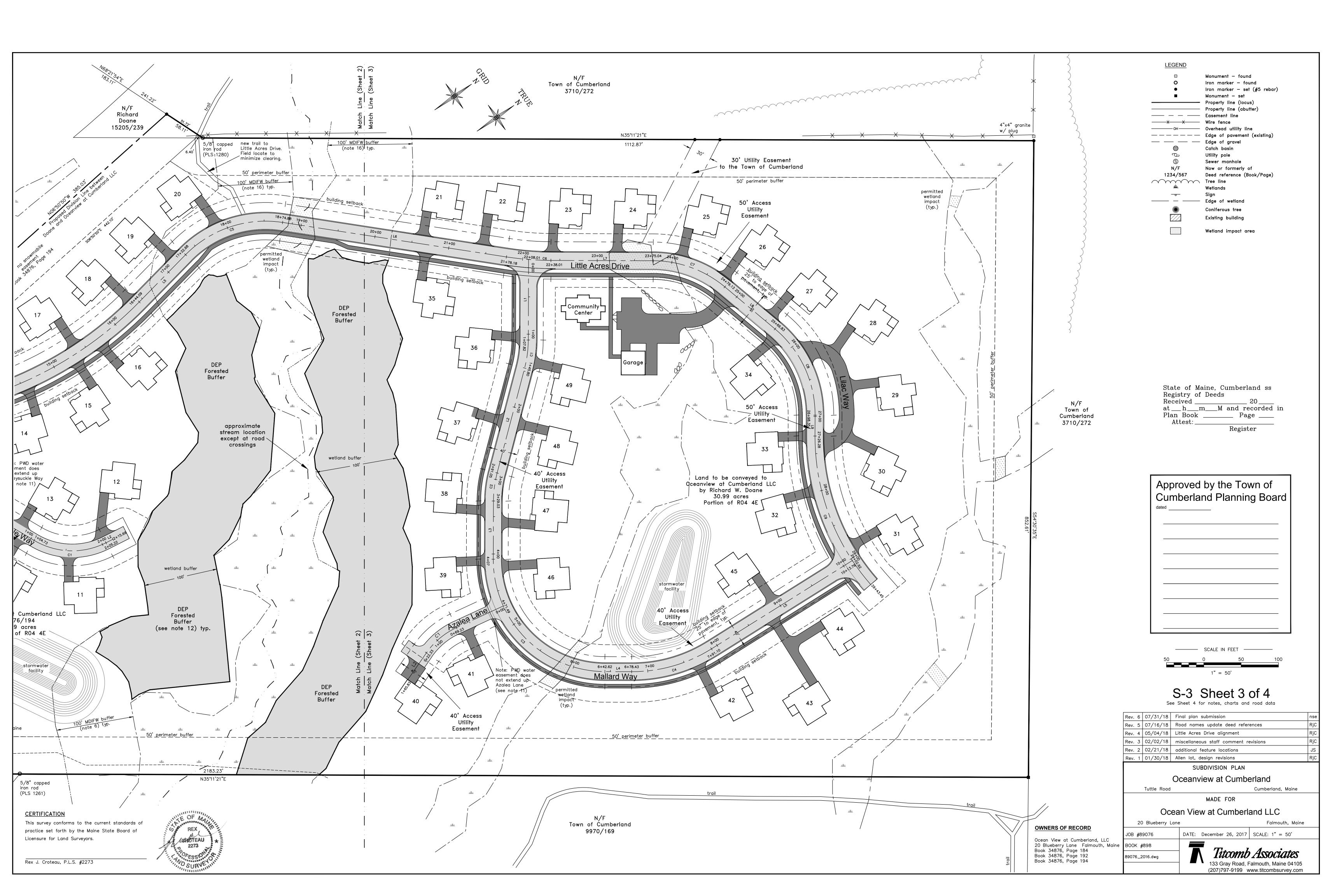
 RESIDENTIAL SUBDIVISIONS 63 Second Avenue, Augusta, Maine 04330 Ph 207-622-1462, Cell 207-242-5713

DRN BY: JOB #: 109 CH'D BY SS: FILE: DATE: 7-31-2018









LITTLE ACRES DRIVE

LINE	BE	EARING		DISTANCE
L1	S	35°42'06"	W	24.33'
L2	S	20°58'41"	W	494.63'
L3	S	13°35'55"	W	313.39
L4	S	40°49'17"	W	48.62'
L5	N	10°33'29"	W	88.59'
L6	S	43°45'29"	W	303.30'
L7	N	35°11'21"	Ε	137.03
L8	S	74 ° 57 ' 02"	W	87.70'
Па	N	54°48'30"	۱۸/	27 92'

[L9]N	54°48'39" W	[27.92]		
CURVE	ARC LENGTH	RADIUS	CHORD BEARING CHORD LEN	1G
C1	38.55	150.00	N 28°20'23" E 38.44'	
C1 C2	38.64'		S 17*17'18" W 38.61'	
C3	237.56'	500.00'	S 27°12'36" W 235.33'	
C4	448.37'	500.00'	S 15°07'54" W 433.50'	
C3 C4 C5 C6	142.20'		N 16°36'00" E 136.93'	
C6	59.82'		N 39°28'25" E 59.77'	
	404407	4 = 0 0 0 1	0 =====================================	

PERIWINKLE DRIVE

LINE	BE			DISTANCE
L1	z	68 ° 23'46"	W	37.50
L2	Z	01*59'54"	W	102.43
L3	Ν	13 ' 38'39"	W	24.77
L4	S	01°59'54"	Ε	4.17
	LINE L1 L2 L3 L4	LINE BE L1 N L2 N L3 N L4 S	L3 N 13'38'39"	L1 N 68*23'46" W L2 N 01*59'54" W L3 N 13*38'39" W

CURVE ARC LENGTH RADIUS CHORD BEARING CHORD LENG
C1 173.83' 150.00' N 35*11'50" W 164.26'
C2 216.89' 35.41' N 02*31'31" F 5.59'

HONEYSUCKLE WAY

LINE BEARING DISTANCE
L1 S 65*42'42" W 104.73'
L2 N 08*08'04" E 10.47'

CURVE ARC LENGTH RADIUS CHORD BEARING CHORD LENGT

IVY LANE

LINE BEARING DISTANCE

L1 N 13*33'32" E 40.69'

L2 N 31*28'07" E 54.53'

L3 N 13*07'56" E 37.13'

CURVE ARC LENGTH RADIUS CHORD BEARING CHORD LENGTH
C1 31.26' 100.00' S 22'30'49" W 31.13'
C2 32.00' 100.00' N 22'18'01" F 31.87'

MALLARD WAY

	_			
LINE		EARING		DISTANCE
L1	S	54°48'39"	Ε	107.82
L2	N	40°18'22"	W	145.26
L3	N	54°48'39"	W	77.97
L4	S	35°11'21"	W	35.81
L5	S	02°54'45"	W	222.67

	ARC LENGTH	RADIUS	CHORD BEARING	CHORD LENGTI
C1	37.97	150.00	N 47°33'30" W	37.87
C1 C2 C3	37.97'	150.00'	N 47°33'30" W	37.87
C3	235.62'	150.00'	S 80°11'21" W	212.13'
CA	110 67'	$\alpha \alpha \alpha \alpha \alpha \alpha'$	C 10°07'07" W	111 10'

AZALEA LANE

CURVE ARC LENGTH RADIUS CHORD BEARING CHORD LENGTH

OV AT CUMBERLAND SUBDIV PLAN NOTES

1) THIS PROJECT IS BEING PROPOSED AS A SENIOR HOUSING COMMUNITY PERMITTED UNDER THE TOWN OF CUMBERLAND LAND USE ORDINANCE SECTION 315-28.4. THE PROJECT INCLUDES 52 COTTAGE UNITS, A COMMUNITY CENTER AND ASSOCIATED INFRASTRUCTURE.

2) PROJECT LIES WITHIN THE RR1 ZONING DISTRICT AND SENIOR HOUSING COMMUNITY (SHC) OVERLAY DISTRICT

3) WETLANDS MAPPING BY HAMPTON ASSOCIATES, FALL 2016 AND LOCATED BY GPS SURVEY (HAMPTON ASSOC. AND TITCOMB ASSOC, SURVEYORS.)

4) SITE TOPOGRAPHY AND EXISTING CONDITIONS FROM A FIELD SURVEY BY TITCOMB ASSOCIATES, SURVEYORS WITH INFORMATION SUPPLEMENTED FROM THE STATE OF MAINE GIS DIGITAL ORTHO AND LIDAR MAPPING AS NOTED.

5) PROJECT TO BE SERVICED BY PUBLIC WATER, PRIVATE ON—SITE LOW PRESSURE SEWER SYSTEM DISCHARGING TO THE PORTLAND WATER DISTRICT PUBLIC SEWERAGE SYSTEM IN TUTTLE ROAD, NATURAL GAS AND UNDERGROUND CABLE UTILITIES.

6) AZALIA LANE, HONEYSUCKLE WAY, IVY LANE, LILAC WAY, LITTLE ACRES DRIVE, MALLARD WAY, AND PERIWINKLE DRIVE SHALL REMAIN PRIVATE.

7) COTTAGE UNITS AND FOOTPRINT STYLES AND DRIVEWAY LOCATIONS ARE SHOWN IN THE GENERAL LOCATIONS INTENDED TO BE CONSTRUCTED. HOWEVER APPROVAL. FINAL LOCATIONS AND BUILDING TYPES MAY VARY SLIGHTLY TO FIT FIELD CONDITIONS.

8) THERE SHALL BE NO LESS THAN TWO PARKING SPACE PER UNIT PER ORDINANCE SECTION 315—28.4.F. GARAGES AND ONE SPACE IN THE DRIVEWAY MAY BE USED TO MEET THIS REQUIREMENT.

9) REFER TO SITE DATA TABLE FOR SETBACKS AND DIMENSIONAL REQUIREMENTS.

10) THIS PLAT SHALL BE RECORDED WITHIN 90 DAYS OF FINAL SUBDIVISION APPROVAL AND SIGNING OF THE PLAT BY THE TOWN OF CUMBERLAND PLANNING BOARD, SUBJECT TO THE ESTABLISHMENT OF ANY PERFORMANCE GUARANTEE. APPROVAL OF ANY SUBDIVISION PLAN NOT RECORDED WITHIN 90 DAYS AFTER FINAL PLAN APPROVAL SHALL BECOME NULL AND VOID.

11) ACCESS AND UTILITY EASEMENT WIDTHS:

LII	THE ACRE DRIVE:	50	LEE I.
ΑZ	ALEA LANE:	40	FEET
HC	NEYSUCKLE WAY:	40	FEET
IV	/ LANE:	40	FEET
LIL	AC WAY:	N/	Α
MA	LLARD WAY:	40	FEET:
PE	RIWINKLE DRIVE:	40	FEET:

*DENOTES UTILITY EASEMENTS TO THE PORTLAND WATER DISTRICT IN ADDITION TO OTHER UTILITIES.

12) DEP MEADOW AND FORESTED BUFFERS AS SHOWN SHALL BE MONUMENTED OR MARKED IN THE FIELD USING IRON RODS AND PLASTIC "BUFFER CAPS"OR SIMILAR MARKINGS. LOCATIONS OF FORESTED BUFFER MONUMENTS SHALL BE FIELD DETERMINED AT REASONABLE LOCATIONS DUE TO THE IRREGULAR AND LARGE SIZE OF THESE BUFFERS.

13) RIGHTS TO BE RESERVED TO RICHARD W.DOANE AND HIS ATTORNEY—IN—FACT RICHARD W. DOANE OVER THE 50—FOOT ACCESS AND UTILITY EASEMENT FOR ACCESS TO LOT RO4—4D TO PROVIDE A DRIVEWAY ACCESS AND CURB CUT OFF LITTLE ACRES DRIVE FOR A MAXIMUM OF TWO (2) DWELLING UNITS OR RESIDENCES ON LOTS RO4—4D AND RO4—4B. LOCATION OF SAID DRIVEWAY SHALL BE FIELD DETERMINED.

14) THE SNOWMOBILE TRAIL SHOWN ON THE 3.29 ALLEN LOT IS SHOWN GENERALLY ONLY FOR ILLUSTRATIVE PURPOSES.

OCEANVIEW AT CUMBERLAND MAKES NO WARRANTIES AS TO THE FUTURE EXISTENCE, LICENSE, LOCATION OR WINTER MAINTENANCE OF SAID SECTION OF TRAIL OVER THE ALLEN LOT.

15) OCEANVIEW AT CUMBERLAND, LLC SHALL PROVIDE A REVOCABLE LICENSE TO THE TOWN OF CUMBERLAND FOR USE OF A MULTI-USE/SNOWMOBILE TRAIL LOCATED GENERALLY WITHIN THE 50-FOOT PERIMETER BUFFER AS SHOWN SUBJECT TO CONDITIONS OF DEP OR CORPS OF ENGINEERS WETLAND PERMITS FOR CROSSING OF REGULATED WETLANDS. FINAL LOCATION OF THE TRAIL SHALL BE DETERMINED IN THE FIELD. SAID LICENSE TO BE EXECUTED AND RECORDED IN THE CCRD FOLLOWING PROJECT APPROVALS.

16) 100— FOOT MAINE DEPARTMENT OF INLAND FISHERIES & WILDLIFE (MDIFW) BUFFERS ARE SHOWN ALONG STREAM ASSOCIATED WETLANDS EXCEPTING PERMITTED AREAS OF ENCROACHMENT FOR ROADS AND INFRASTRUCTURE AS SHOWN ON THIS PLAN AND THE ACCOMPANYING ENGINEERING PLANS. THE BUFFER LINE SHOWN IN THE AREAS OF UNITS 50—52 DOES INCLUDES EXISTING DEVELOPED AREAS OF THE ALLEN RESIDENCE AND IS LIMITED ONLY TO NO CUTTING BEYOND THE CURRENT TREELINE EXCEPT FOR CONSTRUCTION OF A PORTION OF LITTLE ACRES DRIVE AS SHOWN WITHIN THE 100—FOOT BUFFER.

SURVEY NOTES

1) BOOK AND PAGE REFERENCES ARE TO THE CUMBERLAND COUNTY REGISTRY OF DEEDS.

2) BEARINGS ARE REFERENCED TO GRID NORTH, MAINE STATE PLANE COORDINATE SYSTEM, NAD83, WEST ZONE.

4) UTILITY INFORMATION ON THIS PLAN IS APPROXIMATE, BASED ON LOCATION OF VISIBLE FEATURES. DIGSAFE AND/OR THE APPROPRIATE UTILITIES SHOULD BE CONTACTED PRIOR TO ANY CONSTRUCTION.

5) PROPERTY LIES WITHIN ZONE C BASED ON FIRM COMMUNITY #230162 PANEL #0015 B, DATED MAY 19, 1981. IT DOES NOT LIE WITHIN A SPECIAL FLOOD HAZARD AREA.

OWNERS OF RECORD

Ocean View at Cumberland, LLC Book 34876, Page 184 Book 34876, Page 192 Book 34876, Page 194

PROJECT AREA

Land conveyed to Oceanview at Cumberland LLC by Richard W. Doane: Book 34876, Page 194	30.99 acres
Land conveyed to Oceanview at Cumberland LLC by Richard L Doane and Hilary G. Doane: Book 34876, Page	192 0.22 acres
Land conveyed to Oceanview LLC by Laurence S. Allen: Book 34876, Page 184	5.35 acres
Total project area in fee	36.56 acres
50' Access Easement over Allen parcel Total Project Area	0.53 acres 37.09 acres

SITE DATA TABLE						
ZONING	RR1 AND SENIOR HOUSING COMMUNITY (SHC) OVERLAY DISTRICT					
STANDARD	REQUIRED SHC	PROVIDED				
MIN. LOT AREA (AC)	5 AC	37.09				
MIN. FRONTAGE (FT)	0	50				
SETBACKS:						
A. EDGE PAVED ROAD	25	25+				
B. BETWEEN STRUCTURES	20	20+				
C. DEVELOPMENT PROPERTY LINE	30	50+				
MAXIMUM DENSITY (LAND AREA/UNIT) (3.)	10,000	31,003				
MAX. ALLOWABLE UNITS (2)	161	52				
OPEN SPACE	20% (7.4 AC.)	78% (28.7 AC.)				
MAX. STRUCTURE HEIGHT (FT.)	40	40 (4.)				
PERIMETER BUFFER (FT.)	50	50				

NOTES:

- PROJECT EXCLUDES 2.8 ACRE ALLEN OUT-LOT
 NOT INCLUDING PROPOSED COMMUNITY CENTER
- 3. DENSITY BASED ON LOT AREA OF 37.01 ACRES NO DEDUCTS REQUIRED
- 4. TYPICAL COTTAGE HEIGHTS ARE 23 FEET+/-. NO BUILDING SHALL EXCEED 40 FT.

PLAN REFERENCES

1) RIGHT-OF-WAY AND TRACK MAP, MAINE CENTRAL R.R., STATION 307+80 TO STATION 360+60, JUNE 30, 1916. MCRR FILE NO. V2/S1 AND V2/S2.

2) STANDARD BOUNDARY SURVEY PREPARED FOR MARION B. SMALL BY GARY E. JOHNSON, RLS. 1261, DATED AUG. 1987. UNRECORDED.

3) PLAN OF WYMAN FARM, CUMBERLAND CENTER, MAINE, BY EARL RAND, DATED MAY 2, 1931. UNRECORDED.

4) PLAN OF TUTTLE ROAD IN CUMBERLAND FROM CUMBERLAND CENTER TO FEDERAL ROAD, SURVEYED OCT. 11, 1926 BY WM. E. WINSLOW. RECORDED IN THE CUMBERLAND COUNTY COMMISSIONERS PLAN BOOK 5, PAGE 2.

5) ORIGINAL LOTTING PLAN OF NORTH YARMOUTH, RECORDED INTHE CUMBERLAND COUNTY REGISTRY OF DEEDS, PLAN BOOK 24,PAGE 14. CUMBERLAND COUNTY REGISTRY OF DEEDS IN PLAN BOOK 203, PAGE 82.

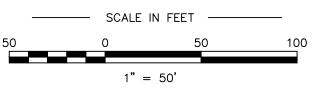
6) AMENDED PLAN OF PRIVATE WAY MADE FOR RICHARD DOANE BY TITCOMB ASSOCIATES DATED MAY 7, 1990 AND REVISED THROUGH NOV. 11. 2009 AND RECORDED IN PLAN BOOK 204, PAGE 895

7) RECORDING PLAT OF SMALL'S BROOK CROSSING SUBDIVISION MADE BY LAND USE CONSULTANTS, DATED OCTOBER 14, 1991 AND REVISED THROUGH OCTOBER 7, 1992 AND RECORDED IN PLAN BOOK 192, PAGE 312-314.

8) PLAN OF PROPOSED CONVEYANCES MADE FOR OCEAN VIEW AT CUMBERLAND LLC BY TITCOMB ASSOCIATES DATED APRIL 6, 2018 AND REVISED THROUGH MAY 30, 2018.

State of Maine, Cumberland ss
Registry of Deeds
Received ______ 20___
at ___h ___m ___M and recorded in
Plan Book _____ Page ____
Attest: _____
Register

Approved by the Town of Cumberland Planning Board



S-4 Sheet 4 of 4 18 Final plan submission

Rev. 607/31/18Final plan submissionnseRev. 507/16/18Road names update deed referencesRjCRev. 405/04/18Little Acres Drive alignmentRjCRev. 303/02/18miscellaneous staff comment revisionsRjCRev. 202/21/18additional feature locationsJSRev. 101/30/18Allen lot, design revisionsRjC

Oceanview at Cumberland
Cumberland, Maine

MADE FOR

(207)797-9199 www.titcombsurvey.com

Ocean View at Cumberland LLC

20 Blueberry Lane Falmouth, Maine

Tuttle Road

JOB #89076

DATE: December 26, 2017 SCALE: 1" = 50'

BOOK #898

B9076_2016.dwg

Titcomb Associates

133 Gray Road, Falmouth, Maine 04105



<u>CERTIFICATION</u>

OWNERS OF RECORD

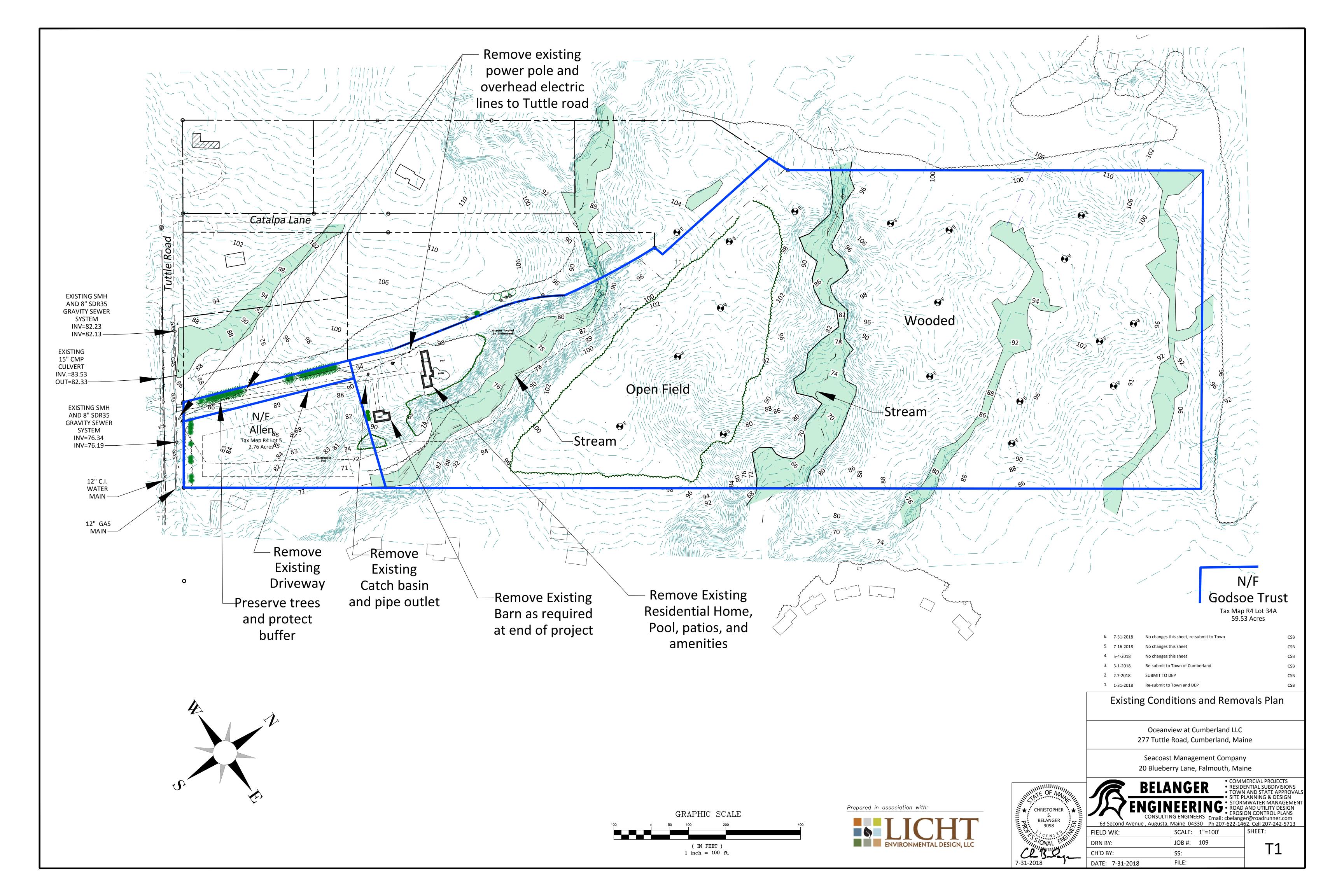
Book 34876, Page 184

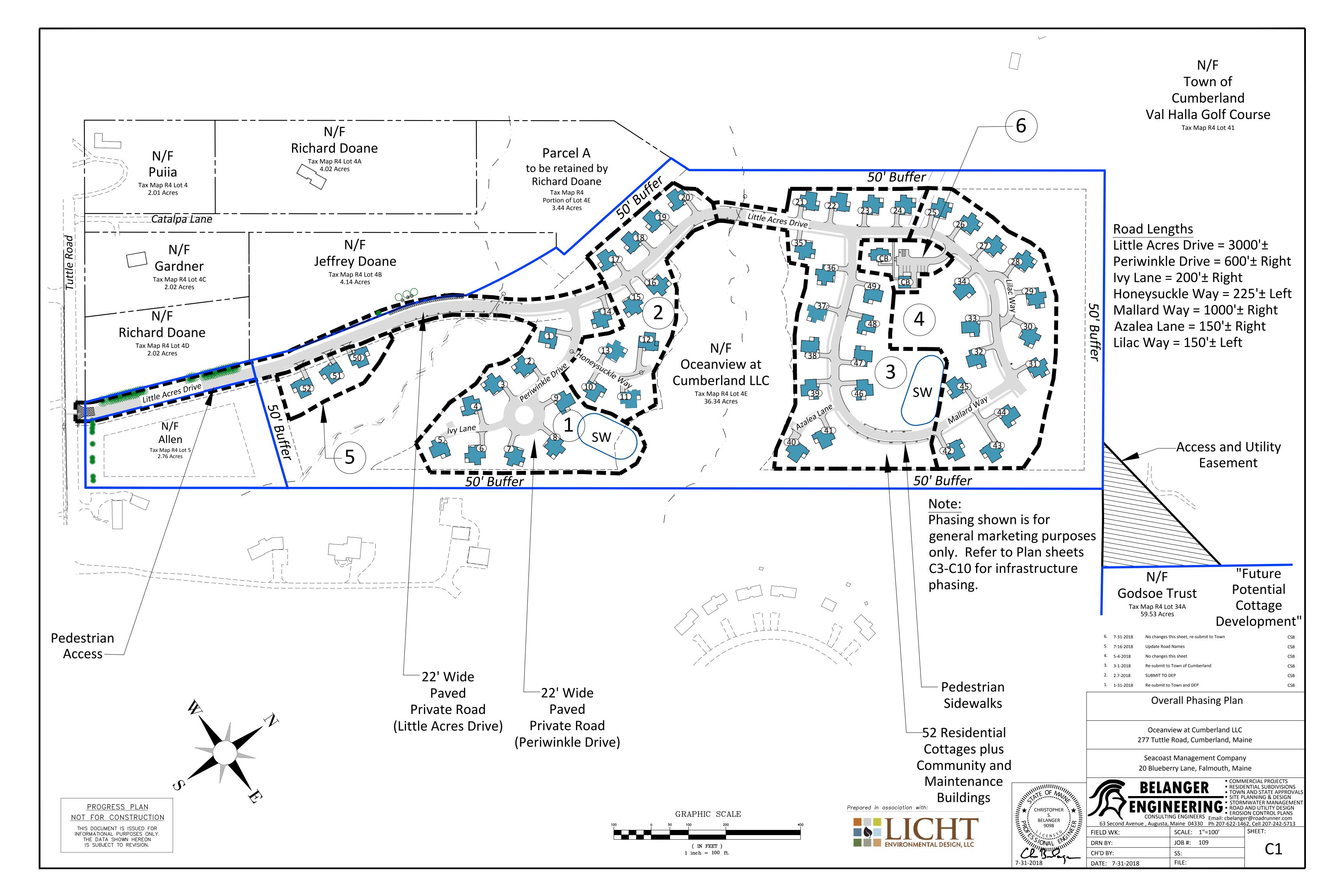
Book 34876, Page 192 Book 34876, Page 194

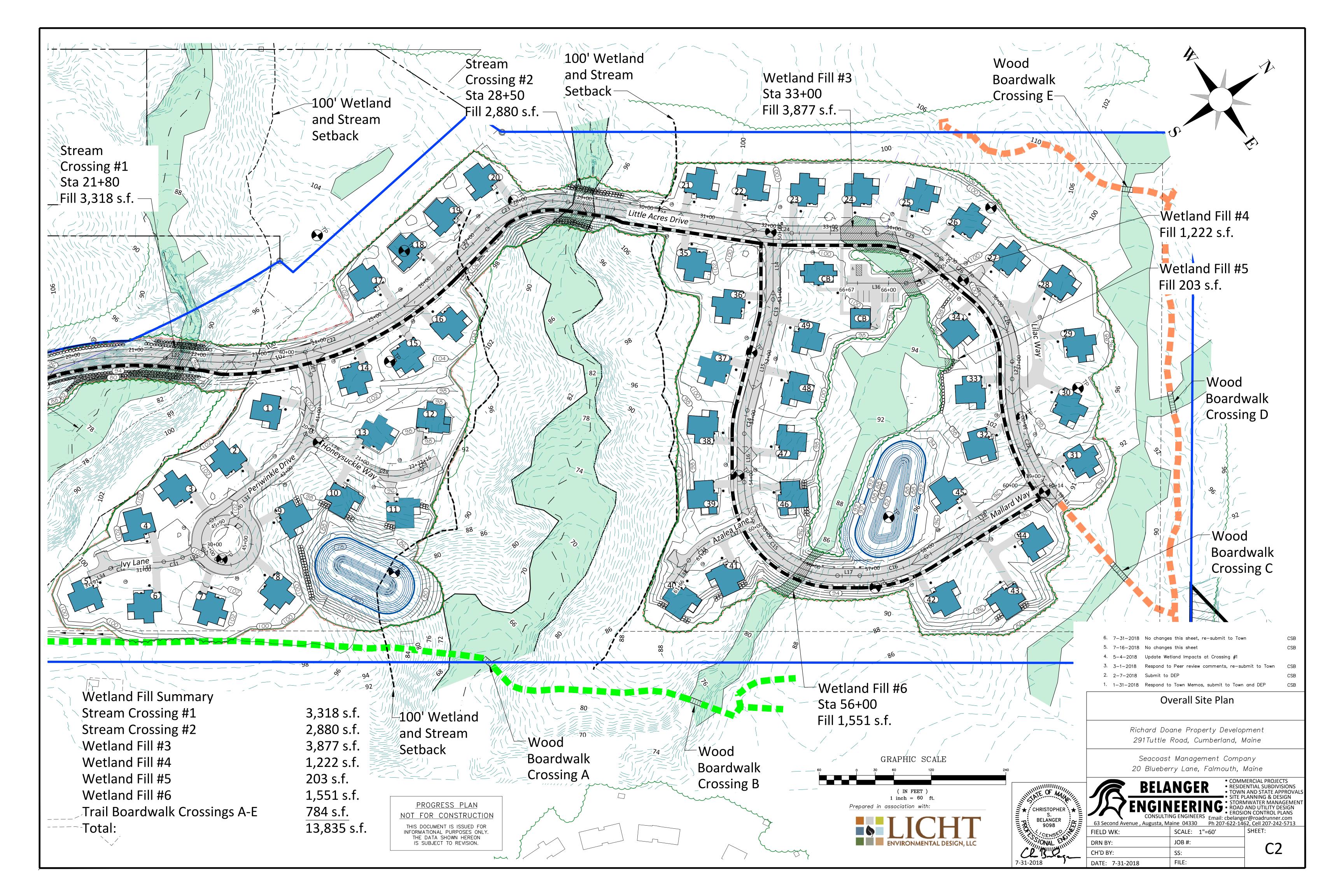
Ocean View at Cumberland, LLC 20 Blueberry Lane Falmouth, Maine

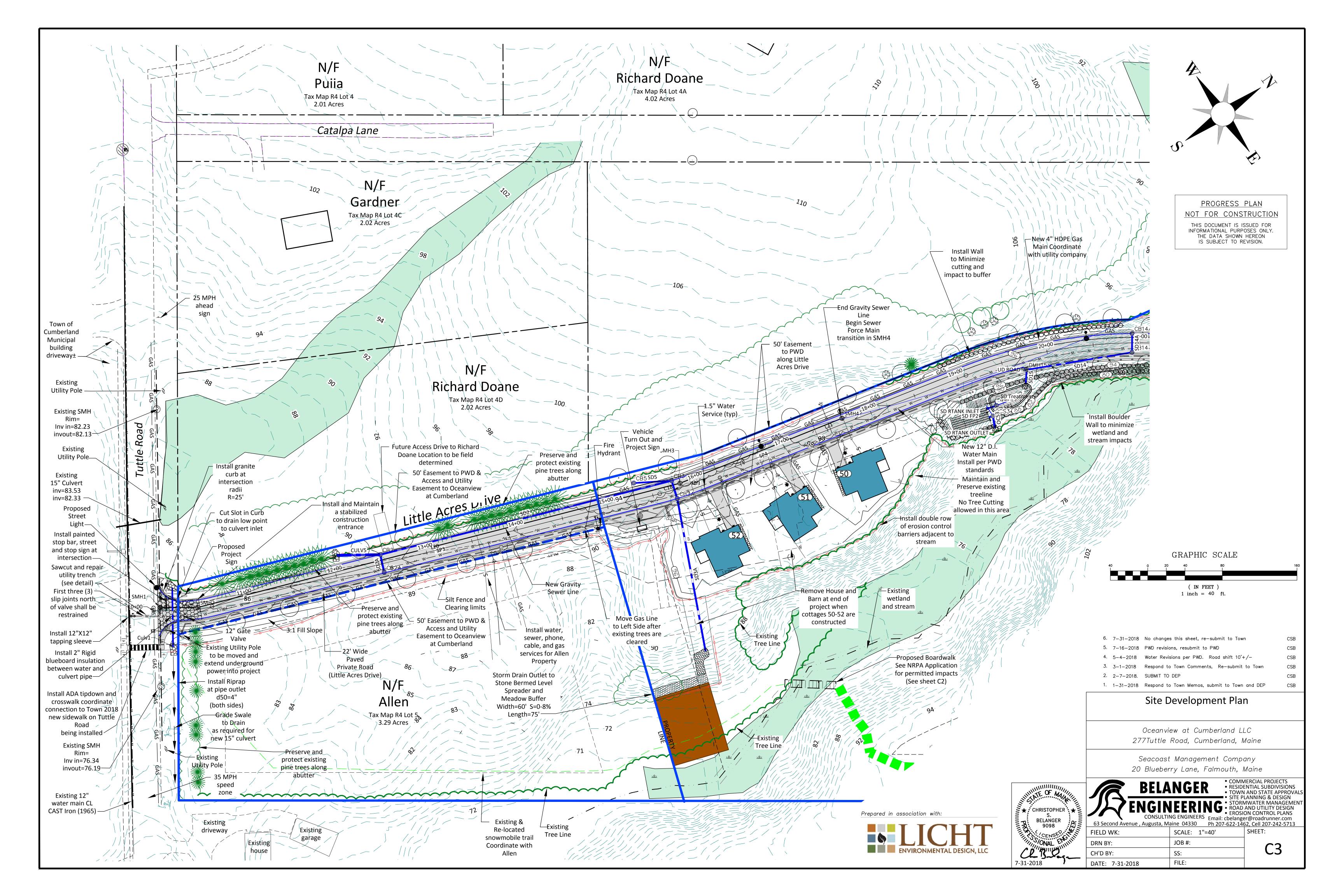
This survey conforms to the current standards of practice set forth by the Maine State Board of Licensure for Land Surveyors.

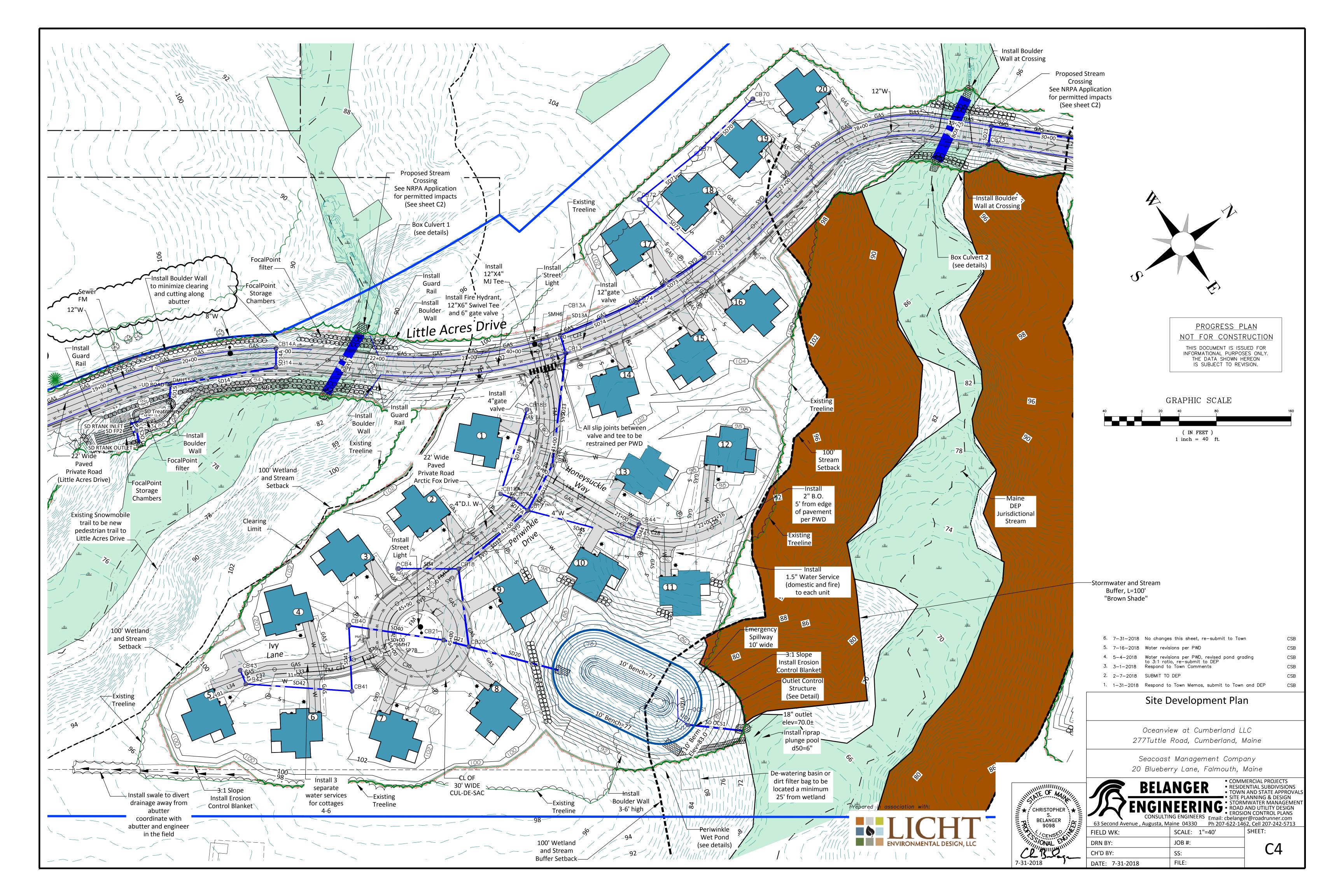
Rex J. Croteau, P.L.S. #2273

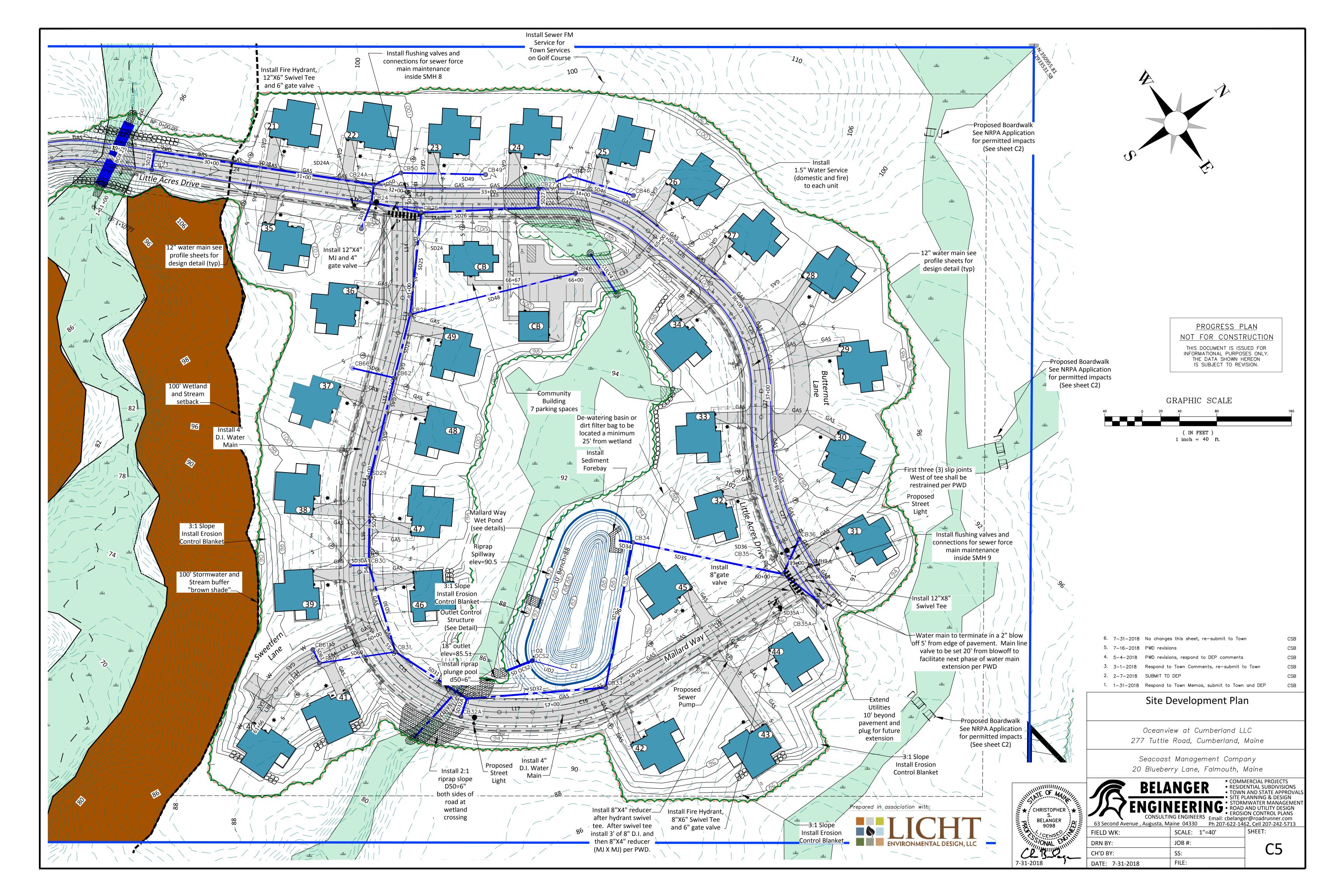


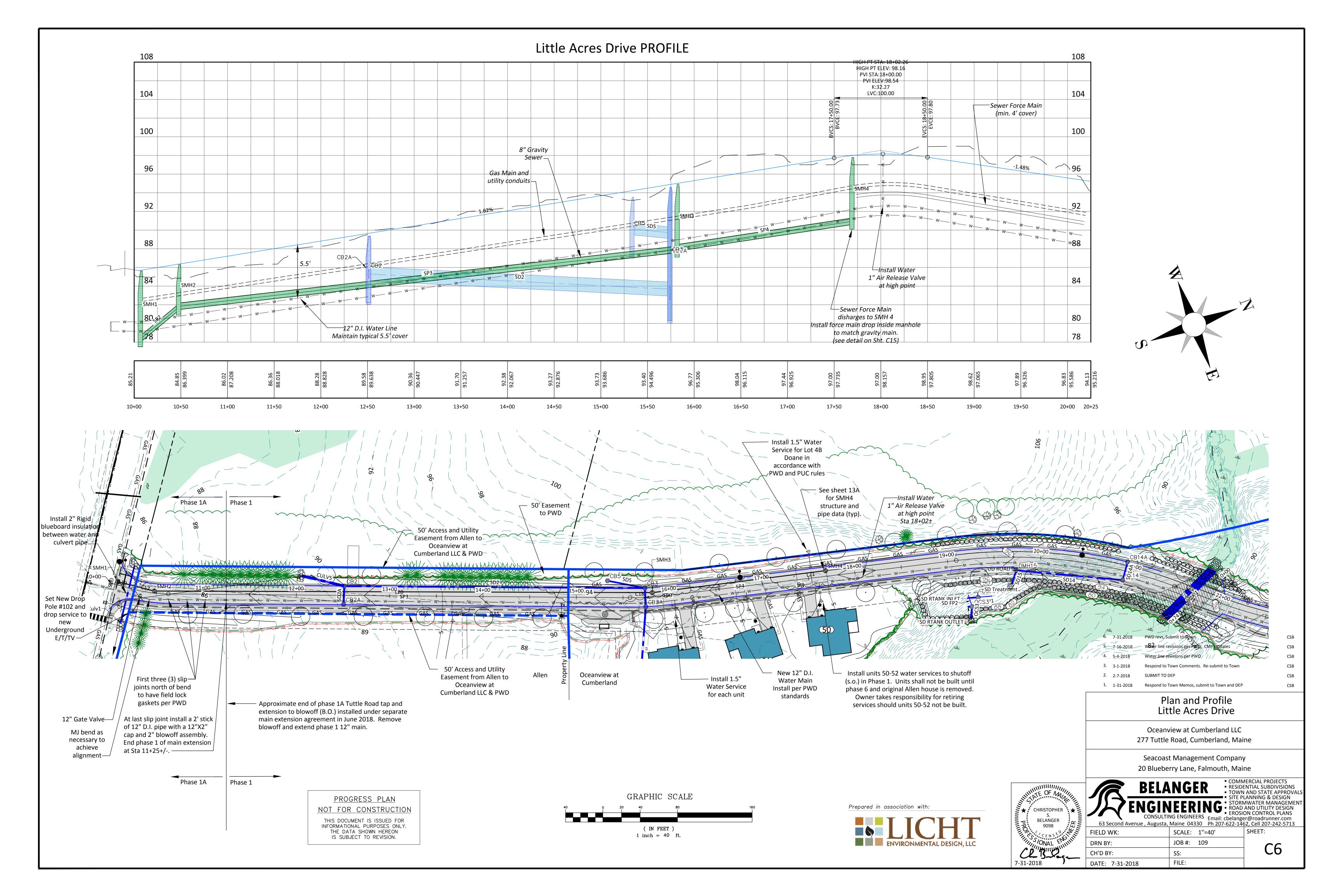


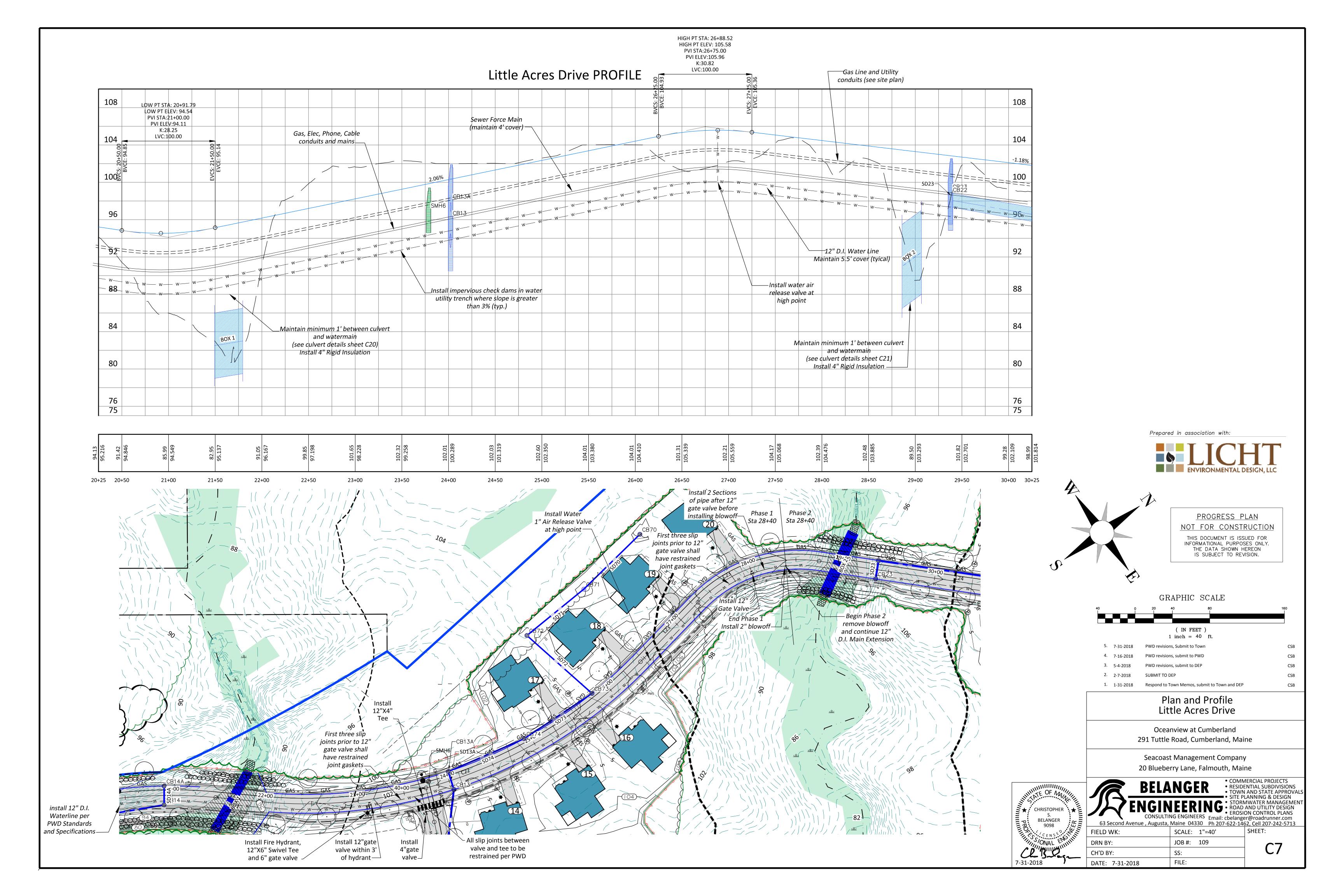


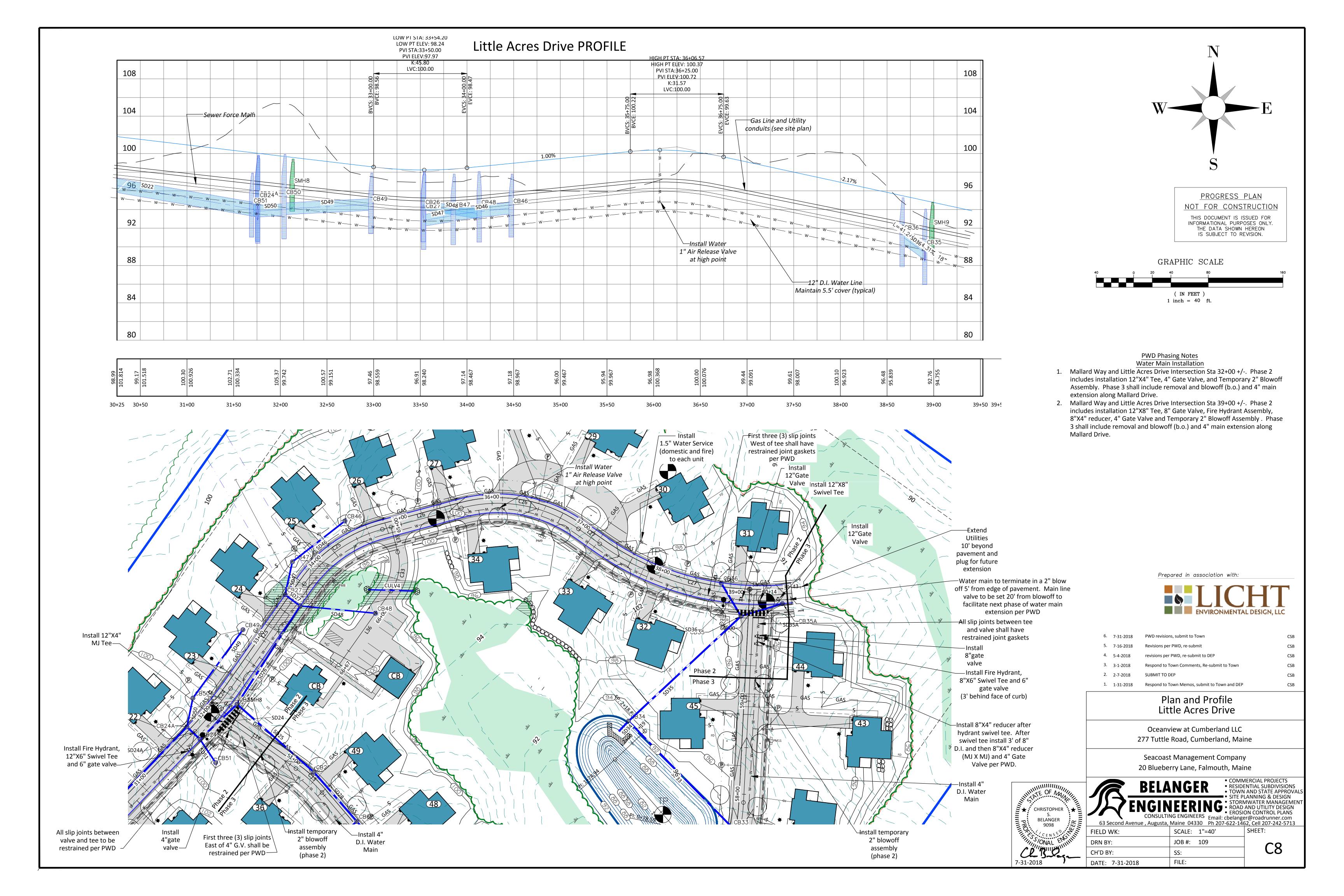


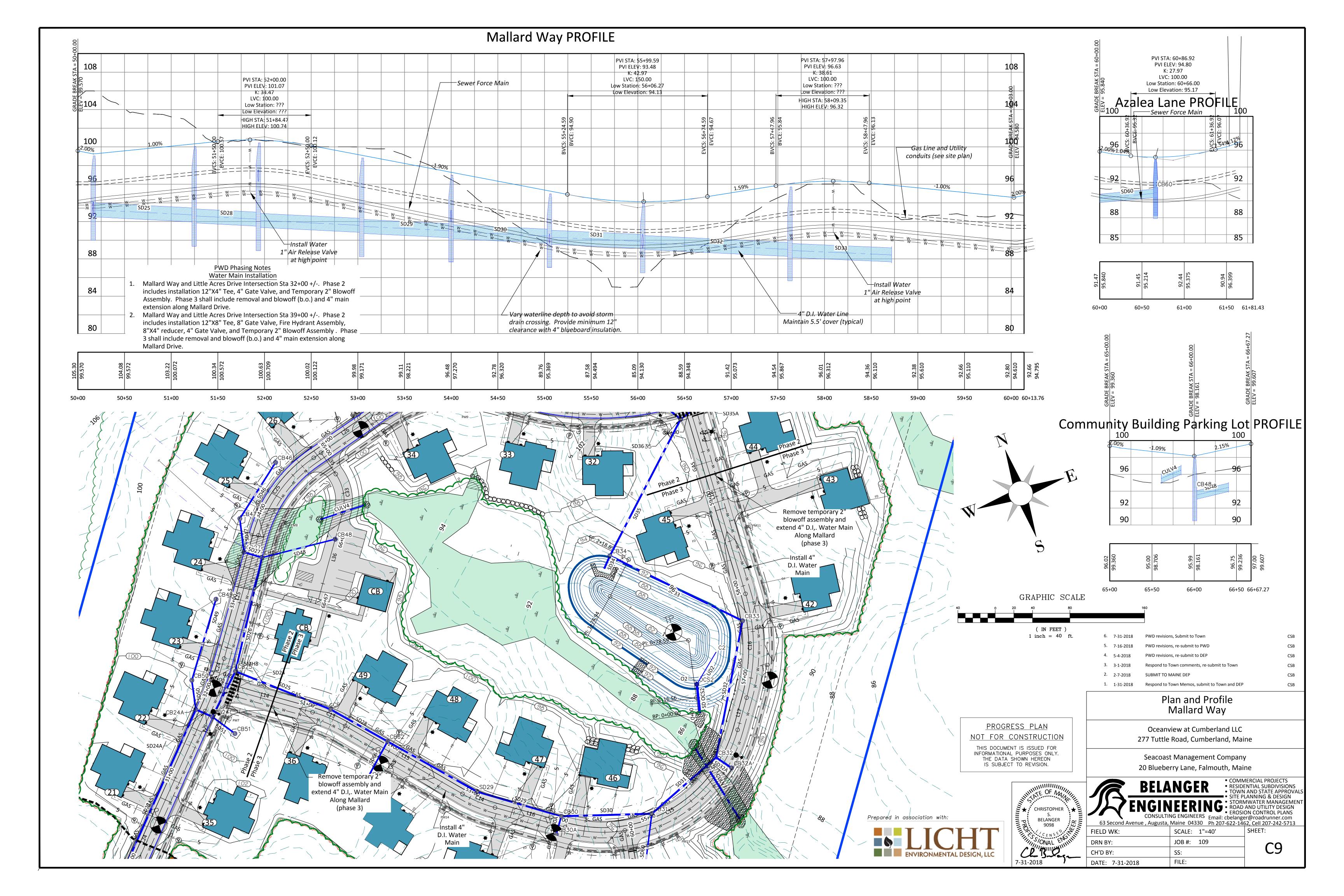


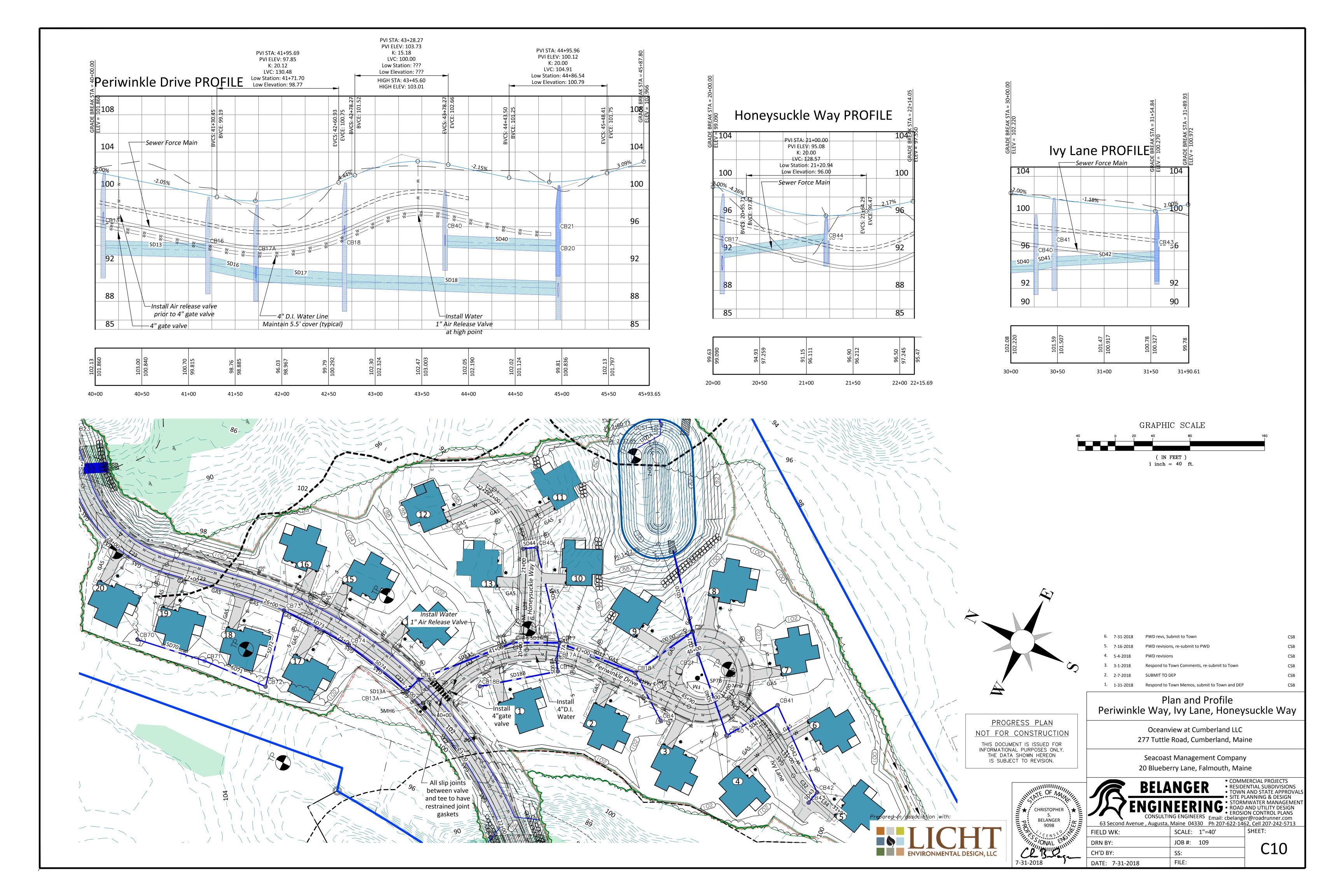


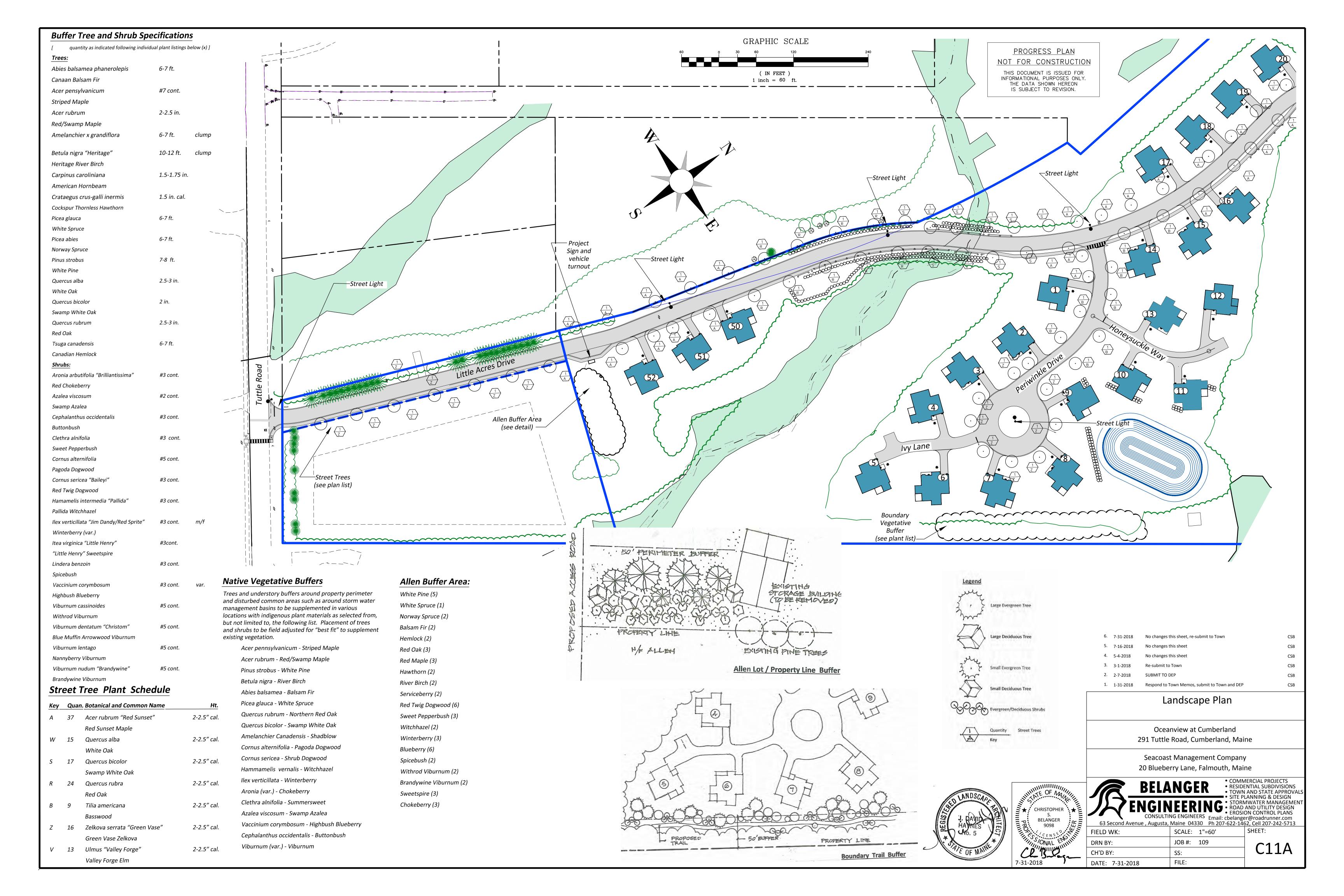


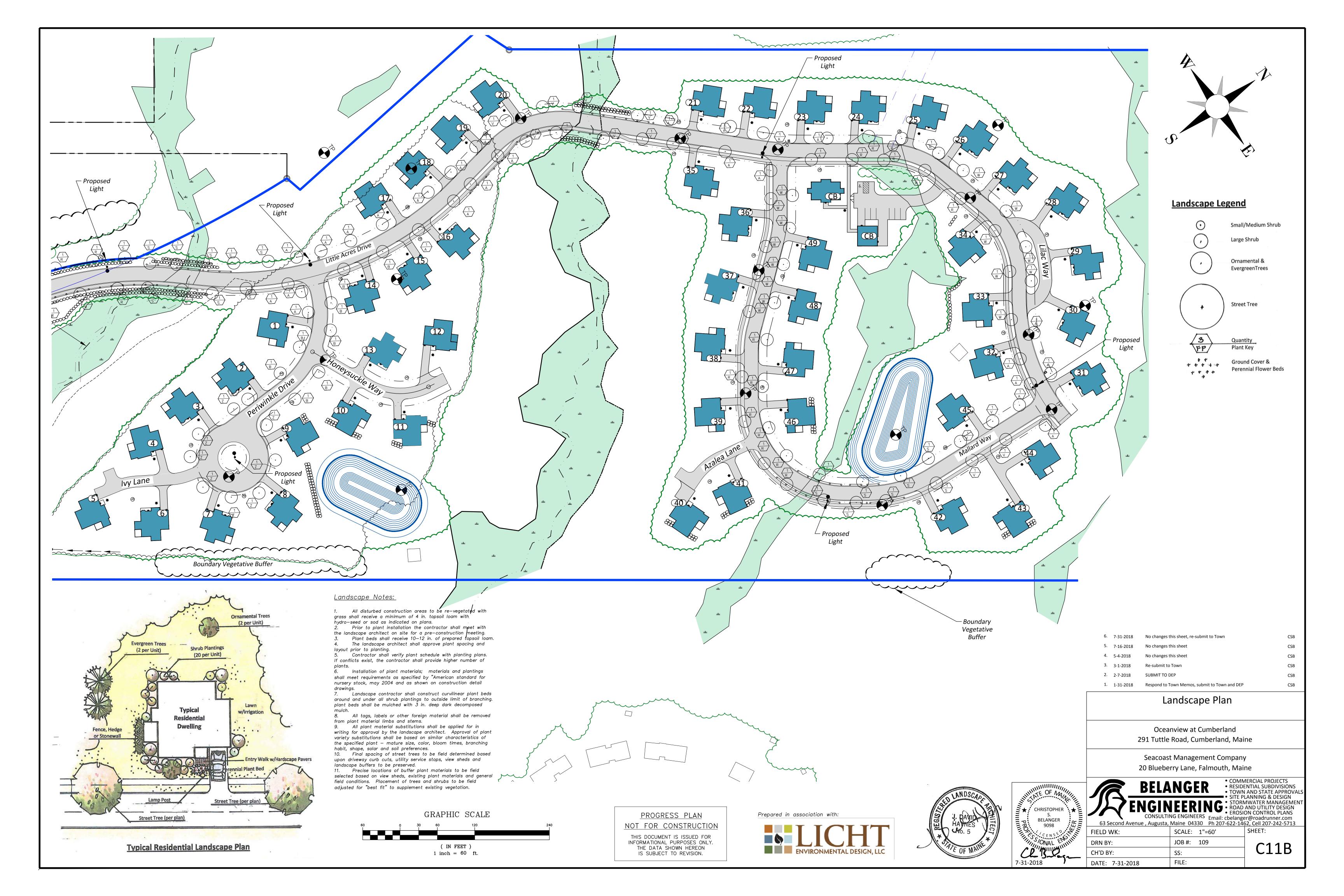


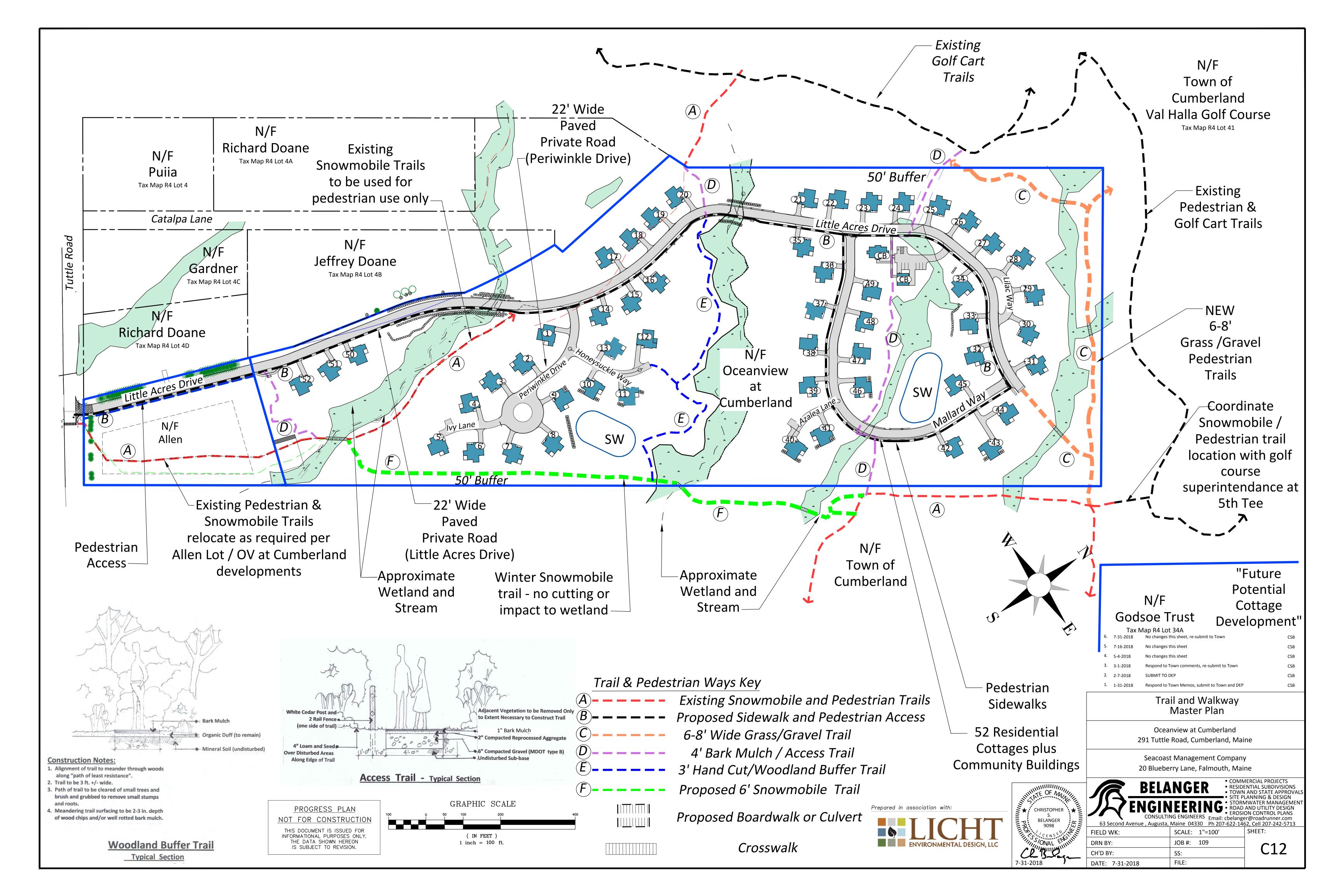


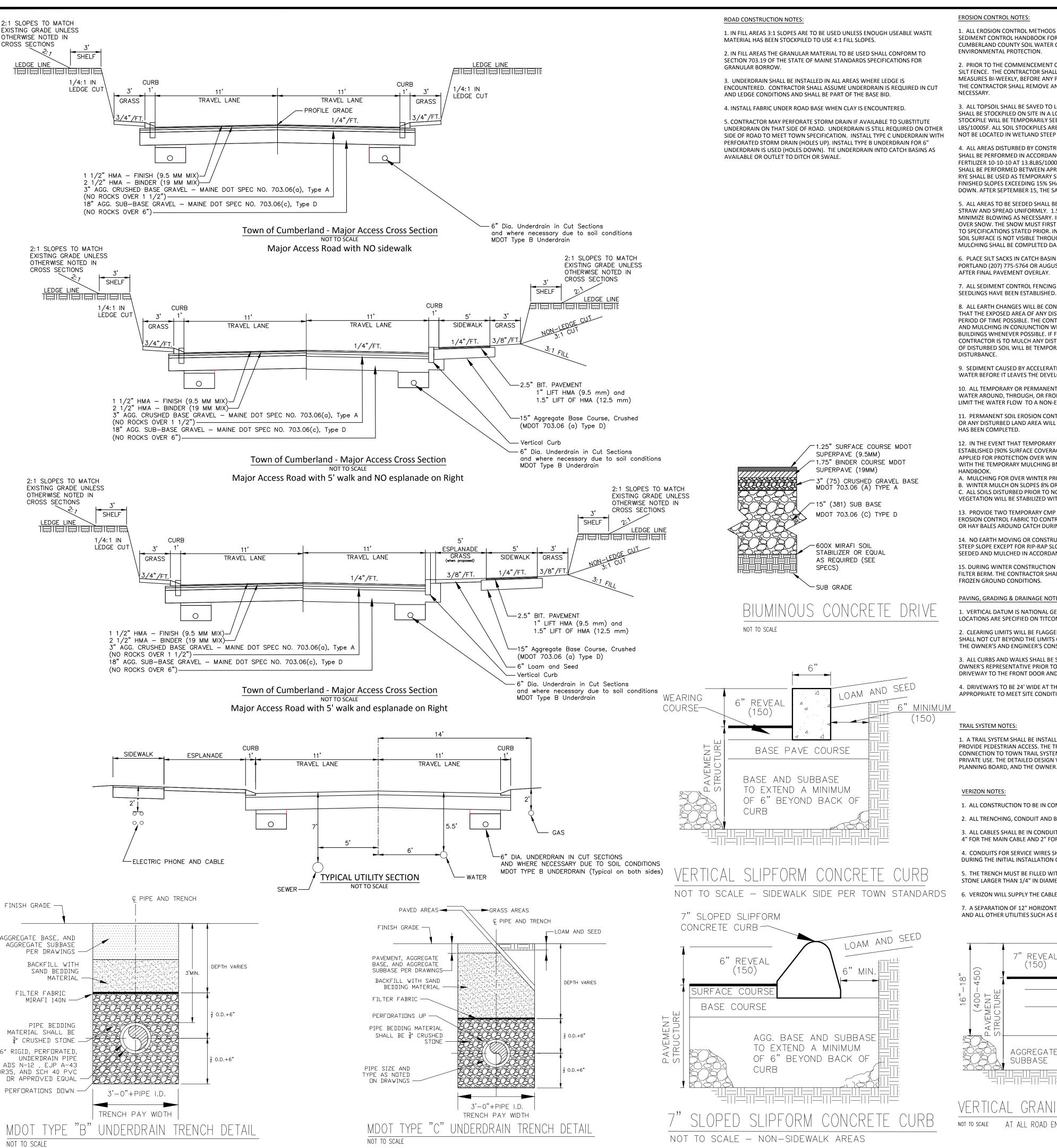












EROSION CONTROL NOTES:

1. ALL EROSION CONTROL METHODS SHALL CONFORM TO THE MAINE EROSION AND SEDIMENT CONTROL HANDBOOK FOR CONSTRUCTION BEST MANAGEMENT PRACTICES BY THE 1. ALL UTILITIES TO BE LOCATED UNDERGROUND. CUMBERLAND COUNTY SOIL WATER CONSERVATION DISTRICT, AND THE DEPARTMENT OF ENVIRONMENTAL PROTECTION.

2. PRIOR TO THE COMMENCEMENT OF CONSTRUCTION, THE CONTRACTOR SHALL PLACE THE WITH THE RESPECTIVE OWNERS. THE CONTRACTOR SHALL BE RESPONSIBLE FOR COMPLYING SILT FENCE. THE CONTRACTOR SHALL INSPECT THE BARRIER AND OTHER PREVENTATIVE MEASURES BI-WEEKLY, BEFORE ANY PREDICTED RAIN EVENT, AND AFTER ANY RAIN EVENT. THE CONTRACTOR SHALL REMOVE ANY ACCUMULATED SILT AND/OR MAKE REPAIRS AS

3. ALL TOPSOIL SHALL BE SAVED TO LOAM LANDSCAPED AREAS TO A DEPTH OF 4". LOAM SHALL BE STOCKPILED ON SITE IN A LOCATION CONVENIENT TO THE CONTRACTOR. THE STOCKPILE WILL BE TEMPORARILY SEEDED WITH RYE GRASS AND MULCHED AT 75 90 LBS/1000SF. ALL SOIL STOCKPILES ARE TO BE ENCLOSED WITH SILT FENCE. STOCKPILES SHALL PRE-CONSTRUCTION CONFERENCE MUST BE HELD WITH ALL UTILITY REPRESENTATIVES. NOT BE LOCATED IN WETLAND STEEP SLOPES, OR AREAS OF CONCERTRATING FLOW.

5. A MINIMUM OF 12" HORIZONTAL SPACING IS NECESSARY BETWEEN CABLES. 4. ALL AREAS DISTURBED BY CONSTRUCTION SHALL BE PERMANENTLY SEEDED. SEEDING SHALL BE PERFORMED IN ACCORDANCE WITH MDOT SPECIFICATION: LIME AT 3 TONS/ACRE: 6. 4" CABLE & TELEPHONE SERVICE WILL BE CONSTRUCTED IN THE SAME TRENCH AS ELECTRIC. FERTILIZER 10-10-10 AT 13.8LBS/1000 SF: SEED MDOT PARK MIX AT 3 LBS/1000 SF. - SEEDING SHALL BE PERFORMED BETWEEN APRIL 15 - JUNE 15 OR AUGUST 15 - SEPTEMBER 15. WINTER RYE SHALL BE USED AS TEMPORARY SEED BETWEEN SEPTEMBER 15 - OCTOBER 15. ALL FINISHED SLOPES EXCEEDING 15% SHALL ALSO HAVE MULCH NETTING INSTALLED AND PINNED PADS. THE ROAD CONTRACTOR SHALL INSTALL ANY ADDITIONAL CONDUIT NEEDED WHERE DOWN. AFTER SEPTEMBER 15, THE SAME APPLIES TO ALL SLOPES EXCEEDING 8%.

5. ALL AREAS TO BE SEEDED SHALL BE MULCHED. MULCH SHALL BE LONG FIBERED HAY OR STRAW AND SPREAD UNIFORMLY. 1.5 TO 2.0 TONS PER ACRE. TO BE MAINTAINED MOIST TO MINIMIZE BLOWING AS NECESSARY. IN WINTER CONDITIONS, NO MULCH IS TO BE APPLIED OVER SNOW. THE SNOW MUST FIRST BE REMOVED AND THEN MULCH APPLIED ACCORDING TO SPECIFICATIONS STATED PRIOR. IN ALL CASES MULCH SHALL BE APPLIED SUCH THAT THE SOIL SURFACE IS NOT VISIBLE THROUGH THE MULCH. DURING NOVEMBER 1 THROUGH APRIL 1 BEFORE CONSTRUCTION.

MULCHING SHALL BE COMPLETED DAILY BY THE END OF THE WORK DAY. 6. PLACE SILT SACKS IN CATCH BASIN INLET DURING CONSTRUCTION. CONTACT AH HARRIS IN PORTLAND (207) 775-5764 OR AUGUSTA (207) 622-0821 SILT SACKS SHALL BE REMOVED

AFTER FINAL PAVEMENT OVERLAY. POWER COMPANY 7. ALL SEDIMENT CONTROL FENCING AND SILT SACKS BARRIERS WILL REMAIN IN PLACE UNTIL

8. ALL EARTH CHANGES WILL BE CONSTRUCTED AND COMPLETED IN SUCH A MANNER SO THAT THE EXPOSED AREA OF ANY DISTURBED LAND WILL BE LIMITED TO THE SHORTEST PERIOD OF TIME POSSIBLE. THE CONTRACTOR SHALL COMPLETE FINAL GRADING, SEEDING, AND MULCHING IN CONJUNCTION WITH THE COMPLETION OF THE CORRESPONDING BUILDINGS WHENEVER POSSIBLE. IF FINAL GRADING CANNOT BE COMPLETED THEN THE CONTRACTOR IS TO MULCH ANY DISTURBED LAND AND WORK ON TOP OF THE MULCH. AREAS OF DISTURBED SOIL WILL BE TEMPORARILY MULCHED OR SEEDED WITHIN 30 DAYS OF INITIAL

9. SEDIMENT CAUSED BY ACCELERATED SOIL EROSION WILL BE REMOVED FROM RUNOFF WATER BEFORE IT LEAVES THE DEVELOPMENT SITE.

10. ALL TEMPORARY OR PERMANENT FACILITY CONSTRUCTED FOR THE CONVEYANCE OF WATER AROUND, THROUGH, OR FROM THE DEVELOPMENT SITE WILL BE CONSTRUCTED TO LIMIT THE WATER FLOW TO A NON-EROSIVE VELOCITY.

11. PERMANENT SOIL EROSION CONTROL MEASURES FOR ALL SLOPES, CHANNELS, DITCHES, OR ANY DISTURBED LAND AREA WILL BE COMPLETED WITHIN 15 DAYS AFTER FINAL GRADING HAS BEEN COMPLETED.

12. IN THE EVENT THAT TEMPORARY OR PERMANENT SEEDLINGS HAVE NOT BEEN ESTABLISHED (90% SURFACE COVERAGE) BY SEPTEMBER 15. TEMPORARY MULCHING SHALL BE APPLIED FOR PROTECTION OVER WINTER (PAST THE GROWING SEASON) IN ACCORDANCE WITH THE TEMPORARY MULCHING BMP OF THE MAINE EROSION AND SEDIMENT CONTROL

HANDBOOK. A. MULCHING FOR OVER WINTER PROTECTION WILL BE COMPLETED BY NOVEMBER 15 B. WINTER MULCH ON SLOPES 8% OR GREATER WILL BE ANCHORED WITH NETTING. C. ALL SOILS DISTURBED PRIOR TO NOVEMBER 1 AND NOT HAVING THE REQUIRED COVER OF VEGETATION WILL BE STABILIZED WITH ANCHORED MULCH BY NOVEMBER 15.

13. PROVIDE TWO TEMPORARY CMP RISERS AT EXISTING CATCH BASIN AND WRAP WITH EROSION CONTROL FABRIC TO CONTROL POTENTIAL SEDIMENTATION. INSTALL STONE BERM OR HAY BALES AROUND CATCH DURING CONSTRUCTION..

14. NO EARTH MOVING OR CONSTRUCTION OPERATIONS ARE ANTICIPATED ON THE EXISTING STEEP SLOPE EXCEPT FOR RIP-RAP SLOPE PROTECTION. ALL DISTURBED AREAS SHALL BE SEEDED AND MULCHED IN ACCORDANCE WITH OTHER EROSION CONTROL NOTES.

15. DURING WINTER CONSTRUCTION THE CONTRACTOR SHALL INSTALL AN EROSION CONTROL FILTER BERM. THE CONTRACTOR SHALL INSTALL THE BERMS AS SEDIMENT BARRIERS DURING FROZEN GROUND CONDITIONS.

1. VERTICAL DATUM IS NATIONAL GEODETIC DATUM 1929 DEFINITION. BENCHMARK LOCATIONS ARE SPECIFIED ON TITCOMB SURVEY.

2. CLEARING LIMITS WILL BE FLAGGED BY THE ENGINEER AND THE OWNER. THE CONTRACTOR 6. THE CABLE COMPANY WILL SUPPLY THE SERVICE WIRES. SHALL NOT CUT BEYOND THE LIMITS OR REMOVE A TREE DESIGNATED TO BE SAVED WITHOUT THE OWNER'S AND ENGINEER'S CONSENT.

3. ALL CURBS AND WALKS SHALL BE STAKED OUT BY THE CONTRACTOR AND APPROVED BY THE OWNER'S REPRESENTATIVE PRIOR TO INSTALLATION. SIDEWALKS TO BE 4' WIDE FROM DRIVEWAY TO THE FRONT DOOR AND SET BACK 4' FROM THE HOUSE

APPROPRIATE TO MEET SITE CONDITIONS

TRAIL SYSTEM NOTES:

1. A TRAIL SYSTEM SHALL BE INSTALLED THROUGH OCEANVIEW AT CUMBERLAND PROPERTY TO PROVIDE PEDESTRIAN ACCESS. THE TRAIL SYSTEM WILL FORM LINKS TO ABUTTING PARCELS AND CONNECTION TO TOWN TRAIL SYSTEMS. THE TRAIL SYSTEM WILL BE AVAILABLE FOR PUBLIC & PRIVATE USE. THE DETAILED DESIGN WILL BE COORDINATED WITH THE TOWN PLANNER, PLANNING BOARD, AND THE OWNER.

1. ALL CONSTRUCTION TO BE IN COMPLIANCE WITH VERIZON CONSTRUCTION STANDARDS.

2. ALL TRENCHING, CONDUIT AND BACK FILLING IS THE CONTRACTOR'S RESPONSIBILITY.

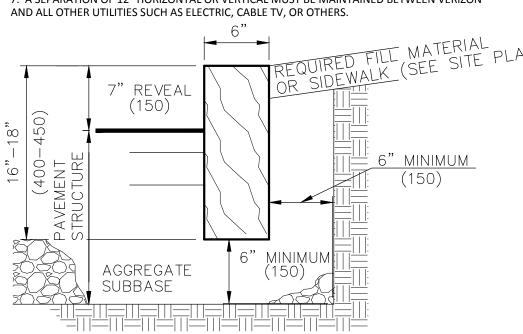
3. ALL CABLES SHALL BE IN CONDUIT UNDER ALL PAVED ROADS, DRIVEWAYS AND WALKWAYS. 4" FOR THE MAIN CABLE AND 2" FOR SERVICE WIRES.

4. CONDUITS FOR SERVICE WIRES SHOULD BE INSTALLED AT ALL LOCATIONS WHERE REQUIRED DURING THE INITIAL INSTALLATION OF THE MAIN CABLE. 5. THE TRENCH MUST BE FILLED WITH "SUITABLE" BACK FILL, I.E., SAND BACK FILL WITH NO

STONE LARGER THAN 1/4" IN DIAMETER

6. VERIZON WILL SUPPLY THE CABLE AND LABOR TO INSTALL SAME.

7. A SEPARATION OF 12" HORIZONTAL OR VERTICAL MUST BE MAINTAINED BETWEEN VERIZON



NOT TO SCALE AT ALL ROAD ENTRANCE RADII AT INTERSECTIONS

UTILITIES GENERAL NOTES

OF CUMBERLAND STANDARD SPECIFICATIONS. 2. THE LOCATION OF EXISTING UNDERGROUND UTILITIES IS NOT GUARANTEED. THE 2. MINIMUM DIAMETER FOR MAINLINE SEWER IS EIGHT INCH (8") WITH A MINIMUM SLOPE CONTRACTOR SHALL VERIFY THE LOCATION OF UNDERGROUND UTILITIES AND STRUCTURES WITH THE REQUIREMENTS OF UTILITY AN STRUCTURE OWNERS REGARDING NOTIFICATION OF WORK AND PROTECTION OF EXISTING FACILITIES. 3. SANITARY SEWER SERVICE STUBS TO BE SIX INCH (6") DIAMETER MINIMUM AND TO BE

SEWER CONSTRUCTION NOTES:

COPIES OF UTILITY PLAN.

1. SEWER LINE CONSTRUCTION SHALL BE CONSTRUCTED IN ACCORDANCE WITH THE TOWN

INSTALLED BEYOND THE EDGE OF PAVEMENT, AND UTILITY TRENCH AS SHOWN ON PLAN.

BITUMINOUS COATING. WITH SMOOTH CHANNELED INVERTS. AND PROPERLY SIZED AND

ORIENTED PRECAST PIPE OPENINGS WITH FLEXIBLE PIPE BOOTS. STEPS TO BE INSTALLED

PARALLEL TO INVERT CHANNEL. SERVICE CONNECTIONS TO BE INCORPORATED IN INVERT

6. MANHOLE FRAMES AND COVERS TO BE SUITABLE FOR HIGHWAY LOADING AND TO BE TO

7. DESIGN AND CONSTRUCTION OF PROJECT SANITARY SEWER UTILITY WILL BE CARRIED OU

TO SPECIFICALLY EXCLUDE THE INTRODUCTION OF NON-SANITARY GROUND AND / OR

8. ALL GRAVITY SEWER TO BE LOW PRESSURE AIR AND DEFLECTION TESTED AFTER BACK

9. PRIOR TO THE START OF CONSTRUCTION, DEVELOPER TO PROVIDE TO DISTRICT TWO (2)

10. MINIMUM HORIZONTAL CLEARANCES TO BE MAINTAINED BETWEEN UTILITIES, TO PERMIT

. TEST PITS SHALL BE EXCAVATED AT CROSSINGS OF UTILITIES TO DETERMINE LOCATION

2. MINIMUM DEPTH OF COVER FOR ALL WATER LINES SHALL BE 5.5' FROM FINISHED GRADE

3. PROPOSED PIPELINE, VALVE, AND HYDRANT LOCATIONS ARE APPROXIMATE. FINAL

LOCATION MAY BE ADJUSTED AS REQUIRED TO AVOID CONFLICTS WITH OTHER UTILITIES

4. ANY EXISTING PIPELINE, UTILITY OR STRUCTURE, INCLUDING EXISTING WATER MAINS,

5. ALL PROPERTY REMOVED, DAMAGED OR ALTERED IN THE COURSE OF THE WORK SHALL

BE REPLACED OR RESTORED TO EQUAL OR BETTER CONDITION TO THAT WHICH EXISTED

MATERIALS FOR THE PROJECT INCLUDING PIPE, COUPLINGS, VALVES, FITTINGS, HYDRANTS

PIPING, CURB BOXES, RETAINER GLANDS, AND ACCESSORIES SUCH AS GASKETS, BOLTS,

8. A SEPARATION OF 12" VERTICAL CLEARANCE MUST BE MAINTAINED BETWEEN THE

SERVICED BY A 1 1/2" LINE OFF THE MAIN, SPLIT AT THE UNIT TO PROVIDE A 1"CTS DOMESTIC SUPPLY AND A 1 1/2" SPRINKLER SUPPLY INSTALLED IN ACCORDANCE WITH THE

STANDARDS OF THE PORTLAND WATER DISTRICT. SIZES SHALL BE CONFIRMED BY THE

TESTED BY THE CONTRACTOR PRIOR TO ACCEPTANCE BY THE OWNER, SERVICES SHALL BE

INSTALLED UNDER LINE PRESSURE AFTER THE MAIN HAS BEEN SUCCESSFULLY PRESSURE

9. ALL WATER MAIN SIZES ARE AS INDICATED ON THE PLAN/PROFILES. EACH UNIT SHALL BE

GRAVEL, SAND, AND BORROW SHALL BE FURNISHED BY THE CONTRACTOR.

NUTS, AND GLANDS AS REQUIRED TO MAKE THE PIPING SYSTEMS COMPLETE SHALL MEET

PWD SPECIFICATIONS. ALL CONCRETE AND EARTH MATERIALS INCLUDING CRUSHED STONE

DAMAGED BY CONTRACTOR'S OPERATIONS SHALL BE IMMEDIATELY REPAIRED BY

AND STRUCTURES. NO ADDITIONAL PAYMENT WILL BE MADE FOR EXCAVATION AND BACK

AND DEPTH SUFFICIENTLY IN ADVANCE OF WATER MAIN CONSTRUCTION TO PERMIT

FILLING AND COMPACTION AND PRIOR TO CONNECTION OF BUILDING SEWER.

FUTURE MAINTENANCE OPERATIONS WITHOUT DISTURBING ADJACENT UTILITIES,

ADJUSTMENT OF WATER MAIN LOCATION BY DEFLECTION OF THE PIPE.

FILL BEYOND THE TRENCH LIMITS SHOWN.

BEFORE THE WORK COMMENCED.

WITH GRIP-RING RETAINER GLANDS.

WATER MAIN AND ALL OTHER UTILITIES.

SPRINKLER INSTALLER PRIOR TO CONSTRUCTION.

CONTRACTOR AT NO ADDITIONAL COST TO OWNER.

3. CONTRACTOR SHALL VERIFY ALL CRITICAL DIMENSIONS AND GRADES TO HIS SATISFACTION 4. SANITARY SEWER SERVICE STUBS TO BE CONNECTED TO THE MAIN LINE BY USE OF 8X8X6 BEFORE WORK BEGINS. ANY DISCREPANCIES SHALL BE REPORTED IMMEDIATELY TO THE OWNER'S REPRESENTATIVE. WYES. TEE STUBS WILL NOT BE ALLOWED.

4. ALL UTILITIES ARE TO BE CONSTRUCTED TO THE STANDARDS SET BY THE RESPECTIVE UTILITY. 5. SANITARY SEWER MANHOLES TO BE PER ASTM SPECIFICATIONS, WITH TWO (2) COATS OF

'. THE ROAD CONTRACTOR SHALL BE RESPONSIBLE FOR INSTALLING ELECTRIC, TELEPHONE, & CABLE UP TO AND INCLUDING THE INSTALLATION OF JUNCTION BOXES AND TRANSFORMER INDIVIDUAL UNIT SERVICES CROSS THE ROADWAY. THE SITE CONTRACTOR SHALL BE RESPONSIBLE TO EXTEND INDIVIDUAL SERVICE FROM THE TRANSFORMER PAD TO THE BUILDING. SURFACE WATER INTO THE SANITARY SEWER SYSTEM. THE SITE CONTRACTOR IS REQUIRED TO INSTALL CONDUIT AT ALL PAVEMENT CROSSINGS OTHER

8. THE ROADWAY CONTRACTOR SHALL SET UP A SCOPING MEETING WITH THE SITE CONTRACTOR TO CONFIRM LIMITS OF WORK, SCHEDULING, AND CONSTRUCTION SEQUENCE

THAN THE ROADWAY

1. THE PROPOSED DISTRIBUTION SYSTEM PLAN SHALL BE COORDINATED WITH CENTRAL MAINE WATER CONSTRUCTION NOTES:

2. ALL CONSTRUCTION SHALL BE IN ACCORDANCE WITH CMP'S CONSTRUCTION STANDARDS AND THE LATEST REVISION OF THE NATIONAL ELECTRICAL SAFTEY CODE.

3. ALL TRENCHING, CONDUIT AND BACK FILLING IS THE CONTRACTOR'S RESPONSIBILITY.

4. CONDUITS SHALL BE A MINIMUM OF SCHEDULE 40 PVC OR EQUIVALENT.

5. ALL CABLES SHALL BE IN CONDUIT UNDER ALL PAVED AREAS, ROADWAYS, AND DRIVEWAYS PRIMARY CABLES ARE TO BE INSTALLED IN CONDUIT IF DRIVEWAYS ARE NOT ROUGH GRADED. 6. CONDUITS FOR SECONDARY CABLES SHOULD BE INSTALLED AT ALL LOCATIONS WHERE

REQUIRED DURING THE INITIAL INSTALLATION OF THE PRIMARY CABLE. PRIMARY CABLE TO BE #2 AL 15 KV.

8. SEE CMP'S CONTRACTOR HANDBOOK, SECTION IX, PARAGRAPHS 910, 911, AND 912 FOR SPECIFICATIONS ON BACK-FILL MATERIALS AND DEPTHS, ETC.

9. ALL TRANSFORMER PADS MUST BE SUPPLIED AND INSTALLED BY THE CONTRACTOR. PAD DESIGNS MUST CONFORM TO CMP SPECIFICATIONS. SEE ILLUSTRATIONS NO. 19, NO. 20, NO. 21

6. ALL FITTINGS, VALVES, AND HYDRANTS SHALL HAVE MECHANICAL JOINTS RESTRAINED IN SECTION XII OF THE CONTRACTOR'S HANDBOOK.

10. ALL JUNCTION BOXES WILL BE PURCHASED AND INSTALLED BY THE CONTRACTOR. CMP WILL 7. CONSTRUCTION SHALL FOLLOW PORTLAND WATER DISTRICT STANDARDS. ALL PROVIDE THE JUNCTION BOX, HOWEVER, THE EXCESS COST WILL BE BILLED TO THE OWNER. FIBERGLASS OR CONCRETE PADS REQUIRED FOR STELL CABINETS AND JUNCTION BOXES. TAPPING SLEEVES AND VALVES, VALVE BOXES, CORPORATION STOPS, CURB STOPS, SERVICE

11. CMP WILL SUPPLY THE CABLE, TRANSFORMERS AND LABOR TO INSTALL SAME.

12. ALL METERING ENCLOSURES WILL BE PUNCHED AND INSTALLED BY THE CONTRACTOR.

13. A SEPARATION OF 12" MUST BE MAINTAINED BETWEEN CMP AND ALL OTHER UTILITIES AND/OR TELEPHONE, CABLE ETC.

1. ALL TRENCHING, CONDUIT & BACK FILLING IS THE CONTRACTORS RESPONSIBILITY.

2. CONDUITS SHALL BE SCHEDULE 40 PVC AND WILL BE ROPED WITH 1/4" ROPE.

3. ALL CABLES SHALL BE IN CONDUIT UNDER ALL PAVED ROADS, DRIVEWAYS AND WALKWAYS AS 10. THE COMPLETE PIPING SYSTEM SHALL BE FLUSHED, CHLORINATED, AND PRESSURE NOTED OR SHOWN ON THE PLAN; 4" FOR THE MAIN CABLE AND 2" FOR THE SERVICE WIRES. 4. CONDUITS FOR SERVICE WIRES SHOULD BE INSTALLED AT ALL LOCATIONS WHERE REQUIRED TESTED. DURING THE INSTALLATION OF THE MAIN CABLE.

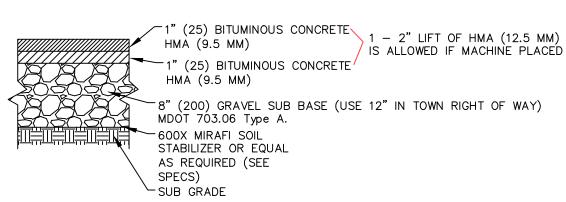
5. THE CABLE COMPANY WILL SUPPLY THE MAIN CABLE AND PEDESTALS AND THE LABOR TO

7. ELECTRICAL CONTRACTOR SHALL COORDINATE WITH THE CABLE COMPANY FOR INTERNAL

8. ALL SERVICE WIRE INSTALLATIONS AND INTERIOR WIRING SHALL CONFORM TO THE CABLE COMPANY SPECIFICATIONS.

4. DRIVEWAYS TO BE 24' WIDE AT THE GARAGE DOOR AND MAY TRANSITION TO 20' WIDTH AS 9. A SEPARATION OF 12" HORIZONTAL OR VERTICAL MUST BE MAINTAINED BETWEEN THE CABLE COMPANY AND ALL OTHER UTILITIES SUCH AS ELECTRIC, TELEPHONE OR OTHERS.

> 10. CONTRACTOR SHALL EXPOSE GROUND ROD AT ALL PAD LOCATIONS TO INSURE PROPER GROUNDING FOR THE CABLE COMPANY.



6.	7-31-2018	No changes this sheet, re-submit to Town	CSB
5.	7-16-2018	No Changes this sheet	CSB
4.	5-4-2018	No changes this sheet	CSB
3.	3-1-2018	Respond to Town Memos, Re-submit to Town	CSB
2.	2-7-2018	SUBMIT TO DEP	CSB
1.	1-31-2018	Re-Submit to Town and Maine DEP	CSB

Roadway Sections and Details

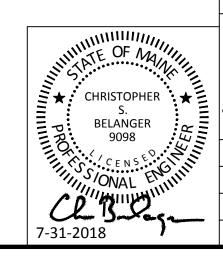
Oceanview at Cumberland 291 Tuttle Road, Cumberland, Maine

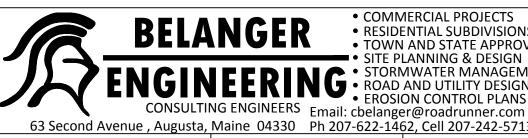
Seacoast Management Company 20 Blueberry Lane, Falmouth, Maine

COMMERCIAL PROJECTS

RESIDENTIAL SUBDIVISIONS

TORMWATER MANAGEMEI





63 Second Avenue, Augusta, Maine 04330 Ph 207-622-1462, Cell 207-242-5713 SHEET: FIELD WK: SCALE: DRN BY: JOB #: 109 CH'D BY: SS: FILE: DATE: 7-31-2018

STRUCTURE TABLE								
STRUCTURE NAME:	RIM ELEVATION	INV. IN:	INV. OUT	STA / OFFSET				
C2	RIM = 87.57		INV OUT =87.00	Sta 38+36.10, Offset 274.81, R				
CB2	RIM = 89.36	INV IN =84.80 INV IN =84.56	INV OUT =84.55	Sta 12+51.28, Offset -9.94, L				
CB2A	RIM = 89.36		INV OUT =84.76	Sta 12+50.68, Offset 9.57, R				
CB3	RIM = 94.58	INV IN =82.93 INV IN =89.09	INV OUT =82.80	Sta 15+59.44, Offset 44.49, R				
CB3A	RIM = 94.58	INV IN =83.09	INV OUT =82.50	Sta 15+73.95, Offset 10.00, R				
CB4	RIM = 99.40		INV OUT =95.80	Sta 43+18.20, Offset 28.98, R				
CB5	RIM = 93.50		INV OUT =89.50	Sta 15+33.30, Offset -17.98, L				
CB13	RIM = 101.90	INV IN =96.36	INV OUT =93.00	Sta 24+02.07, Offset 10.00, R				
CB13A	RIM = 101.90	INV IN =96.85	INV OUT =96.56	Sta 24+02.31, Offset -10.00, L				
CB14	RIM = 94.19	INV IN =89.60	INV OUT =89.50	Sta 20+91.54, Offset 10.14, R				
CB14A	RIM = 94.19		INV OUT =89.81	Sta 20+91.95, Offset -10.00, L				
CB16	RIM = 99.17	INV IN =92.69	INV OUT =91.30	Sta 43+87.04, Offset 37.16, R				
CB17	RIM = 98.32	INV IN =90.24 INV IN =92.62 INV IN =91.47	INV OUT =90.14	Sta 44+34.93, Offset 10.13, R				
CB17A	RIM = 98.33	INV IN =90.52	INV OUT =92.82	Sta 44+41.65, Offset 29.06, R				
CB18	RIM = 100.70	INV IN =89.54 INV IN =95.15	INV OUT =89.44	Sta 42+67.13, Offset -10.11, L				
CB18A	RIM = 99.90	INV IN =91.96	INV OUT =91.80	Sta 44+50.00, Offset 40.60, R				
CB18B	RIM = 99.90		INV OUT =93.00	Sta 22+68.58, Offset 219.16, R				
CB20	RIM = 100.41	INV IN =88.65 INV IN =93.07	INV OUT =88.50	Sta 0+00.60, Offset -0.11, L				
CB21	RIM = 100.40	INV IN =93.31	INV OUT =93.21	Sta 46+79.11, Offset -41.43, L				
CB22	RIM = 102.55	INV IN =97.80	INV OUT =97.34	Sta 28+99.93, Offset -9.87, L				
CB23	RIM = 102.55		INV OUT =98.00	Sta 28+99.71, Offset 9.96, R				
CB24	RIM = 99.74	INV IN =93.00 INV IN =93.00	INV OUT =92.87	Sta 31+75.71, Offset 9.43, R				
CB24A	RIM = 99.84	INV IN =93.20 INV IN =93.20	INV OUT =93.10	Sta 31+75.58, Offset -9.82, L				
CB25	RIM = 99.04	INV IN =92.60 INV IN =92.60	INV OUT =92.50	Sta 31+90.51, Offset 15.48, R				
CB26	RIM = 98.07	INV IN =93.59	INV OUT =93.04	Sta 33+15.17, Offset 10.00, R				
CB27	RIM = 98.06	INV IN =92.21	INV OUT =93.79	Sta 33+53.53, Offset -10.18, L				
CB28	RIM = 100.04	INV IN =91.95 INV IN =92.09	INV OUT =91.85	Sta 51+24.60, Offset -9.12, L				
CB30	RIM = 96.97	INV IN =90.26 INV IN =92.00	INV OUT =90.16	Sta 31+66.96, Offset 396.00, R				
CB30A	RIM = 96.97		INV OUT =92.35	Sta 31+56.84, Offset 397.97, R				
CB31	RIM = 94.95	INV IN =89.67 INV IN =89.67	INV OUT =89.57	Sta 55+05.31, Offset -9.64, L				
CB32	RIM = 93.92	INV IN =89.11 INV IN =89.14	INV OUT =89.00	Sta 56+05.12, Offset -9.95, L				
CB32A	RIM = 93.92		INV OUT =89.34	Sta 38+31.41, Offset 399.48, R				
CB33	RIM = 95.70	INV IN =88.25	INV OUT =88.15	Sta 57+62.97, Offset -9.57, L				
CB34	RIM = 92.25	INV IN =87.68 INV IN =87.66	INV OUT =87.58	Sta 37+77.85, Offset 157.72, R				
CB35	RIM = 94.04	INV IN =88.60 INV IN =88.60	INV OUT =88.46	Sta 38+90.42, Offset 23.37, R				
CB35A	RIM = 93.76		INV OUT =89.65	Sta 39+32.52, Offset 9.99, R				
CB36	RIM = 95.28		INV OUT =90.38	Sta 38+28.26, Offset -9.62, L				
CB40	RIM = 99.90	INV IN =93.92	INV OUT =93.82	Sta 30+26.99, Offset 35.97, R				
CB41	RIM = 101.67	INV IN =94.37	INV OUT =94.27	Sta 30+46.50, Offset -31.32, L				
CB42	RIM = 100.14	INV IN =95.04	INV OUT =94.94	Sta 19+74.10, Offset 344.74, R				
CB43	RIM = 100.15		INV OUT =95.24	Sta 31+56.47, Offset 7.82, R				
CB44	RIM = 95.91	INIV INI -02 17	INV OUT =93.37	Sta ???, Offset ???, ???				
CB45 CB46	RIM = 95.78 RIM = 97.80	INV IN =93.17	INV OUT =93.07 INV OUT =93.54	Sta 21+21.00, Offset 7.90, R Sta 34+47.33, Offset -22.99, L				
CB47	RIM = 97.80	INV IN =92.83	INV OUT =92.73	Sta 33+85.28, Offset -24.50, L				
CB48	RIM = 98.07	52.55	INV OUT =93.00	Sta 66+00.63, Offset 0.01, R				
CB49	RIM = 97.90		INV OUT =93.91	Sta 32+96.95, Offset -25.50, L				
CB50	RIM = 99.90	INV IN =93.46	INV OUT =93.36	Sta 32+04.01, Offset -25.78, L				
CB51	RIM = 97.90		INV OUT =93.54	Sta 31+69.18, Offset 38.89, R				
CB60	RIM = 94.93	INV IN =90.50	INV OUT =90.40	Sta 60+65.91, Offset -8.03, L				

				Pipe	Table	
NAME	SIZE	LENGTH	SLOPE	Inv. in	Inv. out	MATERIAL
BOX 1	96"	73.28'	0.68%	Inv. in=79.50	Inv. out=79.00	96 x 84 inch Concrete Box Culvert (clamshell) Set base 2' below stream bed stream elev 81.5 to 81.0
BOX 2	120"	73.61'	2.04%	Inv. in=88.00	Inv. out=86.50	120 x 108 inch Concrete Box Culvert set base 2' below stream bed stream elev 90.0 to 88.5
Culv1	15"	63.38'	0.63%	Inv. in=83.50	Inv. out=83.10	15 inch Corrugated HDPE Pipe
CULV3	18"	90.56'	0.55%	Inv. in=82.50	Inv. out=82.00	18 inch Corrugated HDPE Pipe
CULV4	12"	51.30'	1.95%	Inv. in=96.00	Inv. out=95.00	12" N-12 ADS
CULV5	12"	46.36'	3.66%	Inv. in=86.50	Inv. out=84.80	12 inch Corrugated HDPE Pipe
CULV5 (1)	12"	46.36'	3.66%	Inv. in=86.50	Inv. out=84.80	12 inch Corrugated HDPE Pipe
CULV5 (2)	12"	46.36'	3.66%	Inv. in=86.50	Inv. out=84.80	12 inch Corrugated HDPE Pipe
01	6"	3.04'	0.99%	Inv. in=74.78	Inv. out=74.75	6" ORIFICE CORED INTO STRUCTURE
02	6"	2.73'	0.00%	Inv. in=89.50	Inv. out=89.50	Cut 6"X6" Notch into top Outlet Control Structure
SD FP1	6"	15.08'	1.00%	Inv. in=83.50	Inv. out=83.35	6" Perforated Drain under Focal Point
SD FP2	4"	13.15'	0.98%	Inv. in=82.00	Inv. out=81.87	12 inch Corrugated HDPE Pipe
SD OCS1	18"	58.06'	6.89%	Inv. in=74.00	Inv. out=70.00	18 inch Corrugated HDPE Pipe
SD OCS2	24"	31.08'	1.61%	Inv. in=86.50	Inv. out=86.00	24" N-12 ADS HDPE Pipe
SD OCS3	18"	12.94'	1.00%	Inv. in=81.50	Inv. out=81.37	18" N12 ADS
SD RTANK INLET	15"	11.44'	0.87%	Inv. in=85.00	Inv. out=84.90	15" N-12 ADS
SD RTANK OUTLET	15"	4.56'	0.69%	Inv. in=82.50	Inv. out=82.47	6" N-12 ADS
SD Treatment	6"	4.64'	1.00%	Inv. in=83.50	Inv. out=83.45	6" overflow
SD2	18"	322.01'	0.50%	Inv. in=84.55	Inv. out=82.93	18 inch Corrugated HDPE Pipe
SD2A	18"	19.52'	1.03%	Inv. in=84.76	Inv. out=84.56	18 inch Corrugated HDPE Pipe
SD3	18"	20.07'	0.50%	Inv. in=82.80	Inv. out=82.70	
SD3A	18"	166.37'	0.63%	Inv. in=82.50	Inv. out=81.45	18 inch Corrugated HDPE Pipe
SD4	12"	64.31'	1.00%	Inv. in=95.80	Inv. out=95.15	
SD5	15"	40.68'	1.00%	Inv. in=89.50	Inv. out=89.09	
SD13	18"	121.11'	0.25%	Inv. in=93.00	Inv. out=92.69	18 inch Corrugated HDPE Pipe
SD13A	15"	20.00'	1.00%	Inv. in=96.56	Inv. out=96.36	
SD14	15"	114.39'	1.01%	Inv. in=89.50	Inv. out=88.35	15 inch Corrugated HDPE Pipe
SD14A	15"	20.14'	1.04%	Inv. in=89.81	Inv. out=89.60	15" N-12 ADS
SD15	15"	15.43'	1.00%	Inv. in=88.20	Inv. out=88.05	15 inch Corrugated HDPE Pipe
SD16	18"	54.99'	1.93%	Inv. in=91.30	Inv. out=90.24	18 inch Corrugated HDPE Pipe
SD17	18"	97.00'	0.61%	Inv. in=90.14	Inv. out=89.54	18 inch Corrugated HDPE Pipe
SD17A	15"	20.09'	0.98%	Inv. in=92.82	Inv. out=92.62	
SD18	18"	83.89'	0.95%	Inv. in=89.44	Inv. out=88.65	18 inch Corrugated HDPE Pipe
SD18A	15"	14.24'	8.96%	Inv. in=91.80	Inv. out=90.52	15 inch Corrugated HDPE Pipe
SD18B	15"	94.43'	1.10%	Inv. in=93.00	Inv. out=91.96	15 inch Corrugated HDPE Pipe
SD20	18"	99.00'	5.56%	Inv. in=88.50	Inv. out=83.00	18 inch Corrugated HDPE Pipe
SD21	18"	27.90'	0.50%	Inv. in=93.21	Inv. out=93.07	18 inch Corrugated HDPE Pipe
SD22	18"	237.72'	1.74%	Inv. in=97.34	Inv. out=93.20	18 inch Corrugated HDPE Pipe
SD23	18"	19.83'	1.00%	Inv. in=98.00	Inv. out=97.80	18 inch Corrugated HDPE Pipe
SD24	18"	54.62'	0.50%	Inv. in=92.87	Inv. out=92.60	18 inch Corrugated HDPE Pipe
SD24A	18"	19.24'	0.50%	Inv. in=93.10	Inv. out=93.00	
SD25	18"	109.74'	0.50%	Inv. in=92.50	Inv. out=91.95	18 inch Corrugated HDPE Pipe
SD26	18"	125.13'	0.35%	Inv. in=93.04	Inv. out=92.60	18 inch Corrugated HDPE Pipe
SD27	15"	20.18'	1.00%	Inv. in=93.79	Inv. out=93.59	15" N-12 ADS
SD28	18"	70.01'	0.50%	Inv. in=91.85	Inv. out=91.50	18 inch Corrugated HDPE Pipe
SD28 (1)	18"	109.90'	0.50%	Inv. in=91.38	Inv. out=90.83	18 inch Corrugated HDPE Pipe
SD29	18"	94.09'	0.50%	Inv. in=90.73	Inv. out=90.26	18 inch Corrugated HDPE Pipe
SD30	18"	97.03'	0.50%	Inv. in=90.16	Inv. out=89.67	18 inch Corrugated HDPE Pipe
SD30A	15"	20.25'	1.73%	Inv. in=92.35	Inv. out=92.00	
SD31	18"	91.58'	0.50%	Inv. in=89.57	Inv. out=89.11	18 inch Corrugated HDPE Pipe
SD32	18"	149.07'	0.50%	Inv. in=89.00	Inv. out=88.25	18 inch Corrugated HDPE Pipe
SD32A	18"	20.01'	1.00%	Inv. in=89.34	Inv. out=89.14	18 inch Corrugated HDPE Pipe
SD33	18"	158.21'	0.30%	Inv. in=88.15	Inv. out=87.68	18 inch Corrugated HDPE Pipe
SD34	18"	14.96'	0.50%	Inv. in=87.58	Inv. out=87.51	18 inch Corrugated HDPE Pipe
SD35	18"	164.82'	0.49%	Inv. in=88.46	Inv. out=87.66	18 inch Corrugated HDPE Pipe
SD35A	15"	46.37'	2.27%	Inv. in=89.65	Inv. out=88.60	·
	18"	41.24'	4.31%	Inv. in=90.38	Inv. out=88.60	18 inch Corrugated HDPE Pipe
SD36				-		
SD36 SD40	15"	102.52'	0.50%	Inv. in=93.82	Inv. out=93.31	15" N-12 ADS
	15" 15"	102.52' 70.34'	0.50%	Inv. in=93.82 Inv. in=94.27	Inv. out=93.31 Inv. out=93.92	15" N-12 ADS

	S	TRUCTURE T	ABLE	
STRUCTURE NAME:	RIM ELEVATION	INV. IN:	INV. OUT	STA / OFFSET
CB61	RIM = 94.92		INV OUT =90.70	Sta 60+66.20, Offset 8.17, R
CB62	RIM = 100.42	INV IN =91.50 INV IN =96.30	INV OUT =91.38	Sta 32+12.04, Offset 193.70, R
CB66	RIM = 101.26		INV OUT =96.76	Sta 51+94.51, Offset 37.51, R
CB70	RIM = 103.50		INV OUT =99.40	Sta 27+38.17, Offset -95.62, L
CB71	RIM = 103.50	INV IN =98.98	INV OUT =98.88	Sta 26+57.70, Offset -97.73, L
CB72	RIM = 103.50	INV IN =98.49	INV OUT =98.39	Sta 25+62.78, Offset -101.76, I
CB73	RIM = 104.20	INV IN =97.93	INV OUT =97.83	Sta 25+82.15, Offset -10.00, L
CB74	RIM = 103.11	INV IN =97.32	INV OUT =97.22	Sta 24+92.84, Offset -10.00, L
DMH15	RIM = 96.27	INV IN =88.35 INV IN =90.50	INV OUT =88.20	Sta 19+74.10, Offset 14.21, R
DMHFP1	RIM = 88.57	INV IN =83.35 INV IN =84.90 INV IN =83.45		Sta 19+29.59, Offset 41.58, R
J1	RIM = 75.18	INV IN =74.64	INV OUT =74.64	Sta 47+54.66, Offset 219.28, R
OCS1	RIM = 79.02	INV IN =74.75 INV IN =74.50	INV OUT =74.00	Sta 2+52.46, Offset 11.88, R
OCS2	RIM = 90.50	INV IN =89.50 INV IN =86.50	INV OUT =86.50	Sta 38+22.42, Offset 304.39, R
OCS3	RIM = 89.00	INV IN =81.87 INV IN =82.47	INV OUT =81.50	Sta 19+21.51, Offset 50.83, R
SD29	RIM = 98.81	INV IN =90.83	INV OUT =90.73	Sta 31+63.17, Offset 302.18, F

	Pipe Table									
NAME SIZE LENGTH SLOPE Inv. in Inv. out MATERIAL										
SD43	12"	15.83'	1.27%	Inv. in=95.24	Inv. out=95.04	12" N-12 ADS				
SD44	12"	16.05'	1.23%	Inv. in=93.37	Inv. out=93.17					
SD45	12"	116.83'	1.37%	Inv. in=93.07	Inv. out=91.47	12" N-12 ADS				
SD46	15"	71.38'	1.00%	Inv. in=93.54	Inv. out=92.83	12" N-12 ADS				
SD47	15"	36.19'	1.42%	Inv. in=92.73	Inv. out=92.21	15" N-12 ADS				
SD48	12"	182.40'	0.50%	Inv. in=93.00	Inv. out=92.09	12 inch Corrugated HDPE Pipe				
SD49	15"	90.73'	0.50%	Inv. in=93.91	Inv. out=93.46	15 inch Corrugated HDPE Pipe				
SD50	15"	31.56'	0.50%	Inv. in=93.36	Inv. out=93.20	15 inch Corrugated HDPE Pipe				
SD51	15"	30.18'	1.79%	Inv. in=93.54	Inv. out=93.00	15 inch Corrugated HDPE Pipe				
SD60	12"	82.29'	0.89%	Inv. in=90.40	Inv. out=89.67					
SD61	12"	16.21'	1.24%	Inv. in=90.70	Inv. out=90.50					
SD66	15"	45.94'	1.00%	Inv. in=96.76	Inv. out=96.30					
SD70	12"	84.00'	0.50%	Inv. in=99.40	Inv. out=98.98	12" N-12 ADS				
SD71	12"	78.64'	0.50%	Inv. in=98.88	Inv. out=98.49	12" N-12 ADS				
SD72	12"	93.34'	0.49%	Inv. in=98.39	Inv. out=97.93	12" N-12 ADS				
SD73	12"	87.40'	0.58%	Inv. in=97.83	Inv. out=97.32	12" N-12 ADS				
SD74	12"	88.60'	0.42%	Inv. in=97.22	Inv. out=96.85	12" N-12 ADS				
UD ROAD	6"	4.62'	10.81%	Inv. in=91.00	Inv. out=90.50	6" UNDERDRAIN				
UD1	6"	12.96'	1.07%	Inv. in=74.64	Inv. out=74.50	6.0 inch PERF. PVC Pipe				

Little Acres Drive							
Number	Radius	Length	Line/Chord Direction				
L19		24.33	N35° 42' 05.55"E				
C17	150.00	38.55	N28° 20' 23.11"E				
L20		494.63	N20° 58' 40.67"E				
C18	300.00	38.64	N17° 17' 17.96"E				
L21		313.39	N13° 35' 55.24"E				
L22		48.62	N40° 49' 16.85"E				
C22	500.00	448.37	N15° 07' 54.05"E				
L23		88.59	N10° 33' 28.75"W				
C23	150.00	142.20	N16° 36' 00.12"E				
L24		303.30	N43° 45' 28.98"E				
C24	400.00	59.82	N39° 28' 24.96"E				
L25		137.03	N35° 11' 20.94"E				
C25	150.00	104.10	N55° 04' 11.47"E				
L26		87.70	N74° 57' 02.00"E				
C26	150.00	131.52	S79° 55' 48.53"E				
L27		27.92	S54° 48' 39.06"E				
C27	300.00	217.18	S75° 32' 59.23"E				

Mallard Way							
Number	Radius	Length	Line/Chord Direction	A Value			
L14		107.82	S54° 48' 39.06"E				
C13	150.00	37.97	S47° 33' 30.29"E				
L15		145.26	S40° 18' 21.52"E				
C14	150.00	37.97	S47° 33' 30.29"E				
L16		77.97	S54° 48' 39.06"E				
C15	150.00	235.62	N80° 11' 20.94"E				
L17		35.81	N35° 11' 20.94"E				
C16	200.00	112.67	N19° 03' 03.11"E				
L18		222.67	N2° 54' 45.29"E				

Periwinkle Drive								
Number	Radius	Length	Line/Chord Direction	A Value				
L30		37.50	S68° 23' 45.76"E					
C29	150.00	173.83	S35° 11' 49.84"E					
L31		130.86	S1° 59' 53.93"E					
C30	40.41	247.52	N2° 31' 31.13"E					

STRUCTURE TABLE								
STRUCTURE NAME:	RIM ELEVATION	INV. IN:	INV. OUT	STA / OFFSET				
SMH1	RIM = 85.63	INV IN =78.00		Sta 10+06.62, Offset -3.43, L				
SMH2	RIM = 86.32	INV IN =81.50	INV OUT =81.40	Sta 10+47.61, Offset -2.21, L				
SMH3	RIM = 94.92	INV IN =87.77	INV OUT =87.60	Sta 15+81.70, Offset -4.68, L				
SMH4	RIM = 97.77		INV OUT =90.60	Sta 17+68.97, Offset -6.05, L				
SMH6	RIM = 99.40	INV IN =95.10 INV IN =95.10	INV OUT =95.10	Sta 23+78.56, Offset -6.00, L				
SMH7	RIM = 101.94	INV IN =96.80 INV IN =96.80		Sta 44+00.72, Offset -7.45, L				
SMH8	RIM = 99.41	INV IN =94.40 INV IN =94.40	INV OUT =94.30	Sta 32+12.64, Offset -6.00, L				
SMH9	RIM = 94.78	INV IN =90.00 INV IN =90.00	INV OUT =90.00	Sta 38+60.04, Offset -6.00, L				

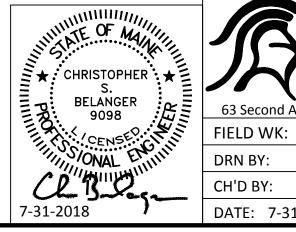
Pipe Table								
NAME	SIZE	LENGTH	SLOPE	Inv. in	Inv. out	MATERIAL		
SP2	8"	40.55'	8.37%	Inv. in=81.40	Inv. out=78.00	8" SDR35		
SP3	8"	533.45'	1.14%	Inv. in=87.60	Inv. out=81.50	8" SDR35		
SP4	8"	187.04'	1.51%	Inv. in=90.60	Inv. out=87.77	8" SDR35		
SP6A	3"	2.89'	-3298.38%	Inv. in=-0.12	Inv. out=95.10	4" FM		
SP6B	3"	3.19'	2987.12%	Inv. in=95.10	Inv. out=-0.12	4" HDPE FM		
SP6C	3"	2.99'	180.86%	Inv. in=100.50	Inv. out=95.10	3 inch HDPE Pipe		
SP7A	3"	3.58'	29.65%	Inv. in=97.86	Inv. out=96.80	3 inch HDPE Pipe		
SP7B	3"	3.27'	45.95%	Inv. in=98.30	Inv. out=96.80	3 inch HDPE Pipe		
SP8A	4"	5.53'	1.00%	Inv. in=94.30	Inv. out=94.24	4" FM		
SP8B	4"	3.00'	12.50%	Inv. in=94.77	Inv. out=94.40	4" HDPE Pipe		
SP8C	3"	3.15'	11.10%	Inv. in=94.75	Inv. out=94.40	2" HDPE FM		
SP9A	3"	3.76'	0.00%	Inv. in=90.00	Inv. out=90.00	3 inch HDPE Pipe		
SP9B	3"	3.46'	0.00%	Inv. in=90.00	Inv. out=90.00	3 inch HDPE Pipe		
SP9C	3"	3.57'	0.00%	Inv. in=90.00	Inv. out=90.00	3 inch HDPE Pipe		

6.	7-31-2018	No changes this sheet, re—submit to Town	CSB
5.	7-16-2018	Re-submit to PWD for final review	CSB
4.	5-4-2018	PWD revisions, re-submit to DEP	CSB
3.	3-1-2018	Respond to Town Comments, re—submit to Town	CSB
2.	2-7-2018	SUBMIT TO DEP	CSB
1.	1-31-2018	Respond to Town Memos, submit to Town and DEP	CSB

Structure and Pipe Tables

Oceanview at Cumberland 277Tuttle Road, Cumberland, Maine

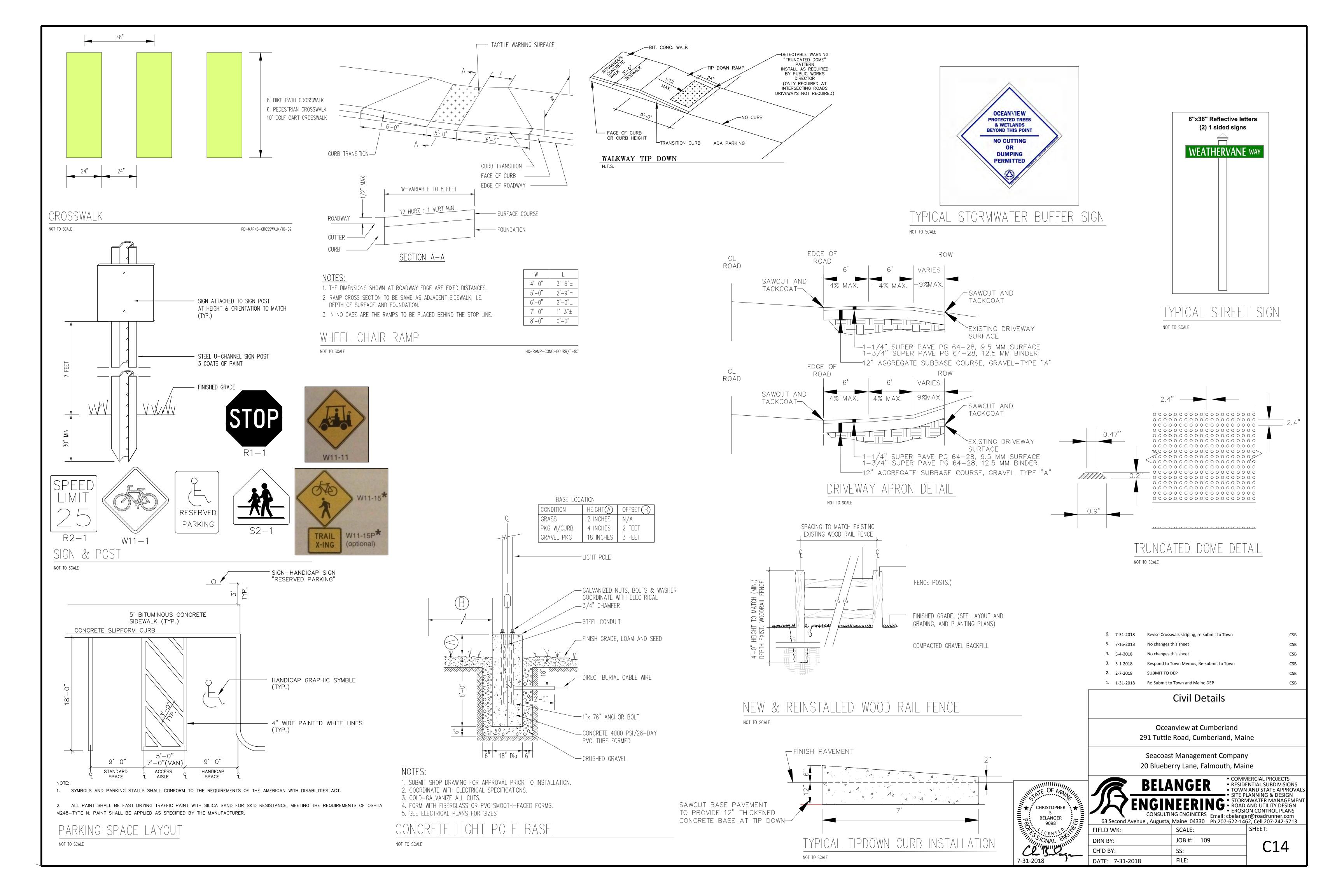
Seacoast Management Company 20 Blueberry Lane, Falmouth, Maine

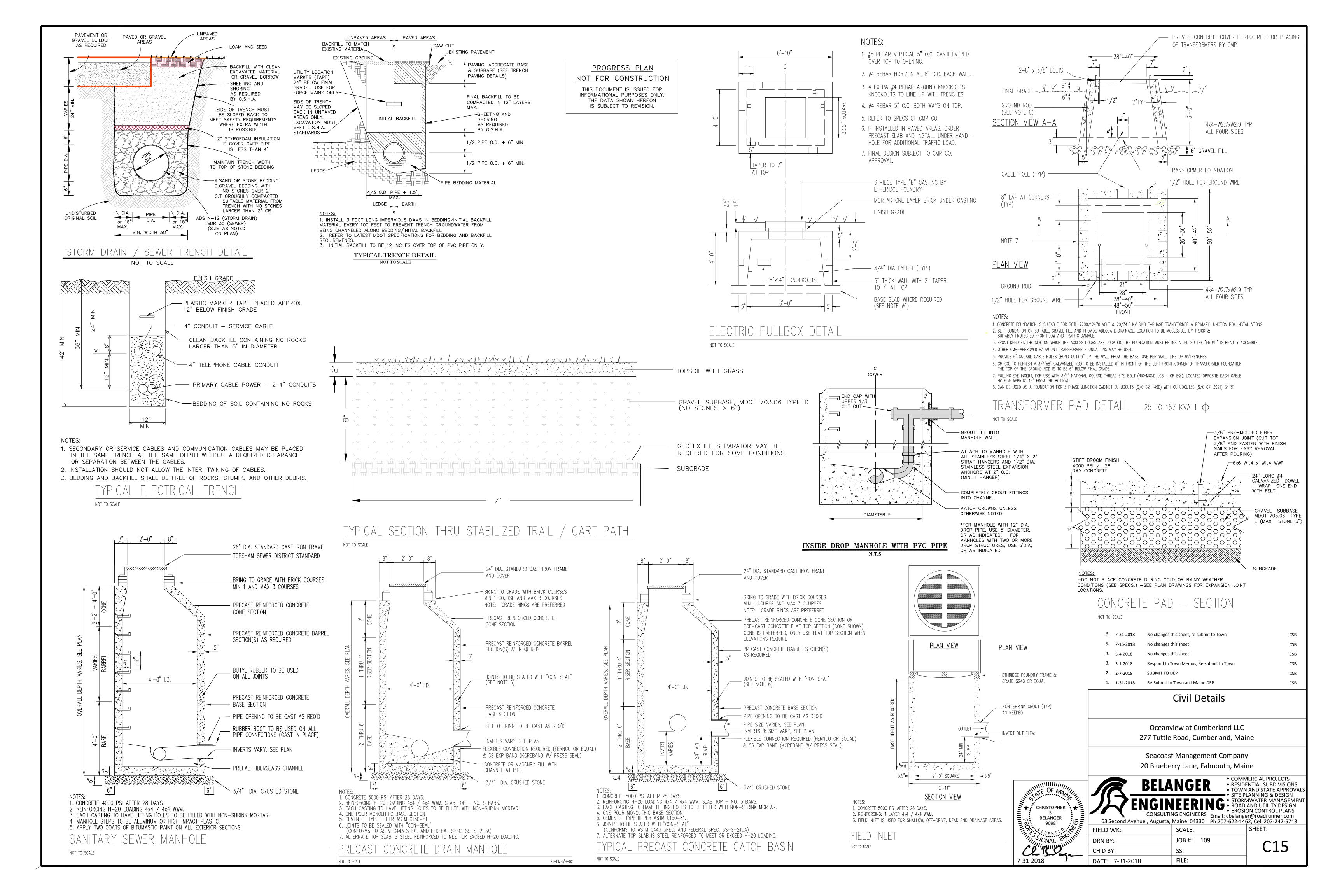


R	BELANGER	
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 COMMERCIAL PROJECTS
 RESIDENTIAL SUBDIVISIONS
 TOWN AND STATE APPROVALS
 SITE PLANNING & DESIGN
 STORMWATER MANAGEMENT
 ROAD AND UTILITY DESIGN
 EROSION CONTROL PLANS
 cbelanger@roadrunner.com
 207-622-1462, Cell 207-242-5713
 SHEET: SCALE:

JOB #: C13A CH'D BY: DATE: 7-31-2018 SS: FILE:





EROSION AND SEDIMENTATION NOTES:

1. The Site Contractor shall follow the "Maine Erosion and Sediment Control BMPs" published by the Maine DEP in 2003 and the "Maine Erosion and Sediment Control Practices Field Guide for Contractors published in 2016 or most current update". The manuals can be found on the Maine DEP web site. A Link to the field guide is shown

http://www.maine.gov/dep/land/erosion/escbmps/index.html

THE CONTRACTOR SHALL ALSO FOLLOW THE GUIDELINES LISTED IN

PROJECT. INSTALL THESE DEVICES AS INDICATED ON THE PLANS.

APPENDICES A, B, C IN MAINE DEP CHAPTER 500 RULES (2015 NOTES PROVIDED ON THIS SHEET).

GENERAL EROSION AND SEDIMENTATION CONTROL PRACTICES:

EROSION/SEDIMENT CONTROL DEVICES: THE FOLLOWING EROSION SEDIMENTATION CONTROL DEVICES ARE PROPOSED FOR CONSTRUCTION ON THIS

1 SILT FENCE: SILT FENCE WILL BE INSTALLED ALONG THE DOWN GRADING EDGES OF DISTURBED AREAS TO TRAP RUNOFF BORNE SEDIMENTS UNTIL THE SITE IS STABILIZED. IN AREAS WHERE STORMWATER DISCHARGES THE SILT FENCE WILL BE REINFORCED WITH HAY BALES TO HELP MAINTAIN THE INTEGRITY OF THE SILT FENCE AND TO PROVIDE ADDITIONAL TREATMENT.

2. HAY BALES: HAY BALES TO BE PLACED IN LOW FLOW DRAINAGE SWALES AND PATHS TO TRAP SEDIMENTS AND REDUCE RUNOFF VELOCITIES. DO NOT PLACE HAY BALES IN FLOWING WATER OR STREAMS.

3. RIPRAP: PROVIDE RIPRAP IN AREAS WHERE CULVERTS DISCHARGE OR AS SHOWN ON THE PLANS.

4. LOAM, SEED, & MULCH: ALL DISTURBED AREAS, WHICH ARE NOT OTHERWISE TREATED, SHALL RECEIVE PERMANENT SEEDING AND MULCH TO STABILIZE THE DISTURBED AREAS. THE DISTURBED AREAS WILL BE REVEGETATED WITHIN 5 DAYS OF FINAL GRADING. SEEDING REQUIREMENTS ARE PROVIDED AT THE END OF THIS SPECIFICATION.

5. STRAW AND HAY MULCH: USED TO COVER DENUDED AREAS UNTIL PERMANENT SEED OR EROSION CONTROL MEASURES ARE IN PLACE. MULCH BY ITSELF CAN BE USED ON SLOPES LESS THAN 15% IN SUMMER AND 8% IN WINTER. JUTE MESH IS TO BE USED OVER MULCH ONLY. CURLEX II AND EXCELSIOR MAY BE USED IN PLACE OF JUTE MESH OVER MULCH.

6. MULCH NETTING SHALL BE USED TO ANCHOR MULCH IN ALL DRAINAGE WAYS WITH A SLOPE GREATER THAN 3% FOR SLOPES EXPOSED TO DIRECT WINDS AND FOR ALL OTHER SLOPES GREATER THAN 8%.

TEMPORARY EROSION/SEDIMENTATION CONTROL MEASURES:

PROVIDE THE FOLLOWING TEMPORARY EROSION/SEDIMENTATION CONTROL MEASURES DURING CONSTRUCTION OF THE DEVELOPMENT:

1. SILTATION FENCE ALONG THE DOWNGRADIENT SIDE OF THE PARKING AREAS AND OF ALL FILL SECTIONS. THE SILTATION FENCE WILL REMAIN IN PLACE UNTIL THE SITE IS 90% REVEGETATED. REMOVE SILTATION FENCE, WITHIN 30 DAYS AFTER PERMANENT STABILIZATION IS ATTAINED. REMOVE ANY ACCUMULATED SEDIMENT AND STABILIZE.

2. HAY BALES PLACED AT KEY LOCATIONS TO SUPPLEMENT THE SILT FENCE.

D. SURROUND STOCKPILE SOIL WITH SILTATION FENCE AT BASE OF PILE.

3. PROTECT TEMPORARY STOCKPILES OF STUMPS, GRUBBINGS, OR COMMON EXCAVATION AS FOLLOWS: A. SOIL STOCKPILE SIDE SLOPES SHALL NOT EXCEED 2:1. B. AVOID PLACING TEMPORARY STOCKPILES IN AREAS WITH SLOPES OVER 10 PERCENT, OR NEAR DRAINAGE

SWALES. SEE ITEM 3 IN CONSTRUCTION PHASE NOTES BELOW. C. STABILIZE STOCKPILES WITHIN 15 DAYS BY TEMPORARILY SEEDING WITH A HYDROSEED METHOD CONTAINING AN EMULSIFIED MULCH TACKIFIER OR BY COVERING THE STOCKPILE WITH MULCH.

4. ALL DENUDED AREAS WHICH HAVE BEEN ROUGH GRADED AND ARE NOT LOCATED WITHIN THE BUILDING PAD, OR PARKING AND DRIVEWAY SUBBASE AREA THAT WILL NOT BE WORKED FOR MORE THAN 7 DAYS SHALL RECEIVE MULCH OR NON-ERODABLE COVER, STABILIZE AREAS WITHIN 75 FEET OF A WETLAND OR WATERBODY WITHIN 48 HOURS OF THE INITIAL DISTURBANCE OR THE SOIL OR PRIOR TO ANY STORM EVENT. WHICHEVER COMES FIRST. IN THE EVENT THE CONTRACTOR COMPLETES FINAL GRADING AND INSTALLATION OF LOAM AND SOD WITHIN THE TIME PERIODS PRESENTED ABOVE, INSTALLATION OF MULCH AND NETTING, WHERE

5. IF WORK IS CONDUCTED BETWEEN OCTOBER 15 AND APRIL 15, ALL DENUDED AREAS ARE TO BE COVERED WITH HAY MULCH, APPLIED AT TWICE THE NORMAL APPLICATION RATE, AND ANCHORED WITH FABRIC NETTING. THE PERIOD BETWEEN FINAL GRADING AND MULCHING SHALL BE REDUCED TO A 15 DAY MAXIMUM.

6. TEMPORARY EROSION CONTROL MEASURES SHALL BE REMOVED ONCE THE SITE HAS BEEN STABILIZED OR IN AREAS WHERE PERMANENT EROSION CONTROL MEASURES HAVE BEEN INSTALLED.

PERMANENT EROSION CONTROL MEASURES:

THE FOLLOWING PERMANENT CONTROL MEASURES ARE REQUIRED BY THIS EROSION/SEDIMENTATION

1. ALL AREAS DISTURBED DURING CONSTRUCTION, BUT NOT SUBJECT TO OTHER RESTORATION (PAVING, RIPRAP, ETC.), WILL BE LOAMED, LIMED, FERTILIZED AND SEEDED. NATIVE TOPSOIL SHALL BE STOCKPILED AND REUSED FOR FINAL RESTORATION WHEN IT IS OF SUFFICIENT QUALITY.

2. IF AN AREAS WILL NOT BE WORKED FOR MORE THAN ONE YEAR OR HAS BEEN BROUGHT TO FINAL GRADE, THEN PERMANENTLY STABILIZE THE AREA WITHIN 7 DAYS BY PLANTING VEGETATION, SEEDING, SOD, OR THROUGH THE USE OF PERMANENT MULCH, OR RIPRAP, OR ROAD SUB-BASE. IF USING VEGETATION FOR STABILIZATION. SELECT THE PROPER VEGETATION FOR THE LIGHT. SOIL. AND MOISTURE CONDITIONS: AMEND AREAS OF DISTURBED SUBSOILS WITH TOPSOIL, COMPOST, OR FERTILIZERS; PROTECT SEEDED AREAS WITH MULCH OR, IF NECESSARY, EROSION CONTROL BLANKETS; AND SCHEDULE SODDING, PLANTING, AND SEEDING TO AVOID DIE-OFF FROM SUMMER DROUGHT AND FALL FROSTS. NEWLY SEEDED OR SODDED AREAS MUST BE PROTECTED FROM VEHICLE TRAFFIC, EXCESSIVE PEDESTRIAN TRAFFIC, AND CONCENTRATED RUNOFF UNTIL THE VEGETATION IS WELL ESTABLISHED. IF NECESSARY, AREAS MUST BE SEEDED AND MULCHED AGAIN IF GERMINATION IS SPARCE, PLANT COVERAGE IS SPOTTY, OR TOPSOIL EROSION IS EVIDENT. ONE OR MORE OF THE FOLLOWING MAY APPLY TO A PARTICULAR SITE.

(a) Seeded areas. For seeded areas, permanent stabilization means a 90% cover of healthy plants with no evidence of washing or rilling of the topsoil.

(b) Sodded areas. For sodded areas, permanent stabilization means the complete binding of the sod roots into the underlying soil with no slumping of the sod or die-off.

(c) Permanent Mulch. For mulched areas, permanent mulching means total coverage of the exposed area with an approved mulch material. Erosion control mix may be used as mulch for permanent stabilization according to the approved application rates and limitations.

(d) Riprap. For areas stabilized with riprap, permanent stabilization means that slopes stabilized with riprap have an appropriate backing of a well-graded gravel or approved geotextile to prevent soil movement from behind the riprap. Stone must be sized appropriately. It is recommended that angular stone be

(e) Agricultural use. For construction projects on land used for agricultural purposes (e.g., pipelines across crop land), permanent stabilization may be accomplished by returning the disturbed land to agricultural

(f) Paved areas. For paved areas, permanent stabilization means the placement of the compacted gravel subbase is completed.

(g) Ditches, channels, and swales. For open channels, permanent stabilization means the channel is stabilized with a 90% cover of healthy vegetation, with a well-graded riprap lining, or with another non-erosive lining such as concrete or asphalt pavement. There must be no evidence of slumping of the channel lining, undercutting of the channel banks, or down-cutting of the channel.

3. SLOPES GREATER THAN 2:1 WILL RECEIVE RIPRAP.

POST-CONSTRUCTION REVEGETATION:

THE FOLLOWING GENERAL PRACTICES WILL BE USED TO PREVENT EROSION AS SOON AS AN AREA IS READY

1. A MINIMUM OF 4" OF LOAM WILL BE SPREAD OVER DISTURBED AREAS AND GRADED TO A UNIFORM DEPTH AND NATURAL APPEARANCE, OR STONE WILL BE PLACED ON SLOPES TO STABILIZE SURFACES.

2. IF FINAL GRADING IS REACHED DURING THE NORMAL GROWING SEASON (4/15 TO 9/15), PERMANENT SEEDING WILL BE DONE AS SPECIFIED BELOW. PRIOR TO SEEDING, LIMESTONE SHALL BE APPLIED AT A RATE OF 138 LBS/1000 SQ. FT. AND 10:20:20 FERTILIZER AT A RATE OF 18.4 LBS/1000 SQ. FT WILL BE APPLIED. BROADCAST SEEDING AT THE FOLLOWING RATES:

KENTUCKY BLUEGRASS 0.46 LBS/1000 SF.

RED TOP 0.05 LBS/1000 SF. CREEPING RED FESCUE 0.46 LBS/1000 SF. TALL FESCUE 0.46 LBS/1000 SF PERENNIAL RYE GRASS 0.11 LB/1000 SF.

3. AN AREA SHALL BE MULCHED IMMEDIATELY AFTER IS HAS BEEN SEEDED. MULCHING SHALL CONSIST OF HAY MULCH. HYDRO-MULCH. JUTE NET OVER MULCH. PRE-MANUFACTURED EROSION MATS OR ANY

SUITABLE SUBSTITUTE DEEMED ACCEPTABLE BY THE DESIGNER. A. HAY MULCH SHALL BE APPLIED AT THE RATE OF 2 TONS PER ACRE. HAY MULCH SHALL BE SECURED BY EITHER: (NOTE: SOIL SHALL NOT BE VISIBLE)

I. BEING DRIVEN OVER BY TRACKED CONSTRUCTION EQUIPMENT ON GRADES OF 5% AND LESS. II. BLANKETED BY TACKED PHOTODEGRADABLE/BIODEGRADABLE NETTING, OR WITH SPRAY, ON GRADES

III. SEE NOTE 6, GENERAL NOTES, AND NOTE 8, WINTER CONSTRUCTION.

B. HYDRO-MULCH SHALL CONSIST OF A MIXTURE OF EITHER ASPHALT, WOOD FIBER OR PAPER FIBER AND WATER SPRAYED OVER A SEEDED AREA. HYDRO-MULCH SHALL NOT BE USED BETWEEN 9/15 AND 4/15.

4. CONSTRUCTION SHALL BE PLANNED TO ELIMINATE THE NEED FOR SEEDING BETWEEN SEPTEMBER 15 AND APRIL 15. SHOULD SEEDING BE NECESSARY BETWEEN SEPTEMBER 15 AND APRIL 15 THE FOLLOWING PROCEDURE SHALL BE FOLLOWED. ALSO REFER TO NOTE 9 OF WINTER CONSTRUCTION.

A. ONLY UNFROZEN LOAM SHALL BE USED. B. LOAMING, SEEDING AND MULCHING WILL NOT BE DONE OVER SNOW OR ICE COVER. IF SNOW EXISTS, IT MUST BE REMOVED PRIOR TO PLACEMENT OF SEED.

C. WHERE PERMANENT SEEDING IS NECESSARY, ANNUAL WINTER RYE (1.2 LBS/1000 SQ.FT) SHALL BE ADDED TO THE PREVIOUSLY NOTED AREAS.

D. WHERE TEMPORARY SEEDING IS REQUIRED, ANNUAL WINTER RYE (2.6 LBS/1000 SQ. FT.) SHALL BE SOWN INSTEAD OF THE PREVIOUSLY NOTED SEEDING RATE E. FERTILIZING, SEEDING AND MULCHING SHALL BE APPLIED TO LOAM THE DAY THE LOAM IS SPREAD BY

F. ALTERNATIVE HAY MULCH SHALL BE SECURED WITH PHOTODEGRADABLE/BIODEGRADABLE NETTING. TRACKING BY MACHINERY ALONE WILL NOT SUFFICE.

5. FOLLOWING FINAL SEEDING, THE SITE WILL BE INSPECTED EVERY 30 DAYS UNTIL 90% COVER HAS BEEN ESTABLISHED. RESEEDING WILL BE CARRIED OUT BY THE CONTRACTOR WITHIN 10 DAYS OF NOTIFICATION BY THE ENGINEER THAT THE EXISTING CATCH IS INADEQUATE.

MONITORING SCHEDULE:

THE CONTRACTOR IS RESPONSIBLE FOR INSTALLING, MONITORING, MAINTAINING, REPAIRING, REPLACING AND REMOVING ALL OF THE EROSION AND SEDIMENTATION CONTROLS OR APPOINTING A QUALIFIED SUBCONTRACTOR TO DO SO. MAINTENANCE MEASURES WILL BE APPLIED AS NEEDED DURING THE ENTIRE CONSTRUCTION CYCLE. AFTER EACH RAINFALL, A VISUAL INSPECTION WILL BE MADE OF ALL EROSION AND SEDIMENTATION CONTROLS AS FOLLOWS:

1. HAY BALE BARRIERS, SILT FENCE, AND STONE CHECK DAMS SHALL BE INSPECTED AND REPAIRED ONCE A WEEK OR IMMEDIATELY FOLLOWING ANY SIGNIFICANT RAINFALL. SEDIMENT TRAPPED BEHIND THESE BARRIERS SHALL BE EXCAVATED WHEN IT REACHES A DEPTH OF 6" AND REDISTRIBUTED TO AREAS UNDERGOING FINAL GRADING. SHOULD THE HAY BALE BARRIERS PROVE TO BE INEFFECTIVE, THE CONTRACTOR SHALL INSTALL SILT FENCE BEHIND THE HAY BALES.

2. VISUALLY INSPECT RIPRAP ONCE A WEEK OR AFTER EACH SIGNIFICANT RAINFALL AND REPAIR AS NEEDED. REMOVE SEDIMENT TRAPPED BEHIND THESE DEVICES ONCE IT ATTAINS A DEPTH EQUAL TO 1/2 THE HEIGHT OF THE DAM OR RISER. DISTRIBUTE REMOVED SEDIMENT OFF-SITE OR TO AN AREA UNDERGOING FINAL GRADING.

3. REVEGETATION OF DISTURBED AREAS WITHIN 25' OF DRAINAGE-COURSE/STREAM WILL BE SEEDED WITH THE "MEADOW AREA MIX" AND INSPECTED ON A WEEKLY BASIS OR AFTER EACH SIGNIFICANT RAINFALL AND RESEEDED AS NEEDED. EXPOSED AREAS WILL BE RESEEDED AS NEEDED UNTIL THE AREA HAS OBTAINED 100% GROWTH RATE. PROVIDE PERMANENT RIPRAP FOR SLOPES IN EXCESS OF 3:1 AND WITHIN 25' OF DRAINAGE COURSE.

EROSION CONTROL DURING WINTER CONSTRUCTION: 1. WINTER CONSTRUCTION PERIOD: NOVEMBER 1 THROUGH APRIL 15.

2. WINTER EXCAVATION AND EARTHWORK SHALL BE COMPLETED SUCH THAT NO MORE THAN 1 ACRE OF THE SITE IS WITHOUT STABILIZATION AT ANY ONE TIME.

3. EXPOSED AREA SHALL BE LIMITED TO THOSE AREAS TO BE MULCHED IN ONE DAY PRIOR TO ANY SNOW EVENT. AT THE END OF EACH WORK WEEK NO AREAS MAY BE LEFT UNSTABILIZED OVER THE

4. CONTINUATION OF EARTHWORK OPERATIONS ON ADDITIONAL AREAS SHALL NOT BEGIN UNTIL THE EXPOSED SOIL SURFACE ON THE AREA BEING WORKED HAS BEEN STABILIZED, SUCH THAT NO LARGER AREA OF THE SITE IS WITHOUT EROSION CONTROL PROTECTION AS LISTED IN ITEM 2 ABOVE.

5. AN AREA SHALL BE CONSIDERED TO HAVE BEEN STABILIZED WHEN EXPOSED SURFACES HAVE BEEN EITHER MULCHED WITH STRAW OR HAY AT A RATE OF 150 LB. PER 1000 S.F. (WITH OR WITHOUT SEEDING) OR DORMANT SEEDED, MULCHED AND ANCHORED SUCH THAT SOIL SURFACE IS NOT VISIBLE THROUGH THE MULCH. NOTE: AN AREA IS ALSO CONSIDERED STABLE IF SODDED, COVERED WITH GRAVEL (PARKING LOTS) OR STRUCTURAL SAND.

6. BETWEEN THE DATES OF OCTOBER 15 AND APRIL 1, LOAM OR SEED WILL NOT BE REQUIRED. DURING PERIODS OF ABOVE FREEZING TEMPERATURES THE SLOPES SHALL BE FINE GRADED AND EITHER PROTECTED WITH MULCH OR TEMPORARILY SEEDED AND MULCHED UNTIL SUCH TIME AS THE FINAL TREATMENT CAN BE APPLIED. IF THE DATE IS AFTER NOVEMBER 1 AND IF THE EXPOSED AREA HAS BEEN LOAMED, FINAL GRADED WITH A UNIFORM SURFACE, THEN THE AREA MAY BE DORMANT SEEDED AT A RATE OF 3 TIMES HIGHER THAN SPECIFIED FOR PERMANENT SEED AND THEN MULCHED. IF CONSTRUCTION CONTINUES DURING FREEZING WEATHER, ALL EXPOSED AREAS SHALL BE CONTINUOUSLY GRADED BEFORE FREEZING AND THE SURFACE TEMPORARILY PROTECTED FROM EROSION BY THE APPLICATION OF MULCH. SLOPES SHALL NOT BE LEFT UNEXPOSED OVER THE WINTER OR ANY OTHER EXTENDED TIME OF WORK SUSPENSION UNLESS TREATED IN THE ABOVE MANNER. UNTIL SUCH TIME AS WEATHER CONDITIONS ALLOW, DITCHES TO BE FINISHED WITH THE PERMANENT SURFACE TREATMENT, EROSION SHALL BE CONTROLLED BY THE INSTALLATION OF BALES OF HAY, SILT FENCE OR STONE CHECK DAMS IN ACCORDANCE WITH THE STANDARD DETAILS SHOWN ON THE DESIGN DRAWINGS. NOTE: DORMANT SEEDING SHOULD NOT BE ATTEMPTED UNLESS SOIL TEMPERATURE REMAINS BELOW 50 DEGREES AND DAY TIME TEMPERATURES REMAIN IN THE 30'S.

7. MULCH NETTING SHALL BE USED TO ANCHOR MULCH IN ALL DRAINAGE WAYS WITH A SLOPE GREATER THAN 3% FOR SLOPES EXPOSED TO DIRECT WINDS AND FOR ALL OTHER SLOPES GREATER THAN 8%. VEGETATED DRAINAGE SWALES SHALL BE LINED WITH EXCELSIOR OR CURLEX.

8. MULCH NETTING SHALL BE USED TO ANCHOR MULCH IN ALL DRAINAGE WAYS WITH SLOPES GREATER THAN 15%. AFTER OCTOBER 1 THE SAME APPLIES FOR ALL SLOPES GREATER THAN 8%.

9. BETWEEN THE DATES OF OCTOBER 15 TO NOVEMBER 1, WINTER RYE IS RECOMMENDED FOR STABILIZATION. AFTER NOVEMBER 1, WINTER RYE IS NOT EFFECTIVE. AROUND NOVEMBER 15 OR LATER, ONCE TEMPERATURES OF THE AIR AND SOIL PERMIT, DORMANT SEEDING IS EFFECTIVE.

10. IN THE EVENT OF SNOWFALL (FRESH OR CUMULATIVE) GREATER THAN 1 INCH DURING WINTER CONSTRUCTION PERIOD ALL SNOW SHALL BE REMOVED FROM THE AREAS OF SEEDING AND MULCHING PRIOR TO PLACEMENT.

CONSTRUCTION OF THE PROJECT IS EXPECTED TO COMMENCE IN LATE SUMMER 2017 FOLLOWING ISSUE OF TOWN AND DEP PERMITS AND ONCE UNITS ARE PRE-SOLD. THE CONSTRUCTION OF THE ROAD AND LITHLITY INFRASTRUCTURE IS EXPECTED TO CONTINUE INTO THE SPRING OF 2018. CONSTRUCTION OF UNITS WILL DEPEND ON MARKET CONDITIONS BUT BASED ON THE RECENT SUCCESS WE WOULD EXPECT THE UNITS TO BE CONSTRUCTED WITHIN 2-3 YEARS. CONSTRUCTION SEQUENCING WILL INCLUDE THE

FOLLOWING: TREE CLEARING AND STUMP REMOVAL.

• REMOVAL OF THE THREE HOUSES AND ASSOCIATED DRIVES AND INFRASTRUCTURE. ROUGH GRADING, SITE BLASTING FOR ROADWAYS AND UNITS AND INSTALLATION OF UTILITIES AND

STORMWATER SYSTEMS. FINISH GRAVELS AND SURFACES & PAVING

LOAM, SEED AND STABILIZATION.

CONSTRUCTION PHASE:

HE FOLLOWING GENERAL PRACTICES WILL BE USED TO PREVENT EROSION DURING CONSTRUCTION OF THIS

1. ONLY THOSE AREAS UNDER ACTIVE CONSTRUCTION WILL BE CLEARED AND LEFT IN AN UNTREATED OR UNVEGETATED CONDITION. IF FINAL GRADING, LOAMING AND SEEDING WILL NOT OCCUR WITHIN 7 DAYS, SEE

2. PRIOR TO THE START OF CONSTRUCTION IN A SPECIFIC AREA, SILT FENCING AND/OR HAY BALES WILL BE INSTALLED AT THE TOE OF SLOPE AND IN AREAS AS LOCATED ON THE PLANS TO PROTECT AGAINST ANY CONSTRUCTION RELATED EROSION. IMMEDIATELY FOLLOWING CONSTRUCTION OF CULVERTS AND SWALES, RIP RAP APRONS SHALL BE INSTALLED, AS SHOWN ON THE PLANS.

3. TOPSOIL WILL BE STOCKPILED WHEN NECESSARY IN AREAS WHICH HAVE MINIMUM POTENTIAL FOR EROSION AND WILL BE KEPT AS FAR AS POSSIBLE FROM THE EXISTING DRAINAGE COURSE. NO STOCKPILE SHALL BE CLOSER THEN 100' OF A RESOURCE INCLUDING, BUT NOT LIMITED TO, WETLANDS, STREAMS, AND OPEN WATER BODIES. ALL STOCKPILES SHALL HAVE A SILTATION FENCE BELOW THEM REGARDLESS OF TIME OF PRESENCE. ALL STOCKPILES EXPECTED TO REMAIN LONGER THAN 15 DAYS SHALL BE:

A. TREATED WITH ANCHORED MULCH (WITHIN 5 DAYS OF THE LAST DEPOSIT OF STOCKPILED SOIL). B. SEEDED WITH CONSERVATION MIX AND MUI CHED IMMEDIATELY

C. INSTALL SILT FENCE AROUND STOCKPILE AT BASE OF PILE. STOCKPILES TO HAVE SILT FENCE INSTALLED AT TIME OF ESTABLISHMENT AT BASE OF PILE.

4. ALL DISTURBED AREAS THAT WILL NOT BE WORKED FOR MORE THAN 7 DAYS SHALL BE EITHER: A. TREATED WITH ANCHORED MULCH IMMEDIATELY, OR B. SEEDED WITH CONSERVATION MIX OF ANNUAL RYE GRASS (0.9 LBS/1000 SQ. FT) AND MULCHED

5. ALL GRADING WILL BE HELD TO A MAXIMUM 2:1 SLOPE WHERE PRACTICAL. ALL SLOPES WILL BE STABILIZED WITH PERMANENT SEEDING, OR WITH STONE, WITHIN 7 DAYS AFTER FINAL GRADING IS COMPLETE. (SEE POST-CONSTRUCTION REVEGETATION FOR SEEDING SPECIFICATION.)

6. ALL CULVERTS WILL BE PROTECTED WITH STONE RIPRAP (D50 = 6" UNLESS OTHERWISE SPECIFIED) AT INLETS AND OUTLETS.

Maine DEP Chapter 500, APPENDIX C. Housekeeping

IMMEDIATELY.

These performance standards apply to all projects except for stormwater PBR projects.

1. Spill prevention. Controls must be used to prevent pollutants from construction and waste materials stored on site to enter stormwater, which includes storage practices to minimize exposure of the materials to stormwater. The site contractor or operator must develop, and implement as necessary, appropriate spill prevention, containment, and response planning measures.

NOTE: Any spill or release of toxic or hazardous substances must be reported to the Department. For oil spills, call 1-800-482-0777 which is available 24 hours a day. For spills of toxic or hazardous material, call 1-800-452-4664 which is available 24 hours a day. For more information, visit the Department's website at: http://www.maine.gov/dep/spills/emergspillresp/

2. Groundwater protection. During construction, liquid petroleum products and other hazardous materials with the potential to contaminate groundwater may not be stored or handled in areas of the site draining to an infiltration area. An "infiltration area" is any area of the site that by design or as a result of soils, topography and other relevant factors accumulates runoff that infiltrates into the soil. Dikes, berms, sumps, and other forms of secondary containment that prevent discharge to groundwater may be used to isolate portions of the site for the purposes of storage and handling of these materials. Any project proposing infiltration of stormwater must provide adequate pre-treatment of stormwater prior to discharge of stormwater to the infiltration area, or provide for treatment within the infiltration area, in order to prevent the accumulation of fines, reduction in infiltration rate, and consequent flooding and

See Appendix D for license by rule standards for infiltration of stormwater.

These materials must be prevented from becoming a pollutant source.

NOTE: Lack of appropriate pollutant removal best management practices (BMPs) may result in violations of the groundwater quality standard established by 38 M.R.S.A. §465-C(1).

3. Fugitive sediment and dust. Actions must be taken to ensure that activities do not result in noticeable erosion of soils or fugitive dust emissions during or after construction. Oil may not be used for dust control, but other water additives may be considered as needed. A stabilized construction entrance (SCE) should be included to minimize tracking of mud and sediment. If off-site tracking occurs, public roads should be swept immediately and no less than once a week and prior to significant storm events. Operations during dry months, that experience fugitive dust problems, should wet down

NOTE: Dewatering a stream without a permit from the Department may violate state water quality standards and the Natural Resources Protection Act

4. Debris and other materials. Minimize the exposure of construction debris, building and landscaping materials, trash, fertilizers, pesticides, herbicides, detergents, sanitary waste and other materials to precipitation and stormwater runoff.

NOTE: To prevent these materials from becoming a source of pollutants, construction and post-construction activities related to a project may be required to comply with applicable provision of rules related to solid, universal, and hazardous waste, including, but not limited to, the Maine solid waste and hazardous waste management rules; Maine hazardous waste management rules; Maine oil conveyance and storage rules; and Maine pesticide requirements

5. Excavation de-watering. Excavation de-watering is the removal of water from trenches, foundations, coffer dams, ponds and other areas within the construction area that retain water after excavation. In most cases the collected water is neavily silted and hinders correct and safe construction practices. The collected water removed from the ponded area, either through gravity or pumping, must be spread through natural wooded buffers or removed to areas that are specifically designed to collect the maximum amount of sediment possible, like a cofferdam sedimentation basin. Avoid allowing the water to flow over disturbed areas of the site. Equivalent measures may be taken if approved by the

NOTE: Dewatering controls are discussed in the "Maine Erosion and Sediment Control BMPs. Maine Department of

6. Authorized Non-stormwater discharges. Identify and prevent contamination by non-stormwater discharges. Where allowed non-stormwater discharges exist, they must be identified and steps should be taken to ensure the mplementation of appropriate pollution prevention measures for the non-stormwater component(s) of the discharge

(a) Discharges from firefighting activity;

(b) Fire hydrant flushings; (c) Vehicle washwater if detergents are not used and washing is limited to the exterior of vehicles (engine, undercarriage and transmission washing is prohibited

(d) Dust control runoff in accordance with permit conditions and Appendix (C)(3):

(e) Routine external building washdown, not including surface paint removal, that does not involve detergents; (f)Pavement washwater (where spills/leaks of toxic or hazardous materials have not occurred, unless all spilled material

(g) Uncontaminated air conditioning or compressor condensate;

(h) Uncontaminated groundwater or spring water

had been removed) if detergents are not used

(i) Foundation or footer drain-water where flows are not contaminated (j) Uncontaminated excavation dewatering (see requirements in Appendix C(5));

(k) Potable water sources including waterline flushings; and

7. Unauthorized non-stormwater discharges . The Department's approval under this Chapter does not authorize a discharge that is mixed with a source of non stormwater, other than those discharges in compliance with Appendix C (6). Specifically, the Department's approval does not authorize discharges of the following:

(a) Wastewater from the washout or cleanout of concrete, stucco, paint, form release oils, curing compounds or other

construction materials;

(b) Fuels, oils or other pollutants used in vehicle and equipment operation and maintenance; (c) Soaps, solvents, or detergents used in vehicle and equipment washing; and

Toxic or hazardous substances from a spill or other release.

(8) Additional requirements. Additional requirements may be applied on a site-specific basis.

Maine DEP Chapter 500, APPENDIX A. Erosion and sedimentation control (2015 Update)

Control BMPs Maine Department of Environmental Protection.'

apply to a particular site.

released from this standard by the Department.

A person who conducts, or causes to be conducted, an activity that involves filling, displacing or exposing soil or other earthen materials shall take measures to prevent unreasonable erosion of soil or sediment beyond the project site or into a protected natural resource as defined in 38 M.R.S. §480-B. Erosion control measures must be in place before the activity begins. Measures must remain in place and functional until the site is permanently stabilized. Adequate and timely temporary and permanent

NOTE: Other requirements may apply, including, but not limited to the Natural Resources Protection Act 38 M.R.S. §480-B. NOTE: The Department has prepared protocols for the control of erosion and sedimentation. See "Maine Erosion and Sediment

1. Pollution prevention. Minimize disturbed areas and protect natural downgradient buffer areas to the extent practicable. Control stormwater volume and velocity within the site to minimize soil erosion. Minimize the disturbance of steep slopes. Control stormwater discharges, including both peak flow rates and volume, to minimize erosion at outlets. The discharge may not result in erosion of any open drainage channels, swales, stream channels or stream banks, upland, or coastal or freshwater wetlands off

Whenever practicable, no disturbance activities should take place within 50 feet of any protected natural resource. If disturbance activities take place between 30 feet and 50 feet of any protected natural resource, and stormwater discharges through the disturbed areas toward the protected natural resource, perimeter erosion controls must be doubled. If disturbance activities take place less than 30 feet from any protected natural resource, and stormwater discharges through the disturbed areas toward the protected natural resource, perimeter erosion controls must be doubled and disturbed areas must be temporarily or permanently stabilized within 7 days.

NOTE: Buffers improve water quality by helping to filter pollutants in run-off both during and after construction. Minimizing disturbed areas through phasing limits the amount of exposed soil on the site through retention of natural cover and by retiring areas as permanently stabilized. Less exposed soil results in fewer erosion controls to install and maintain. If work within an area is not anticipated to begin within two weeks' time, consider leaving the area in its naturally existing cover.

NOTE: Many construction activities within 75 feet of a protected natural resource require a permit under the Natural Resources Protection Act prior to initiation. For more information regarding the applicability of the NRPA to your project, you can visit the Department's website at http://www.maine.gov/dep/land/nrpa/index.html or contact staff of the Division of Land Resource Regulation at the nearest regional office

2. Sediment barriers. Prior to construction, properly install sediment barriers at the downgradient edge of any area to be disturbed and adjacent to any drainage channels within the disturbed area. Sediment barriers should be installed downgradient of soil or sediment stockpiles and stormwater prevented from running onto the stockpile. Maintain the sediment barriers by removing accumulated sediment, or removing and replacing the barrier, until the disturbed area is permanently stabilized. Where a discharge to a storm drain inlet occurs, if the storm drain carries water directly to a surface water and you have authority to access the storm drain inlet, you must install and maintain protection measures that remove sediment from the discharge.

3. Stabilized construction entrance. Prior to construction, properly install a stabilized construction entrance (SCE) at all points of egress from the site. The SCE is a stabilized pad of aggregate, underlain by a geotextile filter fabric, used to prevent traffic from tracking material away from the site onto public ROWs. Maintain the SCE until all disturbed areas are stabilized.

4. Temporary stabilization. Within 7 days of the cessation of construction activities in an area that will not be worked for more than 7 days, stabilize any exposed soil with mulch, or other non-erodible cover. Stabilize areas within 75 feet of a wetland or waterbody within 48 hours of the initial disturbance of the soil or prior to any storm event, whichever comes first.

5. Removal of temporary measures. Remove any temporary control measures, such as silt fence, within 30 days after permanent stabilization is attained. Remove any accumulated sediments and stabilize.

NOTE: It is recommended that silt fences be removed by cutting the fence materials at ground level to avoid additional soil

6. Permanent stabilization. If the area will not be worked for more than one year or has been brought to final grade, then permanently stabilize the area within 7 days by planting vegetation, seeding, sod, or through the use of permanent mulch, or riprap, or road sub-base. If using vegetation for stabilization, select the proper vegetation for the light, moisture, and soil conditions; amend areas of disturbed subsoils with topsoil, compost, or fertilizers; protect seeded areas with mulch or, if $necessary, erosion \ control\ blankets; and \ schedule\ sodding,\ planting,\ and\ seeding\ so\ to\ avoid\ die-off\ from\ summer\ drought\ and$ fall frosts. Newly seeded or sodded areas must be protected from vehicle traffic, excessive pedestrian traffic, and concentrated runoff until the vegetation is well-established with 90% cover by healthy vegetation. If necessary, areas must be reworked and restabilized if germination is sparse, plant coverage is spotty, or topsoil erosion is evident. One or more of the following may

(a) Seeded areas. For seeded areas, permanent stabilization means a 90% cover of the disturbed area with mature, healthy plants with no evidence of washing or rilling of the topsoil.

(b) Sodded areas. For sodded areas, permanent stabilization means the complete binding of the sod roots into the underlying soil

(c) Permanent Mulch. For mulched areas, permanent mulching means total coverage of the exposed area with an approved mulch material. Erosion Control Mix may be used as mulch for permanent stabilization according to the approved application rates and limitations.

(d) Riprap. For areas stabilized with riprap, permanent stabilization means that slopes stabilized with riprap have an appropriate backing of a well-graded gravel or approved geotextile to prevent soil movement from behind the riprap. Stone must be sized appropriately. It is recommended that angular stone be used.

(e) Agricultural use. For construction projects on land used for agricultural purposes (e.g., pipelines across crop land), permanent stabilization may be accomplished by returning the disturbed land to agricultural use.

provided it is free of fine materials that may runoff with a rain event (g) Ditches, channels, and swales. For open channels, permanent stabilization means the channel is stabilized with a 90% cover of healthy vegetation, with a well-graded riprap lining, turf reinforcement mat, or with another non-erosive lining such as concrete or asphalt pavement. There must be no evidence of slumping of the channel lining, undercutting of the channel banks,

(f)Paved areas. For paved areas, permanent stabilization means the placement of the compacted gravel subbase is completed,

7. Winter Construction. "Winter construction" is construction activity performed during the period from November 1 through Apri 15. If disturbed areas are not stabilized with pern es by November 1 or new soil disturbance occurs after Novembe 1, but before April 15, then these areas must be protected and runoff from them must be controlled by additional measures and

of each construction day, areas that have been brought to final grade must be stabilized. Mulch may not be spread on top of (b) Sediment Barriers. All areas within 75 feet of a protected natural resource must be protected with a double row of sediment

(a) Site Stabilization. For winter stabilization, hay mulch is applied at twice the standard temporary stabilization rate. At the end

(c) Ditch. All vegetated ditch lines that have not been stabilized by November 1, or will be worked during the winter construction period, must be stabilized with an appropriate stone lining backed by an appropriate gravel bed or geotextile unless specifically

(d) Slopes. Mulch netting must be used to anchor mulch on all slopes greater than 8% unless erosion control blankets or erosion control mix is being used on these slopes

NOTE: The Department has prepared protocols for the control of erosion and sedimentation during the winter

months. See "Maine Erosion and Sediment Control BMPs Maine Department of Environmental Protection 8. Stormwater channels. Ditches, swales, and other open stormwater channels must be designed, constructed, and stabilized using measures that achieve long-term erosion control. Ditches, swales and other open stormwater channels must be sized to handle, at a minimum, the expected volume run-off. Each channel should be constructed in sections so that the section's grading, shaping, and installation of the permanent lining can be completed the same day. If a channel's final grading or lining installation must be delayed, then diversion berms must be used to divert stormwater away from the channel, properly-spaced check dams must be installed in the channel to slow the water velocity, and a temporary lining installed along the channel to prevent

scouring. Permanent stabilization for channels is addressed under Appendix A(5)(g) above. (a) The channel should receive adequate routine maintenance to maintain capacity and prevent or correct any erosion of the

channel's bottom or side slopes. (b) When the watershed draining to a ditch or swale is less than 1 acre of total drainage and less than ¼ acre of impervious area,

diversion of runoff to adjacent wooded or otherwise vegetated buffer areas is encouraged where the opportunity exists. 9. Sediment basins. Sediment basins must be designed to provide storage for either the calculated runoff from a 2-year, 24-hour storm or provide for 3,600 cubic feet of capacity per acre draining to the basin. Outlet structures must discharge water from the surface of the basin whenever possible. Erosion controls and velocity dissipation devices must be used if the discharging waters are likely to create erosion. Accumulated sediment must be removed as needed from the basin to maintain at least ½ of the

design capacity of the basin. The use of cationic treatment chemicals, such as polymers, flocculants, or other chemicals that contain an overall positive charge designed to reduce turbidity in stormwater must receive prior approval from the Department. When requesting approval to use cationic treatment chemicals, you must describe appropriate controls and implementation procedures to ensure the use will not lead to a violation of water quality standards. In addition, you must specify the type(s) of soil likely to be treated on the site, chemicals to be used and how they are to be applied and in what quantity, any manufacturer's recommendations, and any

training had by personnel who will handle and apply the chemicals. 10. Roads. Gravel and paved roads must be designed and constructed with crowns or other measures, such as water bars, to ensure that stormwater is delivered immediately to adjacent stable ditches, vegetated buffer areas, catch basin inlets, or street

erosion problems. (2) The Department recommends that impervious surfaces, including roads, be designed and constructed so that stormwater is distributed in sheet flow to natural vegetated buffer areas wherever such areas are available. Road ditches should be designed so that stormwater is frequently (at least every 100 to 200 feet) discharged via ditch turnouts in sheet flow to adjacent natural buffer areas wherever possible. 11. Culverts. Culverts must be sized to avoid unintended flooding of upstream areas or frequent overtopping of roadways.

Culvert inlets must be protected with appropriate materials for the expected entrance velocity, and protection must extend at

least as high as the expected maximum elevation of storage behind the culvert. Culvert outlet design must incorporate measures,

such as aprons, to prevent scour of the stream channel. Outlet protection measures must be designed to stay within the channel

NOTE: (1) Gravel and paved roads should be maintained so that they continue to conform to this standard in order to prevent

limits. The design must take account of tailwater depth. 12. Parking areas. Parking areas must be constructed to ensure runoff is delivered to adjacent swales, catch basins, curb gutters, or buffer areas without eroding areas downslope. The parking area's subbase compaction and grading must be done to ensure runoff is evenly distributed to adjacent buffers or side slopes. Catch basins must be located and set to provide enough storage

depth at the inlet to allow inflow of peak runoff rates without by-pass of runoff to other areas. 13. Additional requirements. Additional requirements may be applied on a site-specific basis.

Maine DEP Chapter 500, APPENDIX B. Inspection and maintenance (2015 Update)

This appendix applies to all projects, except that a project that is eligible for stormwater PBR need only meet the standards in Section 1.

See Appendix D(5) for additional maintenance requirements related to infiltration of stormwater

1. During construction. The following standards must be met during construction.

(a) Inspection and corrective action. Inspect disturbed and impervious areas, erosion control measures, materials storage areas that are exposed to precipitation, and locations where vehicles enter or exit the site. Inspect these areas at least once a week as well as before and within 24 hours after a storm event (rainfall), and prior to completing permanent stabilization measures. A person with knowledge of erosion and stormwater control, including the standards and conditions in the permit, shall conduct the inspections

(b) Maintenance, If best management practices (BMPs) need to be repaired, the repair work should be initiated upon discovery of the problem but no later than the end of the next workday. If additional BMPs or significant repair of BMPs are necessary, implementation must be completed within 7 calendar days and prior to any storm event (rainfall). All measures must be maintained in effective operating condition

(c) Documentation. Keep a log (report) summarizing the inspections and any corrective action taken. The log must include the name(s) and qualifications of the person making the inspections, the date(s) of the inspections, and major observations about the operation and naintenance of erosion and sedimentation controls, materials storage areas, and vehicles access points to the parcel. Major observations must include BMPs that need maintenance. BMPs that failed to operate as designed or proved inadequate for a particular location, and location(s) where additional BMPs are needed. For each BMP requiring maintenance, BMP needing replacement, and location needing additional BMPs, note in the log the corrective action taken and when it was taken.

The log must be made accessible to Department staff and a copy must be provided upon request. The permittee shall retain a copy of the log for a period of at least three years from the completion of permanent stabilization.

. Post-construction. The following standards must be met after construction.

(a) Plan. Carry out an approved inspection and maintenance plan that is consistent with the minimum requirements of this section. The plan must address inspection and maintenance of the project's permanent erosion control measures and stormwater management system. This plan may be combined with the plan listed in Section 2(a) of this appendix. See Section 7(C)(2) for submission requirements.

(b) Inspection and maintenance. All measures must be maintained in effective operating condition. A person with knowledge of erosion and stormwater control, including the standards and conditions in the permit, shall conduct the inspections. The following areas, facilities, and neasures must be inspected and identified deficiencies must be corrected. Areas, facilities, and measures other than those listed below may also require inspection on a specific site. Inspection or maintenance tasks other than those discussed below must be included in the maintenance plan developed for a specific site.

NOTE: Expanded and more-detailed descriptions for specific maintenance tasks may be found in the Maine DEP's "Stormwater Management for Maine: Best Management Practices."

(i) Inspect vegetated areas, particularly slopes and embankments, early in the growing season or after heavy rains to identify active or potential rosion problems. Replant bare areas or areas with sparse growth. Where rill erosion is evident, armor the area with an appropriate lining or divert the erosive flows to on-site areas able to withstand the concentrated flows. See permanent stabilization standards in Appendix A(5).

Inspect ditches, swales and other open stormwater channels in the spring, in late fall, and after heavy rains to remove any obstructions to flow, remove accumulated sediments and debris, to control vegetated growth that could obstruct flow, and to repair any erosion of the ditch lining. Vegetated ditches must be mowed at least annually or otherwise maintained to control the growth of woods vegetation and maintain flow capacity. Any woody vegetation growing through riprap linings must also be removed. Repair any slumping side slopes as soon as practicable. If the ditch has a riprap lining, replace riprap on areas where any underlying filter fabric or underdrain gravel is showing through the stone or where stones have dislodged. The channel must receive adequate routine maintenance to maintain capacity and prevent or correct any erosion of the channel's bottom or sideslope

(iii) Inspect culverts in the spring, in late fall, and after heavy rains to remove any obstructions to flow; remove accumulated sediments and

debris at the inlet, at the outlet, and within the conduit; and to repair any erosion damage at the culvert's inlet and outlet.

(iv) Inspect and clean out catch basins. Clean-out must include the removal and legal disposal of any accumulated sediments and debris at the bottom of the basin, at any inlet grates, at any inflow channels to the basin, and at any pipes between basins. If the basin outlet is designed to trap floatable materials, then remove the floating debris and any floating oils (using oil-absorptive pads). (v) Inspect resource and treatment buffers once a year for evidence of erosion, concentrating flow, and encroachment by development. If flows are concentrating within a buffer, site grading, level spreaders, or ditch turn-outs must be used to ensure a more even distribution of flow into a buffer. Check down slope of all spreaders and turn-outs for erosion. If erosion is present, adjust or modify the spreader's or turnout's

lip to ensure a better distribution of flow into a buffer. Clean-out any accumulation of sediment within the spreader bays or turn-out pools. (vi) Inspect at least once per year, each stormwater management pond or basin, including the pond's embankments, outlet structure, and emergency spillway. Remove and dispose of accumulated sediments in the pond. Control woody vegetation on the pond's embankments.

(vii)Inspect at least one per year, each underdrained filter, including the filter embankments, vegetation, underdrain piping, and overflow spillway. Remove and dispose of accumulated sediments in the filter. If needed, rehabilitate any clogged surface linings, and flush underdrain

(viii)Inspect each manufactured system installed on the site, including the system's inlet, treatment chamber(s), and outlet at least once per year, or in accordance with the maintenance guidelines recommended by the manufacturer based on the estimated runoff and pollutant load expected to the system from the project. Remove and dispose of accumulated sediments, debris, and contaminated waters from the system and, if applicable, remove and replace any clogged or spent filter media.

of permanent stabilization

(i) Clear accumulations of winter sand in parking lots and along roadways at least once a year, preferably in the spring. Accumulations on pavement may be removed by pavement sweeping. Accumulations of sand along road shoulders may be removed by grading excess sand to the pavement edge and removing it manually or by a front-end loader. Grading of gravel roads, or grading of the gravel shoulders of gravel or paved roads, must be routinely performed to ensure that stormwater drains immediately off the road surface to adjacent buffer areas or stable ditches, and is not impeded by accumulations of graded material on the road shoulder or by excavation of false ditches in the shoulder If water bars or open-top culverts are used to divert runoff from road surfaces, clean-out any sediments within or at the outlet of these

(ii) Manage each buffer's vegetation consistently with the requirements in any deed restrictions for the buffer. Wooded buffers must remain fully wooded and have no disturbance to the duff layer. Vegetation in non-wooded buffers may not be cut more than three times per year, and may not be cut shorter than six inches.

NOTE: Contact the Department's Division of Watershed Management (Maine DEP) for assistance developing inspection and maintenance requirements for other drainage control and runoff treatment measures installed on the site. The maintenance needs for most measures may be found in the Maine DEP's "Stormwater Management for Maine: Best Management Practices."

name of the inspector or maintenance personnel performing the task. If a maintenance task requires the clean-out of any sediments or debris, indicate where the sediment and debris was disposed after removal. The log must be made accessible to Department staff and a copy provided to the Department upon request. The permittee shall retain a copy of the log for a period of at least five years from the completion

(d) Documentation. Keep a log (report) summarizing inspections, maintenance, and any corrective actions taken. The log must include the date

on which each inspection or maintenance task was performed, a description of the inspection findings or maintenance completed, and the

3. Re-certification. Submit a certification of the following to the Department within three months of the expiration of each five-year interval from the date of issuance of the permit (a) Identification and repair of erosion problems. All areas of the project site have been inspected for areas of erosion, and appropriate steps

(b) Inspection and repair of stormwater control system. All aspects of the stormwater control system have been inspected for damage, wear, and malfunction, and appropriate steps have been taken to repair or replace the system, or portions of the system

(c) Maintenance. The erosion and stormwater maintenance plan for the site is being implemented as written, or modifications to the plan have

been submitted to and approved by the Department, and the maintenance log is being maintaine Municipalities with separate storm sewer systems regulated under the Maine Pollutant Discharge Elimination System (MPDES) Program may report on all regulated systems under their control as part of their required annual reporting in lieu of separate certification of each system Municipalities not regulated by the MPDES Program, but that are responsible for maintenance of permitted stormwater systems, may report on multiple stormwater systems in one report.

4. Duration of maintenance. Perform maintenance as described and required in the permit unless and until the system is formally accepted by the municipality or quasi-municipal district, or is placed under the jurisdiction of a legally created association that will be responsible for the maintenance of the system. If a municipality or quasi-municipal district chooses to accept a stormwater management system, or a componen of a stormwater system, it must provide a letter to the Department stating that it assumes responsibility for the system. The letter must specify the components of the system for which the municipality or district will assume responsibility, and that the municipality or district agrees to maintain those components of the system in compliance with Department standards. Upon such assumption of responsibility, and approval by the Department, the municipality, quasi-municipal district, or association becomes a co-permittee for this purpose only and must comply with

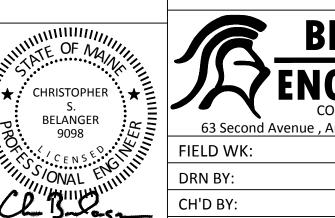
all terms and conditions of the permit. 5. Additional requirements. Additional requirements may be applied on a site-specific basis.

> 6. 7-31-2018 No changes this sheet, re-submit to Town CSB No changes this sheet CSB 5. 7-16-2018 No changes this sheet CSB Respond to Town Memos, Re-submit to Town 3. 3-1-2018 CSB SUBMIT TO DEP Re-Submit to Town and Maine DEP 1. 1-31-2018

> > **Erosion Control Notes**

Oceanview at Cumberland 291 Tuttle Road, Cumberland, Maine

Seacoast Management Company 20 Blueberry Lane, Falmouth, Maine

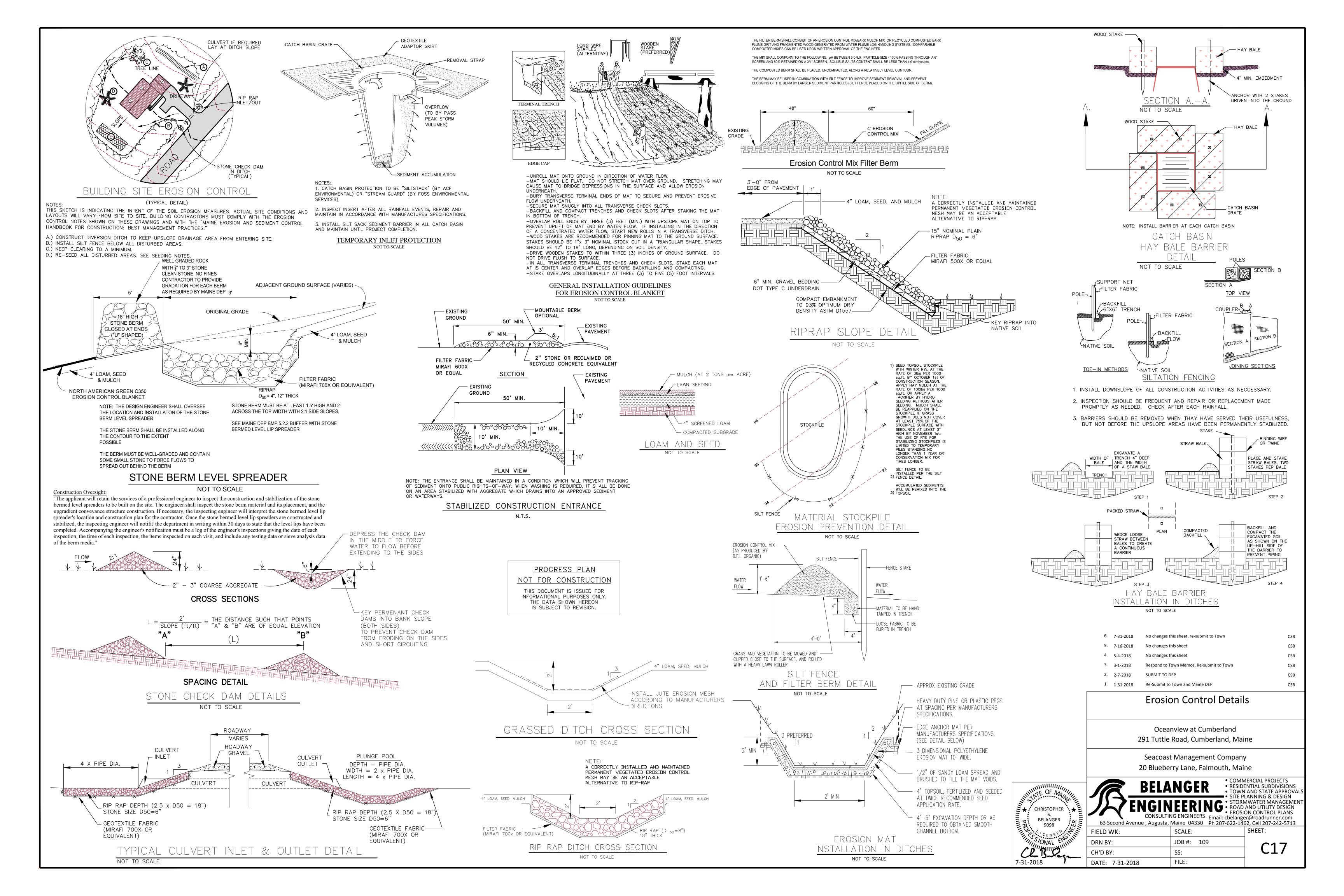


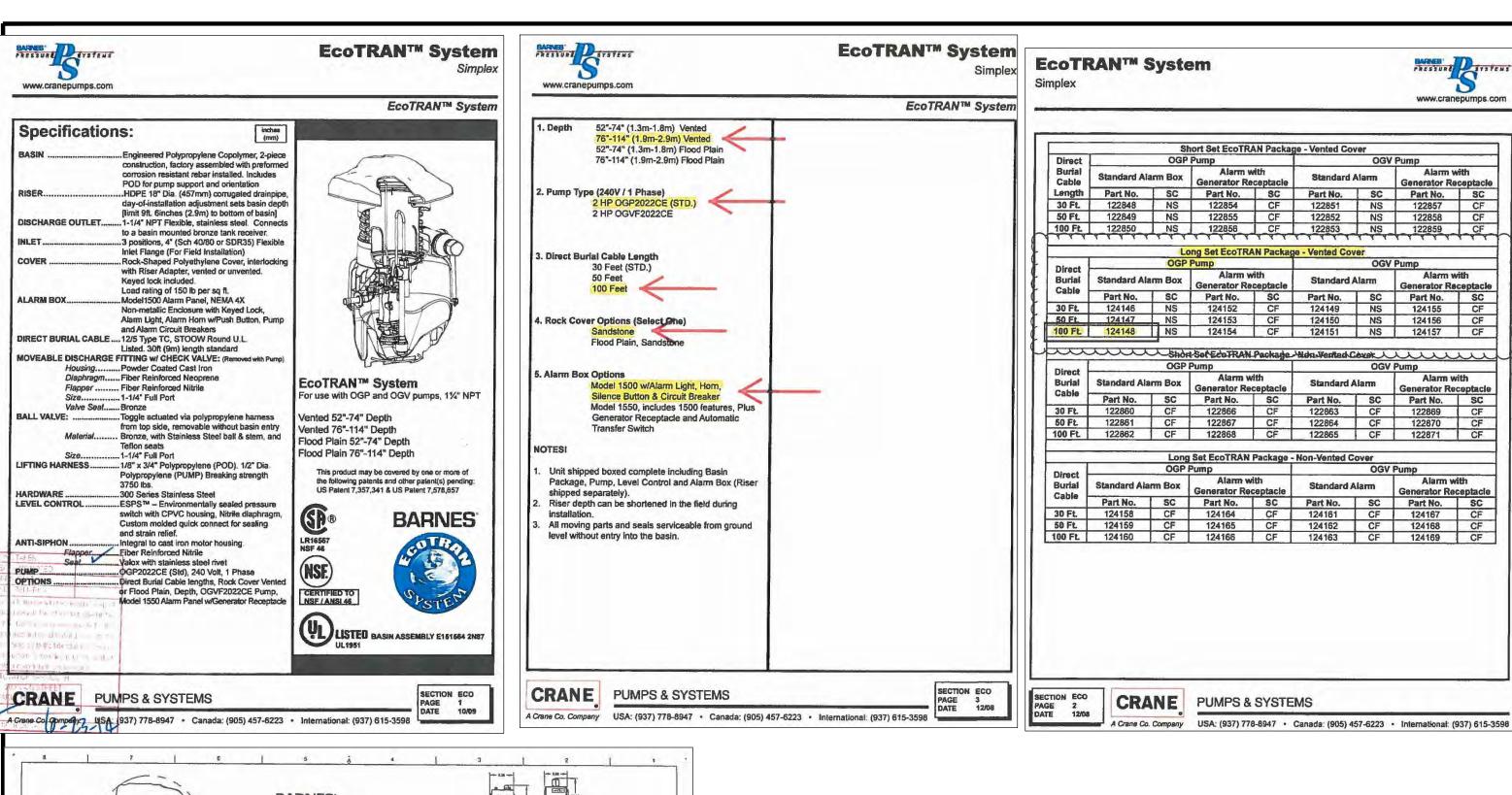


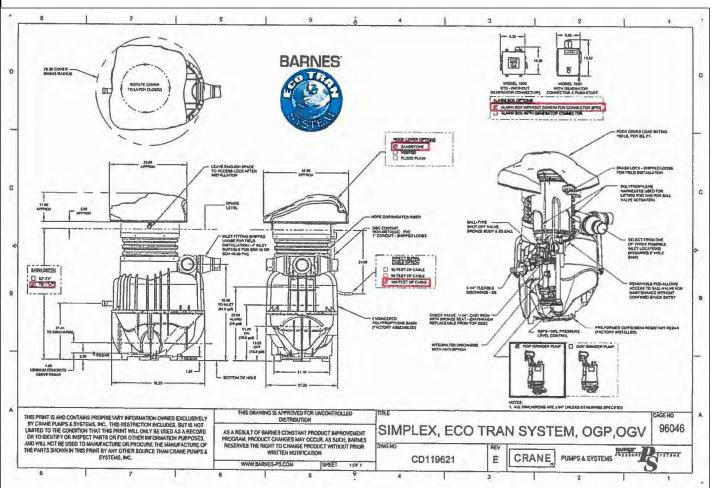
SHEET:

SITE PLANNING & DESIGN

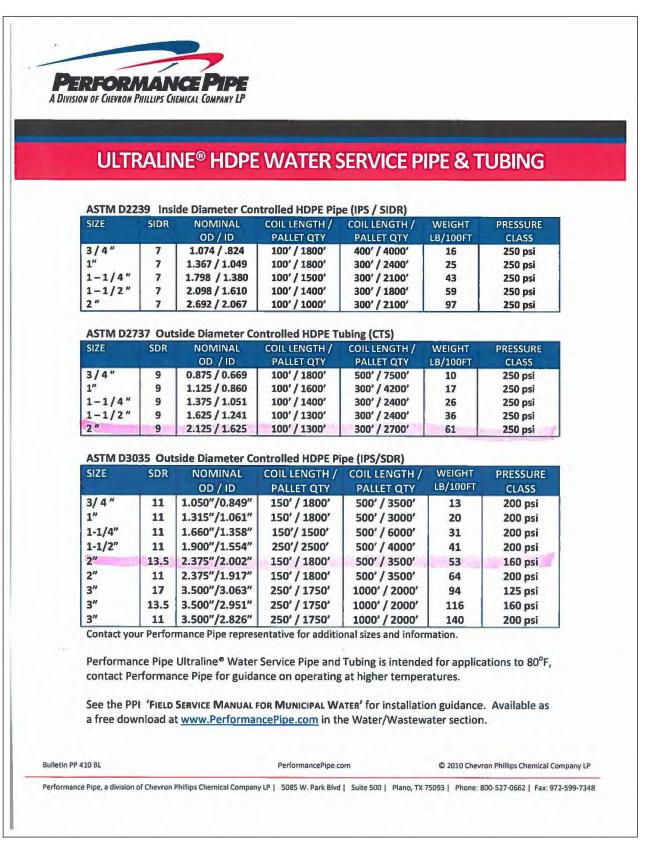
JOB #: 109 SS: FILE: DATE: 7-31-2018

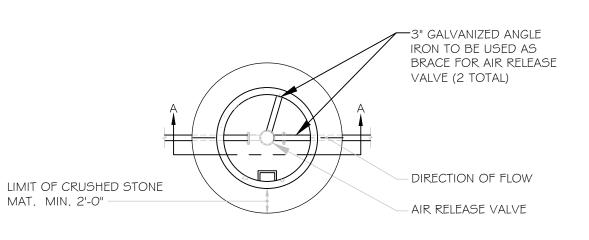












PLAN VIEW

PROPERTY LINE

SEWER

· CURB BOX AND COVER STAMPED "SEWER" W/S.S. ROD AND S.S. PIN.

NOTES

PVC FITTINGS.

CRUSHED STONE.

2" MALE ADAPTOR THREADED BY WELDED.

DO NOT USE FEMALE ADAPTOR DUE TO

POTENTIAL SPLITTING OF THE ADAPTOR.

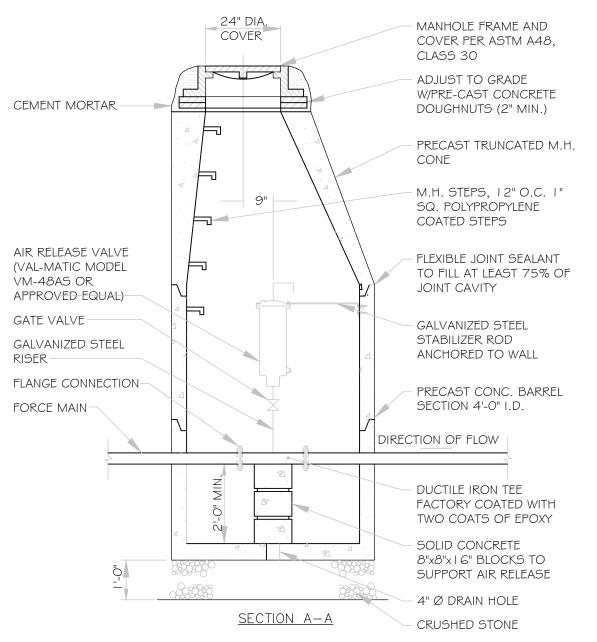
I. THE CONTRACTOR SHALL USE SCHEDULE 80

2. PVC PRIMER/CLEANER SHALL BE USED

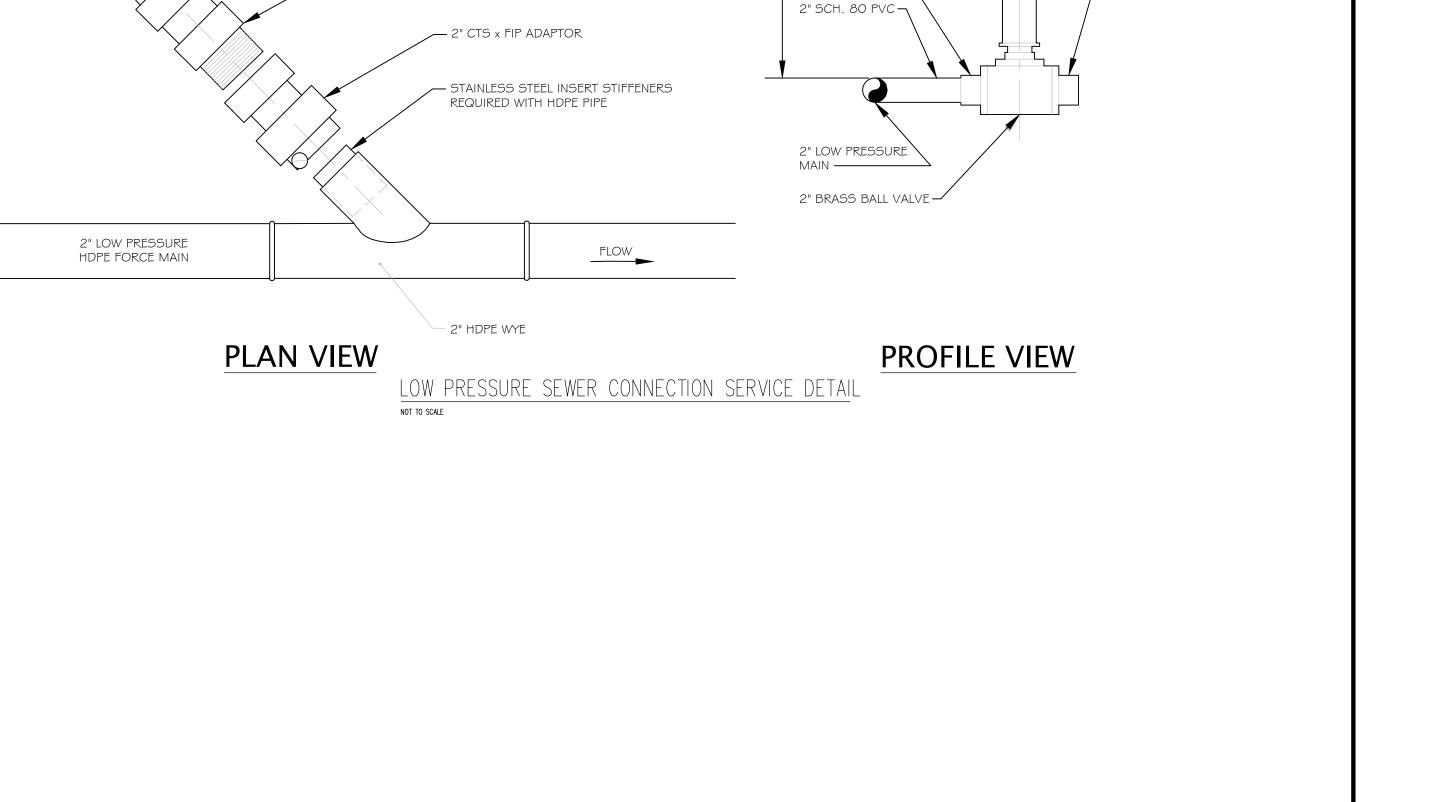
BEFORE PVC CEMENT IS APPLIED.

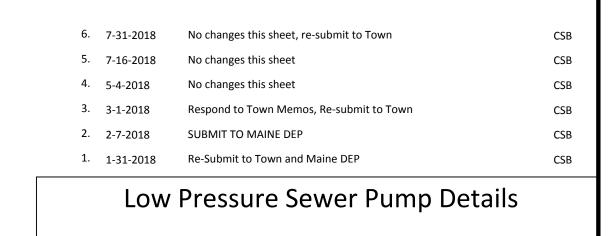
3. BED ALL FITTINGS AND VALVE BOX IN 3/4"

ADJUST FOR MIN. 6" TRAVEL



AIR RELEASE MANHOLE





-PROPERTY LINE

OVER PIPES

PIPES BURIED LESS THAN 4' BELOW

GRADE REQUIRE 2" RIGID INSULATION

____ 2" SCH. 80 PVC MALE ADAPTOR. REDUCE FROM HERE

CURB BOX AND COVER STAMPED

ADJUST FOR MIN. 6" TRAVEL -

2" SCH. 80 PVC

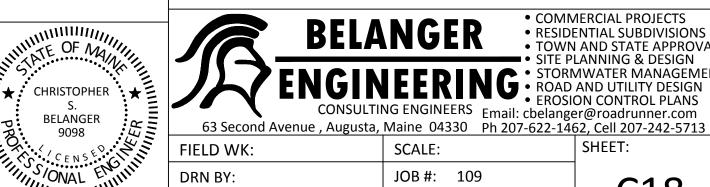
MALE ADAPTOR —

"SEWER" W/S.S. ROD AND S.S. PIN.

FINISHED GRADE

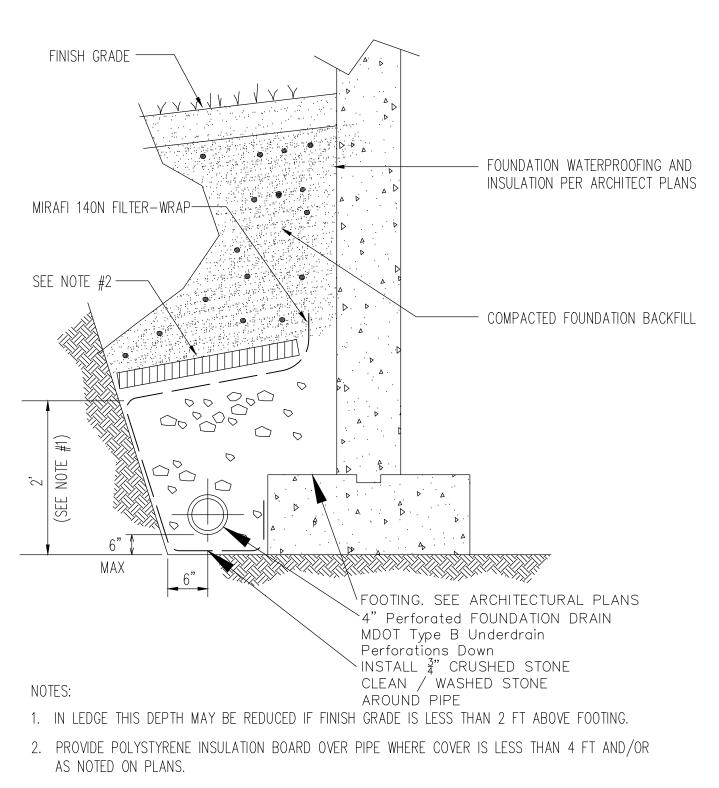
Oceanview at Cumberland 291 Tuttle Road, Cumberland, Maine

Seacoast Management Company 20 Blueberry Lane, Falmouth, Maine



 RESIDENTIAL SUBDIVISIONS TOWN AND STATE APPROVAL SITE PLANNING & DESIGN ENGINEERING STORMWATER MANAGEMENT OF STORMWATE

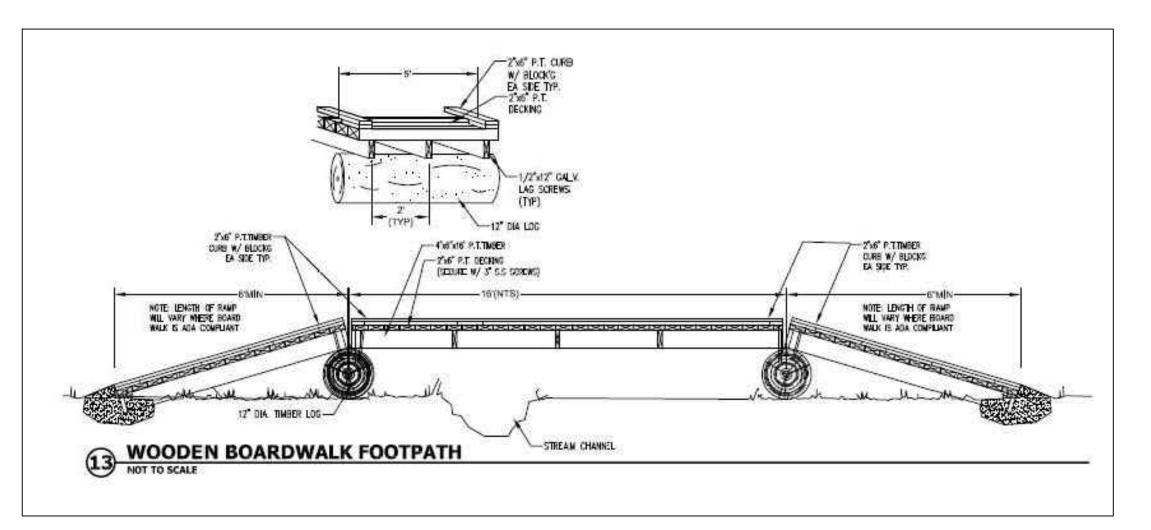
os secona Avenae, Augusta,	Walle 04330 FII 207-022-140	32, Celi 207
FIELD WK:	SCALE:	SHEET:
DRN BY:	JOB #: 109	
CH'D BY:	SS:	
DATE: 7-31-2018	FILE:	

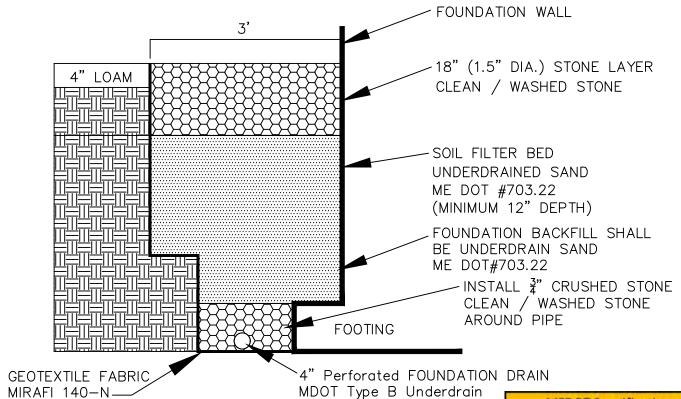


3. SEE PLANS FOR LOCATIONS OF DRAINBOARD AND PERIMETER DRAINS.

PERIMETER OR FOUNDATION DRAIN DETAIL

NOT TO SCALE ST-UD-FOUND/02-97





Perforations Down

OV @ CUMBERLAND SENIOR HOUSING

NOT TO SCALE

MEDOT Specifications for Underdrains (ME DOT #703.22)				
			Sieve Size	% Passing by Weight
			Unde	rdrain Type B
1"	90-100			
1/2"	75-100			
#4	50-100			
#20	15-80			
#50	0-15			
#200	0-5			
Underdrain Type C				
1"	100			
3/4"	90-100			
3/8"	0-75			
#4	0-25			
#10	0-5			

CONSTRUCTION OVERSIGHT ROOF DRIPLINE INSTALLATION

The Contractor will retain the services of a professional engineer of the clients choosing to inspect the construction and stabilization of all stormwater management structures to be built as part of the project. If necessary, the inspecting engineer will interpret the construction plans for the contractor. Once all stormwater management structures are constructed and stabilized, the inspecting engineer will notify the department in writing within 30 days to state that the structures have been completed. Accompanying the engineer's notification must be a copy of the test results for any soil fill, aggregate, or mulch materials used in the construction of the stormwater management structures and a log of the engineer's inspections giving the date of each inspection, the time of each inspection, and the items inspected on each visit.

Roof Dripline Filtration

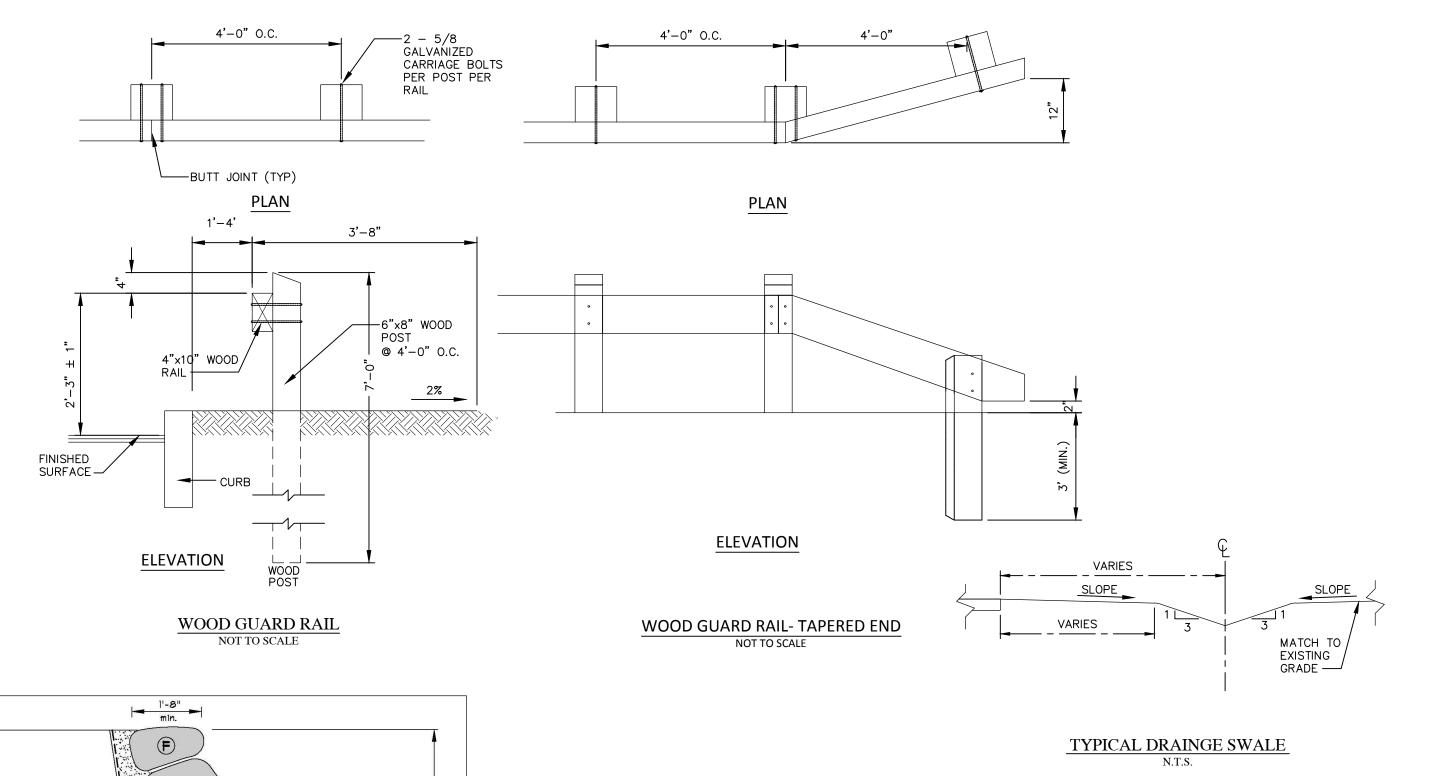
Construction inspections: At a minimum, the professional engineer's inspection will occur after foundation soil preparation but prior to placement of the geotextile lining, after the foundation drain pipe is installed but not yet backfilled, after the pipe bedding gravel is placed but prior to the placement of the gravel filter media, after the gravel filter media has been placed but prior to installing the crushed stone surface layer, and after the surface crushed stone surface layer is installed.

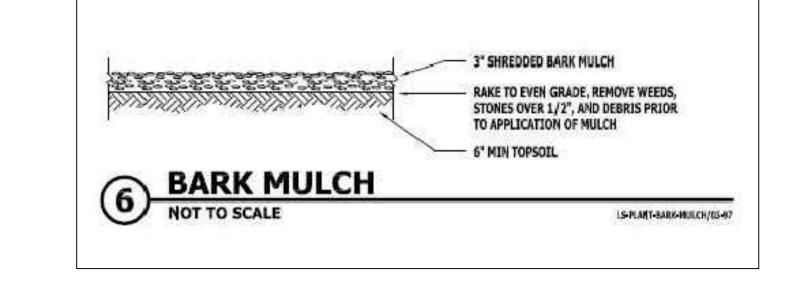
Testing and submittals: The gravel filter media and pipe bedding media used in the roof dripline filtration BMP must be confirmed as suitable by testing. The contractor shall identify the source of these gravels and obtain samples for testing. All testing must be done by a certified laboratory. All results of field and laboratory testing shall be submitted to the project engineer for confirmation. It shall be the contractor's responsibility to ensure completion of the following sampling and testing before the gravel is placed as part of the dripline filter's

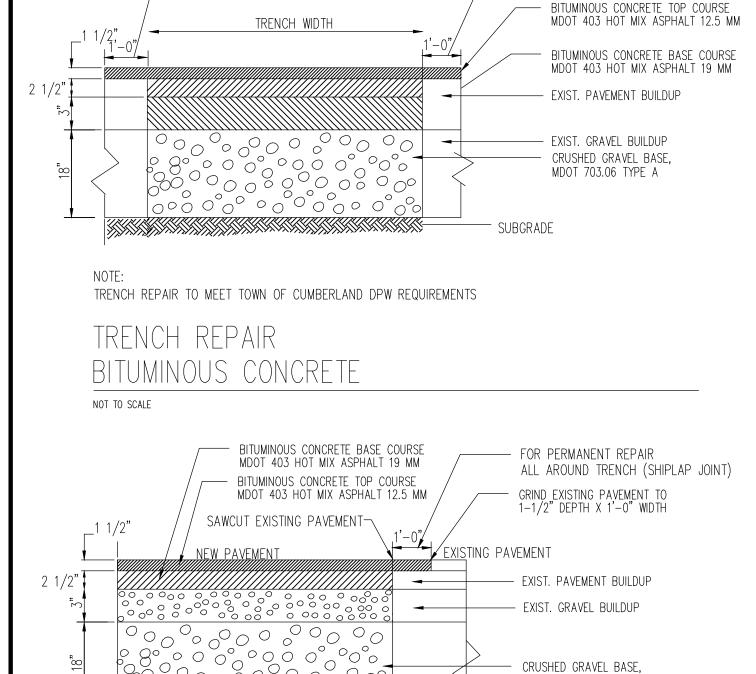
• Obtain a sample of the gravel filter media. The sample must be a composite of three different locations (grabs) from the gravel stockpile. The sample size required will be determined by the testing laboratory. Perform a sieve analysis conforming to ASTM C136 (Standard Test Method for Sieve Analysis of Fine and Coarse Aggregates 1996A) of the sand filter media showing it meets the

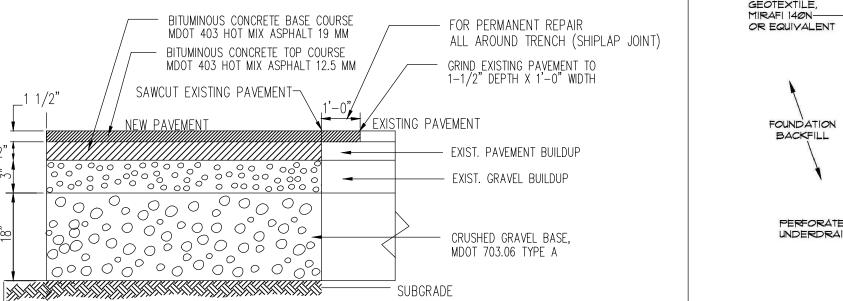
• If the underdrain pipes will be bedded in gravel, obtain a sample of the gravel fill to be used for the pipe bedding. The sample must be a composite of three different locations (grabs) from the stockpile or pit face. The sample size required will be determined by the testing laboratory. Perform a sieve analysis conforming to ASTM C136 (Standard Test Method for Sieve Analysis of Fine and Coarse Aggregates 1996A) of the gravel to be used for the underdrain pipe bedding. The gravel fill must conform to MEDOT specification 703.22 Underdrain

If the underdrain pipes will be bedded in crushed stone, obtain a sample of the crushed stone to be used for the pipe bedding. The sample must be a composite of three different locations (grabs) from the stockpile. The sample size required will be determined by the testing laboratory. Perform a sieve analysis conforming to ASTM C136 (Standard Test Method for Sieve Analysis of Fine and Coarse Aggregates 1996A) of the crushed stone to be used for the underdrain pipe bedding. The crushed stone fill must conform to MEDOT specification 703.22 Underdrain Type C.









FOR PERMANENT REPAIR

FOR TEMPORARY REPAIR

ALL AROUND TRENCH (SHIPLAP JOINT)

ALL AROUND TRENCH (SHIPLAP JOINT)

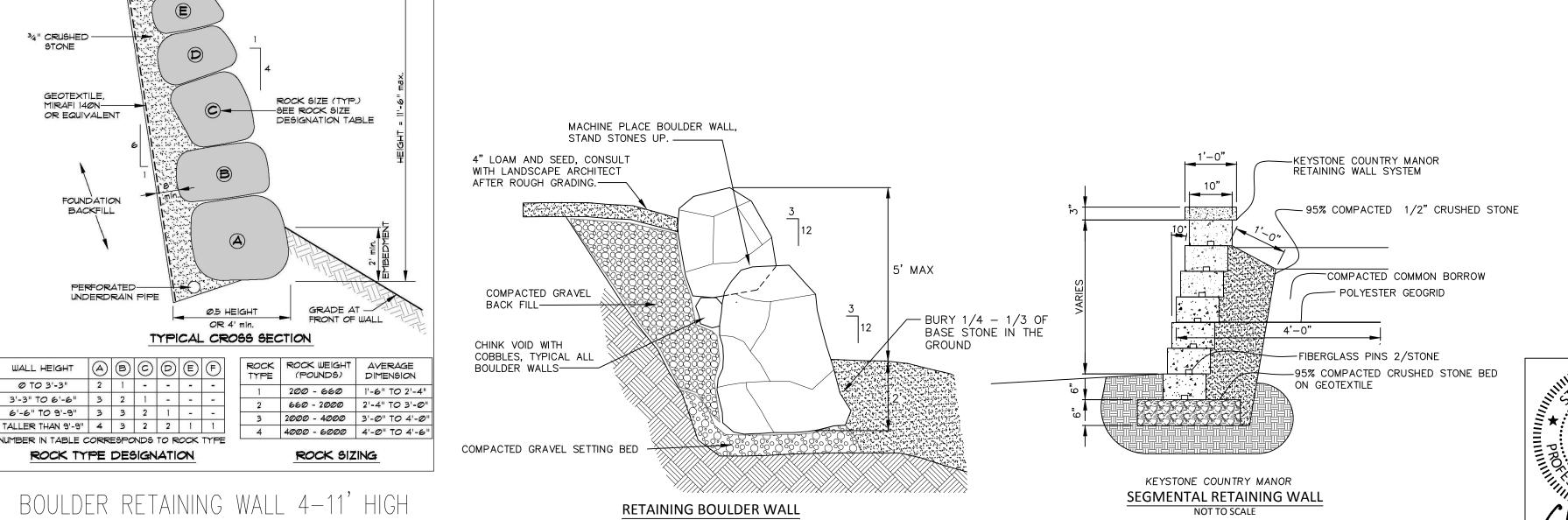
34" CRUSHED -

NOT TO SCALE

TRENCH REPAIR TO MEET TOWN OF CUMBERLAND DPW REQUIREMENTS

PAVEMENT BUTT JOINT DETAIL BITUMINOUS CONCRETE

NOT TO SCALE



NOT TO SCALE

CSB CSB Respond to Town Memos, Re-submit to Town 2. 2-7-2018 Re-Submit to Town and Maine DEP 1. 1-31-2018

CSB

6. 7-31-2018 No changes this sheet, re-submit to Town

Roof Dripline BMP and Misc. Details

Oceanview at Cumberland 277 Tuttle Road, Cumberland, Maine

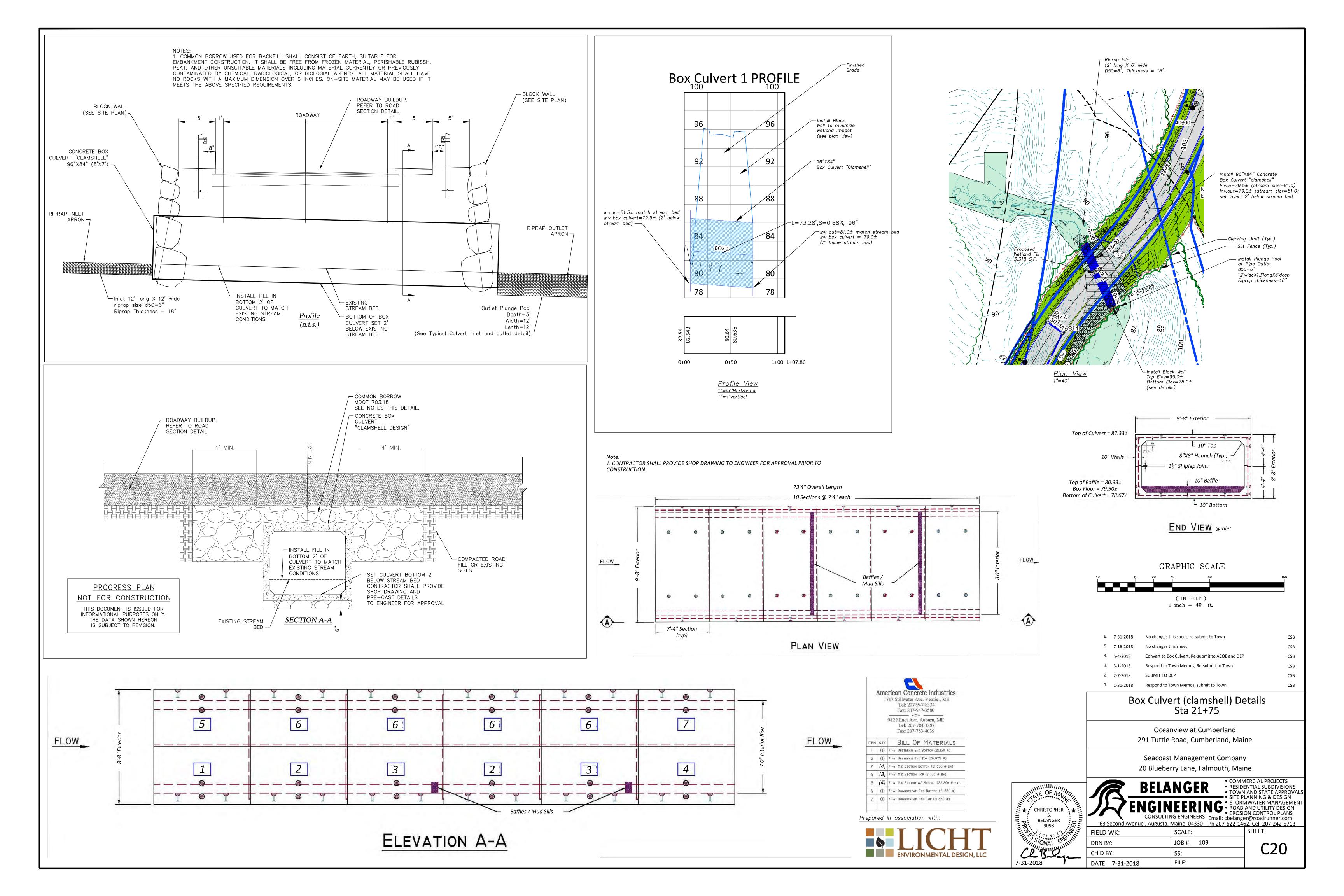
Seacoast Management Company 20 Blueberry Lane, Falmouth, Maine

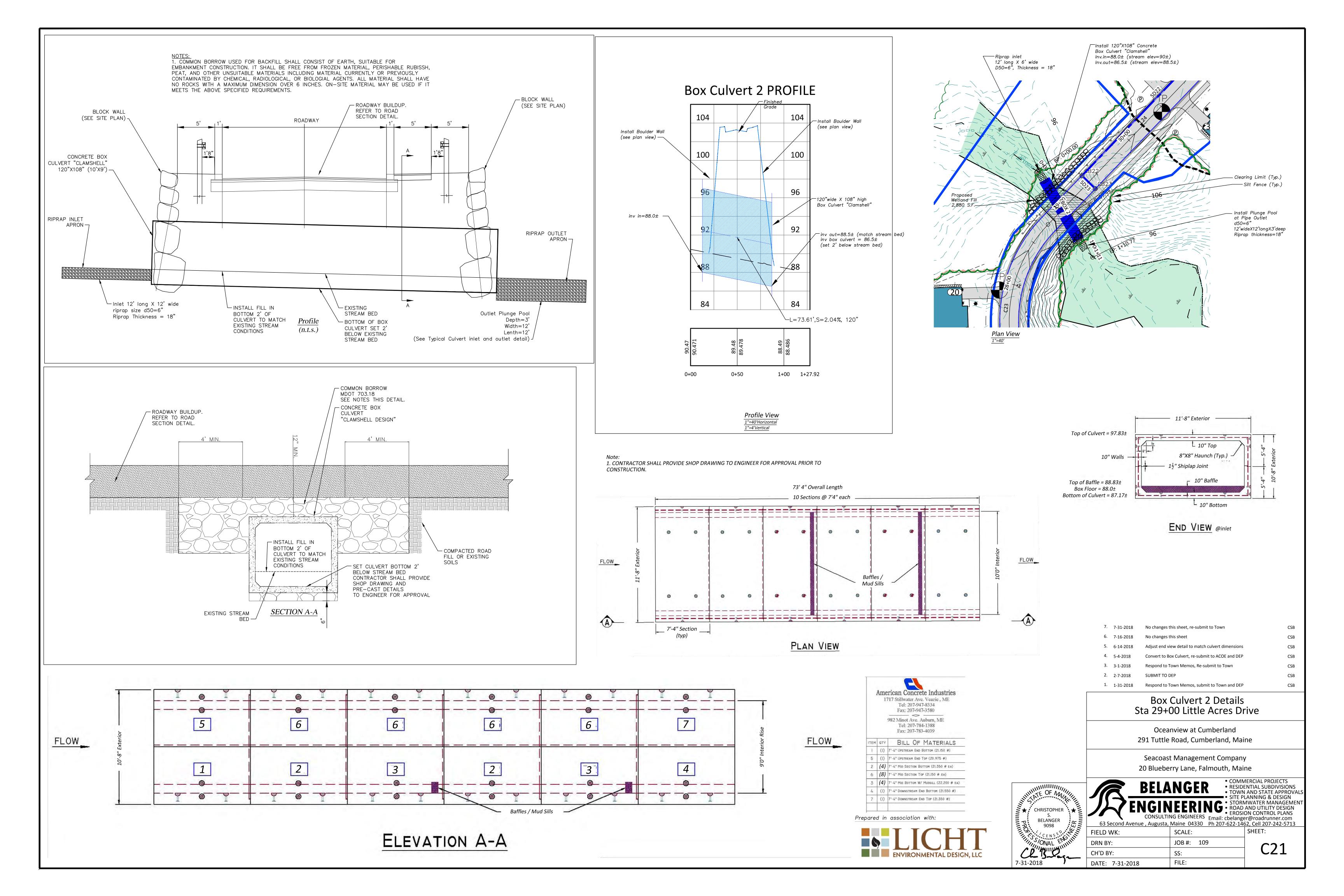


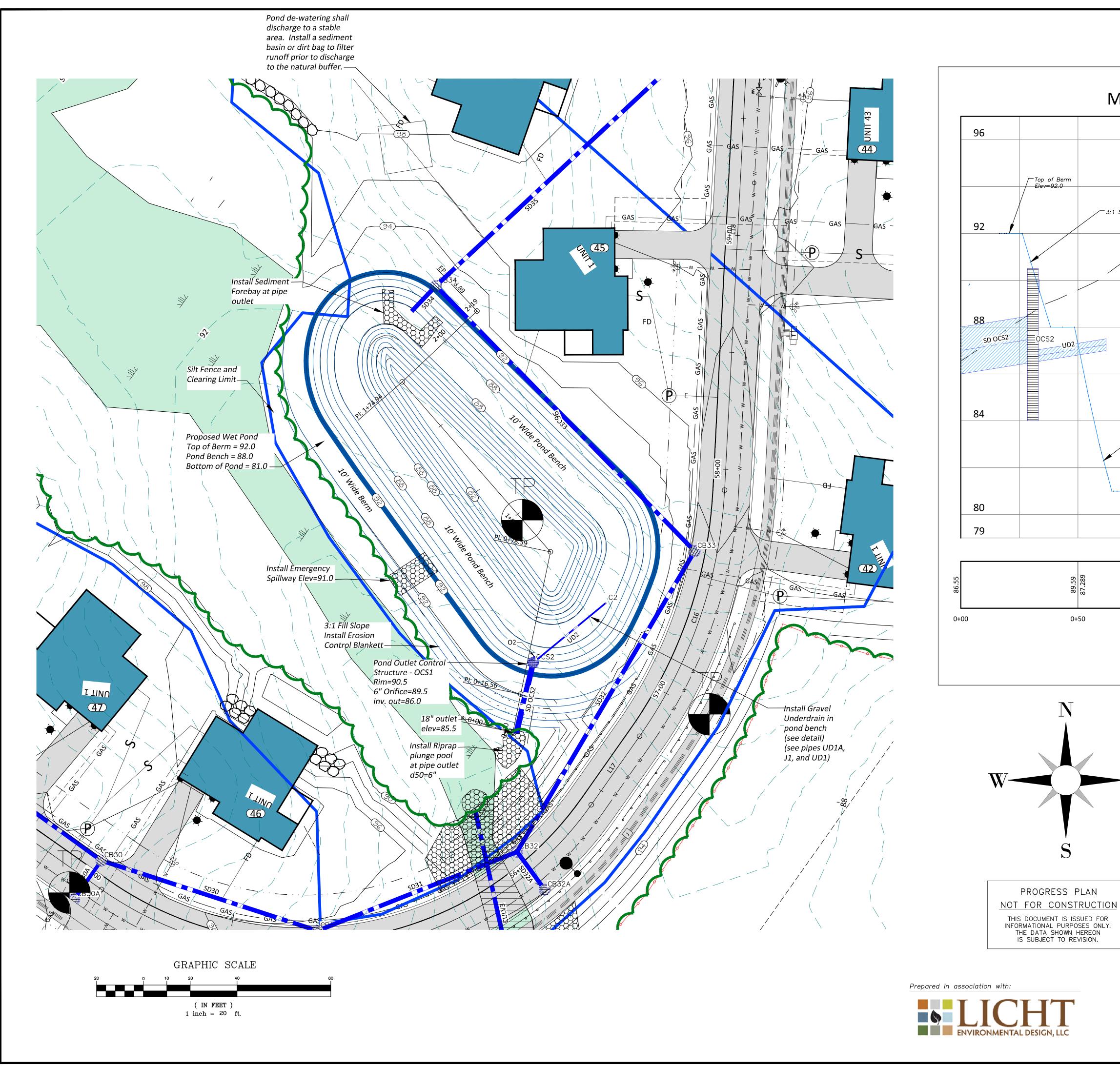
■ • SITE PLANNING & DESIGN CONSULTING ENGINEERS Email: cbelanger@roadrunner.com 63 Second Avenue , Augusta, Maine 04330 Ph 207-622-1462, Cell 207-242-5713 SCALE: JOB #: 109

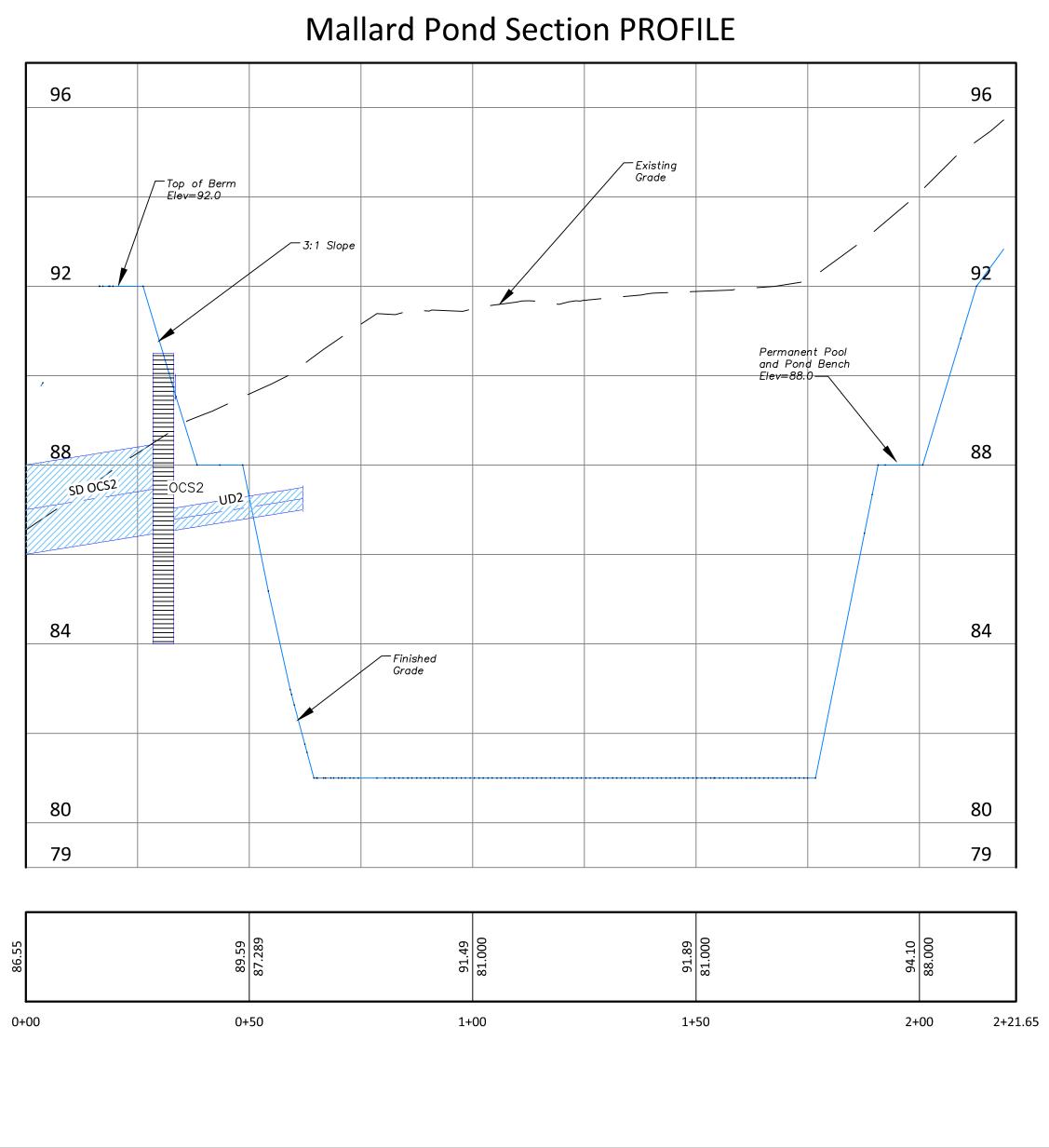
• RESIDENTIAL SUBDIVISIONS

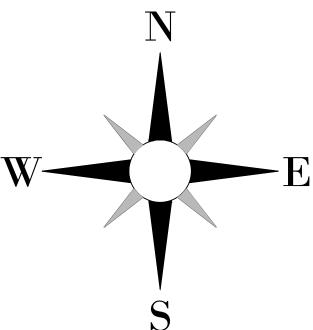
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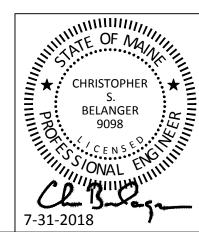


6.	7-31-2018	No changes this sheet, re-submit to Town	CSB
5.	7-16-2018	No changes this sheet	CSB
4.	5-4-2018	No changes this sheet	CSB
3.	3-1-2018	Respond to Town Memos, Re-submit to Town	CSB
2.	2-7-2018	SUBMIT TO DEP	CSB
1.	1-31-2018	Respond to Town Memos, submit to Town and DEP	CSB

Mallard Way Wet Pond Plan and Profile

Oceanview at Cumberland 291 Tuttle Road, Cumberland, Maine

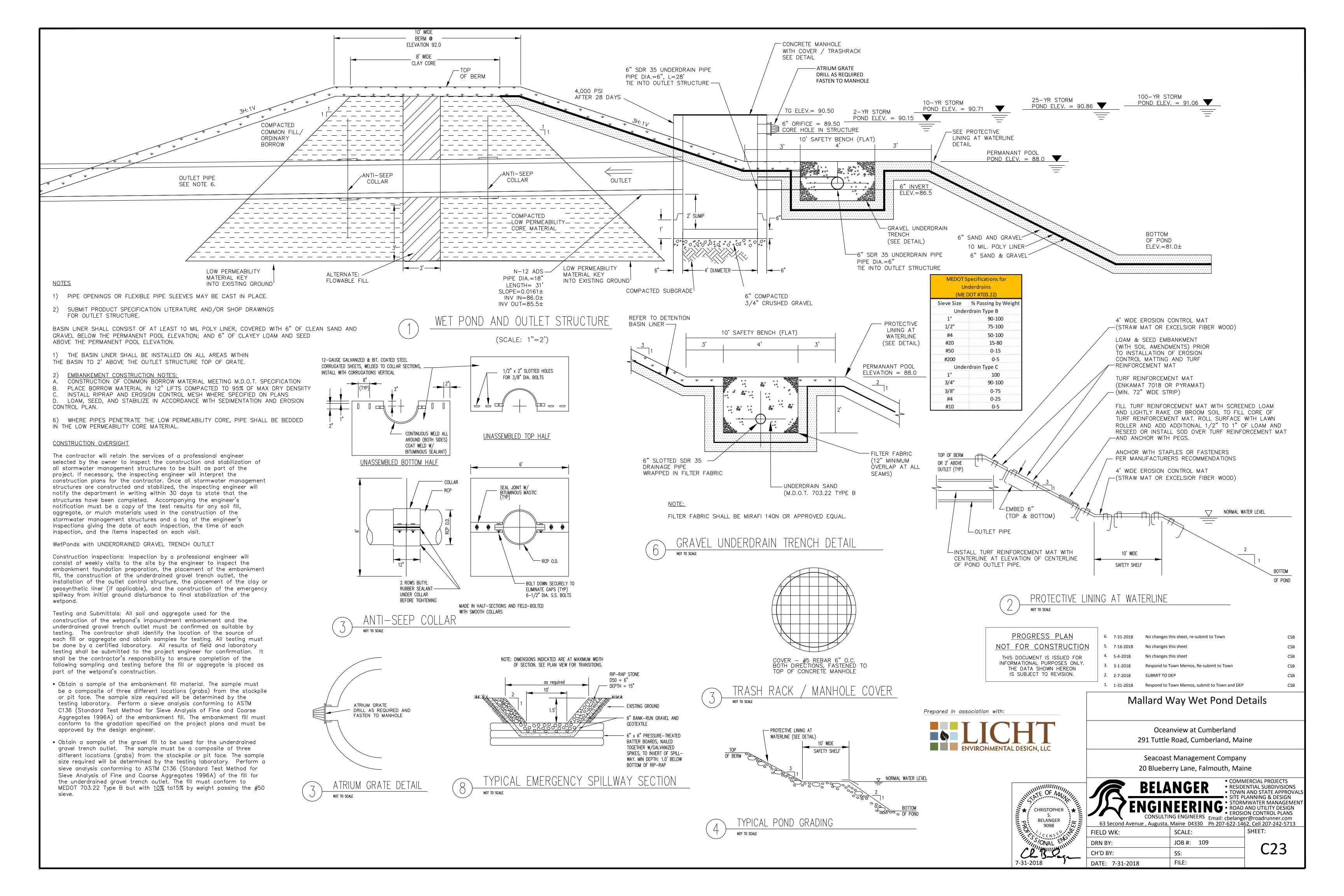
Seacoast Management Company 20 Blueberry Lane, Falmouth, Maine

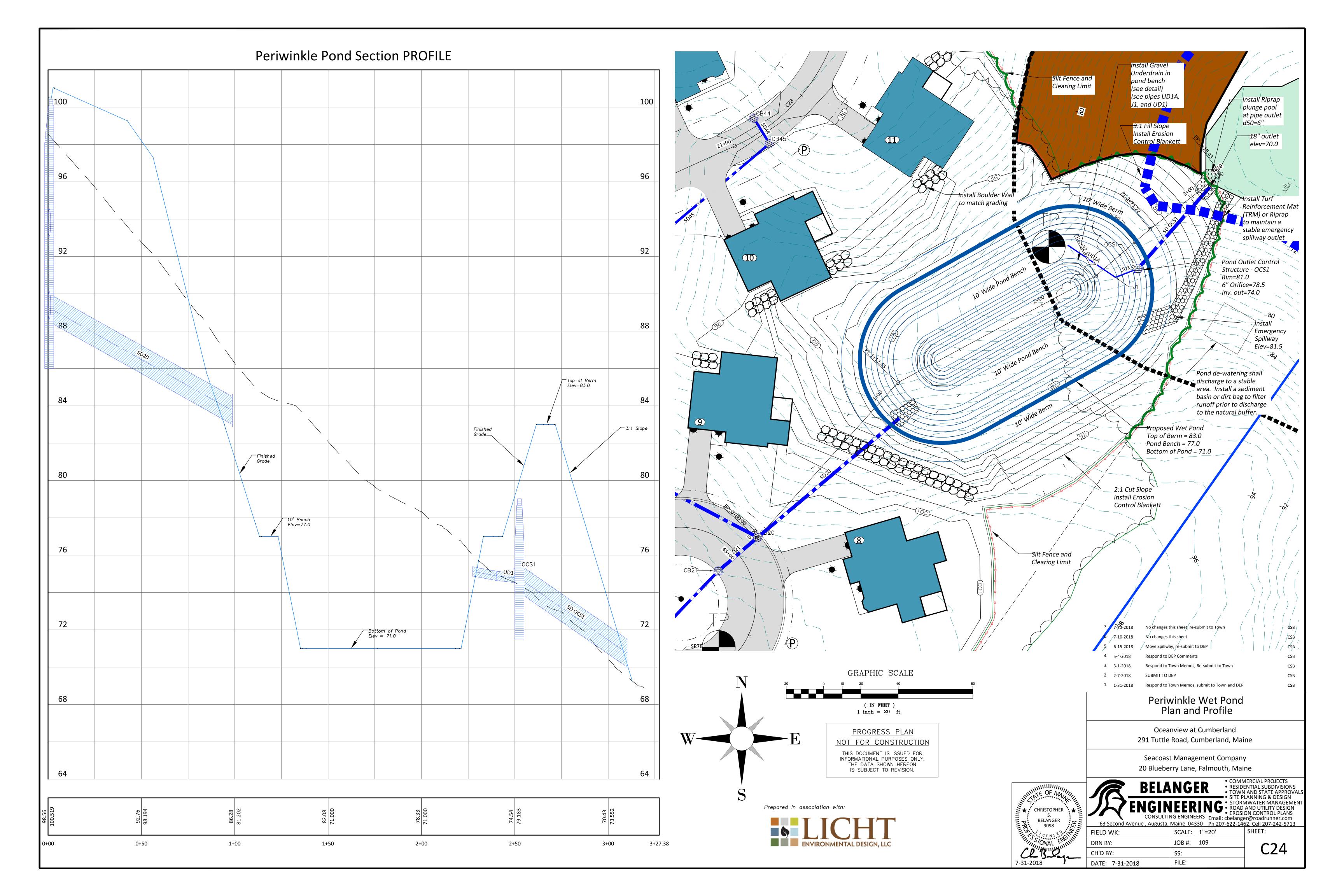


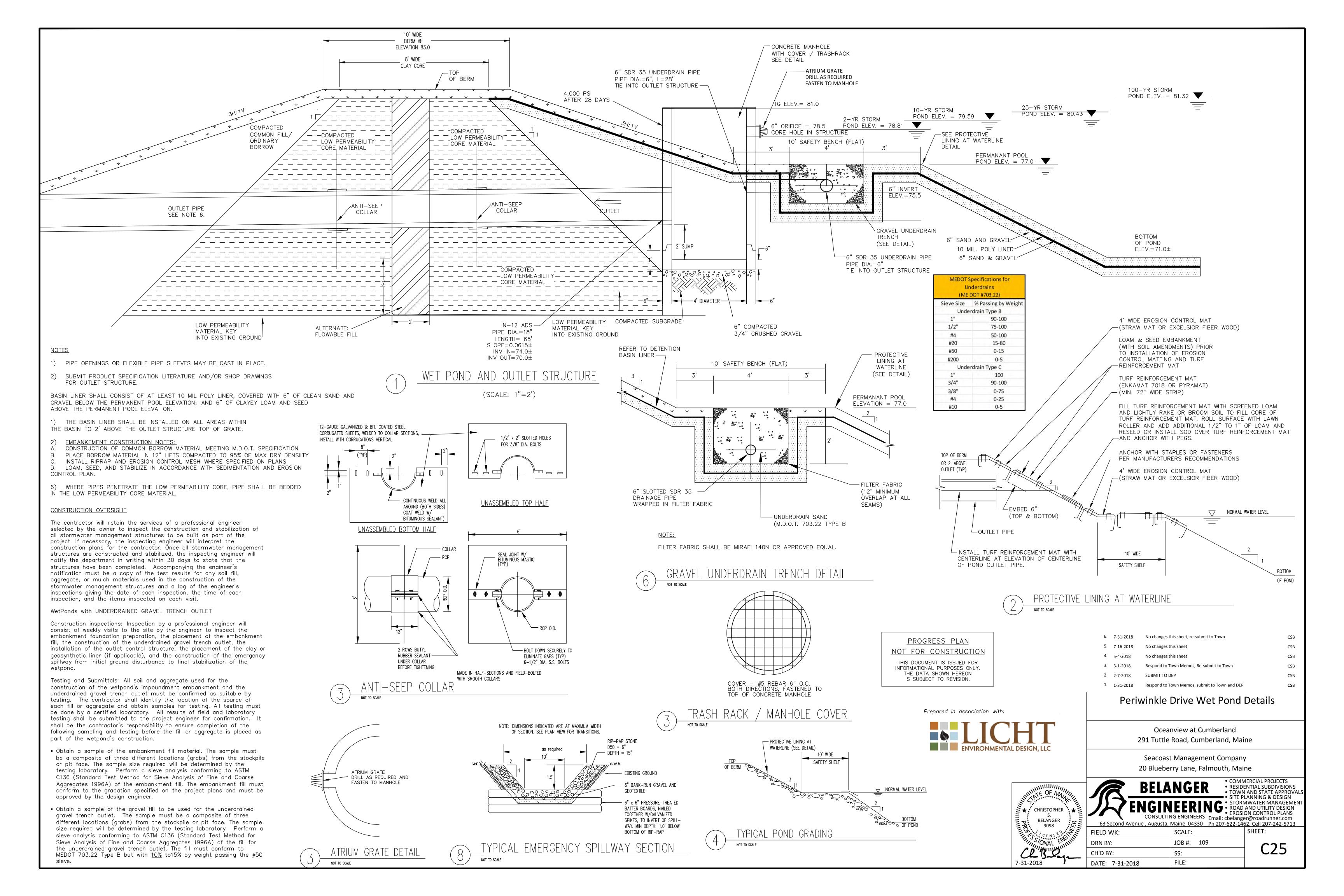
	_	•
	BELANGER	
	ENGINEERII	NG:
63 Second Av	venue , Augusta, Maine 04330	Ph 207-6

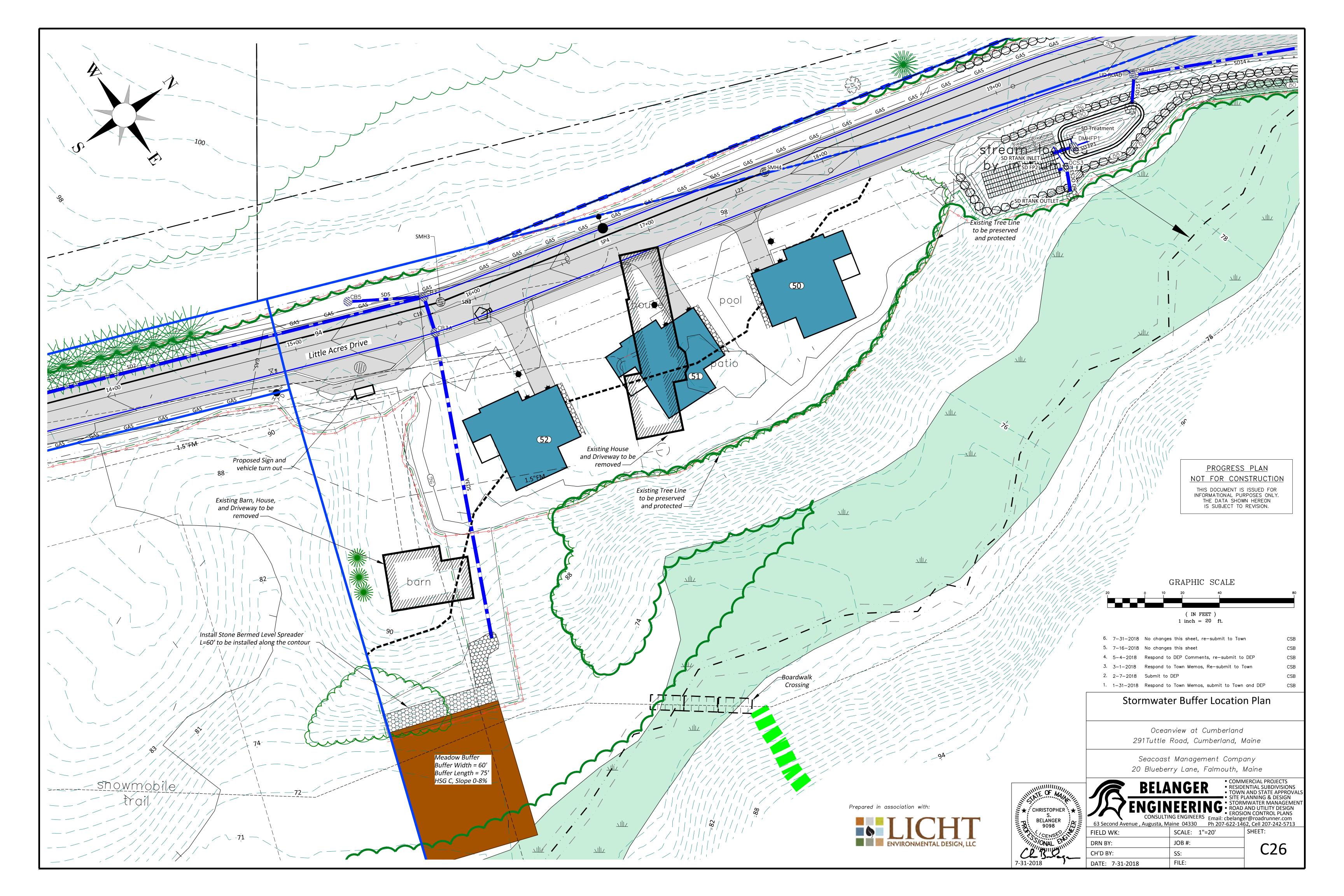
COMMERCIAL PROJECTS
RESIDENTIAL SUBDIVISIONS
TOWN AND STATE APPROVALS
SITE PLANNING & DESIGN
STORMWATER MANAGEMENT
ROAD AND UTILITY DESIGN
EROSION CONTROL PLANS
I: cbelanger@roadrunner.com
17.622.1462. Cell 207.242.5713

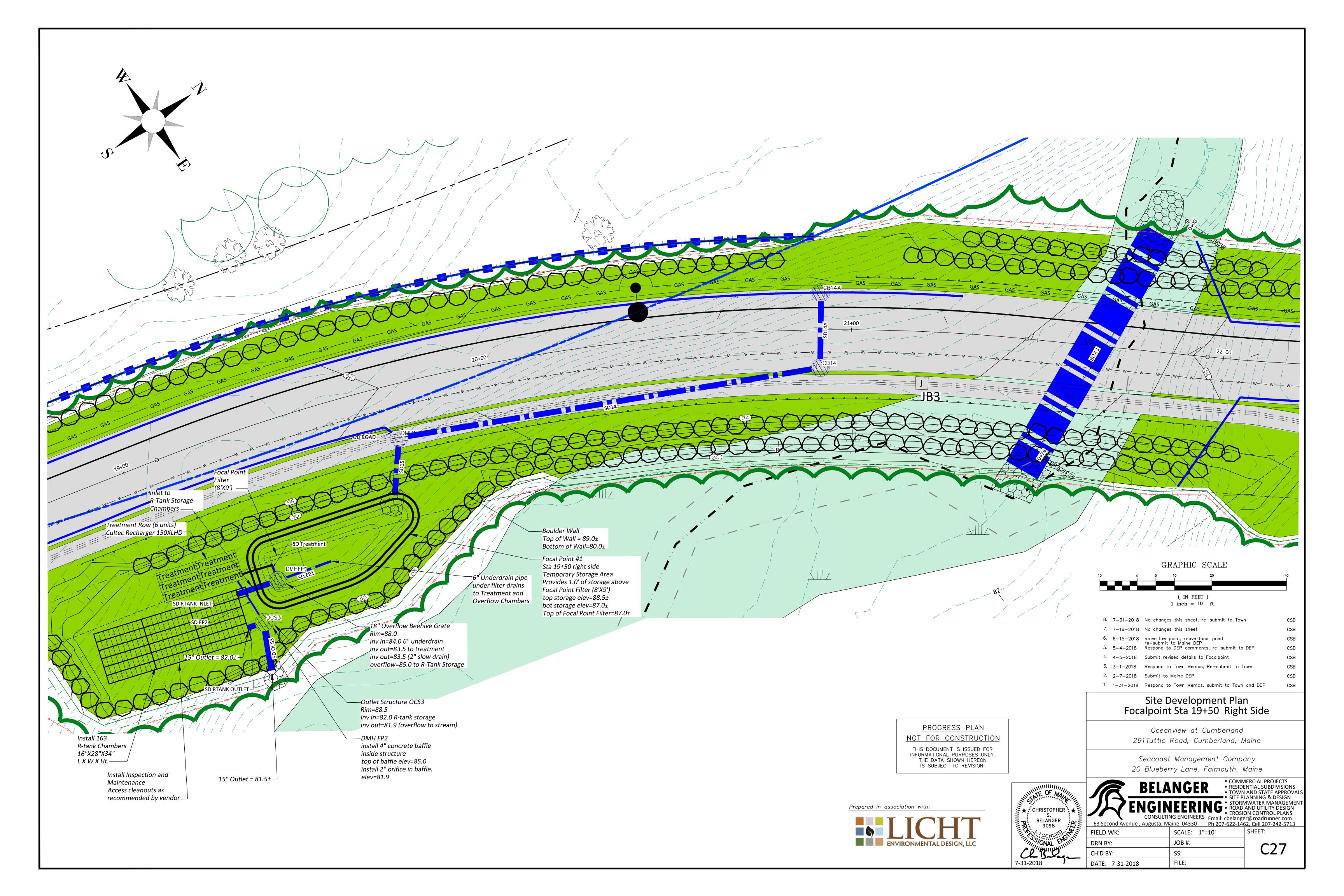
63 Second Avenue , Augusta,	Maine 04330 Ph 207-622-14	62, Cell 207-242-5713
FIELD WK:	SCALE: 1"=20'	SHEET:
DRN BY:	JOB #: 109	C22
CH'D BY:	SS:	CZZ
DATE: 7-31-2018	FILE:	

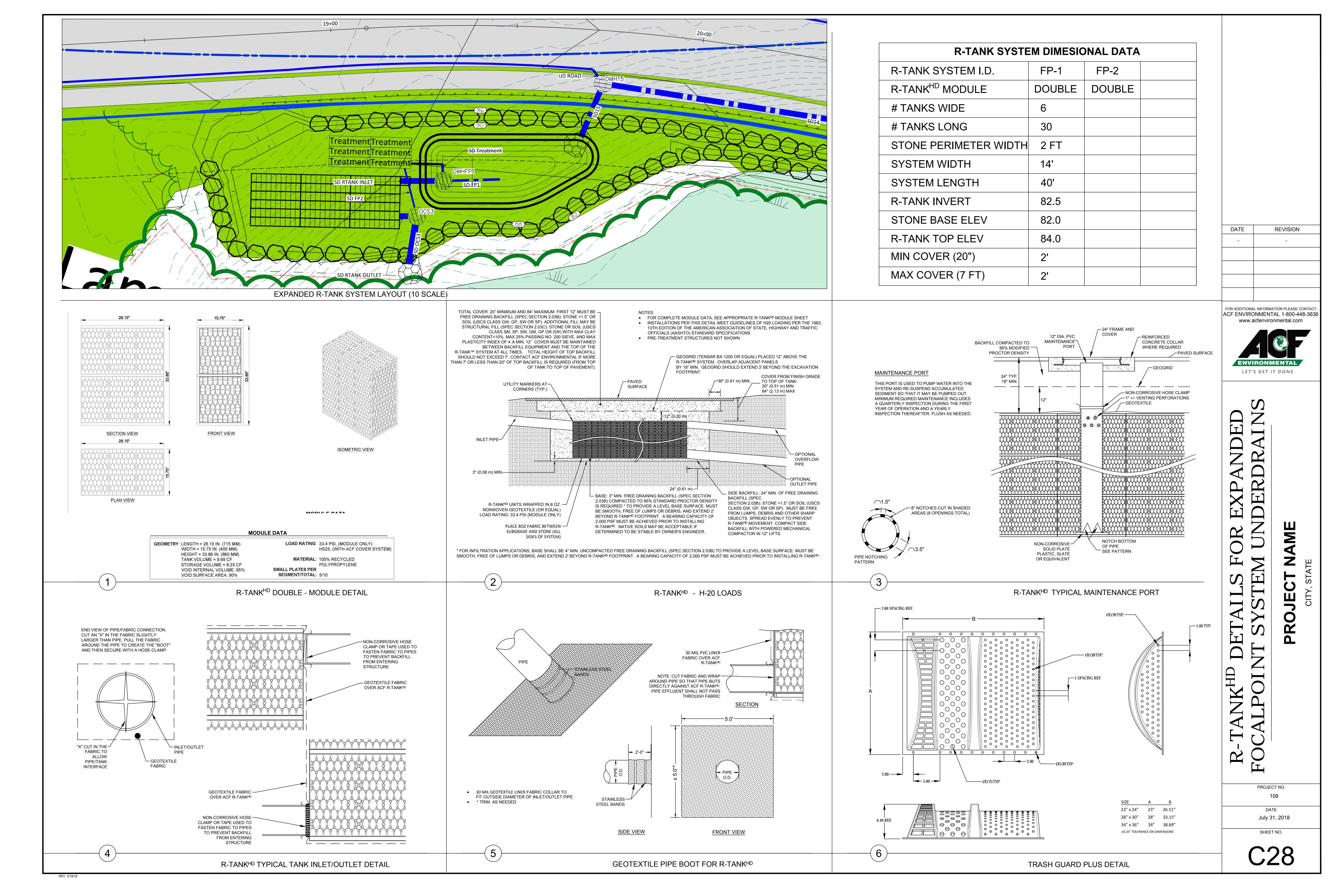


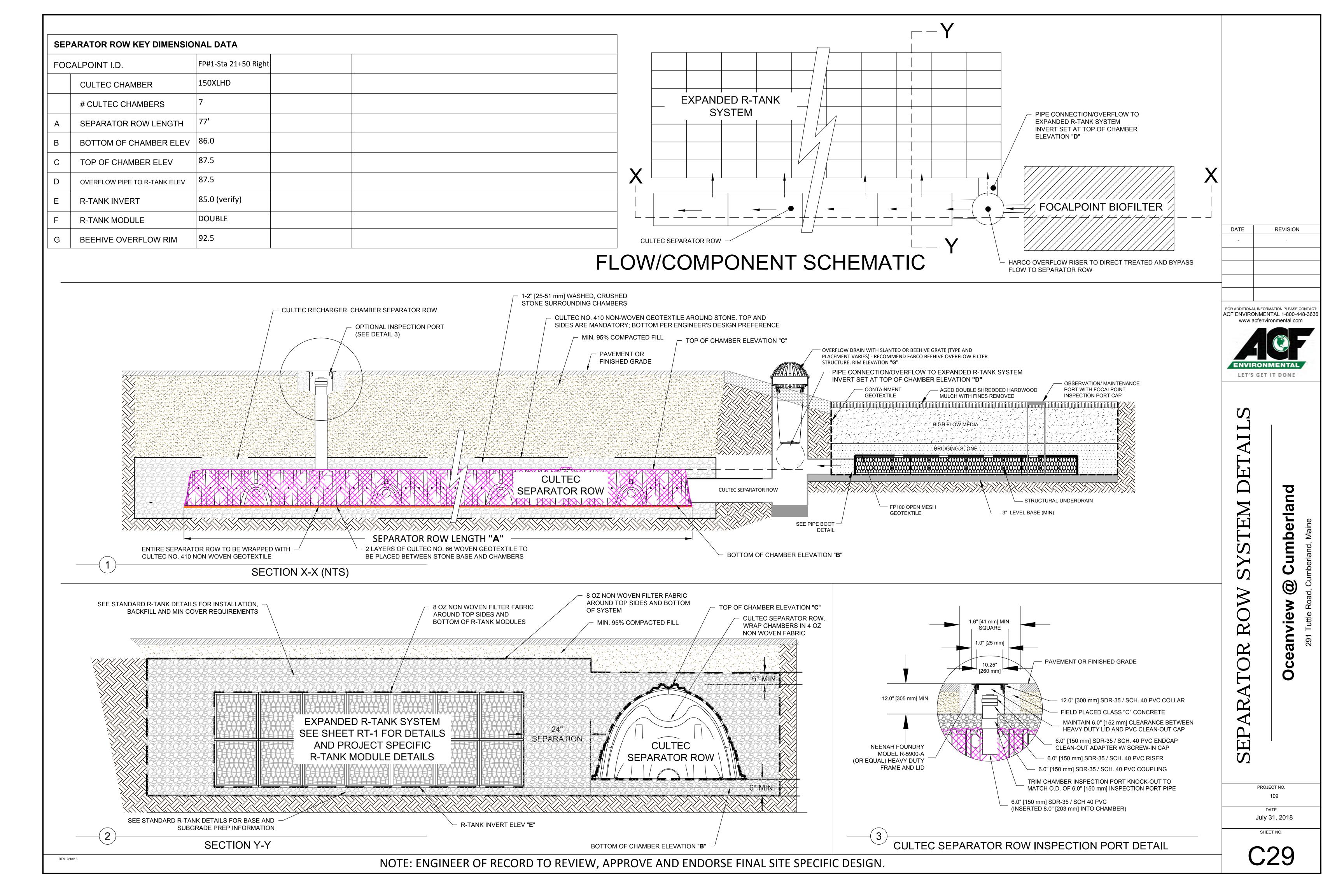




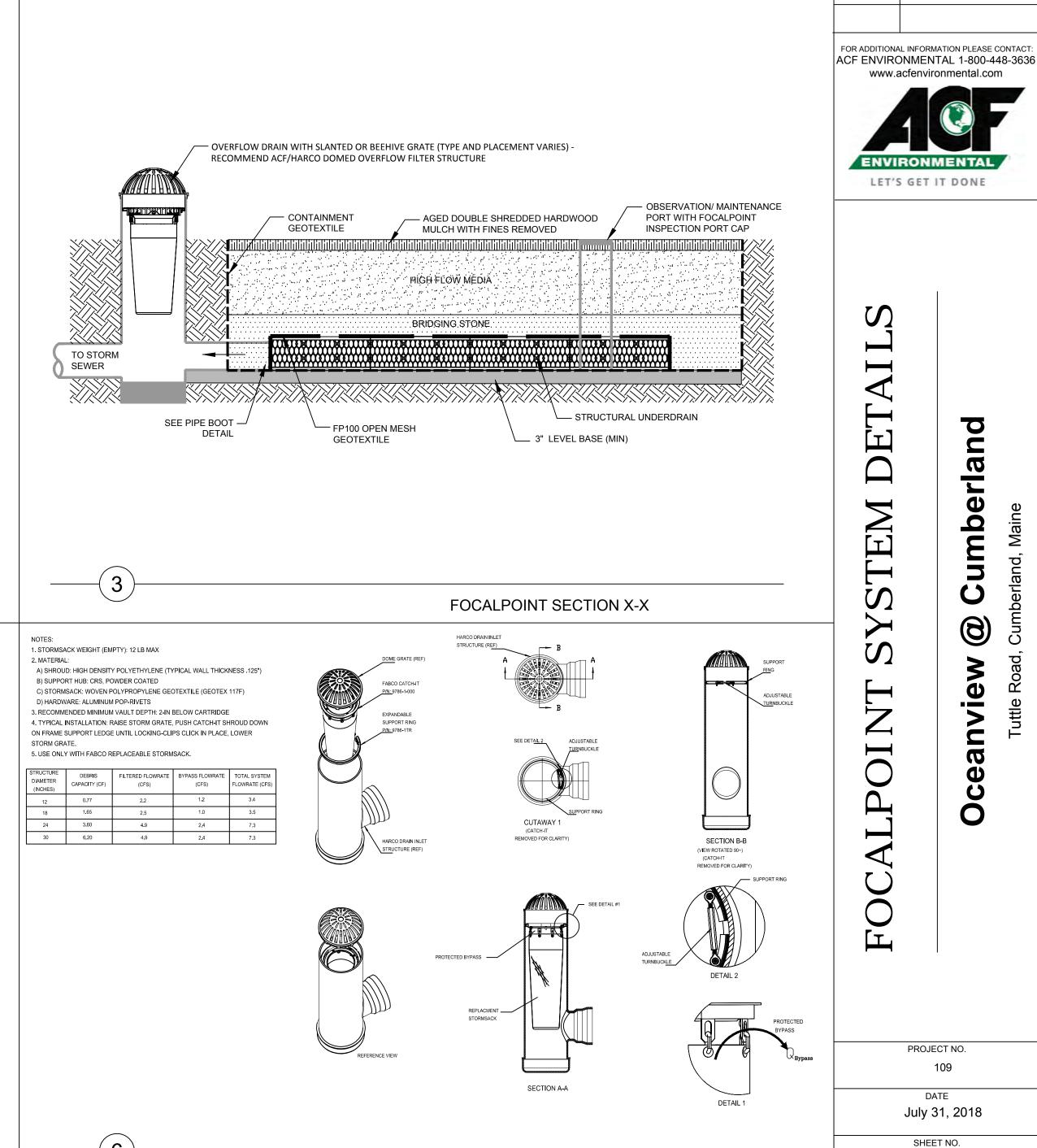


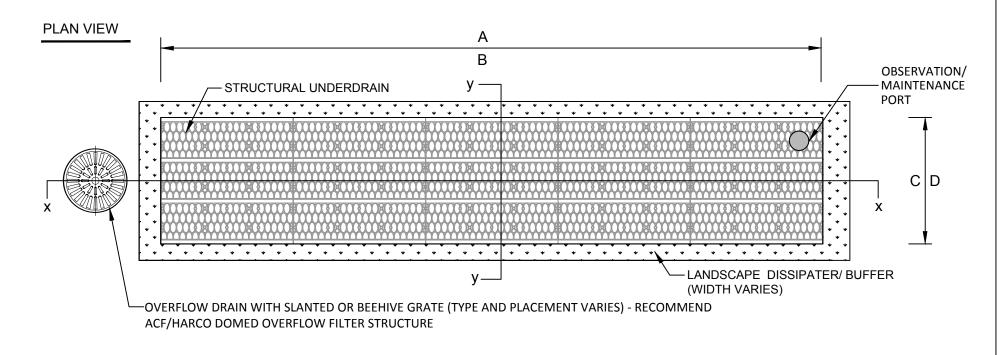


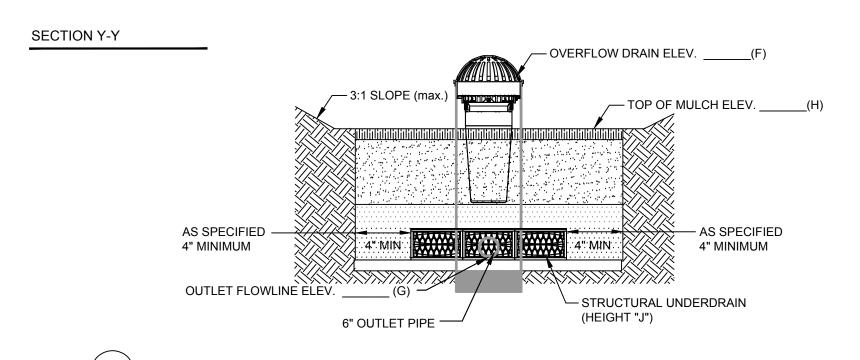




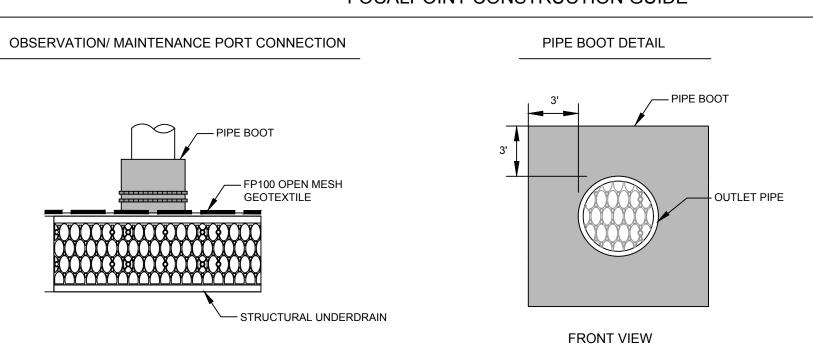
FOCALPOINT KEY DIMENSIONAL DATA						
FOCALPOINT I.D.		#1-Sta 21+50 Rt.				
Α	FOCALPOINT LENGTH	9'				
В	# UNDERDRAIN LONG	9'				
С	FOCALPOINT WIDTH	8'				
D	# UNDERDRAIN WIDE	3'				
E	WATER QUALITY VOLUME	1350 c.f.				
F	OVERFLOW ELEVATION	88.0				
G	OUTLET FLOWLINE	84.0				
Н	TOP OF MULCH	88.5				
J	UNDERDRAIN HEIGHT	MINI				

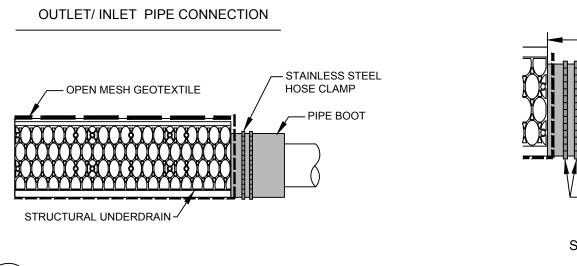






FOCALPOINT CONSTRUCTION GUIDE

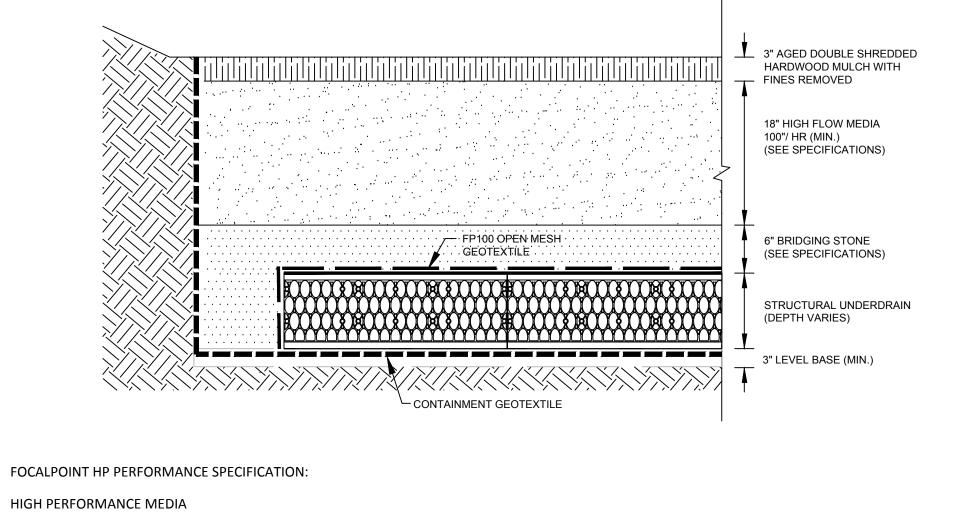




REV 3/18/16

— STAINLESS STEEL HOSE SIDE VIEW

FOCALPOINT PIPE CONNECTION DETAIL



HIGH PERFORMANCE MEDIA MUST MEET A MINIMUM OF 100" PER HOUR INFILTRATION RATE. HIGH PERFORMANCE STRUCTURAL UNDERDRAIN MUST HAVE A MINIMUM OF 19 SQUARE INCHES OF ORIFICE OPENING PER SQUARE FOOT. MUST MEET H20 LOADING REQUIREMENTS. MUST BE MODULAR IN NATURE AND ASSEMBLED ON SITE. MUST HAVE MINIMUM 90% INTERIOR VOID SPACE.

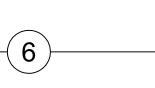
PORT USED FOR INSPECTION PURPOSES AND FOR SYSTEM MAINTENANCE AS

OBSERVATION/ MAINTENANCE PORT

FOCALPOINT DETAILED CROSS SECTION

REQUIRED. WATER SHALL BE PUMPED INTO THE SYSTEM AND RESUSPEND OBSERVATION/ MAINTENANCE PORT WITH ACCUMULATED SEDIMENT. MINIMUM REQUIRED MAINTENANCE INCLUDES A FOCALPOINT INSPECTION PORT CAP QUARTERLY INSPECTION FOR THE FIRST YEAR OF OPERATION AND A YEARLY INSPECTION THEREAFTER FLUSH AS NEEDED. 6" PVC MAINTENANCE PORT -STAINLESS STEEL GEOTEXTILE PIPE BOOT ___ - NOTCH PATTERN AT BOTTOM OF PIPE (SEE NOTCH PATTERN DETAIL) PIPE NOTCH PATTERN DETAIL

FOCALPOINT OBSERVATION PORT DETAIL



ACF/HARCO DOMED OVERFLOW FILTER RISER

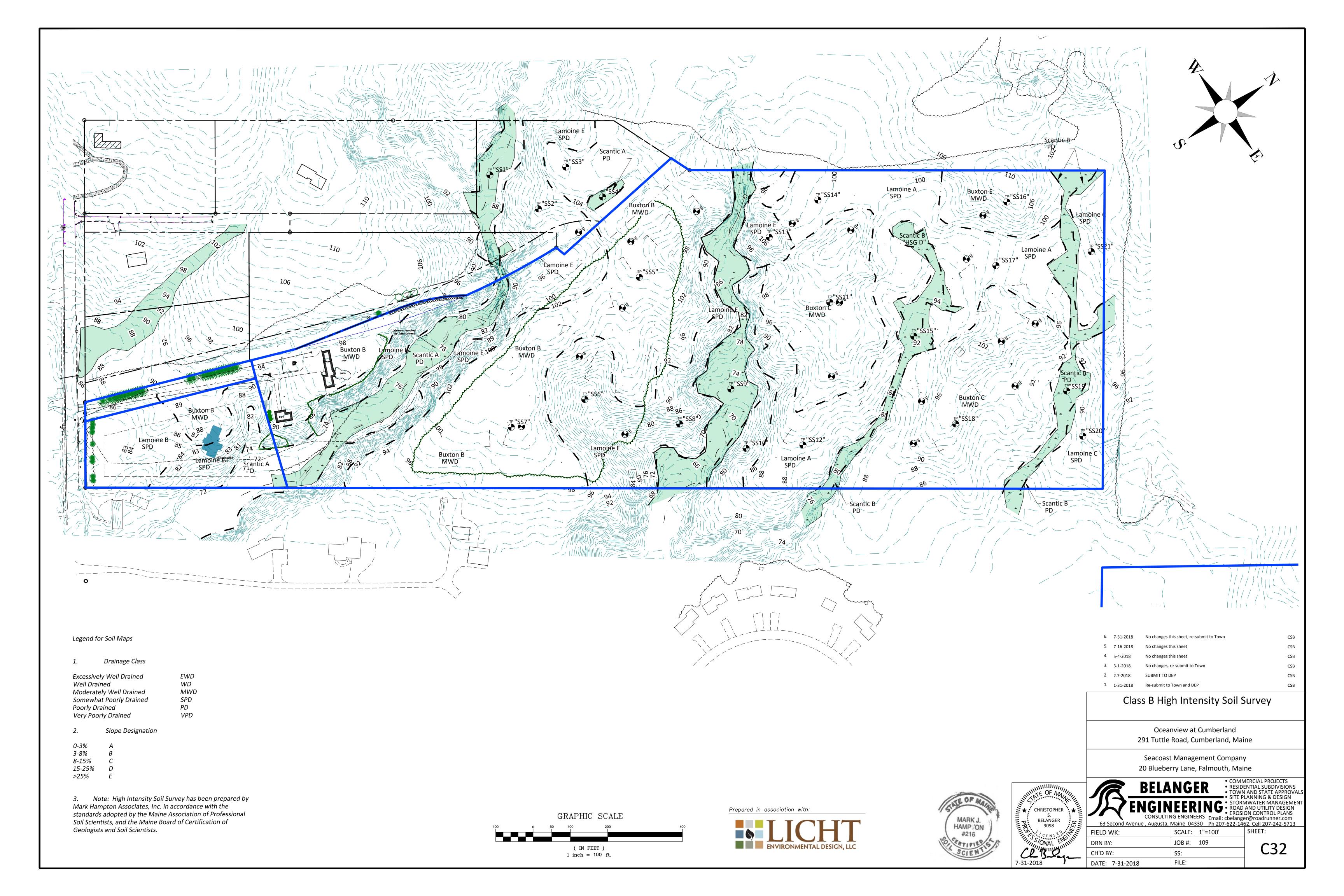
PROJECT NO. 109

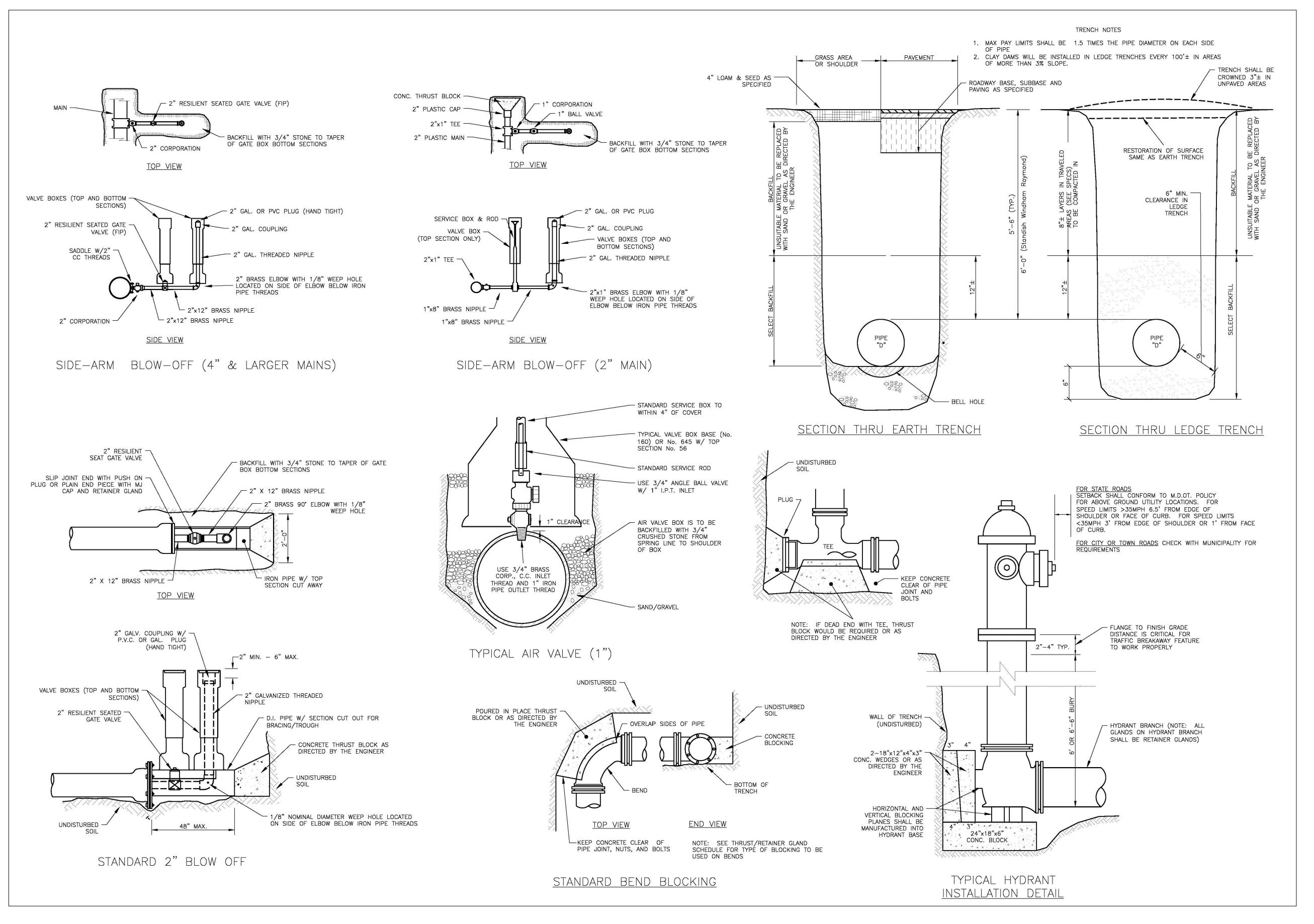
July 31, 2018

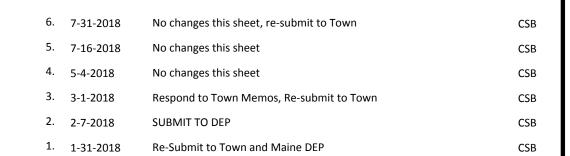
DATE

REVISION

NOTE: ENGINEER OF RECORD TO REVIEW, APPROVE AND ENDORSE FINAL SITE SPECIFIC DESIGN.



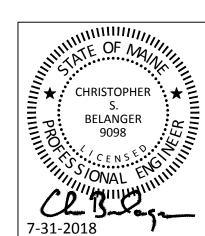




PORTLAND WATER DISCRICT STANDARD DETAILS 1

Oceanview at Cumberland 277 Tuttle Road, Cumberland, Maine

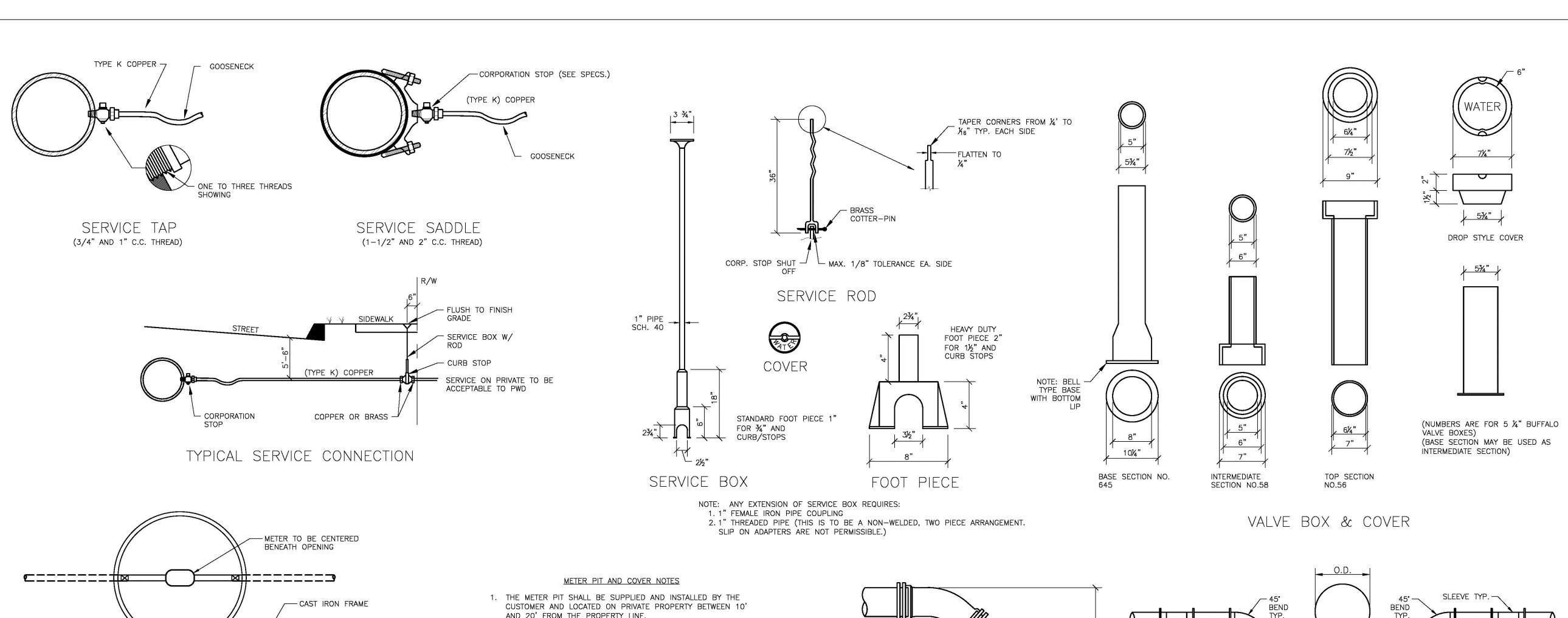
Seacoast Management Company 20 Blueberry Lane, Falmouth, Maine

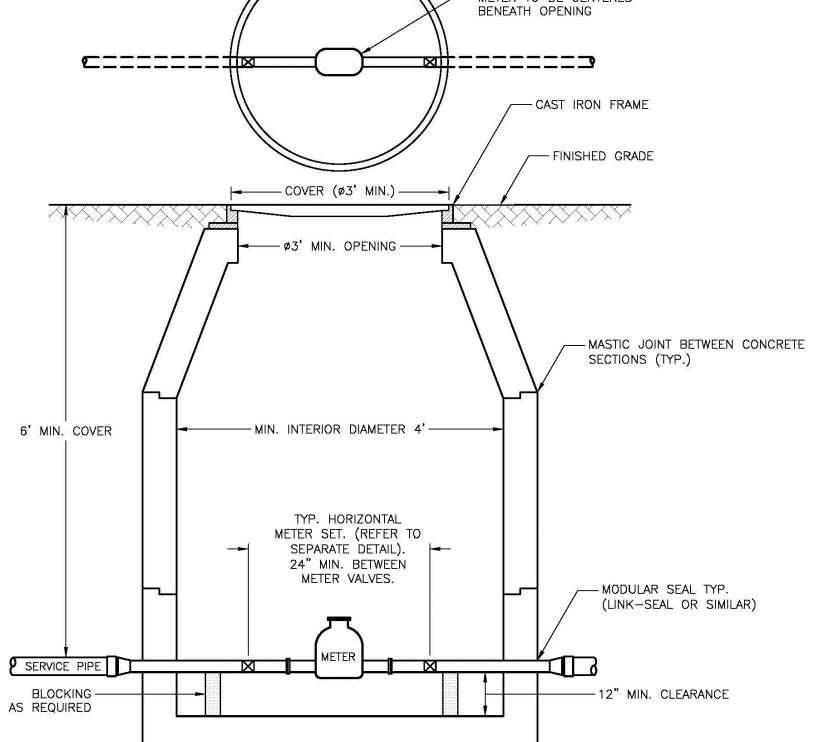


				• COMM	TERCIAL PROJECTS	
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				TOWN	AND STATE APPR	OVALS
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	"	ENGIN	IFFDII	■ • STORN	лwater managi	EMENT
1		ENGIN	IEEKIN	• ROAD	AND UTILITY DESI	GN
				- LIVOSIV	ON CONTINUE I LA	113
_	_		NG ENGINEERS	Email: cbelange	er@roadrunner.co	m
	63 Second	Avenue, Augusta,	Maine 04330	Ph 207-622-146	52, Cell 207-242-5	713

SITE PLANNING & DESIGN
STORMWATER MANAGEMENT **ROAD AND UTILITY DESIGN** EROSION CONTROL PLANS pelanger@roadrunner.com 622-1462, Cell 207-242-5713 SHEET: SCALE:

FIELD WK: DRN BY: JOB #: 109 C33 CH'D BY: SS: FILE: DATE: 7-31-2018



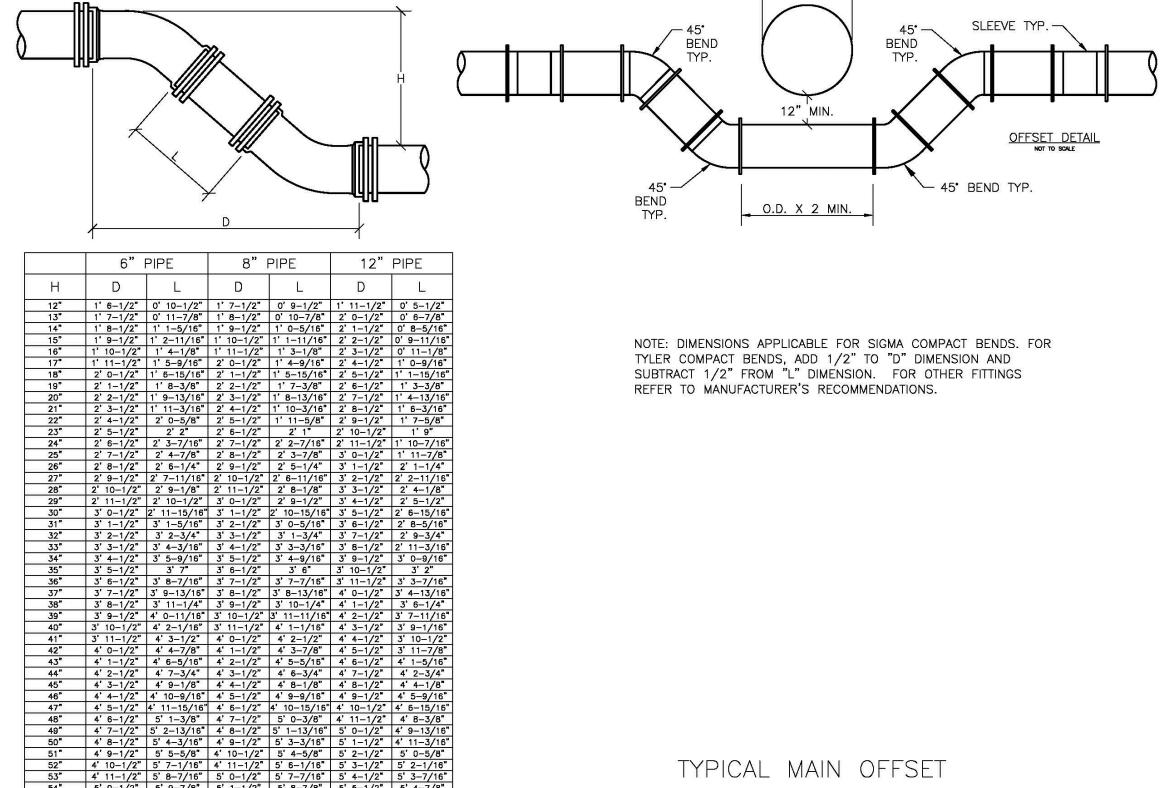


TYPICAL SMALL METER PIT (%" TO 2" METER)

- AND 20' FROM THE PROPERTY LINE.
- 2. THE METER PIT SHALL BE MADE OF PRECAST CONCRETE OF SUFFICIENT SIZE TO PROVIDE 5.5' MINIMUM GROUND COVER FROM FINISHED GRADE TO THE TOP OF THE SERVICE PIPE. ANY SEAMS BETWEEN CONCRETE SECTIONS SHALL BE SEALED WITH MASTIC JOINT. ALL OPENINGS IN THE CONCRETE FOR SERVICE PIPING SHALL BE SEALED WITH A MODULAR SEAL (LINK-SEAL OR SIMILAR).
- 3. THE INTERIOR OF THE METER PIT SHALL BE A MINIMUM OF 4' IN DIAMETER, AND THE METER PIT OPENING SHALL BE A MINIMUM OF 30" IN DIAMETER WITH A CAST IRON FRAME. THE METER PIT COVER SHALL BE CAST IRON, 32" MINIMUM IN DIAMETER, AND BE EITHER PERMANENTLY LABELED "WATER" OR HAVE NO LABEL. ANY STEEL PLATE MATERIAL SHALL BE COATED WITH A RUST INHIBITOR PAINT.
- 4. WALL-MOUNTED LADDER RUNGS SHALL NOT BE INSTALLED WITHIN METER PIT.
- 5. ALL PIPING INSIDE AND EXTENDING THROUGH THE METER PIT SHALL BE MADE OF COPPER, WITH A MINIMUM OF 6" CLEARANCE FROM THE METER PIT FLOOR. BLOCKING SHALL BE INSTALLED AS REQUIRED TO SUPPORT THE PIPE.
- 6. CUSTOMER SHALL ENSURE THE METER PIT AND COVER ARE PROPERLY RATED FOR TRAFFIC FLOW, IF APPLICABLE.

METER NOTES

- 7. ONLY PWD PERSONNEL ARE AUTHORIZED TO INSTALL WATER METERS. PWD PERSONNEL ARE ADDITIONALLY AUTHORIZED TO OPERATE METER VALVES AS NEEDED FOR INSTALLATION AND
- 8. PWD WILL SUPPLY THE WATER METER. ALL OTHER FITTINGS, INCLUDING A METER RESETTER FOR 1" OR SMALLER METERS, SHALL BE SUPPLIED AND INSTALLED BY CUSTOMER.
- 9. FOR 1.5" AND 2" METERS, CUSTOMER SHALL INSTALL A FLANGED METER SPOOL PIECE, SUPPLIED BY PWD AT NO ADDITIONAL CHARGE, PRIOR TO METER SET. THE METER SPOOL WILL BE MADE AVAILABLE FOR CUSTOMER PICKUP AT PWD CUSTOMER SERVICE, 225 DOUGLASS STREET, PORTLAND DURING NORMAL BUSINESS HOURS.
- 10. CUSTOMER WILL INSTALL TWO BALL VALVES AT LEAST 24" APART FOR METER INSTALLATION, ALLOWING FOR THE WATER METER TO BE CENTERED UNDER THE METER PIT OPENING. THE BALL VALVES SHALL BE SOLDERED IN PLACE.
- 11. THE METER PIT MAY HOUSE UP TO TWO 5/8", 3/4" OR 1" METERS WITH PRIOR APPROVAL FROM PWD.

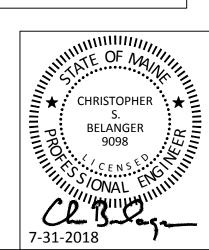


6. 7-31-2018 No changes this sheet, re-submit to Town CSB 5. 7-16-2018 No changes this seet CSB 4. 5-4-2018 CSB No changes this sheet Respond to Town Memos, Re-submit to Town 2. 2-7-2018 SUBMIT TO DEP 1. 1-31-2018 Re-Submit to Town and Maine DEP CSB

PORTLAND WATER DISCRICT STANDARD DETAILS 2

Oceanview at Cumberland 277 Tuttle Road, Cumberland, Maine

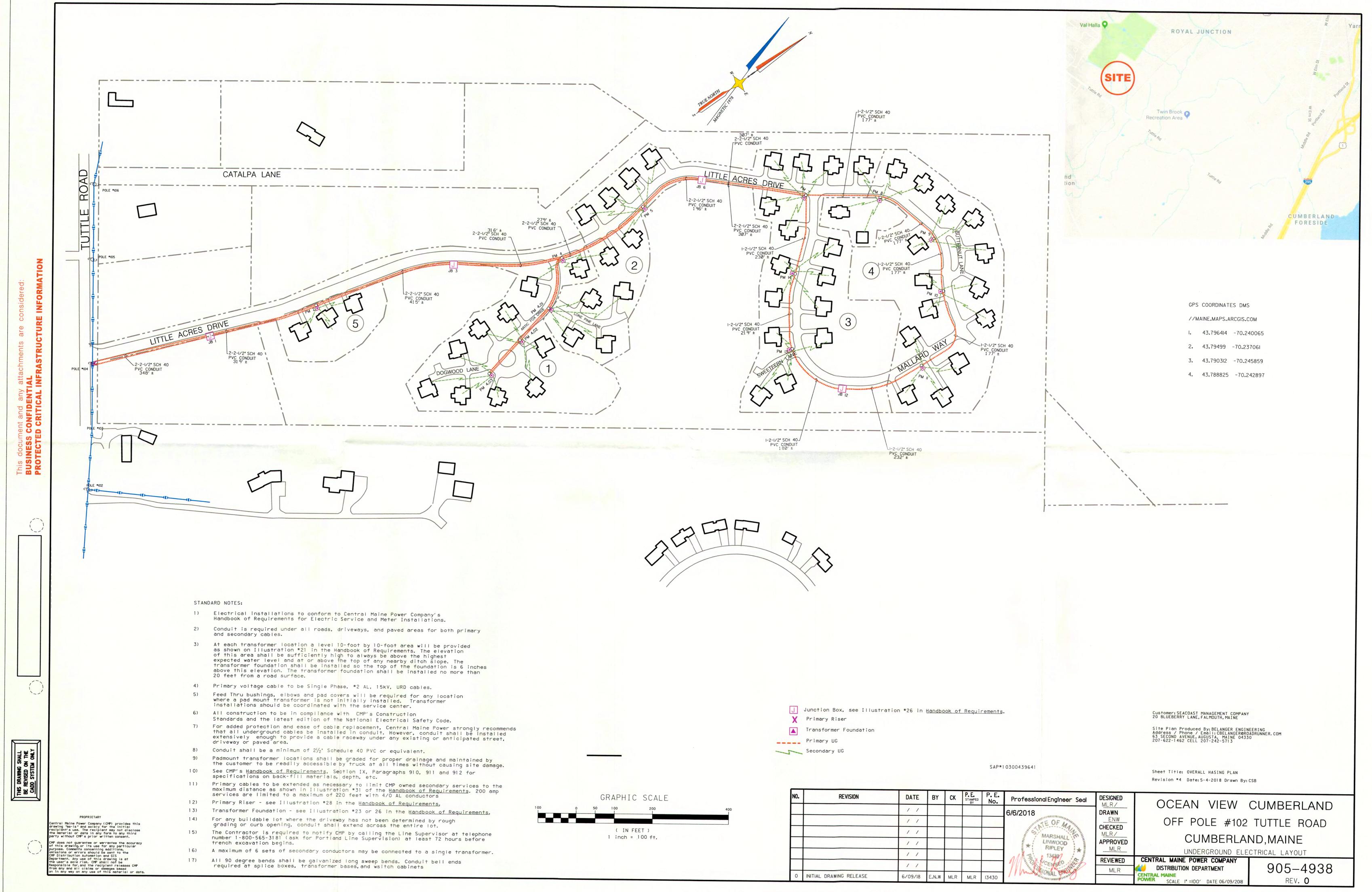
Seacoast Management Company 20 Blueberry Lane, Falmouth, Maine

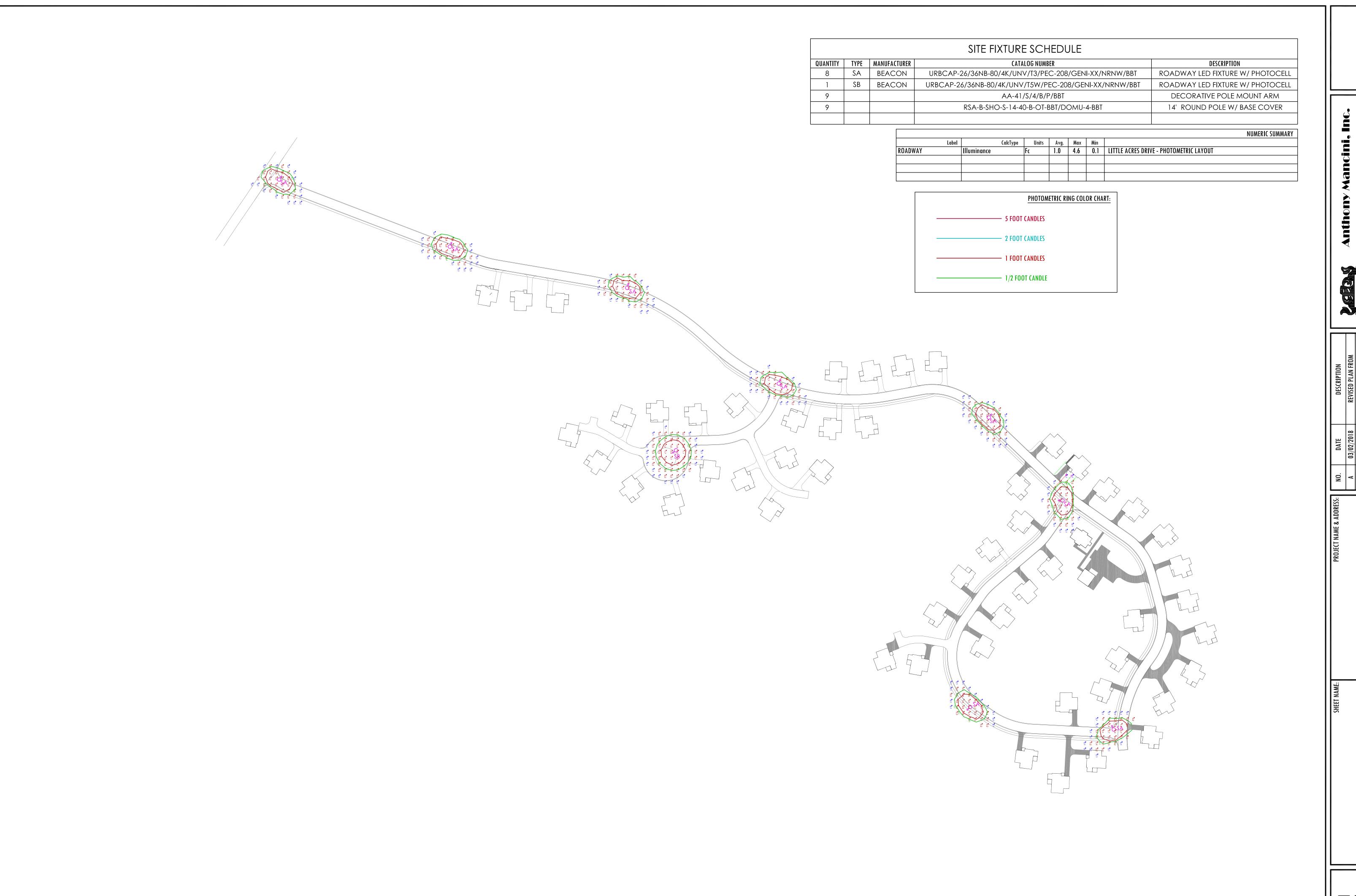


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 COMMERCIAL PROJECTS RESIDENTIAL SUBDIVISIONS TOWN AND STATE APPROVALS SITE PLANNING & DESIGNSTORMWATER MANAGEMENT ROAD AND UTILITY DESIGN • EROSION CONTROL PLANS : cbelanger@roadrunner.com

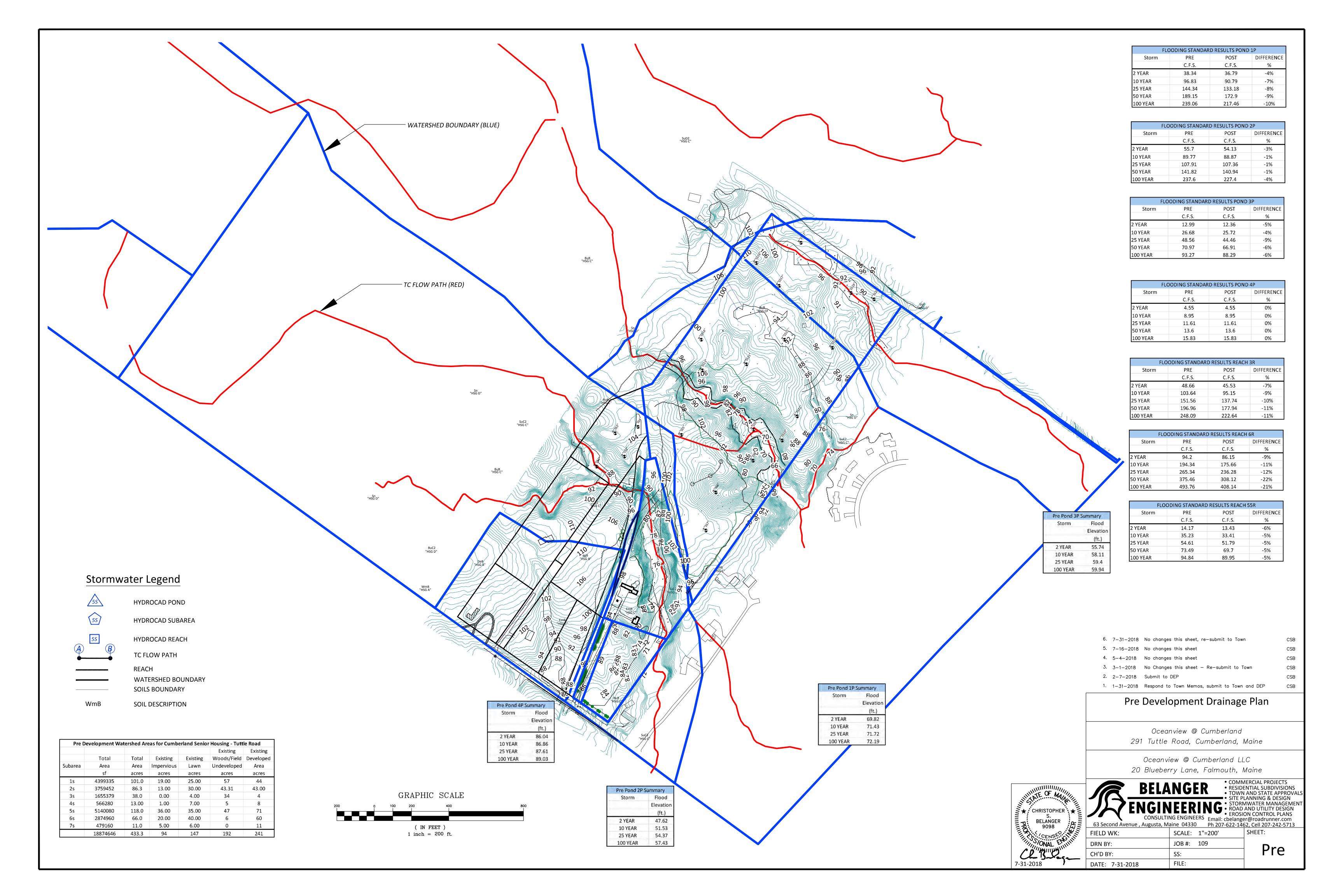
7-622-1462, Cell 207-242-5713 SHEET: SCALE: FIELD WK: JOB #: 109 DRN BY: CH'D BY: SS: FILE: DATE: 7-31-2018

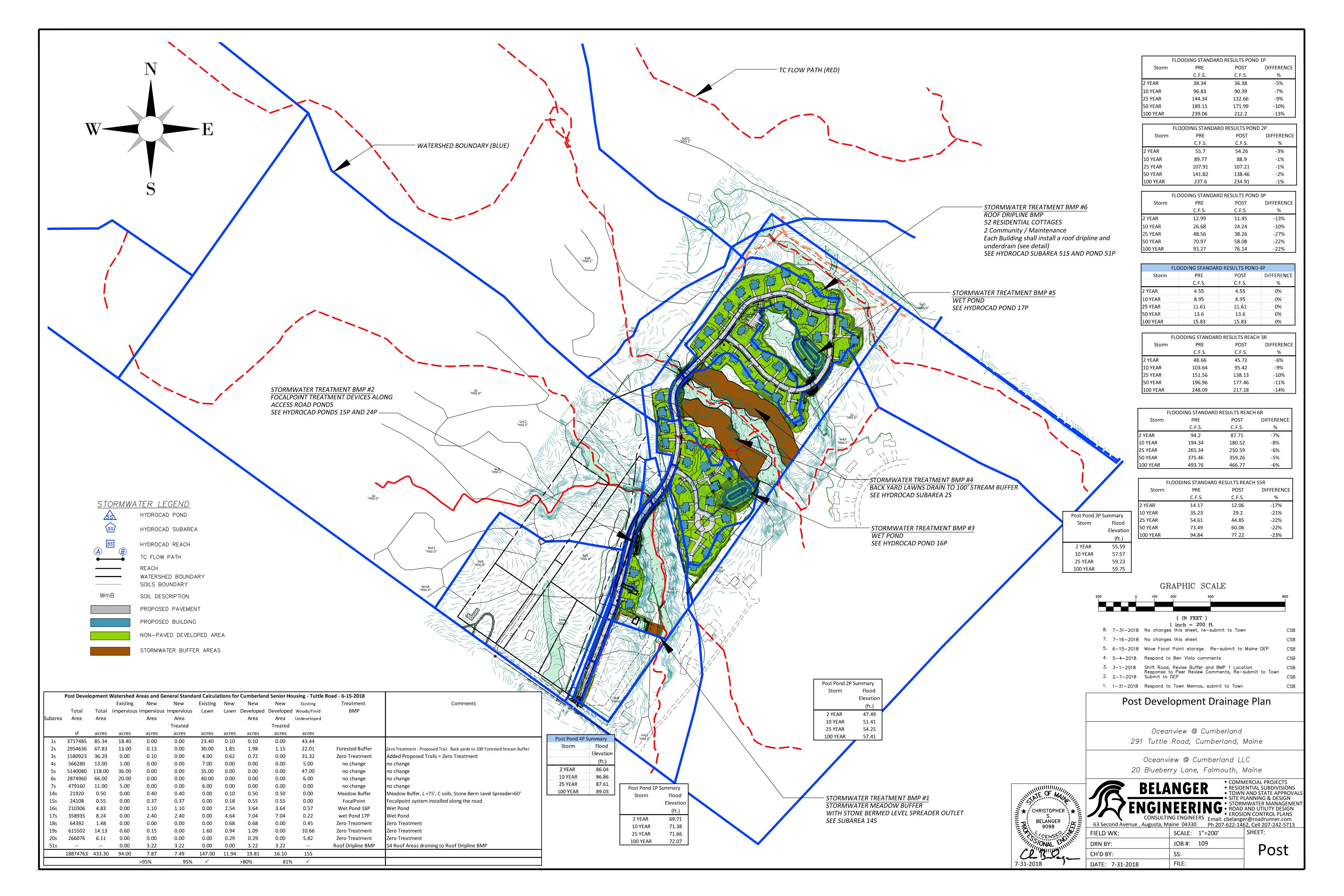






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Maine DEP SLODA Permit Application STORMWATER MANAGEMENT REPORT

Project: OceanView @ Cumberland Expansion Project

Tuttle Road, Cumberland, Maine

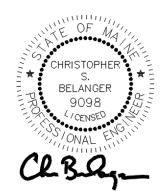


Prepared By:

Belanger Engineering 63 Second Avenue Augusta, ME 04330 207-622-1462

Prepared For:

Seacoast Management Company 20 Blueberry Lane Falmouth, Maine 207-233-4194 - Chris Wasileski



March 1, 2018 Date:

Site Planning and Design Commercial Projects 63 Second Avenue, Augusta, Maine 04330

Road and Utility Design Residential Subdivisions

Stormwater Management Town and State Approvals Phone: (207) 622-1462

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Stormwater Narrative – March 1, 2018 Oceanview @ Cumberland Senior Housing Community

Tuttle Road, Cumberland, Maine

Belanger Engineering has evaluated the proposed stormwater impacts resulting from the creation of a new residential Senior Housing Community located off Tuttle Road in Cumberland. The property is shown on Town Tax Map R4 Lot 4E+5 and is approximately 36.83 acres in size.

This approval will focus on the proposed development expansions located on Lot 4C. In particular, the project creates 7.87 acres (was 8.04) of new impervious area and 19.81 acres (was 19.76) of new developed area. Approximately 3.15 acres (was 3.24) of road, 1.27 acres of driveway, and 3.22 acres of building roof will be created. We expect to construct 52 residential cottages and community facilities to support them. A community building and maintenance building is also planned to support the project. We have modeled 54 buildings in the enclosed calculations. We have also added 0.23 acres of impervious area into the calculations to include the proposed pedestrian trails.

<u>Project Location</u>: The project is located off Tuttle Road in Cumberland, Maine. The site is located across the street from the Cumberland Town Hall building.

<u>DEP Jurisdiction</u>: The proposed project includes the development of 19.81 acres of developed area and 7.87 acres of impervious area. The project does trigger the Site Law. The project is not within an urban impaired stream or a severely blooming lake. As a result, the Basic Standards, General Standards, and the Flooding Standard apply to this project. See Section 4A and 4B of the Chapter 500 Rules, pages 4&5.

Basic Standards

- 1. Erosion and sedimentation control plan See Appendix A of Chapter 500 Rules
- 2. Inspection and Maintenance Plan See Appendix A and B of Chapter 500 Rules
- 3. Housekeeping See Appendix C of the Chapter 500 Rules

General Standards

- 1. Narrative
- 2. Drainage Plans
- 3. Calculations
- 4. Details, designs, and specifications for Underdrained vegetated filters, & Buffers.

Flooding Standards

1. Stormwater Management System must detain, retain, or result in infiltration of stormwater for the 2,10,25 storms such that the peak flows do not exceed "pre-development" conditions.

<u>Surface water on or abutting the site</u>: Runoff from the site drains southerly toward two separate un-named streams. The first stream crosses Tuttle Road via two 24" culverts. The second stream crosses Crossing Brook Road and the railroad line via a 24" culvert. Runoff continues to drain toward Mill Brook and the Piscataquis River.

<u>Alterations to Land Cover:</u> The drainage study is conducted on the sites 36.83 acres. The existing ground cover is 100% woods and meadow. The proposed ground cover will result in approximately: 18% impervious, 17% lawn, and 65% woods and meadow.

<u>Downstream ponds and Lakes</u>: Runoff from the site drains to Mill Brook and the Piscataquis River. Enclosed is a U.S.G.S. Map showing the site location.

<u>Historic Flooding</u>: The property is fairly uniform with mildly irregular topography and typical slopes between 2 % and 18 %. The stream area may have localized flooding but is located within

ravine areas and outside development areas. There site is not located within any designated 100-year flood elevation zones. See enclosed Firm Maps.

<u>Alterations to natural drainage ways</u>: Natural drainage ways will not be altered as a result of the proposed development. Pipe Arch's and Culverts will be installed to maintain current drainage flow patterns.

<u>Proposed BMP's</u>: Steep slopes will be rip rapped. Silt fence is shown at the bottom of all fill slopes, hay bale barriers and stone check dams will be used in ditches and/or around catch basins. BMP's proposed for this project are shown and described on the enclosed plans.

Pre D	Pre Development Watershed Areas for Cumberland Senior Housing - Tuttle Road								
					Existing	Existing			
	Total	Total	Existing	Existing	Woods/Field	Developed			
Subarea	Area	Area	Impervious	Lawn	Undeveloped	Area			
	sf	acres	acres	acres	acres	acres			
1s	4399335	101.0	19.00	25.00	57	44			
2s	3759452	86.3	13.00	30.00	43.31	43.00			
3s	1655379	38.0	0.00	4.00	34	4			
4s	566280	13.00	1.00	7.00	5	8			
5s	5140080	118.0	36.00	35.00	47	71			
6s	2874960	66.0	20.00	40.00	6	60			
7s	479160	11.0	5.00	6.00	0	11			
	18874646	433.3	94	147	192	241			

<u>Proposed Conditions - Oceanview Cumberland Senior Housing Project</u>

The project will be accessed from a 50' right way off Tuttle Road and will extend a new road to the project area. The main access road is approximately 2950' long, 22' wide, curbed, and a 5' sidewalk will be installed on the right side. The Arctic Fox Drive is 865' long and will be 22' wide and curbed. Mallard Way at the end is approximately 1013' long and will be 22' wide. The roads create 3.15 acres of impervious area and 6.52 acres of developed area.

The developer is proposing to construct 52 residential homes. We have assumed each house will have approximately 2700 s.f. (.06 ac.) of building footprint area including an optional garage. We have also assumed each driveway will be 24' by 40' (.02 acres) in area. This will accommodate a 2 bay garage option and four (4) vehicles. Impervious area per cottage is .08 acres each based on the above assumptions. We will also assume a small community building and amenities at 0.2 acres. The residential construction creates 4.49 acres of impervious area and 13.29 acres of developed area.

The project creates 7.87 acres of impervious area and 19.81 acres of developed area. This is the basis of the general standards calculations below.

OV Cumberland Road Impervious Area Summary - 3-1-2018								
Description	Road	Impervi	ous Area	Lawn	Area	Develop	ed Area	Comments
	Length							
	feet	s.f.	acres	s.f.	acres			
Little Acres Drive	2953	79278	1.82	91543	2.10	170821	3.92	@22', curb, 5' sidewalk
Arctic Fox Drive	594	16711	0.38	12989	0.30	29700	0.68	@22', curb, no sidewalk, 30' sac
Arctic Fox Drive Spur 1	205	3712	0.09	3712	0.09	7424	0.17	18', no curb
Arctic Fox Drive Spur 2	150	3621	0.08	3621	0.08	7242	0.17	18', no curb
Mallard Way	1013	27314	0.63	28000	0.64	55314	1.27	@22', curb, 5' sidewalk
Mallard Way Spur	130	2777	0.06	2777	0.06	5554	0.13	18' no curb
Eyebrow Road 1	175	4013	0.09	4013	0.09	8026	0.18	20' no curb
Road Totals	5220	137426	3.15	146655	3.37	284081	6.52	

General Standard Narrative and Selected BMP's:

The developer will utilize the following BMP's for stormwater treatment and storage.

- 1. Wet Ponds (2) Maine BMP's Chapter 4.
- 2. Roof Dripline BMP Maine BMP's Chapter 7.5.
- 3. FocalPoint Proprietary Subsurface Treatment and Storage Systems.
- 4. Forested Buffers adjacent to development
- 5. Forested Buffers with Stone Bermed Level Lip Spreader

Wet Pond

Two (2) Wet Ponds will be developed to support the project. The pond has been sized to store 2.0" X the watersheds impervious area and 0.8"X the watersheds "disturbed" below the permanent pool. In addition, the Pond will store 1" X the watershed impervious area and 0.4" X the watershed disturbed area above the permanent pool and will discharge to a gravel filter drain to cool runoff and provide a slow release of runoff. An outlet control structure and spillway has been implemented in the ponds to provide emergency overflow as required. The outlet control structure will also be the gravel drain outlet. Runoff will discharge to the adjacent wetland.

Roof Dripline

Roof driplines with capture roof areas and drain them through foundation backfill and discharge to footing drains. The roof dripline will be 3' wide and 1.5' deep and will be installed in roof drainage areas. Once treated, 4" drain pipes will outlet into the street catch basins or can daylight in forested areas behind the buildings as conditions allow. The roof driplines will store 1" X roof areas utilizing 40% voids.

Focal Point Proprietary System

Along the main access road, the developer has secured a 50' access easement. We will utilize focalpoint which is an approved proprietary stormwater treatment system. We have followed the sizing guidelines from the manufacturer and the Departments approval letter dated February 2, 2017. Utilizing the Chapter 500 Design Worksheet / Checklist enclosed, we have sized each focal point system based on the drainage area being captured and treated. The following design elements are included with each location.

- 1. FocalPoint Bed Area (min. 174 square feet per acre of impervious area (e.g. 0.2 acres=35 s.f.)).
- 2. Verify a 0.95 inch Type III rainfall event is treated prior to activation of the overflow (typically 6-12"). We have provided 12" of storage in each treatment area.
- 3. Maintain a ratio of filter media (s.f.) to the temporary ponding volume (c.f.) at 1:5.
- 4. Subsurface Chamber Treatment row must be sized to treat the peak flow from a 1 year-24 hr storm event. The cultic 150XLHD requires (1 chamber per 0.185 cfs).

- 5. The subsurface storage basin will provide storage of 1" X Impervious Area and will control release over 24-48 hrs.
- 6. The design has been reviewed by the Manufacturer. The letter is attached.

Stormwater from one travel lane (11' wide) drains 500' along the gutter line before it outlets into a curb slot. Runoff passes through a grassed filter strip prior to entering the focalpoint filter system. This strip captures the majority of the coarse sediment and provides pre-treatment prior to draining into the focalpoint media. Runoff then drains from the focalpoint system to the subsurface treatment row sized for the 1 year peak flow. In this case the system treats 5500 s.f. (500'X11') of impervious area (0.12 acres). The minimum focalpoint bed area is calculated to be 21 s.f. (.06 X 174). We have provided a 3'X7' bed area (21' s.f.). The system was modeled with a 0.95 inch storm and stores the volume without breaching the overflow outlet as required. The ratio of surface area to temporary volume is approximately 1:5. The subsurface treatment row requires 2 units of cultic 150XLHD chambers by ACF environment. In addition, approximately 10 units are needed to provide 1" storage. In total 12 storage units will treat this portion of the road. The focalpoint systems are installed prior to each basin along the access road.

Forested Buffer

Portions of the back yard lawn areas that cannot be practically captured will drain toward the buffers located along the stream protection corridor. The back yards are largely pervious and will be graded to sheet flow into the undeveloped forested area below the back yard area. Note that buildings and pavement are being routed to other BMP devices and will not drain to the buffers. We have provided 100' buffers below the back yard lawn areas along the stream corridor as required by site law projects. We will utilize BMP 5.1 – Buffer Adjacent to Residential, Largely Pervious or Small Impervious Area Approximately 1.15 acres of lawn will be treated. Further, the fill slopes adjacent to the lawn areas will not be mowed and will be allowed to revert back to a natural meadow buffer condition. Approximately 0.6 acres will be converted back to meadow buffer. Approximately 0.54 acres of lawn will be treated by the buffers.

General Standard Calculations

<u>Calculations</u>: BMP's will be utilized to treat impervious and developed areas as far as practical. The project is required to effectively treat 95% of the impervious area and 80% disturbed area as described in the rules as far as practical. Certain areas cannot practically receive treatment. Where treatment of 95% of the impervious area is not practical, the department may allow treatment as low as 90% of the impervious area if the applicant is able to demonstrate that treatment of a greater depth of runoff than specified in the standards will result in at least an equivalent amount of overall treatment for the impervious area. As described in the calculation, the project captures 95% of the "new" projects impervious area and 81% of the projects overall developed areas. At 90-95%, DEP recommends 05" & 0.02" additional storage per % below 95%. The BMP's captures proposed areas to the extent practical. The treatment area summary and general standard calculations are attached.

The project as developed meets the General Standards as outlined in the Chapter 500 stormwater rules. The General Standard calculation is shown on the post development drainage plan and is included in this report.

Arctic Fox Drive Wet Pond Design Criteria Pond 16P:

A wet pond at Arctic Fox Drive will be constructed to support the project. Since this project will be required to meet the Flooding Standard per Town Ordinances and Site Law projects, the wet pond has been designed to store and hold 2.0" X the watershed impervious area and 0.8" of the watersheds non-impervious developed area below the permanent pool and an additional 1" over the watersheds impervious area and 0.4" X the watersheds non-impervious development area over the permanent pool that will drain through a gravel filter. An outlet structure with a 18" outlet pipe will control flow. The structure Rim is set at 81.0 with a 6" vertical orifice controlling flow into the Tuttle Road storm drain system. The permanent pool is elevation 77.0. The pond shape length to width ratio is 3:1. Approximately 1.1 acres of impervious area and 2.54 acres of lawn will be treated. A pond bench of 10' is provided.

Gravel Filter Drain Sizing:

The gravel trench will be 4' wide X 3' deep. The underdrain piping shall be 6" slotted, rigid schedule 40 PVC or SDR 35 pipe. The trench shall be located in the pond bench. The trench length shall be 3' of gravel trench per 1000 c.f. of channel protection volume (volume above permanent pool). The pond gravel outlet is set at 77.0 to provide 1.5' of gravel drain storage above the permanent pool.

	Oce	anview at Cum	berland				
Arctic	Fox Drive Wet F	ond Design Crit	eria - Hyd	rocad Pond :	16P		
	acres	s.f.					
Impervious Area Draining to Pond	1.1	47916					
Lawn Area draining to Pond	2.54	110642					
Permanent Pool Elevation	77						
Treatment Volume	Above Pool	1" X Impervious Area + 0.4" X Lawn				7628	c.f.
	Below Pool	2" X Impervio	us Area + (0.8" X Lawn		11522	c.f.
Pond Storage Provided	Above Pool					12172	✓
	Below Pool					18632	✓
Mean Depth	Volume of Pe	rmanent Pool /	Surface A	rea 1' below	pool =	4.7	ft.
	Volume of Pe	ermanent Pool	18632	c.f.			
	Surface Area	1' below Pool	4000	s.f.			
Gravel Filter Drain Sizing	3' per 1000 c	f. of channel pr	otection	olume:	23		
	Channel Protection Volume 76						

Groundwater Impacts

A soil borings / Test Pits was cored within the wet pond area. The borings and probe was completed Mark Hampton. Groundwater is expected to be near the existing ground surface. The pond will be lined with a 10 mil poly liner installed to prevent mixing of groundwater and pond water. The project will be served by public water and sewer utilities. Water will be routed through the outlet structure and discharged in the adjacent wetlands. The proposed pond will not significantly impact groundwater.

Bedrock

Ledge was observed within the boring areas. The bottom of pond is set at elevation 71.0. Vertical ledge or boulder walls may be excavated should ledge be encountered to provide the pond storage required.

Mallard Way Wet Pond Design Criteria:

A wet pond will be constructed off Mallard Way to support the project. Since this project will be required to meet the Flooding Standard per Town Ordinances and Site Law projects, the wet pond has been designed to store and hold 2.0" X the watershed impervious area and 0.8" of the watersheds non-impervious developed area below the permanent pool and an additional 1" over the watersheds impervious area and 0.4" X the watersheds non-impervious development area over the permanent pool that will drain through a gravel filter. An outlet structure with a 18" outlet pipe will control flow. The structure Rim is set at 90.5 with a 6" vertical orifice controlling flow into the Tuttle Road storm drain system. The permanent pool is elevation 88.0. The pond shape length to width ratio is 4:1. Approximately 2.4 acres of impervious area and 4.64 acres of lawn will be treated. A pond bench of 10' is provided.

Gravel Filter Drain Sizing:

The gravel trench will be 4' wide X 3' deep. The underdrain piping shall be 6" slotted, rigid schedule 40 PVC or SDR 35 pipe. The trench shall be located in the pond bench. The trench length shall be 3' of gravel trench per 1000 c.f. of channel protection volume (volume above permanent pool). The pond gravel outlet is set at 89.5 to provide 1.5' of storage above the permanent pool.

	Oce	anview at Cum	berland				
	Mallard W	/ay Wet Pond D	esign Crite	eria			
	acres	s.f.					
Impervious Area Draining to Pond	2.4	104544					
Lawn Area draining to Pond	4.64	202118					
Permanent Pool Elevation	88						
Treatment Volume	Above Pool	1" X Impervio		15347	c.f.		
	Below Pool	2" X Impervio	23174	c.f.			
Pond Storage Provided	Above Pool					19786	✓
	Below Pool					23438	✓
Mean Depth	Volume of Pe	rmanent Pool /	Surface A	⊥ .rea 1' below	/ pool =	4.8	ft.
	Volume of Pe	rmanent Pool	23438	c.f.			
	Surface Area	1' below Pool	4879	s.f.			
Gravel Filter Drain Sizing	3' per 1000 c.f. of channel protection volume:						
_	Channel Protection Volume 15347						

Groundwater Impacts

A soil borings / Test Pits was cored within the wet pond area. The borings and probe was completed Mark Hampton. The pond will be lined with a 10 mil poly liner installed to prevent mixing of groundwater and pond water. The project will be served by public water and sewer utilities. Water will be routed through the outlet structure and discharged in the adjacent wetlands. The proposed pond will not significantly impact groundwater.

Bedrock

Ledge was observed within the boring areas. The bottom of pond is set at elevation 81.0. Vertical ledge or boulder walls may be excavated should ledge be encountered to provide the pond storage required.

Post Area Summary and General Standard Calculation

			Existing	New	New	Existing	New	New	New	Existing	Treatment
	Total	Total	Impervious	Impervious	Impervious	Lawn	Lawn	Developed	Developed	Woods/Field	BMP
ubarea	Area	Area		Area	Area			Area	Area	Undeveloped	
					Treated				Treated		
	sf	acres	acres	acres	acres	acres	acres	acres	acres	acres	
1s	3717485	85.34	18.40	0.00	0.00	23.40	0.10	0.10	0.00	43.44	
2s	2954636	67.83	13.00	0.13	0.00	30.00	1.85	1.98	1.15	22.01	Forested Buffer
3s	1580923	36.29	0.00	0.10	0.00	4.00	0.62	0.72	0.00	31.32	Zero Treatment
4s	566280	13.00	1.00	0.00	0.00	7.00	0.00	0.00	0.00	5.00	no change
5s	5140080	118.00	36.00	0.00	0.00	35.00	0.00	0.00	0.00	47.00	no change
6s	2874960	66.00	20.00	0.00	0.00	40.00	0.00	0.00	0.00	6.00	no change
7s	479160	11.00	5.00	0.00	0.00	6.00	0.00	0.00	0.00	0.00	no change
14s	21920	0.50	0.00	0.40	0.40	0.00	0.10	0.50	0.50	0.00	Forested Buffer
15s	24108	0.55	0.00	0.37	0.37	0.00	0.18	0.55	0.55	0.00	FocalPoint
16s	210306	4.83	0.00	1.10	1.10	0.00	2.54	3.64	3.64	0.57	Wet Pond 16P
17s	358935	8.24	0.00	2.40	2.40	0.00	4.64	7.04	7.04	0.22	wet Pond 17P
18s	64392	1.48	0.00	0.00	0.00	0.00	0.68	0.68	0.00	0.45	Zero Treatment
19s	615502	14.13	0.60	0.15	0.00	1.60	0.94	1.09	0.00	10.66	Zero Treatment
20s	266076	6.11	0.00	0.00	0.00	0.00	0.29	0.29	0.00	5.82	Zero Treatment
51s			0.00	3.22	3.22	0.00	0.00	3.22	3.22		Roof Dripline BMP
	18874763	433.30	94.00	7.87	7.49	147.00	11.94	19.81	16.10	155	
				>95%	95%	✓		>80%	81%	✓	-

Flooding Standard

This drainage study will focus on the proposed impacts created by the Oceanview at Cumberland Senior Housing project. The model compares flooding standard results as they cross the project boundary. The intent is to meet the pre-development peak flows.

Watershed 1 has been estimated to be 101 acres and is adjacent to Tuttle Road and Main Street. The top end of the watershed is the Greely Middle School entrance. Ponds were observed on site. The Pond outlet at the Tuttle Road Middle School entrance is a 30" concrete culvert and drains toward a swale and ditch adjacent to Tuttle Road. Runoff travels through the residential neighborhood and crosses Meadow Way via 2 - 24" culverts. Runoff travels overland through woods and field until it drains to a stream above the Oceanview Cumberland Senior Housing site. Soils in the vicinity of the project site show the natural wooded areas to Scantic and Buxton soils which is a "D" soil. The fields are predominately Suffield which is a C soil condition. This stream drains through the development site and crosses Tuttle Road by one 30" and one 24" culvert. The site primary access road is located over an existing driveway serving the Allen property. The tracks and crossing have been removed. We will cross the stream and will install a new arch culvert at the crossing.





Pond at Greely Middle School





Watershed drains through Cumberland Common





Two culverts Crossing Tuttle Road 30" & 24" (below site) – Hydrocad Pond 1P

Watershed 2 is approximately 67 acres and is below the existing 48" culvert crossing the cart path at the Val Halla Golf Course. The 48" culvert controls the upper watershed subareas 5 and 6. This upper watershed area includes Greely High School, a residential neighborhood of approximately 150 homes, public Val Halla Golf Course, and undeveloped areas. Watershed 2 is the area being developed with the project.





Greely High School Drainage





Hemlock Drive Culvert crossing onto Val Halla properties





Two 30" Culverts draining to Val Halla Golf Course Below Hemlock Drive





48" culvert crossing Golf Cart Path and pond storage below outlet





Pond controls outlet of two (2) – 48" culverts – drains Hydrocad Subarea 5 and 6





Golf Cart Path crossing Controls flow out of pond – Oval 4'X3' and 30" overflow pipe Pond 5P





48" culvert crossing cart path inlet – Hydrocad Pond 6P





48" culvert crossing cart path outlet – Hydrocad Pond 6P





4'X6' Box Culvert under old Railroad Bed



These drainage areas are defined in our Stormwater Model as shown on the HydroCAD diagrams. Full-size drainage plans and stormwater calculations for the existing and developed site conditions are included with this report. Refer to the HydroCAD diagrams, calculations, report and drainage plans for modeling assumptions, subcatchments, flowpaths, drainage reaches, etc. Runoff calculations were performed for the 2-year, 10 year, and 25 year storm events in accordance with Cumberland Ordinances and DEP requirements. Results of the calculations are shown in the Summary Table for ease of comparison. In order to significantly reduce the volume of paper required to reproduce complete data and calculation reports for all design storms, partial HydroCAD reports were generated for the 2-10-25-year storm events (pre- & post-) for selected subcatchments.

Modeling assumptions: The flooding standard is required with this development because this is a Site Law Project. We have modeled the pond areas to demonstrate that the outlets have the required storage volume capacity and that they will pass the 25 year storm event without flooding the pond embankments. The "HydroCad" computer program was used to determine the peak storm water runoff for the pre- and post-development conditions. HydroCad is a storm water modeling system, which utilizes the TR-20 method developed by the Soil Conservation Service (SCS).

The design assumptions used for this project are:

Design storm: 24 hour, Type III rainfall distribution.

Rainfall: 24 hour precipitation values from U.S. Weather Bureau Technical Release No.

2 year storm = 3.1 inches

10 year storm = $\frac{4.6}{10}$ inches

25 year storm = $\frac{5.80}{100}$ inches

50 year storm = 6.90 inches

100 year storm = 8.10 inches

500 year storm = 12.10 inches

Site specific parameters for the project are listed below:

Soils: Soils information to determine the hydrologic soil group for the site, are derived from the Soil Survey of Cumberland County by the United States Department of Agriculture Soil Conservation Service. The soils and hydrologic group are listed below:

Soil Classification	Hydrologic Group
BgB – Belgrade very fine Sandy Loam	HSG B
BuB – Lamoine silt loam	HSG C
BuC2 – Buxton Silt Loam	HSG D
DeB - Deerfield Loam Sand	HSG B
EmB – Elmwood Fine Sandy Loam	HSG C
Ls – Limerick – Saco silt loams	HSG C
Sn – Scantic Silt Loam	HSG D
SuC2 – Suffield Silt Loam	HSG C
SuD2 – Suffield Silt Loam	HSG C
SuE2 – Suffield Silt Loam	HSG C
WmB – Windsor Loamy Sand	HSG A
MeC – Melrose fine sandy loam	HSG C
Sz – Swanton fine sandy loam	HSG C/D

Ground Cover:

Pre-& Post Development: The watershed ground cover is modeled as woods, grass, meadow and impervious.

Cover Description	<u>Curve Number:</u>
Impervious	98
Woods	70
Lawn	74

PRE- & POST-DEVELOPMENT HYDROLOGIC RESULTS

<u>At Allen Property Line</u>

FLOODING STANDARD RESULTS REACH 3R							
Storm	PRE	POST	DIFFERENCE				
	C.F.S.	C.F.S.	%				
2 YEAR	48.66	45.78	-6%				
10 YEAR	103.64	95.56	-8%				
25 YEAR	151.56	138.31	-10%				
50 YEAR	196.96	177.65	-11%				
100 YEAR	248.09	217.25	-14%				

FLOODING STANDARD RESULTS POND 1P							
Storm	PRE	POST	DIFFERENCE				
	C.F.S.	C.F.S.	%				
2 YEAR	38.34	36.55	-5%				
10 YEAR	96.83	90.56	-7%				
25 YEAR	144.34	132.86	-9%				
50 YEAR	189.15	172.21	-10%				
100 YEAR	239.06	212.37	-13%				

Pre Pond 1P Summary		Post Pond 1P S	ummary
Storm	Flood	Storm	Flood
	Elevation		Elevation
	(ft.)		(ft.)
2 YEAR	69.82	2 YEAR	69.72
10 YEAR	71.43	10 YEAR	71.38
25 YEAR	71.72	25 YEAR	71.66
100 YEAR	72.19	100 YEAR	72.07

Stream at Lower Property Line

FLOODING STANDARD RESULTS REACH 6R							
Storm	PRE	POST	DIFFERENCE				
	C.F.S.	C.F.S.	%				
2 YEAR	94.2	87.63	-7%				
10 YEAR	194.34	180.21	-8%				
25 YEAR	265.34	250.22	-6%				
50 YEAR	375.46	357.08	-5%				
100 YEAR	493.76	462.13	-7%				

FLOODING STANDARD RESULTS POND 2P										
Storm	PRE	POST	DIFFERENCE							
	C.F.S.	C.F.S.	%							
2 YEAR	55.7	54.15	-3%							
10 YEAR	89.77	88.83	-1%							
25 YEAR	107.91	107.16	-1%							
50 YEAR	141.82	137.87	-3%							
100 YEAR	237.6	234.77	-1%							

Pre Pond 2P Su	ımmary	Post Pond 2P S	ummary
Storm	Flood	Storm	Flood
	Elevation		Elevation
	(ft.)		(ft.)
2 YEAR	47.62	2 YEAR	47.48
10 YEAR	51.53	10 YEAR	51.4
25 YEAR	54.37	25 YEAR	54.24
100 YEAR	57.43	100 YEAR	57.41

Forested Wetland below site

FLOODING STANDARD RESULTS REACH 55R											
Storm	PRE	POST	DIFFERENCE								
	C.F.S.	C.F.S.	%								
2 YEAR	14.17	12.06	-17%								
10 YEAR	35.23	29.2	-21%								
25 YEAR	54.61	44.85	-22%								
50 YEAR	73.49	60.06	-22%								
100 YEAR	94.84	77.22	-23%								

FLOODING STANDARD RESULTS POND 3P											
Storm	PRE	POST	DIFFERENCE								
	C.F.S.	C.F.S.	%								
2 YEAR	12.99	11.45	-13%								
10 YEAR	26.68	24.24	-10%								
25 YEAR	48.56	38.26	-27%								
50 YEAR	70.97	58.08	-22%								
100 YEAR	93.27	76.14	-22%								

Pre Pond 3P S	ummary	Post Pond 3P S	ummary
Storm	Flood	Storm	Flood
	Elevation		Elevation
	(ft.)		(ft.)
2 YEAR	55.74	2 YEAR	55.59
10 YEAR	58.11	10 YEAR	57.57
25 YEAR	59.4	25 YEAR	59.23
100 YEAR	59.94	100 YEAR	59.75

15" Culvert at Tuttle Road

FLOODING STA	NDARD RESU	JLTS POND 4	P AT PROPERTY LINE
Storm	PRE	POST	DIFFERENCE
	C.F.S.	C.F.S.	%
2 YEAR	4.55	4.55	0%
10 YEAR	8.95	8.95	0%
25 YEAR	11.61	11.61	0%
50 YEAR	13.6	13.6	0%
100 YEAR	15.83	15.83	0%

Pre Pond 4P Summary								
Storm	Flood							
	Elevation							
	(ft.)							
2 YEAR	86.04							
10 YEAR	86.86							
25 YEAR	87.61							
100 YEAR	89.03							

Post Pond 4P Summary								
Storm	Flood							
	Elevation							
	(ft.)							
2 YEAR	86.04							
10 YEAR	86.86							
25 YEAR	87.61							
100 YEAR	89.03							

Conclusion:

The above analysis points are located where the project crosses the property line and points of interest along Crossing Brook Road and Tuttle Road. (See Ponds 1P and 2P above). Peak flows are being maintained for the 2, 10 and 25 year storms at the existing twin 30" culverts at Crossing Brook Road (Pond 2P) the two culverts at Tuttle Road (one 24" and one 30"). Peak flows are less than pre development flows at the (existing 15" culvert (Pond 4P) crossing Tuttle Road at the proposed entrance. Pond 3P is located toward the back and drains toward a culvert at the RR crossings. Peak flows are being maintained in all four locations below the site. The project will maintain the pre-development peak flow as required for the existing project. Reach 3R, 6R, and 55R model the stream and wetland as it crosses the property line. These locations also maintain the pre-development flows as required.

Two wet ponds are being constructed to provide water quality and quantity treatment. The proposed ponds have the capacity to control flow from the 100 year storm which exceeds the DEP Flooding Standards. Adjacent properties will not be flooded as a result of this project. The project does not significantly impact downstream structures or properties. We submit that the Flooding Standard has been met or exceeded with this development.

The proposed project captures 95% of the newly developed impervious area and 81% of the developed area as required to meet the General Standards. Two Wet Ponds will be constructed to provide impervious treatment and storage. Each cottage will provide roof driplines (BMP 7.6) to provide building roof treatment and storage. The access road will install focal point devices to provide treatment and storage along the road. Finally, back yard lawn areas, that cannot be practically captured, adjacent to the stream will be sent to the forested buffer for treatment. The General Standard will be met with the above BMP's installed.

The Basic Standards will be met with the proposed erosion control plans and stabilization details provided. No additional water quality or quantity measures are warranted for the OceanView @ Cumberland Cottage Expansion Project. We submit that the project meets the Basic, General, and the Flooding standard as outlined in the Maine DEP Chapter 500 Stormwater Rules. The proposal maintains these standards as required.

OceanView @ Cumberland Property Maintenance:

PART 1: RESPONSIBILITY FOR MAINTENANCE

OceanView @ Cumberland Retirement Community will be responsible for maintenance of the stormwater systems. Contact Chris Wasileski at Seacoast Management Company.

PART 2: INSPECTIONS – During Construction and Post Construction

• Detention Facilities: Two (2) Wet Ponds

Embankment inspection and maintenance

Spillway maintenance

Outlet Structure sump cleaning and maintenance

Sediment removal and disposal

• Detention Facilities: Focalpoint Devices and Detention Ponds

Debris removal from stone storage area (leaves, branches, trash, etc.)

Sediment removal and disposal

• Ditches, Swales, or other open stormwater channels

Embankment inspection and maintenance

Channel inspection

Sediment removal and disposal

• Culverts, catch basins, stormwater control structures

Embankment inspection and maintenance

Inlet and Outlet inspection

Debris removal and disposal

Roof Dripline Filter BMP Maintenance

Sediment removal and disposal

Filter and Underdrain replacement

Debris removal and disposal

Stone Dripline Replacement

Foundation Sealant

Foundation Backfill

• Focalpoint filter media and underground pipe storage

Embankment inspection and maintenance

Channel inspection

Sediment removal and disposal

Pipe flushing and cleaning

Filter media replacement

Coarse sediment removal at focalpoint media inlet

The owners representative will inspect the detention ponds, roof driplines, swales, channels, stormwater structures, focalpoint devices to determine if the soil blockage or impaired capacity to pass flow exists. Inspections will be performed on a monthly basis from March to November, and quarterly during the remainder of the year. A record of inspections and maintenance or corrective measures shall be kept by the owner (see part 4).

PART 3: MAINTENANCE AND CLEANING

The owner will regularly inspect for sediment accumulation, obstructions, debris, and other potential causes for operational difficulty in the conveyance and detention system as described in Part 2. Immediate action shall be taken to remedy detrimental obstructions. This may include replacing the filter pond and roof driplines filter beds as necessary to allow infiltration and treatment to occur.

Cleaning out of catch basins, culvert cleaning, and other means necessary to ensure the stormwater system is maintained. Some additional measures (but not limited to) are shown below:

• Wet Pond maintenance – Arctic Fox Wet Pond and Mallard Way Wet Pond

Gravel Drain Inspection

Gravel Drain replacement

Outlet Structure sump cleaning and maintenance

Sediment removal and disposal

Mowing

Harvesting and Weeding

The owner will regularly inspect the wet pond after every major storm event in the first few months to ensure proper function. There after the pond should be inspected biannually to ensure that it is draining within 24 hours. Sediment shall be removed from the pond when sediment reduces the pond volume by 25%. The removed sediment shall be hauled off site and disposed of. Mowing of the pond area shall be limited to 2 times per year to maintain grass heights to less than 12". Weeding and pruning of growth within the pond and pond back slopes will be completed as necessary. The pond outlet shall be inspected for erosion and make repairs as needed annually.

• Focalpoint filter Maintenance – two (2) locations Sta 21+50 right and left sides along Little Acres Drive:

Soil Filter Inspection

Soil Filter replacement

Outlet Structure sump cleaning and maintenance

Sediment removal and disposal

Mowing

Harvesting and Weeding

The owner will regularly inspect the soil filter after every major storm event in the first few months to ensure proper function. There after the filter should be inspected biannually to ensure that it is draining within 24 hours. The top several inches of the filter shall be replaced with fresh material when water ponds on the surface of the bed for more than 72 hours. Sediment shall be removed from the filter bed annually. The bed shall be hand raked and re-seeded as necessary. The removed sediment shall be hauled off site

and disposed of in a stabilized area. Mowing of the filter area shall be limited to 2 times per year to maintain grass heights to less than 12". Weeding and pruning of growth within the filter zone will be completed as necessary.

• Stormwater Facilities: Catch basins, Wet Ponds, Culverts, A mandatory scheduled maintenance will be performed every four weeks for a period of one hundred and twenty (120) days and will begin after satisfactory completion and acceptance of landscape construction. Ongoing maintenance will be required as necessary.

• Parking/Display Areas:

All sand, salt, etc. accumulated when sweeping the parking and display areas, shall be trucked off-site for disposal. The parking lot shall be swept annually in the spring.

PART 4: RECORD KEEPING

The owner will maintain inspection records, with recordings of condition of basins, and pipes and annotation of substantial precipitation events or mitigating circumstances in the intervening time for trending to develop the anticipated preventive maintenance schedule.

PART 5: MAINTENANCE CONTRACT

Should proprietary devices be utilized, a maintenance contract will be established with the manufacturer for regular maintenance and cleaning of the device. Focalpoint manufactures will be on site through the installation process. A maintenance contract will be maintained as necessary to ensure proper system performance of the focal point system. Other facilities included catch basins, culverts, wet ponds will also be maintained annually or as required by inspection. The intent being to maintain a working system.

PART 6: RE-CERTIFICATION

The owner shall submit a certification to Maine DEP within three months of the expiration of each five year interval from the date of issuance of the permit. The owner shall submit the maintenance log which identifies inspections completed, erosion problems found, when corrective action was taken, and who completed the work. The certification will include a statement indicating that the stormwater system is working and is being maintained in working condition in accordance with the permit requirements.

Maintenance Log Sheet OceanView @ Cumberland Retirement Community

Name	Maintenance Task Completed	Date

Maine DEP Chapter 500 Appendix C. Housekeeping - Updated 2017

These performance standards apply to all projects.

1. Spill prevention. Controls must be used to prevent pollutants from construction and waste materials stored on site to enter stormwater, which includes storage practices to minimize exposure of the materials to stormwater. The site contractor or operator must develop, and implement as necessary, appropriate spill prevention, containment, and response planning measures.

NOTE: Any spill or release of toxic or hazardous substances must be reported to the Department. For oil spills, call 1-800-482-0777 which is available 24 hours a day. For spills of toxic or hazardous material, call 1-800-452-4664 which is available 24 hours a day. For more information, visit the Department's website at

http://www.maine.gov/dep/spills/emergspillresp/

2. Groundwater protection. During construction, liquid petroleum products and other hazardous materials with the potential to contaminate groundwater may not be stored or handled in areas of the site draining to an infiltration area. An "infiltration area" is any area of the site that by design or as a result of soils, topography and other relevant factors accumulates runoff that infiltrates into the soil. Dikes, berms, sumps, and other forms of secondary containment that prevent discharge to groundwater may be used to isolate portions of the site for the purposes of storage and handling of these materials. Any project proposing infiltration of stormwater must provide adequate pre-treatment of stormwater prior to discharge of stormwater to the infiltration area, or provide for treatment within the infiltration area, in order to prevent the accumulation of fines, reduction in infiltration rate, and consequent flooding and destabilization.

See Appendix D for license by rule standards for infiltration of stormwater.

NOTE: Lack of appropriate pollutant removal best management practices (BMPs) may result in violations of the groundwater quality standard established by 38 M.R.S.A. §465-C(1).

3. Fugitive sediment and dust. Actions must be taken to ensure that activities do not result in noticeable erosion of soils or fugitive dust emissions during or after construction. Oil may not be used for dust control, but other water additives may be considered as needed. A stabilized construction entrance (SCE) should be included to minimize tracking of mud and sediment. If off-site tracking occurs, public roads should be swept immediately and no less than once a week and prior to significant storm events. Operations during dry months, that experience fugitive dust problems, should wet down unpaved access roads once a week or more frequently as needed with a water additive to suppress fugitive sediment and dust.

NOTE: Dewatering a stream without a permit from the Department may violate state water quality standards and the Natural Resources Protection Act.

4. Debris and other materials. Minimize the exposure of construction debris, building and landscaping materials, trash, fertilizers, pesticides, herbicides, detergents, sanitary waste and other materials to precipitation and stormwater runoff. These materials must be prevented from becoming a pollutant source.

NOTE: To prevent these materials from becoming a source of pollutants, construction and post-construction activities related to a project may be required to comply with applicable provision of rules related to solid, universal, and hazardous waste, including, but not limited to, the Maine solid waste and hazardous waste management rules; Maine hazardous waste management rules; Maine oil conveyance and storage rules; and Maine pesticide requirements.

5. Excavation de-watering. Excavation de-watering is the removal of water from trenches, foundations, coffer dams, ponds, and other areas within the construction area that retain water after excavation. In most cases the collected water is heavily silted and hinders correct and safe construction practices. The collected water removed from the ponded area, either through gravity or pumping, must be spread through natural wooded buffers or removed to areas that are specifically designed to collect the maximum amount of sediment possible, like a cofferdam sedimentation basin. Avoid allowing the water to flow over disturbed areas of the site. Equivalent measures may be taken if approved by the Department.

NOTE: Dewatering controls are discussed in the "Maine Erosion and Sediment Control BMPs, Maine Department of Environmental Protection."

- 6. Authorized Non-stormwater discharges. Identify and prevent contamination by non-stormwater discharges. Where allowed non-stormwater discharges exist, they must be identified and steps should be taken to ensure the implementation of appropriate pollution prevention measures for the non-stormwater component(s) of the discharge. Authorized non-stormwater discharges are:
- (a) Discharges from firefighting activity;
- (b) Fire hydrant flushings;
- (c) Vehicle washwater if detergents are not used and washing is limited to the exterior of vehicles (engine, undercarriage and transmission washing is prohibited);
- (d) Dust control runoff in accordance with permit conditions and Appendix (C)(3);
- (e) Routine external building washdown, not including surface paint removal, that does not involve detergents;
- (f) Pavement washwater (where spills/leaks of toxic or hazardous materials have not occurred, unless all spilled material had been removed) if detergents are not used;
- (g) Uncontaminated air conditioning or compressor condensate;
- (h) Uncontaminated groundwater or spring water;
- (i) Foundation or footer drain-water where flows are not contaminated;
- (j) Uncontaminated excavation dewatering (see requirements in Appendix C(5));
- (k) Potable water sources including waterline flushings; and
- (I) Landscape irrigation.
- 7. Unauthorized non-stormwater discharges. The Department's approval under this Chapter does not authorize a discharge that is mixed with a source of non_stormwater, other than those discharges in compliance with Appendix C (6). Specifically, the Department's approval does not authorize discharges of the following:
- (a) Wastewater from the washout or cleanout of concrete, stucco, paint, form release oils, curing compounds or other construction materials;
- (b) Fuels, oils or other pollutants used in vehicle and equipment operation and maintenance;
- (c) Soaps, solvents, or detergents used in vehicle and equipment washing; and
- (d) Toxic or hazardous substances from a spill or other release.
- (8) Additional requirements. Additional requirements may be applied on a site-specific basis.

EROSION AND SEDIMENT CONTROL INSPECTION REPORT FOR CONSTRUCTION SITES AN ACRE OR GREATER

		Inspection Date:						Project Type:						
		Project Address / Location: 291 Tuttle Road								Inspection Duration:				
			R4-4C							Inspector:				
		Project in Shoreland Zone ¹ :		Y		N				Inspector Qualifications:	Contractor MCGP Reporting			
		Property Owner:	ileski						Owner Contact Info:	207-233-4194 chrisw@oceanviewrc.com				
		Excavation Contractor: S	storey Bro	others						Contractor Contact Info:	207-829-4282 Robsto@maine.rr.com			
		DEP ESC-certified contractor? ¹		Y	\top	N				Photos:	Y N			
		Weather / Temp:		_	_		_	_	_	Date & inches last precip:				
		Inspection Criteria ²	nspection	n Res	ult ³					Observations / Corrective	Actions Needed			
	00/MCGP ITATION	SECTION A. Erosion Control &	Sedime	nt Co	ntrol	Prac	ctice	s - I	nst	alled According to Approv	ed Plan.			
API	PENDIX A		l measure	es mu	ıst be i	in pla	ace l	befo	re t	the activity begins. Measure	t site or into a protected natural resource as defined by es must remain in place and functional until the site is nust be taken."			
Part V	Record Retention	ESC plan & MCGP permit on site		N/A	М		Р		F					
^ ^	Pollution Prevention	Disturbed areas minimized		N/A	M		P		F					
		Natural buffers protected		N/A	М		P		F					
		Discharges not eroding		N/A	M		P		F					
^ ^	Sediment Barriers	Properly installed and maintained;		N/A	М		P		F					
		Downgradient of disturbance(s)/stock	piles	N/A	М	Щ	P	\Box	F					
		Adjacent to drainage channels	\perp	N/A	M	Ц	P	\perp	F					
		Perimeter controls prior to construction	on	N/A	М	Щ	P	\dashv	F					
^ ^	Temporary Stabilization	Areas unworked for >7days		N/A	М	Щ	P	_	F					
		Stabilized w/mulch or non-eroding co		N/A	M	Щ	P	\dashv	F					
		Stabilized w/in 48hrs of storm event a wetland or waterbody (w/in 75')	llong	N/A	М		P		F					
Ann	Permanent	Accumulated sediments removed	$-\!\!\!+$	N/A	M	\dashv	P	\dashv	F	Commont should (1) identify	which areas, so a copy of a site plan may be needed; and (2)			
^ ^	Stabilization	If final grade, permanently stabled <7	·	N/A	М	Щ	P	\dashv	F		n should be noted in each area			
	(a) Seeded Areas	Protected with mulch or erosion contriblanket		N/A	М		P	\perp	F					
		Achieved 90% cover of disturbed area No evidence of washing/rilling of top		N/A N/A	M M	_	P P	\dashv	F F					
	(0) 000000	Binding of sod roots to soil	50.1	N/A	М		Р	コ	F					
		No evidence of slumping of die off	$\overline{+}$	N/A	M	igwdap	P	\dashv	F					
	Mulch	Total coverage of exposed areas with approved mulch materials		N/A	М	Щ	Р		F					
	(d) Riprap	Appropriate backing of a well-graded gravel or geo-textile		N/A	M		P		F					
		No evidence of soil movemement from behind rip-rap	m	N/A	М		Р	\rfloor	F					
		Stone is appropriately sized to stay in	place	N/A	M		P		F					
	. , .	Land returned to Ag use		N/A	М		P		F					
	(f) Paved Areas	Placement of compacted subbase is complete		N/A	М	\Box	P		F					
	(a) Ditches	90% coverage of health veg.		N/A	М	П	Р	\dashv	F					
	swales	Well graded rip-rap lining or other no erosive lining	n-	N/A	М		Р		F					
		No evidence of undercutting of banks	,	N/A	М		Р		F					
		No evidence of down-cutting of channel	nel	N/A	М	П	Р	\exists	F					
		No evidence of slumping of channel l	ining	N/A	М		P		F					
App	Winter	Occurring Nov 1 - April 15		N/A	М	П	P	П	F					
A(6)	Construction (a) Site	Hay mulch is applied at 2x standard		N/A	М	Н	P	\dashv	F					

EROSION AND SEDIMENT CONTROL INSPECTION REPORT FOR CONSTRUCTION SITES AN ACRE OR GREATER

	Stabilization	Areas brought to final grade are stabilized each day	N/A	М	P		F
	(b) Sediment barriers	Areas W/I 75' of protected natural resource must be double row of barriers	N/A	М	P	П	F
	(c) Ditch	Stabilized with geotextile, gravel bed and	N/A	М	P	\vdash	F
	(c) Diteil	stone lining Netting used to anchor mulch on 8% slopes	+	++	-	+	
	(d) Slopes	unless;	N/A	М	P		F
	(d) Slopes	Erosion control blankets or erosion control mix is in place	N/A	М	P		F
pp (7)		Stabilized for long-term erosion control	N/A	М	P		F
. ,		Sized to handle runoff	N/A	М	P		F
	Stormwater	Constructed and completed w/in same day	N/A	М	P		F
	Channels	If delayed, diversion berms used	N/A	М	P		F
		Check dams installed appropriately	N/A	M	P		F
		Temporary lining installed/prevent scour	N/A	M	P	Щ	F
ор (8)	Roads - Gravel & Paved	Roads & parking drain to stable area	N/A	М	P	Ц	F
		No evidence of overtopping or flooding	N/A	М	P		F
pp (9)	Culverts	Culvert outlet has apron or plunge pools installed	N/A	М	P		F
		Culvert inlets protected with appropriate materials to prevent erosion	N/A	M	P		F
.pp	D 11	Run-off is evenly distrubuted to buffers	N/A	М	P		F
(10)	Parking Areas	Catch basin(s) are capturing run-off without by-pass to other areas	N/A	М	P	\sqcap	F
.pp .(11)	-	Site specific additional measures needed	N/A	М	P		F
	500/MCGP ITATION	SECTION B. Inspection & Maintenance	e (I&M)			
pp	I&M						
(1)		Sediment barriers are functioning as	ТТ	Т Т		П	
	Sediment Barriers	installed. Excess sediment removed from behind	N/A	М	P		F
	Stormwater Channels,	Channel, banks and slopes free of erosion	N/A	M	P		F
	Swales & Ditches	Check dams are functioning as required and being maintained	N/A	M	P		F
	Storage Area	Exposure to stormwater is minimzied in material storage areas	N/A	M	P		F
	Parking and	Impervious areas are draining to stabilized buffer or conveyance	N/A	М	P		F
	Roads	Downslopes are free from erosion	N/A	M	P		F
	Culverts	Inlets and outlets are free from erosion	N/A	М	P		F
	Cuiverts	Aprons and plunge pools are functioning as required and maintained	N/A	М	P		F
		Contractor ESC log up to date	N/A	М	P		F
		Name of inspector is documented	N/A	М	P	\sqcap	F
рр В	Reports	Qualifications listed	N/A	М	P	\sqcap	F
		BMP corrective actions are documented	N/A	М	P		F
		Modifications or additional BMPs were completed w/I 7 days	N/A	М	P		F
	00/MCGP ITATION	SECTION C. Housekeeping					
	Spill Prevention	A spill prevention, containment and response plan is on site	N/A	М	P		F
		Controls are in place to prevent petroleum or other hazardous materials from	N/A	М	P	\parallel	F
(1)		discharging	1,4,1	"			

Prepared by the Interlocal Stormwater Working Group (ISWG)

EROSION AND SEDIMENT CONTROL INSPECTION REPORT FOR CONSTRUCTION SITES AN ACRE OR GREATER

App C(2)	water protection	materials stored or handled that drains to an infiltration area.	1	V/A	N	1	1	2		F	
г.	Fugitivo	Tracking of mud/soil onto public roadway]	V/A	N	1	1	?		F	
Арр	Fugitive sediment and	Stabilized construction entrance]	V/A	N	1	1	?		F	
C(3)	dust	Non-oil dust control used]	V/A	N	1	1	?		F	
	uust	Weekly sweeping of roads]	V/A	N	1	1	?		F	
App C(4)	Debris and other Materials	Litter, construction debris/chemicals protected from exposure to stormwater]	N/A	N	1	1	P		F	
App De-watering	De-watering	Discharging to a wooded buffer, sediment bag, or specifically designated BMP]	V/A	N	1	1	?		F	
	De watering	Discharge is prevented from flowing across disturbed areas]	V/A	N	1	1	?		F	
App C(6)	Non- Stormwater Discharges	Pollution prevention measures are in place for allowable stormwater discharges	1	N/A	N	1	1	2		F	
App C(7)	Additional Requirement	Site specific requirements	1	N/A	N	1	1	P		F	
 Contractor MUST BE certified by DEP in ESC if working within 250' of a river, coastal or freshwater wetland; or 75' of stream. Refer to Maine Erosion & Sediment Control BMPs N/A = Not Applicable; M = Maintenance Needed; P = Pass; F = Fail Chapter 500 specific. 											

- 5. Chapter 500 specific, MCGP proposed changes to match
- 6. Permit language differs, MCGP proposed changes to match

12/26/2017 ISWG Construction Inspection 2041



June 10, 2015

Christopher Belanger, P.E. Belanger Engineering 63 Second Avenue Augusta, ME 04330

RE:

Local and State Permitting Authorization Town Hall Village, Highland Green and OceanView at Falmouth Communities

For Sea Coast Management Company

Dear Chris,

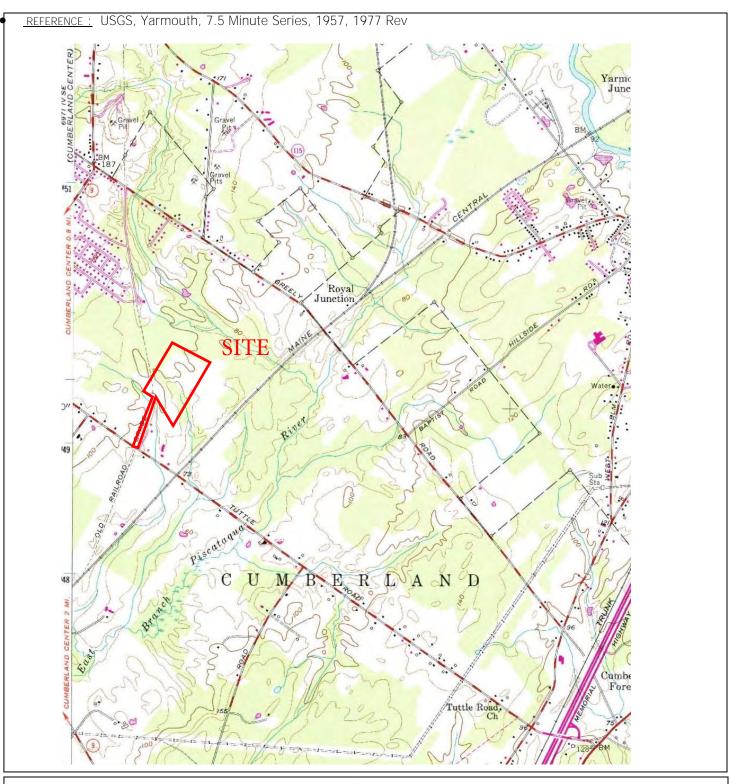
Please accept this letter as the full authorization for Belanger Engineering to act as agent for Sea Coast Management Company with regard to various land use permitting requirements for all of its communities including, but not limited to, Town Hall Village at the Highlands, Highland Green and OceanView at Falmouth. This authorization includes any and all submissions to DEP, DOT, EPA, ACOE and the Towns of Topsham and Falmouth.

Very Truly Yours,

Matthew D. Teare

Director of Development

Sea Coast Management Company





PREPARED FOR:

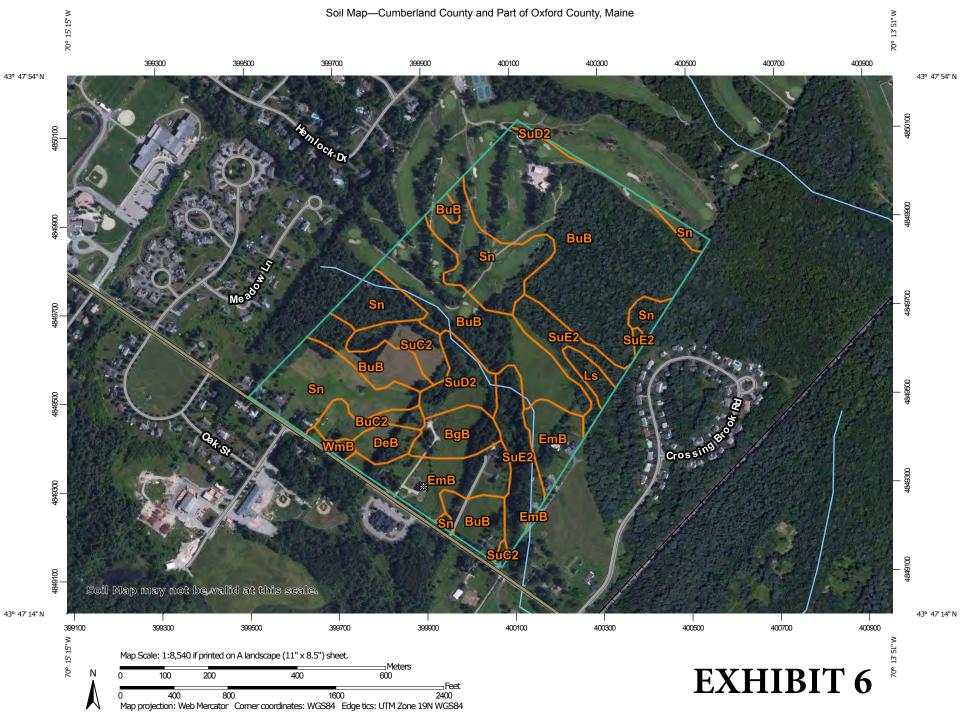
TITLE:

OCEANVIEW AT CUMBERLAND TUTTLE ROAD CUMBERLAND

USGS Locus Map

<u>DATE:</u> 12.2017**■** <u>SCALE:</u> **1″=1000[♠]** <u>JOB NO:</u> 16.084

Exhibit 3



MAP LEGEND

Area of Interest (AOI)

Area of Interest (AOI)

Soils

Soil Survey Areas



Soil Map Unit Points

Soil Map Unit Lines

Special Point Features

(Blowout

Borrow Pit

Clay Spot

Closed Depression

Gravel Pit

Gravelly Spot

Landfill

▲ Lava Flow

Marsh or swamp

Mine or Quarry

Miscellaneous Water

Rock Outcrop

Perennial Water

Sandy Spot

Severely Eroded Spot

Sinkhole

Slide or Slip

Sodic Spot

Spoil Area

Stony Spot

Wery Stony Spot

Wet Spot

Other

Special Line Features

Water Features

Δ

Streams and Canals

Transportation

+++ Rails

Interstate Highways

 \sim

US Routes
Maior Roads

Local Roads

Background

Aerial Photography

MAP INFORMATION

The soil surveys that comprise your AOI were mapped at 1:24.000.

Warning: Soil Map may not be valid at this scale.

Enlargement of maps beyond the scale of mapping can cause misunderstanding of the detail of mapping and accuracy of soil line placement. The maps do not show the small areas of contrasting soils that could have been shown at a more detailed scale.

Please rely on the bar scale on each map sheet for map measurements.

Source of Map: Natural Resources Conservation Service Web Soil Survey URL:

Coordinate System: Web Mercator (EPSG:3857)

Maps from the Web Soil Survey are based on the Web Mercator projection, which preserves direction and shape but distorts distance and area. A projection that preserves area, such as the Albers equal-area conic projection, should be used if more accurate calculations of distance or area are required.

This product is generated from the USDA-NRCS certified data as of the version date(s) listed below.

Soil Survey Area: Cumberland County and Part of Oxford County, Maine

Survey Area Data: Version 12, Sep 15, 2016

Soil map units are labeled (as space allows) for map scales 1:50,000 or larger.

Date(s) aerial images were photographed: Jun 20, 2010—Jul 18, 2010

The orthophoto or other base map on which the soil lines were compiled and digitized probably differs from the background imagery displayed on these maps. As a result, some minor shifting of map unit boundaries may be evident.

Map Unit Legend

Cumberland County and Part of Oxford County, Maine (ME005)				
Map Unit Symbol	Map Unit Name	Acres in AOI	Percent of AOI	
BgB	Belgrade very fine sandy loam, 0 to 8 percent slopes	4.4	3.4%	
BuB	Lamoine silt loam, 3 to 8 percent slopes	59.1	45.8%	
BuC2	Buxton silt loam, 8 to 15 percent slopes	2.9	2.2%	
DeB	Deerfield loamy sand, 3 to 8 percent slopes	2.3	1.8%	
EmB	Elmwood fine sandy loam, 0 to 8 percent slopes	12.4	9.6%	
Ls	Limerick-Saco silt loams	1.5	1.2%	
Sn	Scantic silt loam, 0 to 3 percent slopes	25.3	19.6%	
SuC2	Suffield silt loam, 8 to 15 percent slopes, eroded	4.1	3.2%	
SuD2	Suffield silt loam, 15 to 25 percent slopes, eroded	5.1	3.9%	
SuE2	Suffield silt loam, 25 to 45 percent slopes, eroded	11.2	8.7%	
WmB	Windsor loamy sand, 0 to 8 percent slopes	0.8	0.6%	
Totals for Area of Interest		129.0	100.0%	



SOIL EVALUATION • WETLAND DELINEATIONS • SOIL SURVEYS • WETLAND PERMITTING

4674

Oceanview
Catalpa Lane
Oceanview at Cumberland, LLC
Cumberland, ME

Soil Narrative Report

DATE:

Soil Profiles observed on July 19, 2017

BASE MAP:

Base plan provided by Titcomb Associates

scale 1 inch equals 100 feet and two foot contours.

GROUND CONTROL:

Soil survey boundaries located by Mark Hampton Associates,

Inc. for Class B Soil Survey

Class B-High Intensity Soil Survey (Minimum Standards)

Mapping units of 1 acre or larger.

Scale of 1"= 100 feet or larger.

Up to 25% inclusions in mapping units of which no more than 15% may be dissimilar soils.

Ground Control – test pits located accurately under direction of registered land surveyor Base Map –2 foot contour intervals

Provided:

Mapping units of 1/2 acre or larger

Base map scale of 1"= 100 feet.

Up to 25 percent inclusions in mapping units of which no more than 15 percent is dissimilar soils.

Baseline information and test pits located by Mark Hampton Associates, Inc. Ground topographic survey with one foot contours and ground control provided.

P.O. BOX 1931 • PORTLAND, ME 04104-1931 • 207-756-2900 • mhampto1@maine.rr.com

Quality services that meet your deadline

The accompanying soil profile descriptions, soil map, and this soil narrative report were done in
accordance with the standards adopted by the Maine Association of Professional Soil Scientists,
and the Maine Board of Certification of Geologists and Soil Scientists.

	C.S.S. #216, L.S.E. #263	
Mark J. Hampton	Date	



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Oceanview Catalpa Lane Oceanview at Cumberland, LLC Cumberland, ME

Buxton

(Aquic Dystric Eutrochrepts)

SETTING

PARENT MATERIAL:

Derived from glaciomarine or glaciolaucustrine

sediments

LANDFORM:

Coastal lowlands and river valleys

POSITION IN LANDSCAPE:

Intermediate positions on landform

SLOPE GRADIENT RANGES:

(B) 3-8%, (C) 8-15%, (D) 15-25%

COMPOSITION AND SOIL CHARACTERISTICS

DRAINAGE CLASS:

Moderately well drained with a perched watertable

from 1.5 to 3.0 feet below the surface at some time from November to May or during periods of heavy

precipitation.

TYPICAL PROFILE:

Surface Layer:

Dark Brown, fine sandy loam 0-7"

Subsurface Layer:

Olive brown, silt loam, 8-15"

Subsoil Layer:

Olive gray silty clay loam,

15-32"

Substratum:

Gray silty clay loam +32"

HYDROLOGIC GROUP:

Group C

SURFACE RUNOFF:

Moderate to moderately slow

PERMEABILITY:

Slow to very slow

DEPTH TO BEDROCK:

Greater than 60 inches

HAZARD TO FLOODING:

None

INCLUSIONS (Within Mapping Unit)

CONTRASTING:

Scantic, Lamoine

USE AND MANAGEMENT

Development: The limiting factor for building site development is wetness due to the presence of a high watertable for a portion of the year. Proper foundation drainage or site modification is recommended.

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4674

Oceanview Catalpa Lane Oceanview at Cumberland, LLC Cumberland, ME

> Lamoine (Aeric Haplaquepts)

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sediments

LANDFORM:

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COMPOSITION AND SOIL CHARACTERISTICS

DRAINAGE CLASS:

Somewhat poorly drained with a perched watertable

from 0.5 to 2.0 feet below the surface at some time from November to June or during periods of heavy

precipitation.

TYPICAL PROFILE:

Surface Layer:

Dark Brown, fine sandy loam 0-7"

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Lt. Olive brown silt loam, 7-14"

Subsoil Layer:

Olive silty clay loam, 14-21"

Substratum:

Olive, silty clay loam, 21-65"

HYDROLOGIC GROUP:

Group D

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Moderate to moderately slow

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Slow to very slow

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4674

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Scantic

(Aquic Haplorthod)

SETTING

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(A) 0-3%, (B) 3-8%

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Poorly drained with a perched watertable from 0.0 to 1.0 feet below the surface at some time from October to May

or during periods of heavy precipitation.

TYPICAL PROFILE:

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Subsurface Layer:

Olive gray silt loam, 9-16" Olive silty clay loam, 16-29"

Subsoil Layer:

Substratum:

Olive gray clay loam, 29-65"

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SURFACE RUNOFF:

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DEPTH TO BEDROCK:

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None

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(Within Mapping Unit)

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Mark J. Hampton	Date	

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Greater than 60 inches

HAZARD TO FLOODING:

None

INCLUSIONS (Within Mapping Unit)

CONTRASTING:

Scantic, Lamoine

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Development: The limiting factor for building site development is wetness due to the presence of a high watertable for a portion of the year. Proper foundation drainage or site modification is recommended. P.O. BOX 1931 • PORTLAND, ME 04104-1931 • 207-756-2900 • mhampto1@maine.rr.com



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Oceanview Catalpa Lane Oceanview at Cumberland, LLC Cumberland, ME

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Scantic

(Aquic Haplorthod)

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Substratum:

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(Within Mapping Unit)

CONTRASTING:

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HIGH PERFORMANCE MODULAR BIOFILTRATION SYSTEM

MAINE - CHAPTER 500 DESIGN WORKSHEET/CHECKLIST

1.	FocalPoint Bed Area (min 174 square feet per acre of impervio	us area (e.g. 0.2 acres = 35 sf))
•	Tributary Impervious area Min FocalPoint bed area req'd FocalPoint Bed Area provided *	= 0.15 ac. = 26 sf. = 27 sf.
* se	ee criteria 2. to determine if minimum size is appropriate.	→ 3′x9′
2.	A 0.95 inch Type III 24hr rainfall event shall be modelled to der treated prior to activation of the overflow (typically set at 6-12	
•	Temporary storage depth provided Temporary storage volume provided at above depth Peak ponding depth from 0.95" 24hr storm event	= 12 inches (typ 6" to 12") = 14 cubic feet. = inches
3.	Ratio of the surface area of the filter media (sf) to the temporar that 1:5	y ponding volume (cf) shall be no less
•	Ratio of FocalPoint Bed Area : Temporary Storage Vol	=:
4.	Subsurface Chamber Treatment Row must be sized to treat the	
•	1yr 24hr Peak Flowrate	= 0.4 4cfs
•	Chamber model selected	-
	o Cultec 330 XLHD (1 chamber per 0.227 cfs)	
	o Cultec 150XLHD (1 chamber per 0.185 cfs)	
•	Number of Chambers required	$= \frac{2.4 2}{3.4}$
5.	Controlled release of the Channel Protection over 24-48 hrs	
•	Controlled release of the channel protection volume is being achieve	ed by:
	 Expanded subsurface storage basin with OCS 	z
	 Surface detention basin with OCS 	
6.	The Design shall be reviewed by the manufacturer's representative.	ntive prior to submission and installation
	The Design has been reviewed by ACF Environmental	×
	Engineer will coordinate installation inspection with ACF	₽
	Contact ACE Environmental at 1900 449 2525 vi	



HIGH PERFORMANCE MODULAR BIOFILTRATION SYSTEM

MAINE - CHAPTER 500 DESIGN WORKSHEET/CHECKLIST

1.	. FocalPoint Bed Area (min 174 square feet per acre of impervious a	rea (e.g. 0.2 acres = 35 sf))
•	Min FocalPoint bed area req'd 174 X 0.22	= 0.22 ac. = 38 sf. = 39 sf.
* S	see criteria 2. to determine if minimum size is appropriate.	L> 3'x13'
2.	2. A 0.95 inch Type III 24hr rainfall event shall be modelled to demon- treated prior to activation of the overflow (typically set at 6-12" abo	ove the mulch)
•	Temporary storage depth provided Temporary storage volume provided at above depth Peak ponding depth from 0.95" 24hr storm event	= 12" inches (typ 6" to 12") = 96 cubic feet. = 11" inches
3.	Ratio of the surface area of the filter media (sf) to the temporary pothat 1:5	onding volume (cf) shall be no less
•	Ratio of FocalPoint Bed Area : Temporary Storage Vol	=:
4.	. Subsurface Chamber Treatment Row must be sized to treat the peal	k flow from a 1 yr-24hr storm event.
•	 Cultec 330 XLHD (1 chamber per 0.227 cfs) Cultec 150XLHD (1 chamber per 0.185 cfs) 	= 0.63 cfs = 3.4 ~ [4]
5.	. Controlled release of the Channel Protection over 24-48 hrs	
•	Controlled release of the channel protection volume is being achieved by o Expanded subsurface storage basin with OCS o Surface detention basin with OCS	7: ≱ . □
6.	. The Design shall be reviewed by the manufacturer's representative will be overseen by the manufacturer's representative.	prior to submission and installation
	 The Design has been reviewed by ACF Environmental Engineer will coordinate installation inspection with ACF 	로 보
	Contact ACF Environmental at 1800 448 3636 with a	ny questions



CULTEC Contactor® & Recharger® Chamber Specification Information

	Contactor® 100HD	Recharger® 150XLHD	Recharger® 280HD	Recharger® 330XLHD	Recharger® V8HD¹
Longth	8'	11'	8'	8.5'	8'
Length	2.44 m	3.35 m	2.44 m	2.59 m	2.44 m
To aboll and I am able	7.5'	10.25'	7'	7'	7.5'
Installed Length	2.29 m	3.12 m	2.13 m	2.13 m	2.29 m
\\\/: del-	36"	33"	47"	52"	60"
Width	914 mm	838 mm	1194 mm	1321 mm	1524 mm
llo:abt	12.5"	18.5"	26.5"	30.5"	32"
Height	318 mm	470 mm	673 mm	775 mm	813 mm
Bare Chamber	14.00 ft ³	27.16 ft³	42.55 ft ³	52.21 ft ³	65.09 ft³
Storage Capacity	0.40 m³	0.77 m³	1.21 m³	1.48 m³	1.84 m³
Min. Storage Capacity	28.81 ft ³	50.17 ft ³	64.46 ft ³	79.26 ft ³	99.56 ft³
Surrounded in Stone	0.82 m³	1.42 m³	1.83 m³	2.24 m³	2.82 m³
Scan for Product Downloads and CAD details					

Based on installed length. Stone void is calculated at 40%. Includes 6" (152 mm) stone base, 6" (152 mm) stone above chamber crown and stone around units based on typical minimum center to center spacing.

Other CULTEC models are available if the above chambers do not meet your design parameters. Please contact our Technical Department for more information.



Shown L->R- Contactor 100HD, Recharger 150XLHD, Recharger 280HD, Recharger 330XLHD, and Recharger V8HD.

¹ The Recharger V8HD information is based on the V8IHD Intermediate. See pages 12-13 for information on the V8SHD Starter and V8EHD End units.

TECHNICAL INFORMATION



Minimum Fill Requirements

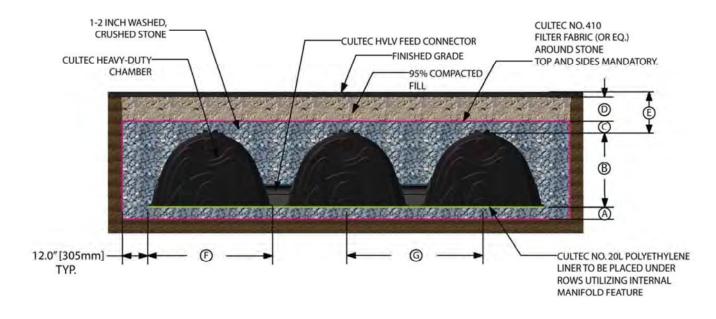
These requirements are for paved traffic applications only. If these models and design parameters do not meet your needs, please call CULTEC's Technical Department at 1-800-4-CULTEC, Ext. 2003 (1-800-428-5832, Ext. 2003) for further information and assistance.

Refer to CULTEC's most current installation instructions for further details including but not limited to acceptable fill materials and vehicle loads.

Table 1

	See Fig. 1	Contactor® 100HD	Recharger® 150XLHD	Recharger® 280HD	Recharger® 330XLHD	Recharger [®] V8HD
Typical Center to	G	3.33′	3.25′	4.33′	4.83′	5.5′
Center Spacing	G	1.02 m	0.99 m	1.32 m	1.47 m	1.68 m
Chamber width	F	36"	33"	47"	52"	60″
Chamber width	Г	914 mm	838 mm	1194 mm	1321 mm	1524 mm
Max. depth of cover allowed	_	12′	12′	12′	12′	8′
above crown of chamber	E	3.66 m	3.66 m	3.66 m	3.66 m	2.44 m
Min. depth required of 95%	Б	8″	8"	8″	10"	12″
Compacted Fill for Paved Traffic Application	D	203 mm	203 mm	203 mm	254 mm	305 mm
Min. depth of stone required	6	6"	6"	6"	6"	6″
above units for traffic applications	С	152 mm	152 mm	152 mm	152 mm	152 mm
Chamban baiabh	В	12.5"	18.5"	26.5"	30.5"	32″
Chamber height	Б	318 mm	470 mm	673 mm	775 mm	813 mm
Min. depth of	۸	6"	6"	6"	6"	6″
stone base	A	152 mm	152 mm	152 mm	152 mm	152 mm

Fig. 1





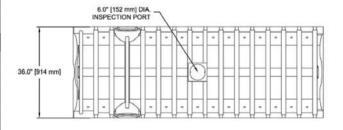
CULTEC Contactor® 100HD

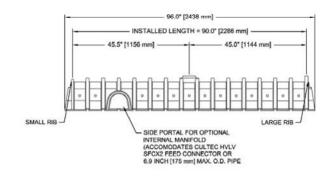
The Contactor® 100HD is a 12.5" (318 mm) tall, low profile chamber and is typically used for installations with depth restrictions or when a larger infiltrative area is required. The Contactor 100HD has the side portal internal manifold feature. The HVLV® SFCx2 Feed Connector is inserted into the side portal of the Contactor 100HD to create the internal manifold.

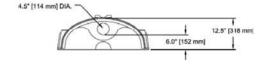
Size (L x W x H)	
512C (L X W X 11)	8' x 36" x 12.5"
	2.44 m x 914 mm x 318 mm
Installed Length	7.5'
	2.29 m
Length Adjustment per Run	0.5'
	0.15 m
Chamber Storage	1.87 ft³/ft
	0.17 m³/m
	14.00 ft ³ /unit
	0.40 m³/unit
Min. Installed Storage	3.84 ft³/ft
	0.36 m³/m
	28.81 ft³/unit
	0.82 m³/unit
Min. Area Required	25 ft ²
	2.32 m ²
Min. Center to Center Spacing	3.33'
	1.02 m
Max. Allowable Cover	12'
	3.66 m
Max. Inlet Opening in Endwall	10"
	250 mm
	6.9"
in Side Portal	175 mm
Compatible Feed Connector	HVLV SFCx2 Feed Connector

	Stone Foundation Depth			
	6"	12"	18"	
	152 mm	305 mm	457 mm	
Chamber and Stone Storage	28.81 ft ³	33.81 ft ³	38.81 ft³	
Per Chamber	0.82 m^3	0.96 m³	1.10 m³	
Min. Effective Depth	2.04'	2.54'	3.04'	
	0.62 m	0.77 m	0.93 m	
Stone Required Per Chamber	1.37 yd³	1.84 yd³	2.30 yd³	
	1.05 m ³	1.40 m³	1.76 m³	









Scan for Contactor 100HD downloads



Calculations are based on installed chamber length. Includes 6" (152 mm) stone above crown of chamber and typical stone surround. Stone void calculated at 40%.

TECHNICAL INFORMATION



CULTEC Recharger® 150XLHD

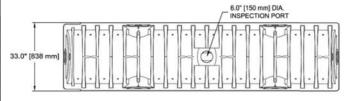
The Recharger® 150XLHD is a 18.5" (470 mm) tall, lower profile chamber and is typically used for installations with depth restrictions or when a larger infiltrative area is required. The Recharger® 150XLHD has the side portal internal manifold feature. HVLV® FC-24 Feed Connectors are inserted into the side portals to create the internal manifold.

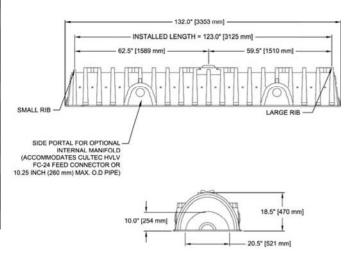
Size (L x W x H) 11' x 33" x 18.5" 3.35 m x 838 mm x 470 mm Installed Length 10.25' 3.12 m Length Adjustment per Run 0.75' 0.23 m Chamber Storage 2.65 ft³/ft 0.25 m³/m 27.16 ft³/unit 0.77 m³/unit Min. Installed Storage 4.89 ft³/ft 0.45 m³/m 50.17 ft³/unit 1.42 m³/unit Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"		
Installed Length 10.25' 3.12 m Length Adjustment per Run 0.75' 0.23 m Chamber Storage 2.65 ft³/ft 0.25 m³/m 27.16 ft³/unit 0.77 m³/unit Min. Installed Storage 4.89 ft³/ft 0.45 m³/m 50.17 ft³/unit 1.42 m³/unit Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"	Size (L x W x H)	11' x 33" x 18.5"
Same		3.35 m x 838 mm x 470 mm
Length Adjustment per Run 0.75' 0.23 m Chamber Storage 2.65 ft³/ft 0.25 m³/m 27.16 ft³/unit 0.77 m³/unit Min. Installed Storage 4.89 ft³/ft 0.45 m³/m 50.17 ft³/unit 1.42 m³/unit Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"	Installed Length	10.25'
O.23 m Chamber Storage 2.65 ft³/ft O.25 m³/m 27.16 ft³/unit O.77 m³/unit O.45 m³/m O.45 m³/m O.45 m³/m O.45 m³/m O.45 m³/m O.45 m³/unit O.45 m³/unit O.45 m³/unit O.45 m³/m O.45 m		3.12 m
Chamber Storage 2.65 ft³/ft 0.25 m³/m 27.16 ft³/unit 0.77 m³/unit Min. Installed Storage 4.89 ft³/ft 0.45 m³/m 50.17 ft³/unit 1.42 m³/unit Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing Min. Center to Center Spacing 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"	Length Adjustment per Run	0.75'
0.25 m³/m 27.16 ft³/unit 0.77 m³/unit Min. Installed Storage 4.89 ft³/ft 0.45 m³/m 50.17 ft³/unit 1.42 m³/unit Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"		0.23 m
27.16 ft³/unit 0.77 m³/unit Min. Installed Storage 4.89 ft³/ft 0.45 m³/m 50.17 ft³/unit 1.42 m³/unit Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"	Chamber Storage	2.65 ft ³ /ft
0.77 m³/unit		0.25 m³/m
Min. Installed Storage 4.89 ft³/ft 0.45 m³/m 50.17 ft³/unit 1.42 m³/unit Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"		27.16 ft³/unit
0.45 m³/m 50.17 ft³/unit 1.42 m³/unit Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"		0.77 m³/unit
50.17 ft³/unit 1.42 m³/unit Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"	Min. Installed Storage	4.89 ft³/ft
1.42 m³/unit Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"		0.45 m³/m
Min. Area Required 33.31 ft² 3.09 m² Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"		50.17 ft³/unit
Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"		1.42 m³/unit
Min. Center to Center Spacing 3.25' 0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"	Min. Area Required	33.31 ft ²
0.99 m Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"		3.09 m ²
Max. Allowable Cover 12' 3.66 m Max. Inlet Opening in Endwall 12"	Min. Center to Center Spacing	3.25'
3.66 m Max. Inlet Opening in Endwall 12"		0.99 m
Max. Inlet Opening in Endwall 12"	Max. Allowable Cover	12'
Than Inde opening in Litarian		3.66 m
200	Max. Inlet Opening in Endwall	12"
300 mm		300 mm
Max. Allowable O.D. 10.25"		10.25"
in Side Portal 260 mm	in Side Portal	260 mm
Compatible Feed Connector HVLV FC-24 Feed Connector	Compatible Feed Connector	HVLV FC-24 Feed Connector

	Stone Foundation Depth			
	6"	12"	18"	
	152 mm	305 mm	457 mm	
Chamber and Stone Storage	50.17 ft ³	56.83 ft ³	63.49 ft³	
Per Chamber	1.42 m³	1.61 m³	1.80 m³	
Min. Effective Depth	2.54'	3.04'	3.54'	
	0.77 m	0.93 m	1.08 m	
Stone Required Per Chamber	2.13 yd³	2.75 yd³	3.36 yd³	
	1.63 m³	2.10 m^3	2.57 m³	

Calculations are based on installed chamber length. Includes 6" (152 mm) stone above crown of chamber and typical stone surround. Stone void calculated at 40%.







Scan for Recharger 150XLHD downloads



STATE OF MAINE DEPARTMENT OF ENVIRONMENTAL PROTECTION





February 2, 2017

Stormwater Systems ACF-Convergent Water Technologies Alliance 23 Faith Drive Gorham, ME 04038 ATTN: Robert Woodman and Scott Gorneau

Dear Mr. Woodman and Mr. Gorneau:

This letter replaces the May 16, 2016 approval from the Department of Environmental Protection (Department) that authorized the use of the FocalPoint system. The FocalPoint system (a high performance modular biofiltration system), when installed in series with a subsurface chamber-based treatment row, meets the requirements of the General Standards (Section 4.C.) of the Stormwater Management Rules (Chapter 500), provided that the system is filled with the FocalPoint engineered filter media; it is sized to meet the requirements of the General Standards (Section 4.B.); and it is installed, operated and maintained in accordance with the following provisions:

- 1. The FocalPoint system must be sized in accordance with the manufacturer's latest field test results with the goal of treating 90% of the annual runoff volume. To accomplish this, the system must be modelled in HydroCAD (or similar TR-55 modelling software) to demonstrate that the entire volume of a 0.95 inch Type III 24-hr storm is treated prior to activation of the bypass/overflow (typically set at 6" to 12" above the mulch surface). When sizing the FocalPoint system to meet Chapter 500, note that runoff from the entire contributing drainage area, including pervious areas, must be included in the modeled runoff values.
- 2. The surface area of the media within the FocalPoint must be a minimum of 174 square feet per 1 acre of impervious area treated (26 sq. ft. per 0.15 acres). The thickness of the media is to be no less than 1.5 ft. (18 inches) and the ratio of the surface area of the filter media bed in square feet to the ponding volume in cubic feet must be no less than 1 to 5.
- 3. The FocalPoint system consists of five components that include: 1) an open cell underdrain; 2) a wide aperture separation mesh wrap around the underdrain; 3) a layer of clean washed, 3/8" diameter bridging stone; 4) advanced high flow rate engineered media with an infiltration rate of 100 inches per hour; and 5) double shredded hardwood mulch. These components are built from the bottom up to create a mostly permeable profile that measures 3 feet from bottom of underdrain to top of mulch. The ponding

17 STATE HOUSE STATION AUGUSTA, MAINE 04333-0017 (207) 287-7688 FAX: (207) 287-7826 (207) 941-4570 FAX: (207) 941-4584

106 HOGAN ROAD, SUITE 6 312 CANCO ROAD BANGOR, MAINE 04401

PORTLAND PORTLAND, MAINE 04103

PRESQUE ISLE 1235 CENTRAL DRIVE, SKYWAY PARK PRESQUE ISLE, MAINE 04769 (207) 822-6300 FAX: (207) 822-6303 (207) 764-0477 FAX: (207) 760-3143

Letter to Robert Woodman and Scott Gorneau February 2, 2017 Page 2 of 3

depth above the mulch surface is typically 6 to 12 inches and varies based on site conditions. An overflow outlet should be placed above the ponding depth.

- 4. The FocalPoint system requires the establishment of vegetation that is tolerant of wet and dry conditions. Plants that are not performing as desired should be replaced as needed. A list of appropriate plants for use in the FocalPoint system is provided at: http://www.acfenvironmental.com/products/stormwater-management/filtration/focal-point/.
- 5. The FocalPoint biofiltration system must be placed in-line with a subsurface chamber-based treatment row that is approved by the Department such that both the treated discharge and the bypass discharge from the FocalPoint system drain to the treatment row. The treatment row must be sized to treat the peak flow from a 1-year, 24-hour storm event. The treatment row structure must be continuous and without obstacle for cleaning, and must have access at both ends for the removal of accumulated sediment and debris. The treatment row must be underlain with a bottom surface consisting of 2 layers of woven geotextile (e.g., ACF S300) that extends 18 to 24 inches beyond all sides of the bottom of the structure.
- 6. Additional storage downstream of the FocalPoint and treatment row will be required to store at least the sum of 1.0 inch of runoff from the impervious areas and 0.4 inches of runoff from the lawn and landscaped areas that drain to the system unless attenuation of the channel protection volume is not required (i.e. direct discharge to a lake, tidal waters, or a major river). An external outlet control structure must control the flow out of a downstream storage system, sized for the entire channel protection volume, and drain in no less than 24 hours or more than 48 hours.
- 7. If required for flooding control, the storage system can be sized to provide for the storage and release of the peak flow with a regulated flow rate from 24-hour storms of the 2, 10, and 25-year frequencies such that the peak flows from the project site do not exceed the peak flow prior to undertaking the project.
- 8. The applicant must demonstrate that the design meets all the manufacturer's specifications and shall be reviewed by the manufacturer prior to submission to the Department for approval. Review and approval of the design by the manufacturer will be sufficient to demonstrate conformance with the manufacturer's specifications. The FocalPoint system must be installed by a manufacturer's certified installer or under the supervision of a manufacturer's representative.
- 9. Components of the system that are delivered in bulk (i.e., mulch, high flow media and clean washed bridging stone), should be contained in nylon super sacks to promote ease of storage and protection during on-site construction activities.

Letter to Robert Woodman and Scott Gorneau February 2, 2017 Page 3 of 3

- 10. The FocalPoint and treatment row system should be inspected and maintained if necessary at least once every six months to maintain the established efficiency for pollutant removal. Prior to construction, a five-year binding inspection and maintenance contract must be provided prior to the Department for review and approval, and must be renewed before contract expiration. The contract will be with a professional with knowledge of erosion and stormwater control, including experience with the proposed system.
- 11. The overall stormwater management design must meet all Department criteria and sizing specifications and will be reviewed and approved by the Department prior to use.
- 12. This approval is conditional on full-scale, cold climate field testing results, performed in accordance with the Department's protocols, confirming that the pollutant removal efficiency and sizing of the FocalPoint system are appropriate. The "permit shield" provision (Section 14) of the Chapter 500 rules will apply, and the Department will not require the replacement of the system if, with proper maintenance, pollutant removals do not satisfy the General Standard Best Management Practices.

Questions concerning this decision should be directed to David Waddell at (207) 215-6932 or Jeff Dennis at (207) 215-6376.

Sincerely,

Mark Bergeron, P.E.

Director

Bureau of Land Resources

Mak & Brevar

cc: Don Witherill, Maine DEP

ACF Environmental 2831 Cardwell Rd Richmond, VA 23234



Engineer of Record

January 10, 2018

SUBJECT: Plan Review and Construction Oversight Commitment

Dear Chris,

Thank you for forwarding the preliminary plans for the OceanView @ Cumberland Expansion project in Cumberland, ME to ACF environmental for review of the proposed FocalPoint biofiltration system.

Our team has reviewed the plans and take no exceptions to the location and application of the FocalPoint system for this project.

It appears that the system has been designed in accordance with the design criteria set forth by Maine DEP in the May 16, 2016 FocalPoint system approval letter and meets the system's specifications etc.

Upon completion of your detail sheet we would be happy to review that also.

With regard to the installation, ACF Environmental will host a preconstruction meeting with the site contractor and will be on-site during the entire installation to ensure that the installation is being conducted in accordance with our standard installation procedures.

ACF Environmental will also provide the first year's maintenance on the FocalPoint bed area.

Please review and contact me with any questions from your office.

We look forward to working with you on this project.

Sincerely,

W. Scott Gorneau, P.E.

National Manager - Stormwater Systems

ACF-Convergent Alliance

cc: Rob Woodman, P.E., Senior Stormwater Engineer, ACF Environmental



SOIL EVALUATION • WETLAND DELINEATIONS • SOIL SURVEYS • WETLAND PERMITTING

4674

January 4, 2018

Mr. Rick Licht Licht Environmental Design LLC 35 Fran Circle Gray, ME 04039

Re: Soil Evaluation, Proposed Stormwater Devices, Oceanview at Cumberland, Cumberland, ME

Dear Rick,

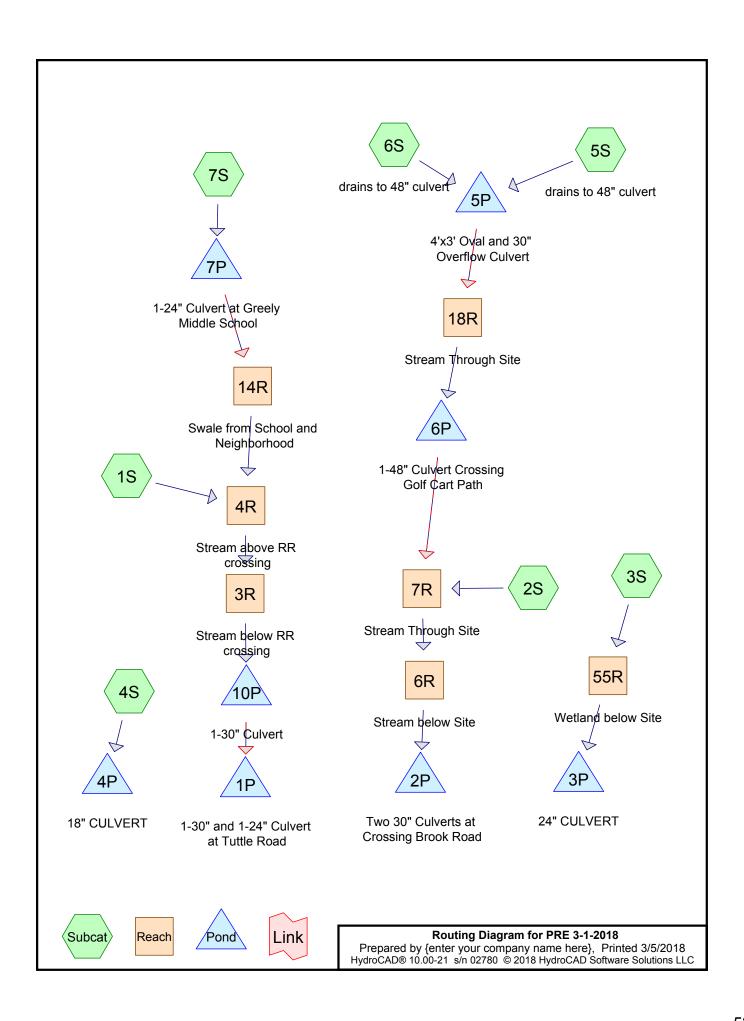
I completed a soil evaluation for the proposed stormwater treatment program for development activities for the proposed Oceanview at Cumberland project Cumberland, ME. The soil evaluation was conducted in accordance with the Maine Subsurface Wastewater Disposal Rules dated August 2015, as amended. I evaluated two backhoe excavated soil test pits in each of both stormwater treatment ponds. The soils found on the parcel are moderately well drained marine lacustrine soils. There is a seasonal high watertable at approximately 14 and 28 inches, respectively. There was no observed groundwater table in either of the soil test pits. The soil test pit log descriptions are attached.

If you have any questions or require additional information, please contact me.

Mark J. Hampton J. F.

Licensed Site Evaluator #263 Certified Soil Scientist #216

		Compelane	-	Boring Probe		1	Project Location		
	Organic hor	zon thickness	Ground surface	ce elev	Explor	ation Symbol # " Organic hor	<u>STW-2</u> izon thickness	Test Pit DE	Boring Probe
	91	" Depth of explora	ation or to refu	sal	Pon	dz	"Depth of explo	ration or to refu	sal
0 -	Fine Sandy	Consistency	Color Daw Brown	Redox Features	0 -	Texture	Consistency	Color	Redox Feature
	408		, , , , , , , , , , , , , , , , , , , ,			(ine sandy	Fride	haye	
3 10-	1 sancy	Fridely	Bucur		(S) 10-	1000		17000	
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20-	Z:144		pline	Company	90 20-		Tribal	BLRIN	
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30-	(orla		21009		Soil S				
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Printed 3/5/2018 Page 2

Area Listing (selected nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
94.000	98	EXISTING IMPERVIOUS AREA (1S, 2S, 4S, 5S, 6S, 7S)
147.000	74	EXISTING LAWN C (1S, 2S, 3S, 4S, 5S, 6S, 7S)
192.310	70	WOODS / FIELD HSG C (1S, 2S, 3S, 4S, 5S, 6S)
433.310	77	TOTAL AREA

Prepared by {enter your company name here}
HydroCAD® 10.00-21 s/n 02780 © 2018 HydroCAD Software Solutions LLC

Printed 3/5/2018

Page 3

Summary for Subcatchment 1S:

Runoff = 48.56 cfs @ 12.85 hrs, Volume= 8.142 af, Depth> 0.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac)	CN	Desc	cription		
*	57.	000	70	WOO	DDS / FIEL	_D HSG C	
*	19.	000	98	EXIS	TING IMP	PERVIOUS	AREA
*	25.	000	74	EXIS	TING LAV	VN C	
	101.	000	76	Weig	hted Aver	age	
	82.	000		81.19	9% Pervio	us Area	
	19.	000		18.8	1% Imperv	ious Area	
	_		_				
	Tc	Length		Slope	Velocity	Capacity	Description
_	(min)	(feet))	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.	0400	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.	0400	0.50		Shallow Concentrated Flow, BC
_							Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1.000) To	otal			

Summary for Subcatchment 2S:

Runoff = 45.47 cfs @ 12.74 hrs, Volume= 6.986 af, Depth> 0.97"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac)	CN	Desc	cription		
*	43.	310	70	WOO	DDS / FIEL	D HSG C	
*	13.	000	98	EXIS	STING IMP	ERVIOUS	AREA
*	30.	000	74	EXIS	STING LAV	VN C	
	86.	310	76	Weig	hted Aver	age	
	73.	310		84.9	4% Pervio	us Area	
	13.	000		15.0	6% Imperv	ious Area	
	Тс	Lengt	h S	Slope	Velocity	Capacity	Description
_	(min)	(feet	:)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	10	0.0	.0400	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	21.7	65	0.0	.0400	0.50		Shallow Concentrated Flow, BC
_							Forest w/Heavy Litter Kv= 2.5 fps
	50.5	75	T C	otal			

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Summary for Subcatchment 3S:

Runoff = 14.23 cfs @ 12.68 hrs, Volume= 2.156 af, Depth> 0.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac) C	N Des	cription		
*	34.	000	70 WO	ODS / FIEI	D HSG C	
*	0.	000	98 EXIS	STING IMF	PERVIOUS	AREA
*	4.	000	74 EXIS	STING LAV	WN C	
			,	ghted Aver	0	
	38.	000	100.	.00% Pervi	ous Area	
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
_	15.0	450	0.0400	0.50		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, BC Forest w/Heavy Litter Kv= 2.5 fps
	43.8	550	Total			

Summary for Subcatchment 4S:

Runoff = 5.49 cfs @ 12.86 hrs, Volume= 0.935 af, Depth> 0.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac)	<u>CN</u>	Desc	cription		
*	5.	000	70	WOO	DDS / FIEL	D HSG C	
*		000	98			PERVIOUS	ΛDEΛ
*							ANLA
_		000	74	EXIS	STING LAV	VN C	
	13.	000	74	Weic	hted Aver	age	
	12.	000			, 1% Pervio		
		000			% Impervi		
	٠.	000		7.03	70 IIIIpci vii	ous Aica	
	Тс	Length	า 5	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100) ().	.0400	0.06		Sheet Flow, AB
					0.00		Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	۱ ۸	0400	0.50		Shallow Concentrated Flow, BC
	30.0	900	<i>)</i> 0.	.0400	0.50		
_							Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000) To	otal			

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Summary for Subcatchment 5S: drains to 48" culvert

Runoff = 46.40 cfs @ 13.55 hrs, Volume= 11.467 af, Depth> 1.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

_	Area	(ac) (CN Des	cription		
*	47.	000	70 WO	ODS / FIEL	D HSG C	
*	36.	000	98 EXI	STING IMF	PERVIOUS	AREA
*	35.	000	74 EXI	STING LAV	VN C	
	118.	000	80 Wei	ghted Aver	age	
	82.	000	69.4	9% Pervio	us Area	
	36.	000	30.5	1% Imperv	ious Area	
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	38.0	100	0.0200	0.04		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	60.0	900	0.0100	0.25		Shallow Concentrated Flow, BC
						Forest w/Heavy Litter Kv= 2.5 fps
	14.8	2,671	0.0400	3.00		Shallow Concentrated Flow, CD
_						Grassed Waterway Kv= 15.0 fps
	112.8	3,671	Total			

Summary for Subcatchment 6S: drains to 48" culvert

Runoff = 54.10 cfs @ 12.54 hrs, Volume= 6.986 af, Depth> 1.27"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac) (CN Des	cription		
*	6.	000	70 WO	ODS / FIEI	LD HSG C	
*	20.	000	98 EXIS	STING IMF	PERVIOUS	AREA
*	40.	000	74 EXIS	STING LAV	WN C	
	66.	000	81 Wei	ghted Aver	age	
	46.	000		0% Pervio		
	20.	000	30.3	0% Imperv	vious Area	
				·		
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	5.0	900	0.0400	3.00		Shallow Concentrated Flow, BC
						Grassed Waterway Kv= 15.0 fps
	3.7	2,500	0.0400	11.41	182.56	Trap/Vee/Rect Channel Flow, CD
						Bot.W=4.00' D=2.00' Z= 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	37.5	3.500	Total			

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Summary for Subcatchment 7S:

Runoff = 19.44 cfs @ 12.12 hrs, Volume= 1.427 af, Depth> 1.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac)	CN	Desc	cription		
*	0.	000	70	WOO	DDS / FIEL	D HSG C	
*	5.	000	98	EXIS	STING IMP	PERVIOUS	AREA
*	6.	000	74	EXIS	STING LAV	VN C	
-	11.	000	85	Weic	hted Aver	age	
	6.	000		_	5% Pervio	•	
	5.	000		45.4	5% Imperv	vious Area	
					•		
	Tc	Lengtl	h S	Slope	Velocity	Capacity	Description
	(min)	(feet	:)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>
	7.5	100	0 0.	0400	0.22		Sheet Flow, AB
							Grass: Short n= 0.150 P2= 3.10"
	1.1	200	0.	0400	3.00		Shallow Concentrated Flow, BC
							Grassed Waterway Kv= 15.0 fps
-	8.6	300	0 To	otal			•

Summary for Reach 3R: Stream below RR crossing

Inflow Area = 112.000 ac, 21.43% Impervious, Inflow Depth > 0.94" for 2 YEAR event

Inflow = 48.80 cfs @ 12.87 hrs, Volume= 8.797 af

Outflow = 48.66 cfs @ 12.95 hrs, Volume= 8.745 af, Atten= 0%, Lag= 4.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity = 5.23 fps, Min. Travel Time = 2.7 min Avg. Velocity = 2.61 fps, Avg. Travel Time = 5.5 min

Peak Storage= 8,009 cf @ 12.90 hrs Average Depth at Peak Storage= 1.28'

Bank-Full Depth= 4.00' Flow Area= 40.0 sf, Capacity= 373.38 cfs

6.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 14.00'

Length= 860.0' Slope= 0.0116 '/'

Inlet Invert= 82.00', Outlet Invert= 72.00'



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Summary for Reach 4R: Stream above RR crossing

Inflow Area = 112.000 ac, 21.43% Impervious, Inflow Depth > 0.94" for 2 YEAR event

Inflow = 48.88 cfs @ 12.85 hrs, Volume= 8.810 af

Outflow = 48.80 cfs @ 12.87 hrs, Volume= 8.797 af, Atten= 0%, Lag= 1.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.97 fps, Min. Travel Time= 0.7 min Avg. Velocity = 2.45 fps, Avg. Travel Time= 1.4 min

Peak Storage= 1,966 cf @ 12.86 hrs Average Depth at Peak Storage= 1.34'

Bank-Full Depth= 4.00' Flow Area= 40.0 sf, Capacity= 346.26 cfs

6.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 14.00'

Length= 200.0' Slope= 0.0100 '/'

Inlet Invert= 84.00', Outlet Invert= 82.00'



Summary for Reach 6R: Stream below Site

Inflow Area = 270.310 ac, 25.53% Impervious, Inflow Depth > 1.09" for 2 YEAR event

Inflow = 94.39 cfs @ 13.05 hrs. Volume= 24.448 af

Outflow = 94.20 cfs @ 13.10 hrs, Volume= 24.384 af, Atten= 0%, Lag= 2.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 5.06 fps, Min. Travel Time= 1.5 min

Avg. Velocity = 2.96 fps, Avg. Travel Time= 2.5 min

Peak Storage= 8,394 cf @ 13.07 hrs

Average Depth at Peak Storage= 1.89'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 538.97 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 61.00', Outlet Invert= 58.00'



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Summary for Reach 7R: Stream Through Site

Inflow Area = 270.310 ac, 25.53% Impervious, Inflow Depth > 1.09" for 2 YEAR event

Inflow 94.57 cfs @ 12.98 hrs. Volume= 24.550 af

94.39 cfs @ 13.05 hrs, Volume= Outflow 24.448 af, Atten= 0%, Lag= 4.4 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.90 fps, Min. Travel Time= 2.3 min Avg. Velocity = 4.54 fps, Avg. Travel Time= 4.0 min

Peak Storage= 13,154 cf @ 13.01 hrs Average Depth at Peak Storage= 1.29'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 683.45 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,100.0' Slope= 0.0245 '/'

Inlet Invert= 88.00', Outlet Invert= 61.00'



Summary for Reach 14R: Swale from School and Neighborhood

Inflow Area = 11.000 ac. 45.45% Impervious, Inflow Depth > 0.85" for 2 YEAR event

1.21 cfs @ 14.58 hrs, Volume= Inflow 0.776 af

Outflow 1.21 cfs @ 15.70 hrs, Volume= 0.668 af, Atten= 0%, Lag= 67.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.54 fps, Min. Travel Time= 36.4 min

Avg. Velocity = 1.17 fps, Avg. Travel Time= 47.8 min

Peak Storage= 2,643 cf @ 15.09 hrs

Average Depth at Peak Storage= 0.19'

Bank-Full Depth= 3.00' Flow Area= 21.0 sf, Capacity= 147.12 cfs

4.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 10.00'

Length= 3,366.0' Slope= 0.0100 '/'

Inlet Invert= 117.66', Outlet Invert= 84.00'



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Summary for Reach 18R: Stream Through Site

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 1.16" for 2 YEAR event

Inflow 67.65 cfs @ 12.77 hrs. Volume= 17.762 af

66.47 cfs @ 12.89 hrs, Volume= Outflow 17.661 af, Atten= 2%, Lag= 7.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.18 fps, Min. Travel Time= 3.2 min Avg. Velocity = 3.42 fps, Avg. Travel Time= 5.8 min

Peak Storage= 12,911 cf @ 12.83 hrs Average Depth at Peak Storage= 1.17'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 563.18 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,200.0' Slope= 0.0167 '/'

Inlet Invert= 125.00', Outlet Invert= 105.00'



Summary for Reach 55R: Wetland below Site

38.000 ac, 0.00% Impervious, Inflow Depth > 0.68" for 2 YEAR event 14.23 cfs @ 12.68 hrs, Volume= 2.156 af Inflow Area =

Inflow

Outflow 14.17 cfs @ 12.76 hrs, Volume= 2.143 af, Atten= 0%, Lag= 4.5 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.69 fps, Min. Travel Time= 2.8 min

Avg. Velocity = 1.37 fps, Avg. Travel Time= 5.5 min

Peak Storage= 2,367 cf @ 12.71 hrs

Average Depth at Peak Storage= 0.61'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 540.76 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 63.02', Outlet Invert= 60.00'



Device Routing

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Summary for Pond 1P: 1-30" and 1-24" Culvert at Tuttle Road

Inflow Area = 112.000 ac, 21.43% Impervious, Inflow Depth > 0.92" for 2 YEAR event

Inflow = 38.99 cfs @ 13.29 hrs, Volume= 8.571 af

Outflow = 38.34 cfs @ 13.37 hrs, Volume= 8.561 af, Atten= 2%, Lag= 5.1 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 69.82' @ 13.37 hrs Surf.Area= 5,442 sf Storage= 8,451 cf

Plug-Flow detention time= 3.2 min calculated for 8.532 af (100% of inflow)

Center-of-Mass det. time= 2.8 min (890.4 - 887.5)

Volume	Invert	Avail.Storage	Storage Description
#1	68.00'	31,683 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
68.00	3,850	0	0
70.00	5,600	9,450	9,450
72.00	7,800	13,400	22,850
73.00	9,865	8,833	31,683

Invert Outlet Devices

#1	Primary	67.50'	30.0" Round Culvert
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf
#2	Primary	67.50'	24.0" Round Culvert
			L= 50.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
#3	Secondary	71.00'	50.0' long x 50.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=38.29 cfs @ 13.37 hrs HW=69.82' (Free Discharge)

1=Culvert (Inlet Controls 24.59 cfs @ 5.18 fps)

-2=Culvert (Inlet Controls 13.70 cfs @ 4.36 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=68.00' (Free Discharge)

-3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: Two 30" Culverts at Crossing Brook Road

Inflow Area =	270.310 ac, 25.53% Impervious, Inflov	v Depth > 1.08" for 2 YEAR event
Inflow =	94.20 cfs @ 13.10 hrs, Volume=	24.384 af
Outflow =	55.70 cfs @ 14.58 hrs, Volume=	22.669 af, Atten= 41%, Lag= 88.8 min
Primary =	55.70 cfs @ 14.58 hrs, Volume=	22.669 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 47.62' @ 14.58 hrs Surf.Area= 96,190 sf Storage= 282,628 cf

Plug-Flow detention time= 75.6 min calculated for 22.594 af (93% of inflow) Center-of-Mass det. time= 56.5 min (947.0 - 890.5)

Volume	Invert	Avail.Sto	rage Storage	e Description		
#1	44.00'	2,030,00	00 cf Custor	n Stage Data (P	rismatic)Listed below (Recalc)	
Elevation			Inc.Store	Cum.Store		
(fee		sq-ft)	(cubic-feet)	(cubic-feet)		
44.0		,000	0	0		
46.0		,000	140,000	140,000		
48.0		,000	180,000	320,000		
50.0		,000	220,000	540,000		
52.0		,000	280,000	820,000		
54.0		,000	340,000 400,000	1,160,000		
56.0		220,000 250,000		1,560,000		
58.0	00 250	,000	470,000	2,030,000		
Device	Routing	Invert	Outlet Device	es		
#1	Primary	44.00'	30.0" Roun	d Culvert		
	•		L= 50.0' RC	P, sq.cut end pro	ojecting, Ke= 0.500	
			Inlet / Outlet	Invert= 44.00' / 4	2.00' S= 0.0400 '/' Cc= 0.900	
					ight & clean, Flow Area= 4.91 sf	
#2	Primary	44.00'	24.0" Roun			
			L= 50.0' CPP, projecting, no headwall, Ke= 0.900			
					2.00' S= 0.0400 '/' Cc= 0.900	
440		50.001			or, Flow Area= 3.14 sf	
#3	Secondary	56.00'			road-Crested Rectangular Weir	
			` ,		0.80 1.00 1.20 1.40 1.60	
			Coei. (Erigiis	511) 2.08 2.70 2.	70 2.64 2.63 2.64 2.64 2.63	

Primary OutFlow Max=55.70 cfs @ 14.58 hrs HW=47.62' (Free Discharge)

1=Culvert (Inlet Controls 36.38 cfs @ 7.41 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=44.00' (Free Discharge)

3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 3P: 24" CULVERT

Inflow Area =	38.000 ac,	0.00% Impervious, Inflow De	epth > 0.68" for 2 YEAR event
Inflow =	14.17 cfs @	12.76 hrs, Volume=	2.143 af
Outflow =	12.99 cfs @	12.91 hrs, Volume=	2.117 af, Atten= 8%, Lag= 9.3 min
Primary =	12.99 cfs @	12.91 hrs, Volume=	2.117 af
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 55.74' @ 12.91 hrs Surf.Area= 6,379 sf Storage= 7,586 cf

Plug-Flow detention time= 12.2 min calculated for 2.117 af (99% of inflow)

²⁼Culvert (Inlet Controls 19.33 cfs @ 6.15 fps)

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Center-of-Mass det. time= 8.2 min (871.4 - 863.2)

<u>Volume</u>	Inver	t Avail.Sto	<u>rage Storage</u>	Description	
#1	54.00	56,34	42 cf Custom	Stage Data (Pi	rismatic)Listed below (Recalc)
Elevation	on S	Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
54.0	00	2,362	0	0	
56.0	00	6,990	9,352	9,352	
58.0	00	10,000	16,990	26,342	
60.0	00	20,000	30,000	56,342	
Device	Routing	Invert	Outlet Devices	S	
#1	Primary	54.00'	24.0" Round	Culvert	
#2	Secondary		Inlet / Outlet In n= 0.011 Cor 25.0' long x 2 Head (feet) 0	nvert= 54.00' / 5 ncrete pipe, strai 25.0' breadth B .20 0.40 0.60	ojecting, Ke= 0.500 3.00' S= 0.0200 '/' Cc= 0.900 ight & clean, Flow Area= 3.14 sf road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=12.97 cfs @ 12.91 hrs HW=55.73' (Free Discharge) 1=Culvert (Inlet Controls 12.97 cfs @ 4.48 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=54.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 4P: 18" CULVERT

Inflow Area =	13.000 ac,	7.69% Impervious, Inflow De	epth > 0.86" for 2 YEAR event
Inflow =	5.49 cfs @	12.86 hrs, Volume=	0.935 af
Outflow =	4.55 cfs @	13.16 hrs, Volume=	0.910 af, Atten= 17%, Lag= 17.9 min
Primary =	4.55 cfs @	13.16 hrs, Volume=	0.910 af
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 86.04' @ 13.16 hrs Surf.Area= 8,631 sf Storage= 6,225 cf

Plug-Flow detention time= 28.3 min calculated for 0.910 af (97% of inflow) Center-of-Mass det. time= 19.6 min (879.1 - 859.5)

Volume	Invert	Avail.Storage	Storage	Description	
#1	85.00'	82,755 cf	Custom	n Stage Data (Pri	smatic)Listed below (Recalc)
Elevation (feet)	Surf.A (sc		c.Store ic-feet)	Cum.Store (cubic-feet)	
85.00	3,3	343	0	0	
86.00	8,4	410	5,877	5,877	
88.00	19,2	234	27,644	33,521	
90.00	30,0	000	49,234	82,755	

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Device	Routing	Invert	Outlet Devices
#1	Primary	85.00'	18.0" Round Culvert
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 85.00' / 84.00' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.77 sf
#2	Secondary	89.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=4.54 cfs @ 13.16 hrs HW=86.04' (Free Discharge) 1=Culvert (Inlet Controls 4.54 cfs @ 3.47 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=85.00' (Free Discharge)

2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 5P: 4'x3' Oval and 30" Overflow Culvert

Inflow Area =	184.000 ac, 30.43% Impervious, Inflov	w Depth > 1.20" for 2 YEAR event
Inflow =	69.48 cfs @ 12.62 hrs, Volume=	18.453 af
Outflow =	67.65 cfs @ 12.77 hrs, Volume=	17.762 af, Atten= 3%, Lag= 8.9 mir
Primary =	38.36 cfs @ 12.77 hrs, Volume=	14.947 af
Secondary =	29.29 cfs @ 12.77 hrs, Volume=	2.815 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 137.32' @ 12.77 hrs Surf.Area= 17,956 sf Storage= 84,792 cf

Plug-Flow detention time= 32.4 min calculated for 17.762 af (96% of inflow) Center-of-Mass det. time= 20.7 min (884.6 - 863.8)

Volume	Invert	Avail.Stor	age Storage [Description	
#1	129.00'	142,73	5 cf Custom	Stage Data (Pri	smatic)Listed below (Recalc)
Elevatio		urf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
129.0	00	4,441	0	0	
130.0	00	6,196	5,319	5,319	
132.0	00	8,225	14,421	19,740	
134.0	00	10,880	19,105	38,845	
136.0	00	14,005	24,885	63,730	
138.0	00	20,000	34,005	97,735	
140.0	00	25,000	45,000	142,735	
<u>Device</u>	Routing	Invert	Outlet Devices		
#1	Primary	129.00'	4.0" W x 3.0" I	H, R=3.0" Ellip	tical Culvert
			L= 30.0' RCP	, sq.cut end pro	jecting, Ke= 0.500
			Inlet / Outlet In	vert= 129.00' / 1	28.00' S= 0.0333 '/' Cc= 0.900
			n= 0.011 Cond	crete pipe, straig	ght & clean, Flow Area= 0.07 sf
#2	Primary	132.00'	30.0" Round		•
	•		L= 50.0' CPP.	projecting, no l	neadwall, Ke= 0.900
					28.00' S= 0.0800 '/' Cc= 0.900
					r, Flow Area= 4.91 sf
#3	Secondary	137.00'		•	oad-Crested Rectangular Weir

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Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.63

Primary OutFlow Max=38.34 cfs @ 12.77 hrs HW=137.31' (Free Discharge)

1=Culvert (Barrel Controls 0.72 cfs @ 10.76 fps)
2=Culvert (Inlet Controls 37.62 cfs @ 7.66 fps)

Secondary OutFlow Max=28.51 cfs @ 12.77 hrs HW=137.31' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 28.51 cfs @ 1.51 fps)

Summary for Pond 6P: 1-48" Culvert Crossing Golf Cart Path

184.000 ac, 30.43% Impervious, Inflow Depth > 1.15" for 2 YEAR event Inflow Area = Inflow 66.47 cfs @ 12.89 hrs, Volume= 17.661 af 61.46 cfs @ 13.39 hrs, Volume= Outflow 17.564 af, Atten= 8%, Lag= 30.1 min 61.46 cfs @ 13.39 hrs, Volume= Primary = 17.564 af 5.00 hrs. Volume= 0.00 cfs @ 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 99.06' @ 13.39 hrs Surf.Area= 22,689 sf Storage= 35,702 cf

Plug-Flow detention time= 9.2 min calculated for 17.564 af (99% of inflow) Center-of-Mass det. time= 7.5 min (897.8 - 890.2)

Avail Storage Storage Description

volume	IIIVE	rt Avaii.Sto	rage Storage	Description	
#1	96.00	0' 280,44	48 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)
Elevation	on S	Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
96.0	00	1,580	0	0	
98.0	00	14,434	16,014	16,014	
100.0	00	30,000	44,434	60,448	
102.0	00	40,000	70,000	130,448	
105.0	00	60,000	150,000	280,448	
Device	Routing	Invert	Outlet Devices	S	
#1	Primary	96.00'	48.0" Round	Culvert	
#2	Secondar	y 103.00'	Inlet / Outlet In n= 0.011 Cor 20.0' long x 2 Head (feet) 0	nvert= 96.00' / 9 ncrete pipe, stra 20.0' breadth B .20 0.40 0.60	ojecting, Ke= 0.500 95.00' S= 0.0333 '/' Cc= 0.900 ight & clean, Flow Area= 12.57 sf road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=61.45 cfs @ 13.39 hrs HW=99.06' (Free Discharge)
1=Culvert (Inlet Controls 61.45 cfs @ 5.96 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 7P: 1-24" Culvert at Greely Middle School

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 1.56" for 2 YEAR event

Inflow = 19.44 cfs @ 12.12 hrs, Volume= 1.427 af

Outflow = 1.21 cfs @ 14.58 hrs, Volume= 0.776 af, Atten= 94%, Lag= 147.2 min

Primary = 1.21 cfs @ 14.58 hrs, Volume= 0.776 af Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 121.90' @ 14.58 hrs Surf.Area= 21,586 sf Storage= 38,151 cf

Plug-Flow detention time= 238.2 min calculated for 0.776 af (54% of inflow)

Center-of-Mass det. time= 158.6 min (952.3 - 793.7)

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	214,248 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	18,593	0	0
122.00	21,745	40,338	40,338
124.00	25,131	46,876	87,214
126.00	32,605	57,736	144,950
128.00	36,693	69,298	214,248

<u>Device</u>	Routing	Invert	Outlet Devices
#1	Primary	120.00'	24.0" Round Culvert
	•		L= 80.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 120.00' / 119.00' S= 0.0125 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Secondary	127.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63
#3	Device 1	120.00'	6.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	126.00'	24.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Primary OutFlow Max=1.21 cfs @ 14.58 hrs HW=121.90' (Free Discharge)

1=Culvert (Passes 1.21 cfs of 14.46 cfs potential flow)

3=Orifice/Grate (Orifice Controls 1.21 cfs @ 6.18 fps)

-4=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=120.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 10P: 1-30" Culvert

Inflow Area =	112.000 ac, 2	1.43% Impervious, Inf	low Depth > 0.94" for 2 YEAR event
Inflow =	48.66 cfs @	12.95 hrs, Volume=	8.745 af
Outflow =	38.99 cfs @	13.29 hrs, Volume=	8.571 af, Atten= 20%, Lag= 20.3 min
Primary =	33.00 cfs @	13.29 hrs, Volume=	8.374 af
Secondary =	6.00 cfs @	13.29 hrs, Volume=	0.198 af

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 71.20' @ 13.29 hrs Surf.Area= 39,042 sf Storage= 54,494 cf

Plug-Flow detention time= 22.7 min calculated for 8.571 af (98% of inflow) Center-of-Mass det. time= 16.4 min (887.5 - 871.1)

Volume	Inve	rt Avail.Sto	rage	Storage	Description	
#1	68.0	68.00' 211,0		8 cf Custom Stage Data (Prismatic)Listed below (Recalc)		
Elevatio		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)	
68.0		8,000		0	0	
70.0 72.0	00	14,434 55,480		22,434 69,914	22,434 92,348	
74.0		63,220		18,700	211,048	
Device Routing Inve		Invert	Outl	et Device	S	
#1	#1 Primary 68		30.0	" Round	Culvert	
#2	#2 Secondary 71.		L= 30.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 68.00' / 67.00' S= 0.0333 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf 25.0' long x 25.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63			

Primary OutFlow Max=32.99 cfs @ 13.29 hrs HW=71.20' (Free Discharge) 1=Culvert (Inlet Controls 32.99 cfs @ 6.72 fps)

Secondary OutFlow Max=5.91 cfs @ 13.29 hrs HW=71.20' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 5.91 cfs @ 1.19 fps)

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Summary for Subcatchment 1S:

Runoff = 103.11 cfs @ 12.82 hrs, Volume= 16.897 af, Depth> 2.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

_	Area	(ac) (CN Des	cription					
,	57.	000	70 WO	WOODS / FIELD HSG C					
7	19.	000	98 EXIS	EXISTING IMPERVIOUS AREA					
5	25.	000	74 EXIS	STING LAV	WN C				
101.000 76 Weighted Average									
82.000 81.19% Pervious Area									
	19.000 18.81% Impervious Area								
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	28.8	100	0.0400	0.06		Sheet Flow, AB			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC			
_						Forest w/Heavy Litter Kv= 2.5 fps			
	58.8	1.000	Total						

Summary for Subcatchment 2S:

Runoff = 96.37 cfs @ 12.71 hrs, Volume= 14.488 af, Depth> 2.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac)	CN	Desc	ription				
*	43.	310	70	WOO	DDS / FIEL	D HSG C			
*	13.	000	98	EXISTING IMPERVIOUS AREA					
*	30.	30.000 74 EXISTING LAWN C							
	86.310 76 Weighted Average								
73.310 84.94% Pervious Area					4% Pervio	us Area			
	13.000 15.06% Impervious Area					ious Area			
	_		_				-		
	Tc	Length		Slope	Velocity	Capacity	Description		
_	(min)	(feet))	(ft/ft)	(ft/sec)	(cfs)			
	28.8	100	0.0	0400	0.06		Sheet Flow, AB		
							Woods: Dense underbrush n= 0.800 P2= 3.10"		
	21.7	650	0.0	0400	0.50		Shallow Concentrated Flow, BC		
_							Forest w/Heavy Litter Kv= 2.5 fps		
	50.5	750) To	otal					

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Summary for Subcatchment 3S:

Runoff = 35.35 cfs @ 12.63 hrs, Volume= 4.992 af, Depth> 1.58"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac) C	N Des	cription			
*	34.	000	70 WO	ODS / FIEI	D HSG C		
*	0.	000	98 EXIS	STING IMF	PERVIOUS	AREA	
*	4.	000	74 EXIS	STING LAV	WN C		
	38.000 70 Weighted Average						
	38.000 100.00% Pervious Area						
	Tc	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	28.8	100	0.0400	0.06		Sheet Flow, AB	
_	15.0	450	0.0400	0.50		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, BC Forest w/Heavy Litter Kv= 2.5 fps	
	43.8	550	Total				

Summary for Subcatchment 4S:

Runoff = 12.23 cfs @ 12.83 hrs, Volume= 2.009 af, Depth> 1.85"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac) (<u>CN I</u>	<u>Desc</u>	ription		
*	5.	000	70 \	WOC	DS / FIEL	D HSG C	
*	1.	000	98 E	EXIS	TING IMP	ERVIOUS	AREA
*	7.	000	74 E	EXIS	TING LAV	VN C	
	13.	000	74 \	Weig	hted Aver	age	
	12.000 92.31% Pervious Area						
	1.000 7.69			7.699	% Impervi	ous Area	
					•		
	Tc	Length	Slo	оре	Velocity	Capacity	Description
	(min)	(feet)	(f	t/ft)	(ft/sec)	(cfs)	
	28.8	100	0.04	400	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.04	400	0.50		Shallow Concentrated Flow, BC
							Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Tota	al			·

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Summary for Subcatchment 5S: drains to 48" culvert

Runoff = 91.32 cfs @ 13.48 hrs, Volume= 22.409 af, Depth> 2.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac) C	N Des	cription		
*	47.	000	70 WO	ODS / FIEL	D HSG C	
*	36.	000	98 EXIS	STING IMF	PERVIOUS	AREA
*	35.	000	74 EXIS	STING LAV	VN C	
	118.000 80 Weighted Average					
	82.000 69.49% Pervious Area					
	36.000 30.51% Impervious Area				vious Area	
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	38.0	100	0.0200	0.04		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	60.0	900	0.0100	0.25		Shallow Concentrated Flow, BC
						Forest w/Heavy Litter Kv= 2.5 fps
	14.8	2,671	0.0400	3.00		Shallow Concentrated Flow, CD
_						Grassed Waterway Kv= 15.0 fps
	112.8	3,671	Total			

Summary for Subcatchment 6S: drains to 48" culvert

Runoff = 103.57 cfs @ 12.52 hrs, Volume= 13.387 af, Depth> 2.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

_	Area	(ac) (CN Des	cription		
*	6.	000	70 WO	DDS / FIEI	D HSG C	
*	20.	000	98 EXIS	STING IMF	PERVIOUS	AREA
*	40.	000	74 EXIS	STING LAV	VN C	
	66.	000	81 Wei	hted Aver	age	
	46.000 69.70% Pervious Area					
	20.000 30.30% Impervious Area				ious Area	
				•		
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	5.0	900	0.0400	3.00		Shallow Concentrated Flow, BC
						Grassed Waterway Kv= 15.0 fps
	3.7	2,500	0.0400	11.41	182.56	Trap/Vee/Rect Channel Flow, CD
						Bot.W=4.00' D=2.00' Z= 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	37.5	3,500	Total			

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Summary for Subcatchment 7S:

Runoff = 34.68 cfs @ 12.12 hrs, Volume= 2.580 af, Depth> 2.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac)	CN	Desc	cription						
*	0.	000	70	WOO	WOODS / FIELD HSG C						
*	5.	000	98	EXIS	STING IMP	PERVIOUS	AREA				
*	6.	000	74	EXIS	STING LAV	VN C					
11.000 85 Weighted Average											
	6.	000		_	5% Pervio	U					
	5.000 45.45% Impervious Area				5% Imperv	ious Area					
					•						
	Tc	Lengt	h	Slope	Velocity	Capacity	Description				
	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	·				
	7.5	10	0	0.0400	0.22		Sheet Flow, AB				
							Grass: Short n= 0.150 P2= 3.10"				
	1.1	20	0	0.0400	3.00		Shallow Concentrated Flow, BC				
							Grassed Waterway Kv= 15.0 fps				
	8.6	30	0	Total			•				

Summary for Reach 3R: Stream below RR crossing

Inflow Area = 112.000 ac. 21.43% Impervious, Inflow Depth > 1.92" for 10 YEAR event

Inflow = 103.92 cfs @ 12.83 hrs, Volume= 17.894 af

Outflow = 103.64 cfs @ 12.89 hrs, Volume= 17.823 af, Atten= 0%, Lag= 3.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity = 6.56 fps, Min. Travel Time = 2.2 min Avg. Velocity = 3.01 fps, Avg. Travel Time = 4.8 min

Peak Storage= 13,594 cf @ 12.86 hrs Average Depth at Peak Storage= 1.98'

Bank-Full Depth= 4.00' Flow Area= 40.0 sf, Capacity= 373.38 cfs

6.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 14.00'

Length= 860.0' Slope= 0.0116 '/'

Inlet Invert= 82.00', Outlet Invert= 72.00'



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Summary for Reach 4R: Stream above RR crossing

Inflow Area = 112.000 ac, 21.43% Impervious, Inflow Depth > 1.92" for 10 YEAR event

Inflow = 103.98 cfs @ 12.82 hrs, Volume= 17.912 af

Outflow = 103.92 cfs @ 12.83 hrs, Volume= 17.894 af, Atten= 0%, Lag= 0.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.22 fps, Min. Travel Time= 0.5 min Avg. Velocity = 2.84 fps, Avg. Travel Time= 1.2 min

Peak Storage= 3,341 cf @ 12.82 hrs Average Depth at Peak Storage= 2.07'

Bank-Full Depth= 4.00' Flow Area= 40.0 sf, Capacity= 346.26 cfs

6.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 14.00'

Length= 200.0' Slope= 0.0100 '/'

Inlet Invert= 84.00', Outlet Invert= 82.00'



Summary for Reach 6R: Stream below Site

Inflow Area = 270.310 ac. 25.53% Impervious, Inflow Depth > 2.18" for 10 YEAR event

Inflow = 194.64 cfs @ 12.87 hrs, Volume= 49.063 af

Outflow = 194.34 cfs @ 12.91 hrs, Volume= 48.974 af, Atten= 0%, Lag= 2.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.27 fps, Min. Travel Time= 1.2 min

Avg. Velocity = 3.41 fps, Avg. Travel Time= 2.2 min

Peak Storage= 13,965 cf @ 12.89 hrs

Average Depth at Peak Storage= 2.86'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 538.97 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 61.00', Outlet Invert= 58.00'



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Summary for Reach 7R: Stream Through Site

Inflow Area = 270.310 ac, 25.53% Impervious, Inflow Depth > 2.18" for 10 YEAR event

Inflow = 194.97 cfs @ 12.82 hrs, Volume= 49.203 af

Outflow = 194.64 cfs @ 12.87 hrs, Volume= 49.063 af, Atten= 0%, Lag= 3.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 9.93 fps, Min. Travel Time= 1.8 min Avg. Velocity = 5.27 fps, Avg. Travel Time= 3.5 min

Peak Storage= 21,590 cf @ 12.84 hrs Average Depth at Peak Storage= 1.97'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 683.45 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,100.0' Slope= 0.0245 '/'

Inlet Invert= 88.00', Outlet Invert= 61.00'



Summary for Reach 14R: Swale from School and Neighborhood

Inflow Area = 11.000 ac. 45.45% Impervious, Inflow Depth > 1.26" for 10 YEAR event

Inflow = 1.70 cfs @ 15.15 hrs, Volume= 1.156 af

Outflow = 1.70 cfs @ 16.05 hrs, Volume= 1.014 af, Atten= 0%, Lag= 53.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity = 1.75 fps, Min. Travel Time = 32.1 min Avg. Velocity = 1.27 fps, Avg. Travel Time = 44.3 min

Peak Storage= 3,268 cf @ 15.51 hrs

Average Depth at Peak Storage= 0.23'

Bank-Full Depth= 3.00' Flow Area= 21.0 sf, Capacity= 147.12 cfs

4.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 10.00'

Length= 3,366.0' Slope= 0.0100 '/'

Inlet Invert= 117.66', Outlet Invert= 84.00'



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Summary for Reach 18R: Stream Through Site

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 2.28" for 10 YEAR event

Inflow 137.41 cfs @ 12.64 hrs, Volume= 35,006 af

137.06 cfs @ 12.71 hrs, Volume= Outflow 34.868 af, Atten= 0%, Lag= 4.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.79 fps, Min. Travel Time= 2.6 min Avg. Velocity = 3.99 fps, Avg. Travel Time= 5.0 min

Peak Storage= 21,119 cf @ 12.67 hrs Average Depth at Peak Storage= 1.80'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 563.18 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,200.0' Slope= 0.0167 '/'

Inlet Invert= 125.00', Outlet Invert= 105.00'



Summary for Reach 55R: Wetland below Site

38.000 ac, 0.00% Impervious, Inflow Depth > 1.58" for 10 YEAR event 35.35 cfs @ 12.63 hrs, Volume= 4.992 af Inflow Area =

Inflow

Outflow 35.23 cfs @ 12.69 hrs, Volume= 4.973 af, Atten= 0%, Lag= 3.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.70 fps, Min. Travel Time= 2.0 min

Avg. Velocity = 1.70 fps, Avg. Travel Time= 4.4 min

Peak Storage= 4,298 cf @ 12.66 hrs

Average Depth at Peak Storage= 1.05'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 540.76 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 63.02', Outlet Invert= 60.00'



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Summary for Pond 1P: 1-30" and 1-24" Culvert at Tuttle Road

Inflow Area = 112.000 ac, 21.43% Impervious, Inflow Depth > 1.88" for 10 YEAR event

Inflow = 96.89 cfs @ 13.07 hrs, Volume= 17.582 af

Outflow = 96.83 cfs @ 13.08 hrs, Volume= 17.553 af, Atten= 0%, Lag= 0.8 min

Primary = 59.10 cfs @ 13.08 hrs, Volume= 15.691 af Secondary = 37.73 cfs @ 13.08 hrs, Volume= 1.863 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 71.43' @ 13.08 hrs Surf.Area= 7,170 sf Storage= 18,562 cf

Plug-Flow detention time= 3.5 min calculated for 17.553 af (100% of inflow) Center-of-Mass det. time= 3.0 min (870.4 - 867.4)

Volume Invert Avail.Storage Storage Description

#1	68.00'	31,683 cf	Custom	Stage Data (Pri	smatic)Listed below (Recalc)
Elevation (feet)	Surf.Area (sq-ft)		c.Store ic-feet)	Cum.Store (cubic-feet)	
68.00	3,850		0	0	
70.00	5,600		9,450	9,450	
72.00	7,800		13,400	22,850	
73.00	9,865		8,833	31,683	
Device Ro	uting Ir	nvert Out	let Devices	i	

#1	Primary	67.50'	30.0" Round Culvert
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf
#2	Primary	67.50'	24.0" Round Culvert
			L= 50.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
#3	Secondary	71.00'	
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=59.09 cfs @ 13.08 hrs HW=71.43' (Free Discharge)

1=Culvert (Inlet Controls 38.67 cfs @ 7.88 fps)

L2=Culvert (Inlet Controls 20.43 cfs @ 6.50 fps)

Secondary OutFlow Max=37.55 cfs @ 13.08 hrs HW=71.43' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 37.55 cfs @ 1.76 fps)

Summary for Pond 2P: Two 30" Culverts at Crossing Brook Road

Inflow Area =	270.310 ac, 25.53% Impervious, Inflo	w Depth > 2.17" for 10 YEAR event
Inflow =	194.34 cfs @ 12.91 hrs, Volume=	48.974 af
Outflow =	89.77 cfs @ 14.98 hrs, Volume=	45.181 af, Atten= 54%, Lag= 124.2 min
Primary =	89.77 cfs @ 14.98 hrs, Volume=	45.181 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 51.53' @ 14.98 hrs Surf.Area= 150,666 sf Storage= 747,506 cf

Plug-Flow detention time= 107.9 min calculated for 45.181 af (92% of inflow) Center-of-Mass det. time= 86.2 min (959.0 - 872.8)

Volume	Invert	Avail.Sto	rage	Storage	Description		
#1	44.00'	2,030,00	00 cf	Custom	Stage Data (Pr	rismatic)Listed below (Recalc)	
Elevation	on Surf.	Δrea	Inc	.Store	Cum.Store		
(fee		sq-ft)		c-feet)	(cubic-feet)		
44.0		,000		0	0		
46.0		,000	14	0,000	140,000		
48.0		,000		0,000	320,000		
50.0		,000		0,000	540,000		
52.0		,000		0,000	820,000		
54.0		,000		0,000	1,160,000		
56.0		,000		0,000	1,560,000		
58.0	00 250	,000	47	0,000	2,030,000		
Device	Routing	Invert	Outle	et Device:	S		
#1	Primary	44.00'	30.0	" Round	Culvert		
						ojecting, Ke= 0.500	
						2.00' S= 0.0400 '/' Cc= 0.900	
						ight & clean, Flow Area= 4.91 sf	
#2	Primary	44.00'		" Round		handwall Ka- 0.000	
				L= 50.0' CPP, projecting, no headwall, Ke= 0.900			
			Inlet / Outlet Invert= 44.00' / 42.00' S= 0.0400 '/' Cc= 0.900 n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf				
#3	Secondary	56.00'				road-Crested Rectangular Weir	
" "	Secondary	30.00				0.80 1.00 1.20 1.40 1.60	
				` ,		70 2.64 2.63 2.64 2.64 2.63	
				,	,		

Primary OutFlow Max=89.77 cfs @ 14.98 hrs HW=51.53' (Free Discharge)

-1=Culvert (Inlet Controls 59.24 cfs @ 12.07 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=44.00' (Free Discharge)

3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 3P: 24" CULVERT

Inflow Area =	38.000 ac,	0.00% Impervious, Inflow D	epth > 1.57" for 1	0 YEAR event
Inflow =	35.23 cfs @	12.69 hrs, Volume=	4.973 af	
Outflow =	26.68 cfs @	12.99 hrs, Volume=	4.935 af, Atten= 24	%, Lag= 18.0 min
Primary =	26.68 cfs @	12.99 hrs, Volume=	4.935 af	•
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 58.11' @ 12.99 hrs Surf.Area= 10,558 sf Storage= 27,489 cf

Plug-Flow detention time= 13.2 min calculated for 4.918 af (99% of inflow)

^{—2=}Culvert (Inlet Controls 30.52 cfs @ 9.72 fps)

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Center-of-Mass det. time= 10.5 min (854.3 - 843.8)

Volume	Inver	t Avail.Sto	rage Storage	Description	
#1	54.00	0' 56,34	42 cf Custon	n Stage Data (P	rismatic)Listed below (Recalc)
Elevation	on S	Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
54.0	00	2,362	0	0	
56.0	00	6,990	9,352	9,352	
58.0	00	10,000	16,990	26,342	
60.0	00	20,000	30,000	56,342	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	54.00'	24.0" Round	d Culvert	
#2 Secondary		y 59.00'	Inlet / Outlet I n= 0.011 Co 25.0' long x Head (feet) (Invert= 54.00' / 5 ncrete pipe, stra 25.0' breadth B 0.20 0.40 0.60	ojecting, Ke= 0.500 63.00' S= 0.0200 '/' Cc= 0.900 ight & clean, Flow Area= 3.14 sf croad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=26.68 cfs @ 12.99 hrs HW=58.11' (Free Discharge) 1=Culvert (Inlet Controls 26.68 cfs @ 8.49 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=54.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 4P: 18" CULVERT

Inflow Area =	13.000 ac,	7.69% Impervious, Inflow D	epth > 1.85" for 10 YEAR event
Inflow =	12.23 cfs @	12.83 hrs, Volume=	2.009 af
Outflow =	8.95 cfs @	13.22 hrs, Volume=	1.973 af, Atten= 27%, Lag= 23.6 min
Primary =	8.95 cfs @	13.22 hrs, Volume=	1.973 af
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 86.86' @ 13.22 hrs Surf.Area= 13,049 sf Storage= 15,074 cf

Plug-Flow detention time= 26.6 min calculated for 1.973 af (98% of inflow) Center-of-Mass det. time= 20.5 min (864.1 - 843.6)

Volume	Invert	Avail.	Storage	Storage	Description		
#1	85.00'	82	2,755 cf	Custon	n Stage Data (Pri	smatic)Listed below (Rec	alc)
Elevation (feet)	Surf.	Area sq-ft)	Inc. (cubic	Store c-feet)	Cum.Store (cubic-feet)		
85.00	3	3,343		0	0		
86.00	8	3,410		5,877	5,877		
88.00	19	9,234	2	7,644	33,521		
90.00	30	0,000	4	9,234	82,755		

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Device	Routing	Invert	Outlet Devices
#1	Primary	85.00'	18.0" Round Culvert
	•		L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 85.00' / 84.00' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.77 sf
#2	Secondary	89.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=8.95 cfs @ 13.22 hrs HW=86.86' (Free Discharge) 1=Culvert (Inlet Controls 8.95 cfs @ 5.06 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=85.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 5P: 4'x3' Oval and 30" Overflow Culvert

Inflow Area =	184.000 ac, 3	0.43% Impervious,	Inflow Depth > 2.3	33" for 10 YEAR event
Inflow =	137.73 cfs @	12.61 hrs, Volume	= 35.796 af	
Outflow =	137.41 cfs @	12.64 hrs, Volume	= 35.006 af,	Atten= 0%, Lag= 1.8 min
Primary =	40.18 cfs @	12.64 hrs, Volume:	= 20.895 af	_
Secondary =	97.23 cfs @	12.64 hrs, Volume:	= 14.111 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 137.72' @ 12.64 hrs Surf.Area= 19,152 sf Storage= 92,199 cf

Plug-Flow detention time= 22.3 min calculated for 34.889 af (97% of inflow) Center-of-Mass det. time= 15.2 min (865.6 - 850.5)

Volume	Inver	rt Avail.Sto	rage Storage	Description		
#1	129.00)' 142,73	35 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)	
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
129.0 130.0 132.0	00 00 00	4,441 6,196 8,225	5,319 14,421	5,319 19,740		
134.0 136.0 138.0 140.0	00 00	10,880 14,005 20,000 25,000	19,105 24,885 34,005 45,000	38,845 63,730 97,735 142,735		
Device	Routing	Invert	Outlet Device	S		
#1	Primary	129.00'	4.0" W x 3.0" H, R=3.0" Elliptical Culvert			
#2	Primary	132.00'	L= 30.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 129.00' / 128.00' S= 0.0333 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.07 sf			
#3	Secondary	y 137.00'			Broad-Crested Rectangular Weir	

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Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60

Primary OutFlow Max=40.17 cfs @ 12.64 hrs HW=137.72' (Free Discharge)

1=Culvert (Barrel Controls 0.74 cfs @ 10.99 fps)
2=Culvert (Inlet Controls 39.44 cfs @ 8.03 fps)

Secondary OutFlow Max=96.98 cfs @ 12.64 hrs HW=137.72' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 96.98 cfs @ 2.26 fps)

Summary for Pond 6P: 1-48" Culvert Crossing Golf Cart Path

Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

184.000 ac, 30.43% Impervious, Inflow Depth > 2.27" for 10 YEAR event Inflow Area = Inflow 137.06 cfs @ 12.71 hrs, Volume= 34.868 af Outflow 115.80 cfs @ 13.58 hrs, Volume= 34.715 af, Atten= 16%, Lag= 51.8 min Primary = 115.80 cfs @ 13.58 hrs, Volume= 34.715 af 5.00 hrs, Volume= 0.00 cfs @ 0.000 af Secondary =

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 101.66' @ 13.58 hrs Surf.Area= 38,314 sf Storage= 117,247 cf

Plug-Flow detention time= 12.5 min calculated for 34.599 af (99% of inflow) Center-of-Mass det. time= 11.1 min (881.4 - 870.3)

Avail Storage Storage Description

volume	INV	eri Avali.Sid	rage Storage	Description		
#1	96.0	00' 280,4	48 cf Custom	Stage Data (Pr	rismatic)Listed below (Recalc)	
Elevation	an.	Surf.Area	Inc.Store	Cum.Store		
	_					
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)		
96.0	00	1,580	0	0		
98.0	00	14,434	16,014	16,014		
100.0	00	30,000	44,434	60,448		
102.0	00	40,000	70,000	130,448		
105.0	00	60,000	150,000	280,448		
Device	Routing	Invert	Outlet Devices	S		
#1	Primary	96.00'	48.0" Round	Culvert		
	•		L= 30.0' RCF	o, sq.cut end pro	ojecting, Ke= 0.500	
			Inlet / Outlet Invert= 96.00' / 95.00' S= 0.0333 '/' Cc= 0.900			
			n= 0.011 Cor	ncrete pipe, strai	ght & clean, Flow Area= 12.57 sf	
#2	Seconda	ry 103.00'	20.0' long x 2	20.0' breadth B	road-Crested Rectangular Weir	
		•	Head (feet) 0	.20 0.40 0.60	0.80 1.00 1.20 1.40 1.60	

Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=115.79 cfs @ 13.58 hrs HW=101.66' (Free Discharge)
1=Culvert (Inlet Controls 115.79 cfs @ 9.21 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 7P: 1-24" Culvert at Greely Middle School

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 2.81" for 10 YEAR event

Inflow = 34.68 cfs @ 12.12 hrs, Volume= 2.580 af

Outflow = 1.70 cfs @ 15.15 hrs, Volume= 1.156 af, Atten= 95%, Lag= 181.6 min

Primary = 1.70 cfs @ 15.15 hrs, Volume= 1.156 afSecondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 123.47' @ 15.15 hrs Surf.Area= 24,239 sf Storage= 74,205 cf

Plug-Flow detention time= 249.6 min calculated for 1.156 af (45% of inflow)

Center-of-Mass det. time= 162.9 min (942.8 - 780.0)

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	214,248 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	18,593	0	0
122.00	21,745	40,338	40,338
124.00	25,131	46,876	87,214
126.00	32,605	57,736	144,950
128.00	36,693	69,298	214,248

Device	Routing	Invert	Outlet Devices
#1	Primary	120.00'	24.0" Round Culvert
			L= 80.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 120.00' / 119.00' S= 0.0125 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Secondary	127.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
	•		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63
#3	Device 1	120.00'	6.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	126.00'	24.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Primary OutFlow Max=1.70 cfs @ 15.15 hrs HW=123.47' (Free Discharge)

1=Culvert (Passes 1.70 cfs of 23.79 cfs potential flow)

3=Orifice/Grate (Orifice Controls 1.70 cfs @ 8.64 fps)

-4=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=120.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 10P: 1-30" Culvert

Inflow Area =	112.000 ac, 21	.43% Impervious,	Inflow Depth > 1.9	91" for 10 YEAR event
Inflow =	103.64 cfs @ 1	12.89 hrs, Volume	= 17.823 af	
Outflow =	96.89 cfs @ 1	13.07 hrs, Volume	= 17.582 af,	Atten= 7%, Lag= 10.4 min
Primary =	38.63 cfs @ 1	13.07 hrs, Volume	= 13.364 af	
Secondary =	58.26 cfs @ 1	13.07 hrs, Volume=	= 4.218 af	

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 71.92' @ 13.07 hrs Surf.Area= 53,867 sf Storage= 88,051 cf

Plug-Flow detention time= 19.5 min calculated for 17.582 af (99% of inflow)

Center-of-Mass det. time= 15.0 min (867.4 - 852.4)

Volume	Inver	t Avail.Sto	rage Storaç	ge Description	
#1	68.00)' 211,04	48 cf Custo	om Stage Data (P	rismatic)Listed below (Recalc)
Elevation	on S	Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
68.0	00	8,000	0	0	
70.0	00	14,434	22,434	22,434	
72.0		55,480	69,914	92,348	
74.0	00	63,220	118,700	211,048	
Device	Routing	Invert	Outlet Devi	ces	
#1	Primary	68.00'	30.0" Rou	nd Culvert	
#2 Secondary		y 71.00'	Inlet / Outle n= 0.011 C 25.0' long Head (feet)	t Invert= 68.00' / 6 concrete pipe, stra x 25.0' breadth B 0.20 0.40 0.60	ojecting, Ke= 0.500 67.00' S= 0.0333 '/' Cc= 0.900 ight & clean, Flow Area= 4.91 sf 6road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=38.62 cfs @ 13.07 hrs HW=71.92' (Free Discharge) 1=Culvert (Inlet Controls 38.62 cfs @ 7.87 fps)

Secondary OutFlow Max=58.10 cfs @ 13.07 hrs HW=71.92' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 58.10 cfs @ 2.53 fps)

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Summary for Subcatchment 1S:

Runoff = 150.79 cfs @ 12.80 hrs, Volume= 24.710 af, Depth> 2.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

_	Area	(ac) (CN Des	cription				
,	57.	000	70 WO	ODS / FIEI	_D HSG C			
7	19.	000	98 EXIS	STING IMF	PERVIOUS	AREA		
5	25.	000	74 EXIS	STING LAV	WN C			
101.000 76 Weighted Average								
	82.	000	81.1	9% Pervio	us Area			
	19.	000	18.8	1% Imperv	ious Area			
	Тс	Length	Slope	Velocity	Capacity	Description		
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)			
	28.8	100	0.0400	0.06		Sheet Flow, AB		
						Woods: Dense underbrush n= 0.800 P2= 3.10"		
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC		
_						Forest w/Heavy Litter Kv= 2.5 fps		
	58.8	1.000	Total					

Summary for Subcatchment 2S:

Runoff = 140.81 cfs @ 12.69 hrs, Volume= 21.182 af, Depth> 2.94"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac)	CN	Desc	ription				
*	43.	310	70	WOO	DS / FIEL	D HSG C			
*	13.	000	98	EXIS	TING IMP	ERVIOUS	AREA		
*	30.	000	74	EXIS	TING LAV	VN C			
	86.	310	76	Weig	hted Aver	age			
	73.	310		84.94	4% Pervio	us Area			
	13.	000		15.06	15.06% Impervious Area				
	Тс	Length	1 S	Slope	Velocity	Capacity	Description		
	(min)	(feet))	(ft/ft)	(ft/sec)	(cfs)			
	28.8	100	0.	0400	0.06		Sheet Flow, AB		
							Woods: Dense underbrush n= 0.800 P2= 3.10"		
	21.7	650	0.	0400	0.50		Shallow Concentrated Flow, BC		
							Forest w/Heavy Litter Kv= 2.5 fps		
	50.5	750	To	otal					

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Summary for Subcatchment 3S:

Runoff = 54.85 cfs @ 12.62 hrs, Volume= 7.643 af, Depth> 2.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac) C	N Des	cription					
*	34.	000	70 WO	ODS / FIEI	D HSG C				
*	0.	000	98 EXIS	STING IMF	PERVIOUS	AREA			
*	4.	000	74 EXIS	STING LAV	WN C				
	38.000 70 Weighted Average								
	38.000 100.00% Pervious Area								
	Tc	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	28.8	100	0.0400	0.06		Sheet Flow, AB			
_	15.0	450	0.0400	0.50		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, BC Forest w/Heavy Litter Kv= 2.5 fps			
	43.8	550	Total						

Summary for Subcatchment 4S:

Runoff = 18.21 cfs @ 12.81 hrs, Volume= 2.982 af, Depth> 2.75"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac)	<u> CN</u>	Desc	ription		
*	5.	000	70	WOO	DDS / FIEL	D HSG C	
*	1.	000	98	EXIS	TING IMP	PERVIOUS	AREA
*	7.	000	74	EXIS	TING LAV	VN C	
13.000 74 Weighted Average							
	12.000 92.31% Pervious Area						
	1.000 7.69%				% Impervi	ous Area	
					•		
	Tc	Length	S	lope	Velocity	Capacity	Description
	(min)	(feet))	(ft/ft)	(ft/sec)	(cfs)	<u> </u>
	28.8	100	0.0	0400	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.0	0400	0.50		Shallow Concentrated Flow, BC
							Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000) To	tal			
	55.6	1,000	10	, tui			

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Summary for Subcatchment 5S: drains to 48" culvert

Runoff = 129.65 cfs @ 13.46 hrs, Volume= 31.922 af, Depth> 3.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac) C	N Des	cription		
*	47.	000	70 WO	ODS / FIEL	D HSG C	
*	36.	000	98 EXIS	STING IMF	PERVIOUS	AREA
*	35.	000	74 EXIS	STING LAV	VN C	
	118.000 80 Weighted Average					
	82.	000	69.4	9% Pervio	us Area	
	36.000 30.51% Impervious Area					
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	38.0	100	0.0200	0.04		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	60.0	900	0.0100	0.25		Shallow Concentrated Flow, BC
						Forest w/Heavy Litter Kv= 2.5 fps
	14.8	2,671	0.0400	3.00		Shallow Concentrated Flow, CD
_						Grassed Waterway Kv= 15.0 fps
	112.8	3,671	Total			

Summary for Subcatchment 6S: drains to 48" culvert

Runoff = 145.08 cfs @ 12.51 hrs, Volume= 18.906 af, Depth> 3.44"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

_	Area	(ac) C	N Des	cription		
*	6.	000	70 WO	ODS / FIEI	LD HSG C	
*	20.	000	98 EXIS	STING IMF	PERVIOUS	AREA
*	40.	000	74 EXIS	STING LAV	WN C	
_	66.	000	81 Wei	hted Aver	age	
	46.	000		0% Pervio		
	20.000			0% Imperv	vious Area	
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	5.0	900	0.0400	3.00		Shallow Concentrated Flow, BC
						Grassed Waterway Kv= 15.0 fps
	3.7	2,500	0.0400	11.41	182.56	Trap/Vee/Rect Channel Flow, CD
						Bot.W=4.00' D=2.00' Z= 2.0 '/' Top.W=12.00'
_						n= 0.030 Earth, grassed & winding
	37.5	3 500	Total			

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Summary for Subcatchment 7S:

Runoff = 47.09 cfs @ 12.12 hrs, Volume= 3.550 af, Depth> 3.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac)	CN	Desc	cription			
*	0.	000	70	WOO	DDS / FIEL	D HSG C		
*	5.	000	98	EXIS	STING IMP	PERVIOUS	AREA	
*	6.	000	74	EXIS	STING LAV	VN C		
-	11.000 85 Weighted Average							
6.000 54.55% Pervious Area								
	5.	000		45.4	5% Imperv	vious Area		
					•			
	Tc	Lengtl	h S	Slope	Velocity	Capacity	Description	
	(min)	(feet	:)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>	
	7.5	100	0 0.	0400	0.22		Sheet Flow, AB	
							Grass: Short n= 0.150 P2= 3.10"	
	1.1	200	0.	0400	3.00		Shallow Concentrated Flow, BC	
							Grassed Waterway Kv= 15.0 fps	
-	8.6	300	0 To	otal			•	

Summary for Reach 3R: Stream below RR crossing

Inflow Area = 112.000 ac. 21.43% Impervious, Inflow Depth > 2.78" for 25 YEAR event

Inflow = 151.93 cfs @ 12.81 hrs, Volume= 25.940 af

Outflow = 151.56 cfs @ 12.87 hrs, Volume= 25.855 af, Atten= 0%, Lag= 3.4 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.32 fps, Min. Travel Time= 2.0 min Avg. Velocity = 3.26 fps, Avg. Travel Time= 4.4 min

Peak Storage= 17,836 cf @ 12.84 hrs Average Depth at Peak Storage= 2.45'

Bank-Full Depth= 4.00' Flow Area= 40.0 sf, Capacity= 373.38 cfs

6.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 14.00'

Length= 860.0' Slope= 0.0116 '/'

Inlet Invert= 82.00', Outlet Invert= 72.00'



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Summary for Reach 4R: Stream above RR crossing

Inflow Area = 112.000 ac, 21.43% Impervious, Inflow Depth > 2.78" for 25 YEAR event

Inflow = 151.98 cfs @ 12.80 hrs, Volume= 25.961 af

Outflow = 151.93 cfs @ 12.81 hrs, Volume= 25.940 af, Atten= 0%, Lag= 0.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.93 fps, Min. Travel Time= 0.5 min Avg. Velocity = 3.07 fps, Avg. Travel Time= 1.1 min

Peak Storage= 4,386 cf @ 12.81 hrs Average Depth at Peak Storage= 2.56'

Bank-Full Depth= 4.00' Flow Area= 40.0 sf, Capacity= 346.26 cfs

 $6.00' \times 4.00'$ deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 14.00'

Length= 200.0' Slope= 0.0100 '/'

Inlet Invert= 84.00', Outlet Invert= 82.00'



Summary for Reach 6R: Stream below Site

Inflow Area = 270.310 ac. 25.53% Impervious, Inflow Depth > 3.13" for 25 YEAR event

Inflow = 265.65 cfs @ 12.84 hrs, Volume= 70.607 af

Outflow = 265.34 cfs @ 12.87 hrs, Volume= 70.499 af, Atten= 0%, Lag= 2.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.84 fps, Min. Travel Time= 1.1 min

Avg. Velocity = 3.69 fps, Avg. Travel Time= 2.0 min

Peak Storage= 17,462 cf @ 12.85 hrs

Average Depth at Peak Storage= 3.40'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 538.97 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 61.00', Outlet Invert= 58.00'



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Summary for Reach 7R: Stream Through Site

Inflow Area = 270.310 ac. 25.53% Impervious. Inflow Depth > 3.14" for 25 YEAR event

Inflow 266.10 cfs @ 12.78 hrs. Volume= 70.776 af

265.65 cfs @ 12.84 hrs, Volume= Outflow 70.607 af, Atten= 0%, Lag= 3.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 10.90 fps, Min. Travel Time= 1.7 min Avg. Velocity = 5.72 fps, Avg. Travel Time= 3.2 min

Peak Storage= 26,847 cf @ 12.81 hrs Average Depth at Peak Storage= 2.36'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 683.45 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,100.0' Slope= 0.0245 '/'

Inlet Invert= 88.00', Outlet Invert= 61.00'



Summary for Reach 14R: Swale from School and Neighborhood

Inflow Area = 11.000 ac. 45.45% Impervious, Inflow Depth > 1.54" for 25 YEAR event

2.00 cfs @ 15.48 hrs, Volume= Inflow 1.411 af

Outflow 2.00 cfs @ 16.31 hrs, Volume= 1.251 af, Atten= 0%, Lag= 49.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.85 fps, Min. Travel Time= 30.3 min

Avg. Velocity = 1.32 fps, Avg. Travel Time= 42.6 min

Peak Storage= 3,624 cf @ 15.80 hrs

Average Depth at Peak Storage= 0.25'

Bank-Full Depth= 3.00' Flow Area= 21.0 sf, Capacity= 147.12 cfs

4.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 10.00'

Length= 3,366.0' Slope= 0.0100 '/'

Inlet Invert= 117.66', Outlet Invert= 84.00'



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Summary for Reach 18R: Stream Through Site

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 3.26" for 25 YEAR event

Inflow 195.61 cfs @ 12.62 hrs. Volume= 49.959 af

195.00 cfs @ 12.69 hrs, Volume= Outflow 49.794 af, Atten= 0%, Lag= 4.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 8.68 fps, Min. Travel Time= 2.3 min Avg. Velocity = 4.33 fps, Avg. Travel Time= 4.6 min

Peak Storage= 26,999 cf @ 12.65 hrs Average Depth at Peak Storage= 2.20'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 563.18 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,200.0' Slope= 0.0167 '/'

Inlet Invert= 125.00', Outlet Invert= 105.00'



Summary for Reach 55R: Wetland below Site

38.000 ac, 0.00% Impervious, Inflow Depth > 2.41" for 25 YEAR event 54.85 cfs @ 12.62 hrs, Volume= 7.643 af Inflow Area =

Inflow

Outflow 54.61 cfs @ 12.67 hrs, Volume= 7.620 af, Atten= 0%, Lag= 3.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.27 fps, Min. Travel Time= 1.8 min

Avg. Velocity = 1.89 fps, Avg. Travel Time= 4.0 min

Peak Storage= 5,767 cf @ 12.64 hrs

Average Depth at Peak Storage= 1.37'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 540.76 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 63.02', Outlet Invert= 60.00'



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Summary for Pond 1P: 1-30" and 1-24" Culvert at Tuttle Road

Inflow Area = 112.000 ac, 21.43% Impervious, Inflow Depth > 2.74" for 25 YEAR event

Inflow = 144.41 cfs @ 13.02 hrs, Volume= 25.567 af

Outflow = 144.34 cfs @ 13.03 hrs, Volume= 25.526 af, Atten= 0%, Lag= 0.7 min

Primary = 62.21 cfs @ 13.03 hrs, Volume= 20.054 af Secondary = 82.13 cfs @ 13.03 hrs, Volume= 5.471 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 71.72' @ 13.03 hrs Surf.Area= 7,497 sf Storage= 20,743 cf

Plug-Flow detention time= 3.3 min calculated for 25.526 af (100% of inflow)

Center-of-Mass det. time= 2.7 min (859.4 - 856.7)

Volume	Inv	ert Ava	ail.Storage	Storage D	Description	
#1	68.	00'	31,683 cf	Custom	Stage Data (Pr	rismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)	
68.0		3,850	,	0	0	
70.0	-	5,600		9,450	9,450	
72.0	00	7,800		13,400	22,850	
73.0	00	9,865		8,833	31,683	
Device	Routing	lı	nvert Out	et Devices		
#1	Primary	6		Round		signating Kon 0.500

,, ,	a.y	01.00	ooio itouiia ouivoit
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf
#2	Primary	67.50'	24.0" Round Culvert
	•		L= 50.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
#3	Secondary	71.00'	50.0' long x 50.0' breadth Broad-Crested Rectangular Weir
	_		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=62.20 cfs @ 13.03 hrs HW=71.72' (Free Discharge)

1=Culvert (Inlet Controls 40.76 cfs @ 8.30 fps)

Secondary OutFlow Max=81.92 cfs @ 13.03 hrs HW=71.72' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 81.92 cfs @ 2.26 fps)

Summary for Pond 2P: Two 30" Culverts at Crossing Brook Road

Inflow Area =	270.310 ac, 25.53% Impervious, Ir	nflow Depth > 3.13" for 25 YEAR event
Inflow =	265.34 cfs @ 12.87 hrs, Volume=	70.499 af
Outflow =	107.91 cfs @ 15.37 hrs, Volume=	60.494 af, Atten= 59%, Lag= 149.9 min
Primary =	107.91 cfs @ 15.37 hrs, Volume=	60.494 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

⁻²⁼Culvert (Inlet Controls 21.44 cfs @ 6.82 fps)

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 54.37' @ 15.37 hrs Surf.Area= 187,335 sf Storage= 1,227,360 cf

Plug-Flow detention time= 135.1 min calculated for 60.293 af (86% of inflow) Center-of-Mass det. time= 98.8 min (963.6 - 864.7)

Volume	Invert	Avail.Sto	age Stor	age Description	
#1	44.00'	2,030,00	00 cf Cus	tom Stage Data (P	rismatic)Listed below (Recalc)
Elevation	on Surf	Area	Inc.Store	e Cum.Store	
(fee		sq-ft)	(cubic-feet)		
44.0		0,000)		
46.0		0,000	140,000	•	
48.0		0,000	180,000	•	
50.0		0,000	220,000		
52.0		0,000	280,000		
54.0		0,000	340,000	•	
56.0		0,000	400,000		
58.0		0,000	470,000		
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	,,,,,,	_,,,,,,,,	
Device	Routing	Invert	Outlet Dev	vices	
#1	Primary	44.00'	30.0" Ro	und Culvert	
	-		L= 50.0'	RCP, sq.cut end pr	ojecting, Ke= 0.500
			Inlet / Out	et Invert= 44.00' / 4	12.00' S= 0.0400 '/' Cc= 0.900
			n= 0.011	Concrete pipe, stra	ight & clean, Flow Area= 4.91 sf
#2	Primary	44.00'		und Culvert	
					headwall, Ke= 0.900
					12.00' S= 0.0400 '/' Cc= 0.900
				•	or, Flow Area= 3.14 sf
#3	Secondary	56.00'			Broad-Crested Rectangular Weir
			,	,	0.80 1.00 1.20 1.40 1.60
			Coef. (Eng	glish) 2.68 2.70 2.	.70 2.64 2.63 2.64 2.64 2.63
			0 45 05 1		B:

Primary OutFlow Max=107.91 cfs @ 15.37 hrs HW=54.37' (Free Discharge)

1=Culvert (Inlet Controls 71.36 cfs @ 14.54 fps)

2=Culvert (Inlet Controls 36.55 cfs @ 11.63 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=44.00' (Free Discharge)

3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 3P: 24" CULVERT

Inflow Area =	38.000 ac,	0.00% Impervious, Inflow	Depth > 2.41" for 25 YEAR event
Inflow =	54.61 cfs @	12.67 hrs, Volume=	7.620 af
Outflow =	48.56 cfs @	12.86 hrs, Volume=	7.573 af, Atten= 11%, Lag= 11.4 min
Primary =	31.72 cfs @	12.86 hrs, Volume=	7.117 af
Secondary =	16.84 cfs @	12.86 hrs, Volume=	0.456 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 59.40' @ 12.86 hrs Surf.Area= 16,981 sf Storage= 45,177 cf

Plug-Flow detention time= 14.6 min calculated for 7.548 af (99% of inflow)

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Center-of-Mass det. time= 12.4 min (846.7 - 834.3)

Volume	Inver	t Avail.Sto	rage Storage	Description	
#1	54.00	56,34	42 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
54.0	00	2,362	0	0	
56.0	00	6,990	9,352	9,352	
58.0	00	10,000	16,990	26,342	
60.0	00	20,000	30,000	56,342	
Device	Routing	Invert	Outlet Device	S	
#1	Primary	54.00'	24.0" Round	Culvert	
#2	Secondary	y 59.00'	Inlet / Outlet I n= 0.011 Cor 25.0' long x Head (feet) 0	nvert= 54.00' / 5 ncrete pipe, stra 25.0' breadth B 0.20 0.40 0.60	ojecting, Ke= 0.500 53.00' S= 0.0200 '/' Cc= 0.900 ight & clean, Flow Area= 3.14 sf broad-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=31.71 cfs @ 12.86 hrs HW=59.39' (Free Discharge) 1=Culvert (Inlet Controls 31.71 cfs @ 10.09 fps)

Secondary OutFlow Max=16.63 cfs @ 12.86 hrs HW=59.39' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 16.63 cfs @ 1.69 fps)

Summary for Pond 4P: 18" CULVERT

Inflow Area =	13.000 ac,	7.69% Impervious, Inflow De	epth > 2.75" for 25 YEAR event	
Inflow =	18.21 cfs @	12.81 hrs, Volume=	2.982 af	
Outflow =	11.61 cfs @	13.31 hrs, Volume=	2.938 af, Atten= 36%, Lag= 30.1 m	nin
Primary =	11.61 cfs @	13.31 hrs, Volume=	2.938 af	
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 87.61' @ 13.31 hrs Surf.Area= 17,137 sf Storage= 26,474 cf

Plug-Flow detention time= 30.0 min calculated for 2.938 af (99% of inflow) Center-of-Mass det. time= 24.9 min (860.1 - 835.2)

Volume	Invert	Avail.Sto	orage	Storage	Description	
#1	85.00'	82,7	55 cf	Custon	n Stage Data (Pr	ismatic)Listed below (Recalc)
Elevation (feet)	Surf. <i>i</i> (s	Area sq-ft)	_	.Store c-feet)	Cum.Store (cubic-feet)	
85.00	3	,343		0	0	
86.00	8	,410		5,877	5,877	
88.00		,234		7,644	33,521	
90.00	30	,000	4	9,234	82,755	

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Device	Routing	Invert	Outlet Devices
#1	Primary	85.00'	18.0" Round Culvert
	-		L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 85.00' / 84.00' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.77 sf
#2	Secondary	89.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=11.61 cfs @ 13.31 hrs HW=87.61' (Free Discharge)
1=Culvert (Inlet Controls 11.61 cfs @ 6.57 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=85.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 5P: 4'x3' Oval and 30" Overflow Culvert

Inflow Area =	184.000 ac, 3	30.43% Impervious, Ir	iflow Depth > 3.3	1" for 25 YEAR event
Inflow =	195.88 cfs @	12.60 hrs, Volume=	50.828 af	
Outflow =	195.61 cfs @	12.62 hrs, Volume=	49.959 af,	Atten= 0%, Lag= 1.4 min
Primary =	41.35 cfs @	12.62 hrs, Volume=	24.775 af	_
Secondary =	154.26 cfs @	12.62 hrs, Volume=	25.185 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 137.98' @ 12.62 hrs Surf.Area= 19,954 sf Storage= 97,425 cf

Plug-Flow detention time= 18.5 min calculated for 49.959 af (98% of inflow) Center-of-Mass det. time= 12.7 min (855.8 - 843.0)

Volume	Inver	rt Avail.Sto	rage Storage	Description			
#1	#1		35 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)		
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
129.00 4,441 130.00 6,196 132.00 8,225		4,441 6,196 8,225	5,319 14,421	5,319 19,740			
134.0 136.0 138.0 140.0	00 00	10,880 14,005 20,000 25,000	19,105 24,885 34,005 45,000	38,845 63,730 97,735 142,735			
Device	Routing	Invert	Outlet Device	S			
#1	Primary	129.00'	4.0" W x 3.0" H, R=3.0" Elliptical Culvert				
#2	Primary	132.00'	L= 30.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 129.00' / 128.00' S= 0.0333 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.07 sf 30.0" Round Culvert L= 50.0' CPP, projecting, no headwall, Ke= 0.900 Inlet / Outlet Invert= 132.00' / 128.00' S= 0.0800 '/' Cc= 0.900				
#3 Secondary 137.00'		n= 0.010 PVC, smooth interior, Flow Area= 4.91 sf 60.0' long x 30.0' breadth Broad-Crested Rectangular Weir					

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Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.63

Primary OutFlow Max=41.34 cfs @ 12.62 hrs HW=137.98' (Free Discharge)

1=Culvert (Barrel Controls 0.75 cfs @ 11.15 fps)
2=Culvert (Inlet Controls 40.59 cfs @ 8.27 fps)

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Secondary OutFlow Max=153.85 cfs @ 12.62 hrs HW=137.98' (Free Discharge) = 3=Broad-Crested Rectangular Weir (Weir Controls 153.85 cfs @ 2.61 fps)

Summary for Pond 6P: 1-48" Culvert Crossing Golf Cart Path

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 3.25" for 25 YEAR event

Inflow = 195.00 cfs @ 12.69 hrs, Volume= 49.794 af

Outflow = 167.75 cfs @ 13.40 hrs, Volume= 49.594 af, Atten= 14%, Lag= 42.0 min

Primary = 143.09 cfs @ 13.40 hrs, Volume= 47.792 af Secondary = 24.65 cfs @ 13.40 hrs, Volume= 1.802 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 103.59' @ 13.40 hrs Surf.Area= 50,620 sf Storage= 202,628 cf

Avail Storage Storage Description

Plug-Flow detention time= 15.7 min calculated for 49.429 af (99% of inflow)

Center-of-Mass det. time= 14.3 min (874.4 - 860.0)

Invort

volume	IIIVEI	t Avaii.Sto	rage Storage i	Jescription				
#1	96.00)' 280,44	48 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)			
Elevation	on S	Surf.Area	Inc.Store	Cum.Store				
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)				
96.0	00	1,580	0	0				
98.0	00	14,434	16,014	16,014				
100.0		30,000	44,434	60,448				
102.0		40,000	70,000	130,448				
105.0	00	60,000	150,000	280,448				
Device	Routing	Invert	Outlet Devices					
#1	Primary	96.00'	48.0" Round	Culvert				
			L= 30.0' RCP	L= 30.0' RCP, sq.cut end projecting, Ke= 0.500				
				Inlet / Outlet Invert= 96.00' / 95.00' S= 0.0333 '/' Cc= 0.900				
					ight & clean, Flow Area= 12.57 sf			
#2	Secondar	y 103.00'			road-Crested Rectangular Weir			
			` '		0.80 1.00 1.20 1.40 1.60			
			Coet. (English)) 2.68 2.70 2.	70 2.64 2.63 2.64 2.64 2.63			

Primary OutFlow Max=143.09 cfs @ 13.40 hrs HW=103.59' (Free Discharge)
1=Culvert (Inlet Controls 143.09 cfs @ 11.39 fps)

Secondary OutFlow Max=24.65 cfs @ 13.40 hrs HW=103.59' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 24.65 cfs @ 2.08 fps)

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Summary for Pond 7P: 1-24" Culvert at Greely Middle School

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 3.87" for 25 YEAR event

Inflow = 47.09 cfs @ 12.12 hrs, Volume= 3.550 af

Outflow = 2.00 cfs @ 15.48 hrs, Volume= 1.411 af, Atten= 96%, Lag= 201.4 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 124.71' @ 15.48 hrs Surf.Area= 27,778 sf Storage= 105,955 cf

Plug-Flow detention time= 256.5 min calculated for 1.411 af (40% of inflow)

Center-of-Mass det. time= 162.0 min (934.4 - 772.4)

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	214,248 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	18,593	0	0
122.00	21,745	40,338	40,338
124.00	25,131	46,876	87,214
126.00	32,605	57,736	144,950
128.00	36,693	69,298	214,248

Device	Routing	Invert	Outlet Devices
#1	Primary	120.00'	24.0" Round Culvert
	-		L= 80.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 120.00' / 119.00' S= 0.0125 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Secondary	127.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63
#3	Device 1	120.00'	6.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	126.00'	24.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Primary OutFlow Max=2.00 cfs @ 15.48 hrs HW=124.71' (Free Discharge)

1=Culvert (Passes 2.00 cfs of 29.13 cfs potential flow)

3=Orifice/Grate (Orifice Controls 2.00 cfs @ 10.17 fps)

-4=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=120.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 10P: 1-30" Culvert

Inflow Area =	112.000 ac, 2	21.43% Impervious,	Inflow Depth > 2.7	7" for 25 YEAR event
Inflow =	151.56 cfs @	12.87 hrs, Volume=	= 25.855 af	
Outflow =	144.41 cfs @	13.02 hrs, Volume=	= 25.567 af,	Atten= 5%, Lag= 8.8 min
Primary =	41.57 cfs @	13.02 hrs, Volume=	= 16.793 af	-
Secondary =	102.84 cfs @	13.02 hrs, Volume=	= 8.774 af	

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 72.34' @ 13.02 hrs Surf.Area= 56,811 sf Storage= 111,654 cf

Plug-Flow detention time= 17.9 min calculated for 25.482 af (99% of inflow) Center-of-Mass det. time= 14.1 min (856.7 - 842.6)

Volume	Inve	rt Avail.Sto	rage	Storage	Description		
#1	68.0	0' 211,04	48 cf	Custom	Stage Data (Pi	rismatic)Listed below (Recalc)	
	Elevation Surf.Area (feet) (sq-ft)			:.Store c-feet)	Cum.Store (cubic-feet)		
68.0		8,000	(Cabi	0	0		
70.0 72.0	00	14,434 55,480		22,434 89,914	22,434 92,348		
74.0		63,220		18,700	211,048		
Device	Routing	Invert	Outl	et Device	S		
#1	Primary	68.00'	30.0" Round Culvert				
#2	·		L= 30.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 68.00' / 67.00' S= 0.0333 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf 25.0' long x 25.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63				

Primary OutFlow Max=41.56 cfs @ 13.02 hrs HW=72.34' (Free Discharge) 1=Culvert (Inlet Controls 41.56 cfs @ 8.47 fps)

Secondary OutFlow Max=102.61 cfs @ 13.02 hrs HW=72.34' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 102.61 cfs @ 3.06 fps)

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Summary for Subcatchment 1S:

Runoff = 246.43 cfs @ 12.78 hrs, Volume= 40.761 af, Depth> 4.84"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

_	Area	(ac) (CN Des	cription					
,	57.	000	70 WO	ODS / FIEI	_D HSG C				
7	19.	000	98 EXIS	STING IMF	PERVIOUS	AREA			
5	25.	000	74 EXIS	STING LAV	WN C				
	101.000 76 Weighted Average								
	82.	000	81.1	9% Pervio	us Area				
	19.	000	18.8	1% Imperv	ious Area				
	Тс	Length	Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	28.8	100	0.0400	0.06		Sheet Flow, AB			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC			
_						Forest w/Heavy Litter Kv= 2.5 fps			
	58.8	1.000	Total						

Summary for Subcatchment 2S:

Runoff = 229.83 cfs @ 12.68 hrs, Volume= 34.931 af, Depth> 4.86"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac)	CN	Desc	cription		
*		310	70	WOO	DDS / FIEL	D HSG C	
*	13.	000	98	EXIS	TING IMF	PERVIOUS	AREA
*	30.	000	74	EXIS	TING LAV	VN C	
	86.	310	76	Weig	hted Aver	age	
	73.	310		84.9	4% Pervio	us Area	
	13.	000		15.00	6% Imperv	vious Area	
	Тс	Length	ı S	lope	Velocity	Capacity	Description
	(min)	(feet		(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0)400	0.06	, ,	Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	21.7	650	0.0	0400	0.50		Shallow Concentrated Flow, BC
_							Forest w/Heavy Litter Kv= 2.5 fps
	50.5	750) To	tal			

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Summary for Subcatchment 3S:

Runoff = 95.27 cfs @ 12.61 hrs, Volume= 13.270 af, Depth> 4.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac) C	CN Des	cription		
*	34.	000	70 WO	ODS / FIEI	D HSG C	
*	0.	000	98 EXIS	STING IMF	PERVIOUS	AREA
*	4.	000	74 EXIS	STING LAV	VN C	
38.000 70 Weighted Average 38.000 100.00% Pervious Area						
_	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	28.8	100	0.0400	0.06		Sheet Flow, AB
	15.0	450	0.0400	0.50		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, BC Forest w/Heavy Litter Kv= 2.5 fps
_	43.8	550	Total	·		

Summary for Subcatchment 4S:

Runoff = 30.35 cfs @ 12.78 hrs, Volume= 5.001 af, Depth> 4.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac)	CN	Desc	ription		
*	5.	000	70	WOO	DDS / FIEL	D HSG C	
*	1.	000	98	EXIS	TING IMP	ERVIOUS	AREA
*	7.	000	74	EXIS	TING LAV	VN C	
	13.	000	74	Weig	hted Aver	age	
	_	000			1% Pervio		
				7.69	% Impervio	ous Area	
					•		
	Tc	Lengtl	า ร	Slope	Velocity	Capacity	Description
	(min)	(feet	()	(ft/ft)	(ft/sec)	(cfs)	•
-	28.8	100	0.	.0400	0.06	` '	Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.	.0400	0.50		Shallow Concentrated Flow, BC
			_		,,,,,		Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000) T	otal			,

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Summary for Subcatchment 5S: drains to 48" culvert

Runoff = 205.17 cfs @ 13.43 hrs, Volume= 51.121 af, Depth> 5.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac) C	N Des	cription		
*	47.	000	70 WO	ODS / FIEL	D HSG C	
*	36.	000	98 EXIS	STING IMF	PERVIOUS	AREA
*	35.	000	74 EXIS	STING LAV	VN C	
	118.	000	80 Wei	ghted Aver	age	
	82.	000	69.4	9% Pervio	us Area	
	36.000 30.51% Impervious Area					
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	38.0	100	0.0200	0.04		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	60.0	900	0.0100	0.25		Shallow Concentrated Flow, BC
						Forest w/Heavy Litter Kv= 2.5 fps
	14.8	2,671	0.0400	3.00		Shallow Concentrated Flow, CD
_						Grassed Waterway Kv= 15.0 fps
	112.8	3,671	Total			

Summary for Subcatchment 6S: drains to 48" culvert

Runoff = 226.05 cfs @ 12.51 hrs, Volume= 29.982 af, Depth> 5.45"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac) C	N Des	cription		
*	6.	000	70 WO	DDS / FIEI	D HSG C	
*	20.	000	98 EXIS	STING IME	PERVIOUS	AREA
*				STING LAV	VN C	
	66	000		hted Aver		
		000	,	0% Pervio		
	_	000		0% Imperv		
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	•
	28.8	100	0.0400	0.06	` '	Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	5.0	900	0.0400	3.00		Shallow Concentrated Flow, BC
						Grassed Waterway Kv= 15.0 fps
	3.7	2,500	0.0400	11.41	182.56	Trap/Vee/Rect Channel Flow, CD
		,				Bot.W=4.00' D=2.00' Z= 2.0 '/' Top.W=12.00'
						n= 0.030 Earth, grassed & winding
	37.5	3.500	Total			

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Summary for Subcatchment 7S:

Runoff = 70.86 cfs @ 12.12 hrs, Volume= 5.462 af, Depth> 5.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

_	Area	(ac)	CN	Desc	cription		
*	0.	000	70	WOO	DDS / FIEL	D HSG C	
*	5.	000	98	EXIS	TING IMP	PERVIOUS	AREA
*	6.	000	74	EXIS	STING LAV	VN C	
_	11.	000	85	Weid	hted Aver	age	
	6.	000			5% Pervio	0	
	5.000 45.45% Impervious Area					ious Area	
					•		
	Tc	Lengtl	า ร	Slope	Velocity	Capacity	Description
	(min)	(feet	()	(ft/ft)	(ft/sec)	(cfs)	
	7.5	100	0.	.0400	0.22		Sheet Flow, AB
							Grass: Short n= 0.150 P2= 3.10"
	1.1	200	0.	.0400	3.00		Shallow Concentrated Flow, BC
							Grassed Waterway Kv= 15.0 fps
_	8.6	300) To	otal			•

Summary for Reach 3R: Stream below RR crossing

Inflow Area = 112.000 ac. 21.43% Impervious, Inflow Depth > 4.60" for 100 YEAR event

Inflow = 248.09 cfs @ 12.80 hrs, Volume= 42.902 af

Outflow = 247.50 cfs @ 12.85 hrs, Volume= 42.796 af, Atten= 0%, Lag= 3.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 8.37 fps, Min. Travel Time= 1.7 min Avg. Velocity = 3.76 fps, Avg. Travel Time= 3.8 min

Peak Storage= 25,467 cf @ 12.82 hrs Average Depth at Peak Storage= 3.21'

Bank-Full Depth= 4.00' Flow Area= 40.0 sf, Capacity= 373.38 cfs

6.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 14.00'

Length= 860.0' Slope= 0.0116 '/'

Inlet Invert= 82.00', Outlet Invert= 72.00'



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Summary for Reach 4R: Stream above RR crossing

Inflow Area = 112.000 ac, 21.43% Impervious, Inflow Depth > 4.60" for 100 YEAR event

Inflow = 248.20 cfs @ 12.78 hrs, Volume= 42.928 af

Outflow = 248.09 cfs @ 12.80 hrs, Volume= 42.902 af, Atten= 0%, Lag= 1.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.93 fps, Min. Travel Time= 0.4 min Avg. Velocity = 3.55 fps, Avg. Travel Time= 0.9 min

Peak Storage= 6,264 cf @ 12.79 hrs Average Depth at Peak Storage= 3.35'

Bank-Full Depth= 4.00' Flow Area= 40.0 sf, Capacity= 346.26 cfs

6.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 14.00'

Length= 200.0' Slope= 0.0100 '/'

Inlet Invert= 84.00', Outlet Invert= 82.00'



Summary for Reach 6R: Stream below Site

Inflow Area = 270.310 ac, 25.53% Impervious, Inflow Depth > 5.07" for 100 YEAR event

Inflow = 494.85 cfs @ 12.85 hrs. Volume= 114.172 af

Outflow = 493.76 cfs @ 12.88 hrs, Volume= 114.029 af, Atten= 0%, Lag= 1.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 8.10 fps, Min. Travel Time= 0.9 min

Avg. Velocity = 4.06 fps, Avg. Travel Time= 1.8 min

Peak Storage= 27,466 cf @ 12.86 hrs

Average Depth at Peak Storage= 4.78'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 538.97 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 61.00', Outlet Invert= 58.00'



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Summary for Reach 7R: Stream Through Site

Inflow Area = 270.310 ac, 25.53% Impervious, Inflow Depth > 5.08" for 100 YEAR event

Inflow = 496.11 cfs @ 12.81 hrs, Volume= 114.395 af

Outflow = 494.85 cfs @ 12.85 hrs, Volume= 114.172 af, Atten= 0%, Lag= 2.5 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 13.03 fps, Min. Travel Time= 1.4 min Avg. Velocity = 6.35 fps, Avg. Travel Time= 2.9 min

Peak Storage= 41,837 cf @ 12.83 hrs Average Depth at Peak Storage= 3.35

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 683.45 cfs

 $8.00' \times 4.00'$ deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,100.0' Slope= 0.0245 '/'

Inlet Invert= 88.00', Outlet Invert= 61.00'



Summary for Reach 14R: Swale from School and Neighborhood

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 2.53" for 100 YEAR event

Inflow = 5.29 cfs @ 13.59 hrs, Volume= 2.323 af

Outflow = 5.15 cfs @ 14.25 hrs, Volume= 2.167 af, Atten= 3%, Lag= 40.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.59 fps, Min. Travel Time= 21.7 min

Avg. Velocity = 1.53 fps, Avg. Travel Time= 36.7 min

Peak Storage= 6,698 cf @ 13.89 hrs

Average Depth at Peak Storage= 0.45'

Bank-Full Depth= 3.00' Flow Area= 21.0 sf, Capacity= 147.12 cfs

4.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 10.00'

Length= 3,366.0' Slope= 0.0100 '/'

Inlet Invert= 117.66', Outlet Invert= 84.00'



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Summary for Reach 18R: Stream Through Site

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 5.22" for 100 YEAR event

Inflow 310.32 cfs @ 12.61 hrs. Volume= 79.993 af

309.46 cfs @ 12.67 hrs, Volume= Outflow 79.772 af, Atten= 0%, Lag= 3.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 9.93 fps, Min. Travel Time= 2.0 min Avg. Velocity = 4.83 fps, Avg. Travel Time= 4.1 min

Peak Storage= 37,431 cf @ 12.64 hrs Average Depth at Peak Storage= 2.87'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 563.18 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,200.0' Slope= 0.0167 '/'

Inlet Invert= 125.00', Outlet Invert= 105.00'



Summary for Reach 55R: Wetland below Site

38.000 ac, 0.00% Impervious, Inflow Depth > 4.19" for 100 YEAR event 95.27 cfs @ 12.61 hrs, Volume= 13.270 af Inflow Area =

Inflow

Outflow 94.84 cfs @ 12.65 hrs, Volume= 13.239 af, Atten= 0%, Lag= 2.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 5.08 fps, Min. Travel Time= 1.5 min

Avg. Velocity = 2.16 fps, Avg. Travel Time= 3.5 min

Peak Storage= 8,420 cf @ 12.62 hrs Average Depth at Peak Storage= 1.89'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 540.76 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 63.02', Outlet Invert= 60.00'



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Summary for Pond 1P: 1-30" and 1-24" Culvert at Tuttle Road

Inflow Area = 112.000 ac, 21.43% Impervious, Inflow Depth > 4.55" for 100 YEAR event

Inflow = 239.14 cfs @ 12.97 hrs, Volume= 42.426 af

Outflow = 239.06 cfs @ 12.98 hrs, Volume= 42.364 af, Atten= 0%, Lag= 0.6 min

Primary = 66.82 cfs @ 12.98 hrs, Volume= 27.779 af Secondary = 172.24 cfs @ 12.98 hrs, Volume= 14.586 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 72.19' @ 12.98 hrs Surf.Area= 8,201 sf Storage= 24,403 cf

Plug-Flow detention time= 2.9 min calculated for 42.364 af (100% of inflow)

Center-of-Mass det. time= 2.4 min (845.4 - 843.1)

Device Routing Invert Outlet Devices

volume	invert A	vail.Storage	Storage	Description	
#1	68.00'	31,683 cf	Custom	Stage Data (Pri	smatic)Listed below (Recalc)
Elevation (feet)	Surf.Are (sq-f		.Store c-feet)	Cum.Store (cubic-feet)	
68.00	3,85	60	0	0	

_	(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
	68.00	3,850	0	0
	70.00	5,600	9,450	9,450
	72.00	7,800	13,400	22,850
	73.00	9,865	8,833	31,683

#1	Primary	67.50'	30.0" Round Culvert
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf
#2	Primary	67.50'	24.0" Round Culvert
			L= 50.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
#3	Secondary	71.00'	50.0' long x 50.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=66.80 cfs @ 12.98 hrs HW=72.19' (Free Discharge)

1=Culvert (Inlet Controls 43.85 cfs @ 8.93 fps)

2=Culvert (Inlet Controls 22.95 cfs @ 7.30 fps)

Secondary OutFlow Max=171.91 cfs @ 12.98 hrs HW=72.19' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 171.91 cfs @ 2.88 fps)

Summary for Pond 2P: Two 30" Culverts at Crossing Brook Road

Inflow Area =	270.310 ac, 2	25.53% Impervious, T	nflow Depth > 5.06	6" for 100 YEAR event
Inflow =	493.76 cfs @	12.88 hrs, Volume=	114.029 af	
Outflow =	237.60 cfs @	14.35 hrs, Volume=	93.222 af, A	Atten= 52%, Lag= 88.1 min
Primary =	124.60 cfs @	14.35 hrs, Volume=	76.641 af	-
Secondary =	113.00 cfs @	14.35 hrs, Volume=	16.581 af	

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 57.43' @ 14.35 hrs Surf.Area= 241,475 sf Storage= 1,890,336 cf

Plug-Flow detention time= 133.0 min calculated for 92.912 af (81% of inflow) Center-of-Mass det. time= 88.6 min (939.0 - 850.4)

Volume	Invert	Avail.Sto	rage Storage	e Description				
#1	44.00'	2,030,00	00 cf Custor	n Stage Data (P	rismatic)Listed below (Recalc)			
Classatia	on Comf	A ====	Ina Ctara	Cuma Chama				
Elevation			Inc.Store	Cum.Store				
(fee		sq-ft)	(cubic-feet)	(cubic-feet)				
44.0		,000	0	0				
46.0		,000	140,000	140,000				
48.0		,000	180,000	320,000				
50.0		,000	220,000	540,000				
52.0		,000	280,000 340,000	820,000				
54.0		180,000		1,160,000				
56.0		220,000		1,560,000				
58.0	00 250	250,000		2,030,000				
Device	Routing	Invert	Outlet Device	es				
#1	Primary	44.00'	30.0" Roun	d Culvert				
	•		L= 50.0' RC	P, sq.cut end pro	ojecting, Ke= 0.500			
			Inlet / Outlet	Invert= 44.00' / 4	2.00' S= 0.0400 '/' Cc= 0.900			
				n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf				
#2	Primary	44.00'	24.0" Roun	d Culvert				
		Ž		L= 50.0' CPP, projecting, no headwall, Ke= 0.900				
				Inlet / Outlet Invert= 44.00' / 42.00' S= 0.0400 '/' Cc= 0.900				
			n= 0.010 PV	C, smooth interior	or, Flow Area= 3.14 sf			
#3	Secondary	56.00'	25.0' long x	25.0' breadth B	road-Crested Rectangular Weir			
					0.80 1.00 1.20 1.40 1.60			
			Coef. (Englis	sh) 2.68 2.70 2.	70 2.64 2.63 2.64 2.64 2.63			

Primary OutFlow Max=124.60 cfs @ 14.35 hrs HW=57.43' (Free Discharge)

-1=Culvert (Inlet Controls 82.49 cfs @ 16.81 fps)

Secondary OutFlow Max=112.99 cfs @ 14.35 hrs HW=57.43' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 112.99 cfs @ 3.16 fps)

Summary for Pond 3P: 24" CULVERT

Inflow Area =	38.000 ac,	0.00% Impervious, Inflow	Depth > 4.18"	for 100 YEAR event
Inflow =	94.84 cfs @	12.65 hrs, Volume=	13.239 af	
Outflow =	93.27 cfs @	12.72 hrs, Volume=	13.176 af, Att	en= 2%, Lag= 4.1 min
Primary =	33.61 cfs @	12.72 hrs, Volume=	10.216 af	•
Secondary =	59.66 cfs @	12.72 hrs, Volume=	2.961 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 59.94' @ 12.72 hrs Surf.Area= 19,682 sf Storage= 55,082 cf

Plug-Flow detention time= 12.8 min calculated for 13.176 af (100% of inflow)

²⁼Culvert (Inlet Controls 42.11 cfs @ 13.40 fps)

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Center-of-Mass det. time= 11.1 min (832.9 - 821.8)

Volume	Inver	t Avail.Sto	rage Storage	Description	
#1	54.00	0' 56,34	42 cf Custon	n Stage Data (P	rismatic)Listed below (Recalc)
Elevation	on S	Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
54.0	00	2,362	0	0	
56.0	00	6,990	9,352	9,352	
58.0	00	10,000	16,990	26,342	
60.0	00	20,000	30,000	56,342	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	54.00'	24.0" Round	d Culvert	
#2 Secondary 59.00'		L= 50.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 54.00' / 53.00' S= 0.0200 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf 25.0' long x 25.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63			

Primary OutFlow Max=33.60 cfs @ 12.72 hrs HW=59.93' (Free Discharge)
1=Culvert (Inlet Controls 33.60 cfs @ 10.70 fps)

Secondary OutFlow Max=59.41 cfs @ 12.72 hrs HW=59.93' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 59.41 cfs @ 2.54 fps)

Summary for Pond 4P: 18" CULVERT

Inflow Area =	13.000 ac,	7.69% Impervious, Inflow D	epth > 4.62" for 100 YEAR event
Inflow =	30.35 cfs @	12.78 hrs, Volume=	5.001 af
Outflow =	15.83 cfs @	13.43 hrs, Volume=	4.943 af, Atten= 48%, Lag= 39.0 min
Primary =	15.41 cfs @	13.43 hrs, Volume=	4.937 af
Secondary =	0.43 cfs @	13.43 hrs, Volume=	0.006 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 89.03' @ 13.43 hrs Surf.Area= 24,770 sf Storage= 56,147 cf

Plug-Flow detention time= 40.7 min calculated for 4.943 af (99% of inflow) Center-of-Mass det. time= 36.5 min (860.4 - 823.9)

Volu	me	Invert	Avai	l.Storage	Storage	e Description		
#1		85.00'	8	82,755 cf	Custor	n Stage Data (Pris	matic)Listed belo	w (Recalc)
Elev	ation (feet)		Area sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)		
	85.00	3	3,343		0	0		
8	86.00	8	3,410		5,877	5,877		
8	88.00	19	9,234	2	7,644	33,521		
(90.00	30	0,000	4	9,234	82,755		

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Device	Routing	Invert	Outlet Devices
#1	Primary	85.00'	18.0" Round Culvert
	•		L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 85.00' / 84.00' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 1.77 sf
#2	Secondary	89.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=15.40 cfs @ 13.43 hrs HW=89.03' (Free Discharge)
1=Culvert (Inlet Controls 15.40 cfs @ 8.72 fps)

Secondary OutFlow Max=0.31 cfs @ 13.43 hrs HW=89.03' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 0.31 cfs @ 0.45 fps)

Summary for Pond 5P: 4'x3' Oval and 30" Overflow Culvert

Inflow Area =	184.000 ac, 3	30.43% Impervious, I	nflow Depth > 5.2	29" for 100 YEAR event
Inflow =	310.62 cfs @	12.59 hrs, Volume=	81.103 af	
Outflow =	310.32 cfs @	12.61 hrs, Volume=	79.993 af,	Atten= 0%, Lag= 1.3 min
Primary =	43.18 cfs @	12.61 hrs, Volume=	30.794 af	-
Secondary =	267.14 cfs @	12.61 hrs, Volume=	49.198 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 138.42' @ 12.61 hrs Surf.Area= 21,043 sf Storage= 106,292 cf

Plug-Flow detention time= 14.3 min calculated for 79.727 af (98% of inflow) Center-of-Mass det. time= 9.6 min (842.4 - 832.8)

Volume	Invert	Avail.Stor	age Storage [Description	
#1	129.00'	142,73	5 cf Custom	Stage Data (Pri	smatic)Listed below (Recalc)
Elevatio		urf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
129.0	00	4,441	0	0	
130.0	00	6,196	5,319	5,319	
132.0	00	8,225	14,421	19,740	
134.0	00	10,880	19,105	38,845	
136.0	00	14,005	24,885	63,730	
138.0	00	20,000	34,005	97,735	
140.0	00	25,000	45,000	142,735	
<u>Device</u>	Routing	Invert	Outlet Devices		
#1	Primary	129.00'	4.0" W x 3.0" I	H, R=3.0" Ellip	tical Culvert
			L= 30.0' RCP	, sq.cut end pro	jecting, Ke= 0.500
			Inlet / Outlet In	vert= 129.00' / 1	28.00' S= 0.0333 '/' Cc= 0.900
			n= 0.011 Cond	crete pipe, straig	ght & clean, Flow Area= 0.07 sf
#2	Primary	132.00'	30.0" Round		•
	,		L= 50.0' CPP.	projecting, no l	neadwall, Ke= 0.900
					28.00' S= 0.0800 '/' Cc= 0.900
					r, Flow Area= 4.91 sf
#3	Secondary	137.00'		•	oad-Crested Rectangular Weir

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Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.63

Primary OutFlow Max=43.17 cfs @ 12.61 hrs HW=138.42' (Free Discharge)

—1=Culvert (Barrel Controls 0.77 cfs @ 11.39 fps)
—2=Culvert (Inlet Controls 42.41 cfs @ 8.64 fps)

Secondary OutFlow Max=266.71 cfs @ 12.61 hrs HW=138.42' (Free Discharge) = 3=Broad-Crested Rectangular Weir (Weir Controls 266.71 cfs @ 3.14 fps)

Summary for Pond 6P: 1-48" Culvert Crossing Golf Cart Path

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 5.20" for 100 YEAR event Inflow = 309.46 cfs @ 12.67 hrs, Volume= 79.772 af

Outflow = 285.90 cfs @ 12.94 hrs, Volume= 79.464 af, Atten= 8%, Lag= 16.1 min Primary = 157.89 cfs @ 12.94 hrs, Volume= 64.473 af

Secondary = 128.01 cfs @ 12.94 hrs, Volume= 14.991 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 104.81' @ 12.94 hrs Surf.Area= 58,728 sf Storage= 269,120 cf

Plug-Flow detention time= 15.3 min calculated for 79.200 af (99% of inflow) Center-of-Mass det. time= 13.9 min (860.1 - 846.2)

Avail Storage Storage Description

volunie	IIIVEI	t Avaii.Sto	rage Storage i	Jescription			
#1	96.00)' 280,44	48 cf Custom	Stage Data (P	rismatic)Listed below (Recalc)		
Elevation	on S	Surf.Area	Inc.Store	Cum.Store			
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)			
96.0	00	1,580	0	0			
98.0	00	14,434	16,014	16,014			
100.0		30,000	44,434	60,448			
102.0		40,000	70,000	130,448			
105.0	00	60,000	150,000	280,448			
Device	Routing	Invert	Outlet Devices				
#1	Primary	96.00'	48.0" Round	Culvert			
			L= 30.0' RCP	, sq.cut end pro	ojecting, Ke= 0.500		
			Inlet / Outlet Invert= 96.00' / 95.00' S= 0.0333 '/' Cc= 0.900				
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 12.57 sf				
#2	Secondar	y 103.00'		20.0' long x 20.0' breadth Broad-Crested Rectangular Weir			
			` '		0.80 1.00 1.20 1.40 1.60		
			Coet. (English)) 2.68 2.70 2.	70 2.64 2.63 2.64 2.64 2.63		

Primary OutFlow Max=157.88 cfs @ 12.94 hrs HW=104.81' (Free Discharge)
1=Culvert (Inlet Controls 157.88 cfs @ 12.56 fps)

Secondary OutFlow Max=127.90 cfs @ 12.94 hrs HW=104.81' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 127.90 cfs @ 3.54 fps)

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Summary for Pond 7P: 1-24" Culvert at Greely Middle School

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 5.96" for 100 YEAR event

Inflow = 70.86 cfs @ 12.12 hrs, Volume= 5.462 af

Outflow = 5.29 cfs @ 13.59 hrs, Volume= 2.323 af, Atten= 93%, Lag= 88.0 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 126.27' @ 13.59 hrs Surf.Area= 33,165 sf Storage= 153,967 cf

Plug-Flow detention time= 234.9 min calculated for 2.323 af (43% of inflow)

Center-of-Mass det. time= 139.3 min (901.6 - 762.3)

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	214,248 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	18,593	0	0
122.00	21,745	40,338	40,338
124.00	25,131	46,876	87,214
126.00	32,605	57,736	144,950
128.00	36,693	69,298	214,248

Device	Routing	Invert	Outlet Devices
#1	Primary	120.00'	24.0" Round Culvert
			L= 80.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 120.00' / 119.00' S= 0.0125 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Secondary	127.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
	•		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63
#3	Device 1	120.00'	6.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	126.00'	24.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Primary OutFlow Max=5.27 cfs @ 13.59 hrs HW=126.27' (Free Discharge)

-1=Culvert (Passes 5.27 cfs of 34.74 cfs potential flow)

3=Orifice/Grate (Orifice Controls 2.32 cfs @ 11.82 fps)

-4=Orifice/Grate (Weir Controls 2.95 cfs @ 1.71 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=120.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 10P: 1-30" Culvert

Inflow Area =	112.000 ac, 2	21.43% Impervious,	Inflow Depth > 4.5	9" for 100 YEAR event
Inflow =	247.50 cfs @	12.85 hrs, Volume=	= 42.796 af	
Outflow =	239.14 cfs @	12.97 hrs, Volume=	= 42.426 af,	Atten= 3%, Lag= 7.3 min
Primary =	46.08 cfs @	12.97 hrs, Volume=	= 22.662 af	_
Secondary =	193.06 cfs @	12.97 hrs, Volume=	= 19.764 af	

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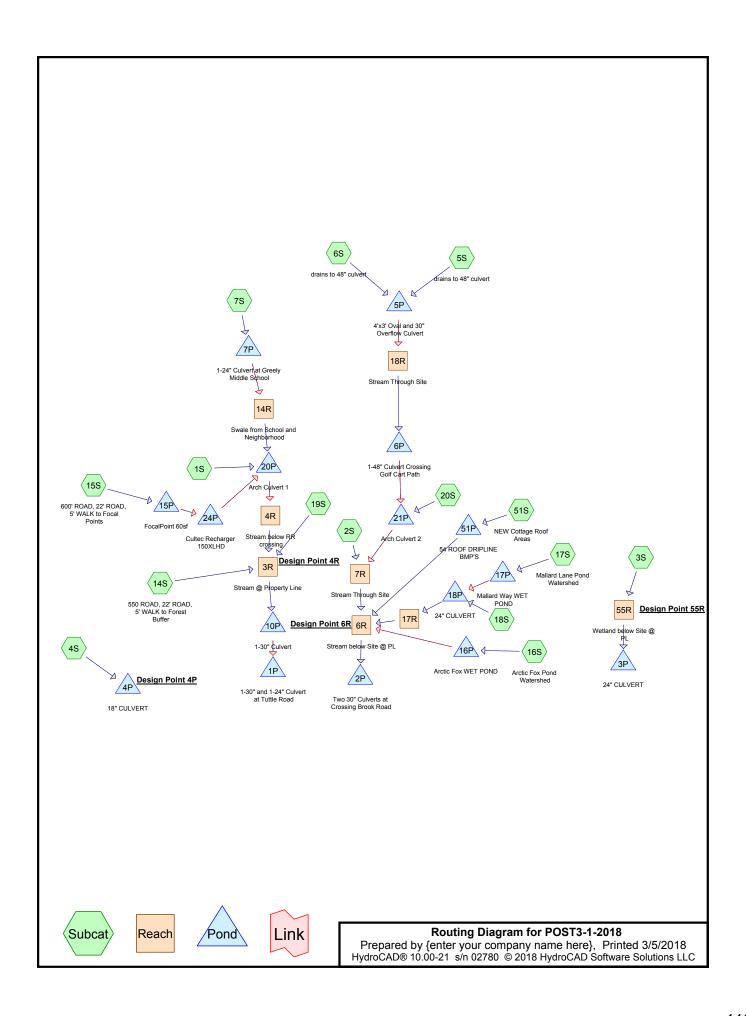
Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 73.05' @ 12.97 hrs Surf.Area= 59,545 sf Storage= 152,766 cf

Plug-Flow detention time= 16.0 min calculated for 42.426 af (99% of inflow) Center-of-Mass det. time= 13.0 min (843.1 - 830.1)

Volume	Inve	ert Avail.Sto	rage Storag	ge Description	
#1	68.0	00' 211,0	48 cf Custo	om Stage Data (P	rismatic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
68.0		8,000	0	0	
70.0 72.0		14,434 55,480	22,434 69,914	22,434 92,348	
74.0		63,220	118,700	211,048	
Device	Routing	Invert	Outlet Devi	ces	
#1	Primary	68.00'	30.0" Rou	nd Culvert	
#2 Secondary 71.00'		L= 30.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 68.00' / 67.00' S= 0.0333 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf 25.0' long x 25.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63			

Primary OutFlow Max=46.06 cfs @ 12.97 hrs HW=73.05' (Free Discharge) 1=Culvert (Inlet Controls 46.06 cfs @ 9.38 fps)

Secondary OutFlow Max=192.71 cfs @ 12.97 hrs HW=73.05' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 192.71 cfs @ 3.76 fps)



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Area Listing (selected nodes)

Area	CN	Description
(acres)		(subcatchment-numbers)
3.220	98	52 Cottage Roofs + Community Buildings (51S)
94.000	98	EXISTING IMPERVIOUS AREA (1S, 2S, 4S, 5S, 6S, 7S, 19S)
147.000	74	EXISTING LAWN C (1S, 2S, 3S, 4S, 5S, 6S, 7S, 19S)
0.410	70	NEW FILL SLOPE (3S)
4.420	98	NEW IMPERVIOUS PAVED AREA (14S, 15S, 16S, 17S, 19S)
11.530	74	NEW LAWN C (1S, 2S, 3S, 14S, 15S, 16S, 17S, 18S, 19S, 20S)
0.100	98	NEW Trails (3S)
0.130	98	New Trails (2S)
172.490	70	WOODS / FIELD HSG C (1S, 2S, 3S, 4S, 5S, 6S, 16S, 17S, 18S, 19S, 20S)
433.300	78	TOTAL AREA

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Summary for Subcatchment 1S:

Runoff = 43.61 cfs @ 12.84 hrs, Volume= 7.268 af, Depth> 1.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area (ac) CN			Desc	ription		
*	* 43.440 70 WOODS / FIELD HSG C					D HSG C	
* 18.400 98 EXISTING IMPERVIOUS AREA						AREA	
* 23.400 74 EXISTING LAWN C				EXIS	TING LAV	VN C	
*	0.	100	74 N	NEW	LAWN C		
85.340 77 Weighted Average							
66.940 78.44% Pervious Area							
	18.400			21.56	3% Imperv	ious Area	
	Tc	Length	Slo	ре	Velocity	Capacity	Description
_	(min)	(feet)	(ft	t/ft)	(ft/sec)	(cfs)	
	28.8	100	0.04	100	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.04	100	0.50		Shallow Concentrated Flow, BC
							Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Tota	 al			

Summary for Subcatchment 2S:

Runoff = 37.50 cfs @ 12.73 hrs, Volume= 5.728 af, Depth> 1.03"

	Area	(ac)	CN	Desc	cription			
*	22.	010	70	WOO	DDS / FIEL	D HSG C		
*	13.	000	98	EXIS	STING IMP	PERVIOUS	AREA	
*	30.	000	74	EXIS	STING LAV	VN C		
*	1.	850	74	NEW	/ LAWN C			
*	0.	000	98	NEW	/ IMPERV	IOUS BUIL	DING AREA (see 51S)	
*	0.	130	98	New	Trails			
	66.	990	77	Weig	hted Aver	age		
	53.	860		80.40% Pervious Area				
	13.	130		19.6	0% Imperv	vious Area		
	_			_				
	Tc	Length		lope	Velocity	Capacity	Description	
_	(min)	(feet)) ((ft/ft)	(ft/sec)	(cfs)		
	28.8	100	0.0	400	0.06		Sheet Flow, AB	
							Woods: Dense underbrush n= 0.800 P2= 3.10"	
	21.7	650	0.0	400	0.50		Shallow Concentrated Flow, BC	
_							Forest w/Heavy Litter Kv= 2.5 fps	
	50.5	750	To	tal				

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Summary for Subcatchment 3S:

Runoff = 12.08 cfs @ 12.91 hrs, Volume= 2.160 af, Depth> 0.72"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac)	CN	Desc	cription						
*	31.	320	70	WOO	DDS / FIEL	D HSG C					
*	0.	000	98	EXIS	EXISTING IMPERVIOUS AREA						
*				EXIS	STING LAV	VN C					
*	0.	210	74	NEW	/ LAWN C						
*	0.	410	70	NEW	NEW FILL SLOPE						
*	0.	000	98	NEV	NEW IMPERVIOUS BUILDING AREA (See 51s)						
*	0.	100	98	NEV	/ Trails						
	36.	040	71	Weig	hted Aver	age					
	35.	940		99.7	2% Pervio	us Area					
	0.	100		0.28	% Impervi	ous Area					
	Тс	Length		Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	28.8	100	0.	0400	0.06		Sheet Flow, AB				
							Woods: Dense underbrush n= 0.800 P2= 3.10"				
	15.0	450	0.	0400	0.50		Shallow Concentrated Flow, BC				
			_				Forest w/Heavy Litter Kv= 2.5 fps				
	16.5	75	5 0.	0900	0.08		Sheet Flow,				
_							Woods: Dense underbrush n= 0.800 P2= 3.10"				
	60.3	625	5 To	otal							

Summary for Subcatchment 4S:

Runoff = 5.49 cfs @ 12.86 hrs, Volume= 0.935 af, Depth> 0.86"

	Area (ac)	CN	Description
*	5.000	70	WOODS / FIELD HSG C
*	1.000	98	EXISTING IMPERVIOUS AREA
*	7.000	74	EXISTING LAWN C
*	0.000	98	NEW IMPERVIOUS PAVED AREA
*	0.000	74	NEW LAWN C
	13.000	74	Weighted Average
	12.000		92.31% Pervious Area
	1.000		7.69% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
_	(111111)	(1661)	(1011)	(11/366)	(613)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC
						Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Total			·

Summary for Subcatchment 5S: drains to 48" culvert

Runoff = 46.40 cfs @ 13.55 hrs, Volume= 11.467 af, Depth> 1.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac) (CN De	escription				
*	47.000 70		70 W	OODS / FIE	LD HSG C			
*	36.	000	98 EX	CISTING IMP	PERVIOUS	AREA		
*	35.	000	74 EX	EXISTING LAWN C				
	118.	000	80 W	eighted Ave	rage			
	82.	000	69	.49% Pervio	us Area			
	36.	000	30	.51% Imper	vious Area			
	_					-		
	Тс	Length			Capacity	Description		
_	(min)	(feet)	(ft/fi	t) (ft/sec)	(cfs)			
	38.0	100	0.020	0.04		Sheet Flow, AB		
						Woods: Dense underbrush n= 0.800 P2= 3.10"		
	60.0	900	0.010	0 0.25		Shallow Concentrated Flow, BC		
						Forest w/Heavy Litter Kv= 2.5 fps		
	14.8	2,671	0.040	0 3.00		Shallow Concentrated Flow, CD		
_						Grassed Waterway Kv= 15.0 fps		
	112.8	3,671	Total					

Summary for Subcatchment 6S: drains to 48" culvert

Runoff = 54.10 cfs @ 12.54 hrs, Volume= 6.986 af, Depth> 1.27"

	Area (ac)	CN	Description
*	6.000	70	WOODS / FIELD HSG C
*	20.000	98	EXISTING IMPERVIOUS AREA
*	40.000	74	EXISTING LAWN C
	66.000	81	Weighted Average
	46.000		69.70% Pervious Area
	20.000		30.30% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
28.8	100	0.0400	0.06		Sheet Flow, AB
					Woods: Dense underbrush n= 0.800 P2= 3.10"
5.0	900	0.0400	3.00		Shallow Concentrated Flow, BC
					Grassed Waterway Kv= 15.0 fps
3.7	2,500	0.0400	11.41	182.56	Trap/Vee/Rect Channel Flow, CD
					Bot.W=4.00' D=2.00' Z= 2.0 '/' Top.W=12.00'
					n= 0.030 Earth, grassed & winding
37.5	3 500	Total			

Summary for Subcatchment 7S:

Runoff = 19.44 cfs @ 12.12 hrs, Volume= 1.427 af, Depth> 1.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac)	CN [Desc	ription		
*	0.	000	70 ١	WOC	DS / FIEL	D HSG C	
*	5.	000	98 E	EXIS	TING IMP	PERVIOUS	AREA
*	6.	000	74 E	<u>EXIS</u>	TING LAV	VN C	
	11.	000	85 \	Weig	hted Aver	age	
	6.	000	5	54.55	5% Pervio	us Area	
	5.	000	4	45.45	5% Imperv	vious Area	
_	Tc (min)	Length (feet)		ppe t/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	7.5	100	0.04	100	0.22		Sheet Flow, AB
	1.1	200	0.04	100	3.00		Grass: Short n= 0.150 P2= 3.10" Shallow Concentrated Flow, BC Grassed Waterway Kv= 15.0 fps
	8.6	300	Tota	al			

Summary for Subcatchment 14S: 550 ROAD, 22' ROAD, 5' WALK to Forest Buffer

Runoff = 0.91 cfs @ 12.26 hrs, Volume= 0.092 af, Depth> 2.21"

	Area (ac)	CN	Description
*	0.400	98	NEW IMPERVIOUS PAVED AREA
*	0.100	74	NEW LAWN C
	0.500	93	Weighted Average
	0.100		20.00% Pervious Area
	0.400		80.00% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
0.2	11	0.0300	1.02		Sheet Flow, AB
					Smooth surfaces n= 0.011 P2= 3.10"
1.2	250	0.0300	3.52		Shallow Concentrated Flow, BC
					Paved Kv= 20.3 fps
18.3	75	0.0700	0.07		Sheet Flow,
					Woods: Dense underbrush n= 0.800 P2= 3.10"
19.7	336	Total		•	

Summary for Subcatchment 15S: 600' ROAD, 22' ROAD, 5' WALK to Focal Points

Runoff = 1.45 cfs @ 12.02 hrs, Volume= 0.090 af, Depth> 1.95"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac) (CN Des	cription			
*	0.	0.370 98 NEW IMPERVIOUS PAVED AREA					
*	0.	180	74 NEV	V LAWN C			
	0.550 90		90 Weig	ghted Aver	age		
	0.180 32.73% Pervious Are			3% Pervio	us Area		
	0.370 67.27% Impervious Area			7% Imperv	vious Area		
	Tc (min)	Length (feet)	•	Velocity (ft/sec)	Capacity (cfs)	Description	
	0.2	11	0.0300	1.02		Sheet Flow, AB	
	1.2	250	0.0300	3.52		Smooth surfaces n= 0.011 P2= 3.10" Shallow Concentrated Flow, BC Paved Kv= 20.3 fps	
	1.4	261	Total				

Summary for Subcatchment 16S: Arctic Fox Pond Watershed

Runoff = 2.55 cfs @ 12.83 hrs, Volume= 0.420 af, Depth> 1.20"

	Area (ac)	CN	Description
*	0.570	70	WOODS / FIELD HSG C
*	0.000	98	EXISTING IMPERVIOUS AREA
*	0.000	74	EXISTING LAWN C
*	1.100	98	NEW IMPERVIOUS PAVED AREA
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (see 51s)
*	2.540	74	NEW LAWN C
	4.210	80	Weighted Average
	3.110		73.87% Pervious Area
	1.100		26.13% Impervious Area

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	Tc	Length	Slope	,		Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC
_						Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Total			

Summary for Subcatchment 17S: Mallard Lane Pond Watershed

Runoff = 4.88 cfs @ 12.82 hrs, Volume= 0.801 af, Depth> 1.32"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac)	CN	Desc	cription		
*	0.	220	70	WOO	DDS / FIEI	_D HSG C	
*	0.	000	98	EXIS	STING IMF	PERVIOUS	AREA
*	0.	000	74	EXIS	STING LAV	VN C	
*	2.	400	98	NEV	VIMPERV	IOUS PAVI	ED AREA
*	0.	000	98	NEV	V IMPERV	IOUS BUIL	DING AREA (see 51s)
*	4.	640	74	NEV	V LAWN C		
	7.	260	82	Weig	ghted Aver	age	
	4.	860		66.9	4% Pervio	us Area	
	2.	400		33.0	6% Imperv	ious Area	
	Тс	Length	ı S	lope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0	0400	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.0	0400	0.50		Shallow Concentrated Flow, BC
_							Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	To	tal			

Summary for Subcatchment 18S:

Runoff = 0.46 cfs @ 12.76 hrs, Volume= 0.072 af, Depth> 0.77"

	Area (ac)	CN	Description
*	0.450	70	WOODS / FIELD HSG C
*	0.680	74	NEW LAWN C
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (see 51s)
	1.130	72	Weighted Average
	1.130		100.00% Pervious Area

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	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	21.7	650	0.0400	0.50		Shallow Concentrated Flow, BC
_						Forest w/Heavy Litter Kv= 2.5 fps
	50.5	750	Total			

Summary for Subcatchment 19S:

Runoff = 11.45 cfs @ 12.15 hrs, Volume= 0.913 af, Depth> 0.79"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac) C	N Des	cription		
*	10.	660	70 WO	ODS / FIEI	D HSG C	
*	0.	600	98 EXI	STING IMF	PERVIOUS	AREA
*	1.	600	74 EXIS	STING LAV	VN C	
*	0.	940	74 NEV	V LAWN C		
*	0.	150	98 NEV	V IMPERV	IOUS PAVI	ED AREA
*	0.	000	98 NEV	V IMPERV	IOUS BUIL	DING AREA (See 51s)
	13.	950	72 Wei	ghted Aver	age	
13.200 94.62% Pervious Area						
	0.	750	5.38	3% Impervi	ous Area	
	Тс	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.5	100	0.0400	0.22		Sheet Flow, AB
						Grass: Short n= 0.150 P2= 3.10"
	1.7	300	0.0400	3.00		Shallow Concentrated Flow, BC
_						Grassed Waterway Kv= 15.0 fps
	92	400	Total			

Summary for Subcatchment 20S:

Runoff = 2.55 cfs @ 12.56 hrs, Volume= 0.348 af, Depth> 0.68"

	Area (ac)	CN	Description
*	5.820	70	WOODS / FIELD HSG C
*	0.000	98	EXISTING IMPERVIOUS AREA
*	0.000	74	EXISTING LAWN C
*	0.290	74	NEW LAWN C
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (See 51s)
	6.110	70	Weighted Average
	6.110		100.00% Pervious Area

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	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	6.7	200	0.0400	0.50		Shallow Concentrated Flow, BC
_						Forest w/Heavy Litter Kv= 2.5 fps
	35.5	300	Total			

Summary for Subcatchment 51S: NEW Cottage Roof Areas

Runoff = 7.24 cfs @ 12.21 hrs, Volume= 0.719 af, Depth> 2.68"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 2 YEAR Rainfall=3.10"

	Area	(ac) C	N Desc	cription		
*	3.	220 9	98 52 C	ottage Ro	ofs + Comn	nunity Buildings
	3.	220	100.	00% Impe	rvious Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.1	20	0.4000	3.25		Sheet Flow, AB Smooth surfaces n= 0.011 P2= 3.10"
	2.5	25	0.0400	0.17		Sheet Flow, BC Grass: Short n= 0.150 P2= 3.10"
	13.1	75	0.1600	0.10		Sheet Flow, CD Woods: Dense underbrush n= 0.800 P2= 3.10"
	15.7	120	Total			

Summary for Reach 3R: Stream @ Property Line

Inflow Area = 111.340 ac, 22.38% Impervious, Inflow Depth > 0.97" for 2 YEAR event

Inflow = 46.00 cfs @ 12.95 hrs, Volume= 8.962 af

Outflow = 45.72 cfs @ 13.07 hrs, Volume= 8.881 af, Atten= 1%, Lag= 6.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.48 fps, Min. Travel Time= 4.1 min Avg. Velocity = 1.30 fps, Avg. Travel Time= 11.0 min

Peak Storage= 11,308 cf @ 13.00 hrs Average Depth at Peak Storage= 1.01'

Bank-Full Depth= 3.00' Flow Area= 45.0 sf, Capacity= 287.21 cfs

12.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 1.0 '/' Top Width= 18.00' Length= 860.0' Slope= 0.0058 '/'

Inlet Invert= 77.00', Outlet Invert= 72.00'

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Summary for Reach 4R: Stream below RR crossing

Inflow Area = 96.890 ac, 24.53% Impervious, Inflow Depth > 0.99" for 2 YEAR event

Inflow = 44.17 cfs @ 12.86 hrs, Volume= 8.018 af

Outflow = 43.95 cfs @ 12.96 hrs, Volume= 7.957 af, Atten= 1%, Lag= 6.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.99 fps, Min. Travel Time= 3.6 min Avg. Velocity = 1.70 fps, Avg. Travel Time= 8.4 min

Peak Storage= 9,488 cf @ 12.90 hrs Average Depth at Peak Storage= 1.48'

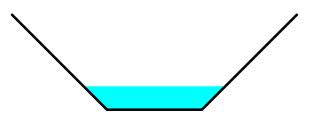
Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 582.42 cfs

6.00' x 6.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 860.0' Slope= 0.0058 '/'

Inlet Invert= 82.00', Outlet Invert= 77.00'



Summary for Reach 6R: Stream below Site @ PL

Inflow Area = 272.920 ac, 27.79% Impervious, Inflow Depth > 1.05" for 2 YEAR event

Inflow = 87.77 cfs @ 13.11 hrs, Volume= 23.928 af

Outflow = 87.63 cfs @ 13.16 hrs, Volume= 23.862 af, Atten= 0%, Lag= 2.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity = 4.94 fps, Min. Travel Time = 1.5 min Avg. Velocity = 3.01 fps, Avg. Travel Time = 2.5 min

Peak Storage= 7,980 cf @ 13.13 hrs Average Depth at Peak Storage= 1.81'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 538.97 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 61.00', Outlet Invert= 58.00'

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Summary for Reach 7R: Stream Through Site

Inflow Area = 257.100 ac, 26.89% Impervious, Inflow Depth > 1.10" for 2 YEAR event

Inflow = 87.49 cfs @ 13.04 hrs, Volume= 23.560 af

Outflow = 87.35 cfs @ 13.11 hrs, Volume= 23.460 af, Atten= 0%, Lag= 4.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity = 7.70 fps, Min. Travel Time = 2.4 min Avg. Velocity = 4.57 fps, Avg. Travel Time = 4.0 min

Peak Storage= 12,483 cf @ 13.07 hrs Average Depth at Peak Storage= 1.23'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 683.45 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,100.0' Slope= 0.0245 '/'

Inlet Invert= 88.00', Outlet Invert= 61.00'



Summary for Reach 14R: Swale from School and Neighborhood

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 0.85" for 2 YEAR event

Inflow = 1.21 cfs @ 14.58 hrs, Volume= 0.776 af

Outflow = 1.21 cfs @ 15.70 hrs, Volume= 0.668 af, Atten= 0%, Lag= 67.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.54 fps, Min. Travel Time= 36.4 min Avg. Velocity = 1.17 fps, Avg. Travel Time= 47.8 min

Peak Storage= 2,643 cf @ 15.09 hrs Average Depth at Peak Storage= 0.19'

Bank-Full Depth= 3.00' Flow Area= 21.0 sf, Capacity= 147.12 cfs

4.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 10.00'

Length= 3,366.0' Slope= 0.0100 '/'

Inlet Invert= 117.66', Outlet Invert= 84.00'

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Summary for Reach 17R:

8.390 ac, 28.61% Impervious, Inflow Depth > 0.55" for 2 YEAR event Inflow Area =

Inflow 0.74 cfs @ 15.44 hrs, Volume= 0.387 af

0.74 cfs @ 15.56 hrs, Volume= Outflow 0.380 af, Atten= 0%, Lag= 7.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.41 fps, Min. Travel Time= 4.8 min Avg. Velocity = 2.11 fps, Avg. Travel Time= 5.5 min

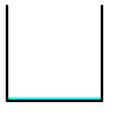
Peak Storage= 214 cf @ 15.48 hrs Average Depth at Peak Storage= 0.10'

Bank-Full Depth= 3.00' Flow Area= 9.0 sf, Capacity= 102.76 cfs

3.00' x 3.00' deep channel, n= 0.022 Earth, clean & straight

Length= 700.0' Slope= 0.0286 '/'

Inlet Invert= 81.00', Outlet Invert= 61.00'



Summary for Reach 18R: Stream Through Site

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 1.16" for 2 YEAR event

67.65 cfs @ 12.77 hrs, Volume= Inflow 17.762 af

66.47 cfs @ 12.89 hrs, Volume= Outflow 17.661 af, Atten= 2%, Lag= 7.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.18 fps. Min. Travel Time= 3.2 min

Avg. Velocity = 3.42 fps, Avg. Travel Time= 5.8 min

Peak Storage= 12,911 cf @ 12.83 hrs Average Depth at Peak Storage= 1.17'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 563.18 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,200.0' Slope= 0.0167 '/'

Inlet Invert= 125.00', Outlet Invert= 105.00'

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Summary for Reach 55R: Wetland below Site @ PL

Inflow Area = 36.040 ac, 0.28% Impervious, Inflow Depth > 0.72" for 2 YEAR event

Inflow = 12.08 cfs @ 12.91 hrs, Volume= 2.160 af

Outflow = 12.06 cfs @ 12.99 hrs, Volume= 2.146 af, Atten= 0%, Lag= 4.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.54 fps, Min. Travel Time= 3.0 min Avg. Velocity = 1.37 fps, Avg. Travel Time= 5.5 min

Peak Storage= 2,134 cf @ 12.94 hrs Average Depth at Peak Storage= 0.55'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 540.76 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 63.02', Outlet Invert= 60.00'



Summary for Pond 1P: 1-30" and 1-24" Culvert at Tuttle Road

Inflow Area = 111.340 ac, 22.38% Impervious, Inflow Depth > 0.94" for 2 YEAR event

Inflow = 36.86 cfs @ 13.41 hrs, Volume= 8.705 af

Outflow = 36.38 cfs @ 13.49 hrs, Volume= 8.694 af, Atten= 1%, Lag= 4.7 min

Primary = 36.38 cfs @ 13.49 hrs, Volume= 8.694 af Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 69.71' @ 13.49 hrs Surf.Area= 5,347 sf Storage= 7,866 cf

Plug-Flow detention time= 3.2 min calculated for 8.694 af (100% of inflow)

Center-of-Mass det. time= 2.8 min (891.6 - 888.8)

Volume	Invert	Avail.Storage	Storage Description
#1	68.00'	31,683 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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#1	Primary	67.50'	30.0" Round C	culvert	K0- (
Device	Routing	Invert	Outlet Devices		
73.0	00	9,865	8,833	31,683	
72.0	00	7,800	13,400	22,850	
70.0	00	5,600	9,450	9,450	
68.0	00	3,850	0	0	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
Elevation	on	Surf.Area	Inc.Store	Cum.Store	

#1	Primary	67.50'	30.0" Round Culvert
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf
#2	Primary	67.50'	
			L= 50.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
#3	Secondary	71.00'	50.0' long x 50.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=36.37 cfs @ 13.49 hrs HW=69.71' (Free Discharge)

1=Culvert (Inlet Controls 23.23 cfs @ 5.06 fps)

-2=Culvert (Inlet Controls 13.13 cfs @ 4.18 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=68.00' (Free Discharge)

3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 2P: Two 30" Culverts at Crossing Brook Road

Inflow Area =	272.920 ac, 27.79% Impervious, Inflow	Depth > 1.05" for 2 YEAR event
Inflow =	87.63 cfs @ 13.16 hrs, Volume=	23.862 af
Outflow =	54.15 cfs @ 14.65 hrs, Volume=	22.111 af, Atten= 38%, Lag= 89.3 min
Primary =	54.15 cfs @ 14.65 hrs, Volume=	22.111 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 47.48' @ 14.65 hrs Surf.Area= 94,846 sf Storage= 269,789 cf

Plug-Flow detention time= 74.8 min calculated for 22.038 af (92% of inflow) Center-of-Mass det. time= 55.0 min (950.6 - 895.5)

Volume	Invert	Avail.Storage	Storage Description
#1	44.00'	2,030,000 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
44.00	60,000	0	0
46.00	80,000	140,000	140,000
48.00	100,000	180,000	320,000
50.00	120,000	220,000	540,000
52.00	160,000	280,000	820,000
54.00	180,000	340,000	1,160,000
56.00	220,000	400,000	1,560,000
58.00	250,000	470,000	2,030,000

Device	Routing	Invert	Outlet Devices		
#1	Primary	44.00'	30.0" Round Culvert		
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500		
			Inlet / Outlet Invert= 44.00' / 42.00' S= 0.0400 '/' Cc= 0.900		
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf		
#2	Primary	44.00'	24.0" Round Culvert		
			L= 50.0' CPP, projecting, no headwall, Ke= 0.900		
			Inlet / Outlet Invert= 44.00' / 42.00' S= 0.0400 '/' Cc= 0.900		
			n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf		
#3	Secondary	56.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir		
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60		
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63		

Primary OutFlow Max=54.15 cfs @ 14.65 hrs HW=47.48' (Free Discharge)

1=Culvert (Inlet Controls 35.33 cfs @ 7.20 fps)

2=Culvert (Inlet Controls 18.82 cfs @ 5.99 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=44.00' (Free Discharge) 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 3P: 24" CULVERT

Inflow Area =	36.040 ac,	0.28% Impervious, Inflow De	epth > 0.71" for 2 YEAR event
Inflow =	12.06 cfs @	12.99 hrs, Volume=	2.146 af
Outflow =	11.45 cfs @	13.14 hrs, Volume=	2.121 af, Atten= 5%, Lag= 9.2 min
Primary =	11.45 cfs @	13.14 hrs, Volume=	2.121 af
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 55.59' @ 13.14 hrs Surf.Area= 6,030 sf Storage= 6,651 cf

Plug-Flow detention time= 12.1 min calculated for 2.121 af (99% of inflow) Center-of-Mass det. time= 8.3 min (881.3 - 873.0)

Volume	Invert	Avail.Storage	Storage Description
#1	54.00'	56.342 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	on	Surf.Area	Inc.Store	Cum.Store		
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)		
54.0	00	2,362	0	0		
56.0	00	6,990	9,352	9,352		
58.0	00	10,000	16,990	26,342		
60.0	00	20,000	30,000	56,342		
Device	Routing	Invert	Outlet Devices			
#1	Primary	54.00'	24.0" Round Culvert			
	·		L= 50.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 54.00' / 53.00' S= 0.0200 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf			
#2	Seconda	ry 59.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir			

Primary OutFlow Max=11.44 cfs @ 13.14 hrs HW=55.58' (Free Discharge) 1=Culvert (Inlet Controls 11.44 cfs @ 4.29 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=54.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 4P: 18" CULVERT

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.63

Inflow Area =	13.000 ac,	7.69% Impervious, Inflow Do	epth > 0.86" for 2 YEAR event
Inflow =	5.49 cfs @	12.86 hrs, Volume=	0.935 af
Outflow =	4.55 cfs @	13.16 hrs, Volume=	0.910 af, Atten= 17%, Lag= 17.9 min
Primary =	4.55 cfs @	13.16 hrs, Volume=	0.910 af
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 86.04' @ 13.16 hrs Surf.Area= 8,631 sf Storage= 6,225 cf

Plug-Flow detention time= 28.3 min calculated for 0.910 af (97% of inflow) Center-of-Mass det. time= 19.6 min (879.1 - 859.5)

Volume	Inver	t Avail.Sto	rage Storag	age Storage Description			
#1	85.00)' 82,7	55 cf Custo	m Stage Data (Prismatio)Listed below (Recalc)		
Elevatio	-	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)			
85.0	00	3,343	0	0			
86.0	00	8,410	5,877	5,877			
88.0	00	19,234	27,644	33,521			
90.0	00	30,000	49,234	82,755			
Device	Routing	Invert	Outlet Devi	es			
#1	Primary	85.00'	18.0" Rou	nd Culvert			
				CP, sq.cut end projecting,			
				Invert= 85.00' / 84.00' S			
40	0			oncrete pipe, straight & cl			
#2	Secondar	y 89.00'	25.0 long	k 25.0' breadth Broad-Cr	ested Rectangular Weir		

Volume

Invert

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Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.63

Primary OutFlow Max=4.54 cfs @ 13.16 hrs HW=86.04' (Free Discharge)
1=Culvert (Inlet Controls 4.54 cfs @ 3.47 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=85.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 5P: 4'x3' Oval and 30" Overflow Culvert

Inflow Area =	184.000 ac, 30.43% Impervious, Inflow	Depth > 1.20" for 2 YEAR event
Inflow =	69.48 cfs @ 12.62 hrs, Volume=	18.453 af
Outflow =	67.65 cfs @ 12.77 hrs, Volume=	17.762 af, Atten= 3%, Lag= 8.9 min
Primary =	38.36 cfs @ 12.77 hrs, Volume=	14.947 af
Secondary =	29.29 cfs @ 12.77 hrs, Volume=	2.815 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 137.32' @ 12.77 hrs Surf.Area= 17,956 sf Storage= 84,792 cf

Plug-Flow detention time= 32.4 min calculated for 17.762 af (96% of inflow) Center-of-Mass det. time= 20.7 min (884.6 - 863.8)

Avail Storage Storage Description

Volume	IIIVEIL	Avaii.0t0	rage Storage Description			
#1	129.00'	142,73	35 cf Custom	Stage Data (Pri	ismatic)Listed below (Recalc)	
Elevation (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
129.0		4,441	0	0		
130.0		6,196	5,319	5,319		
132.0		8,225	14,421	19,740		
134.0		10,880	19,105	38,845		
136.0		14,005	24,885	63,730		
138.0		20,000	34,005	97,735		
	140.00 25,000		45,000	142,735		
		-,	-,	,		
Device	Routing	Invert	Outlet Devices	3		
#1	Primary	129.00'	4.0" W x 3.0"	H, R=3.0" Ellip	tical Culvert	
	,				jecting, Ke= 0.500	
			Inlet / Outlet Ir	nvert= 129.00' / 1	128.00' S= 0.0333 '/' Cc= 0.900	
			n= 0.011 Con	icrete pipe, straiç	ght & clean, Flow Area= 0.07 sf	
#2	Primary	132.00'	30.0" Round	Culvert		
			L= 50.0' CPF	P, projecting, no	headwall, Ke= 0.900	
					128.00' S= 0.0800 '/' Cc= 0.900	
				,	r, Flow Area= 4.91 sf	
#3	Secondary	137.00'			oad-Crested Rectangular Weir	
			` ,		0.80 1.00 1.20 1.40 1.60	
			Coef. (English	i) 2.68 2.70 2.7	70 2.64 2.63 2.64 2.64 2.63	

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Primary OutFlow Max=38.34 cfs @ 12.77 hrs HW=137.31' (Free Discharge)

-1=Culvert (Barrel Controls 0.72 cfs @ 10.76 fps)
-2=Culvert (Inlet Controls 37.62 cfs @ 7.66 fps)

Secondary OutFlow Max=28.51 cfs @ 12.77 hrs HW=137.31' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 28.51 cfs @ 1.51 fps)

Summary for Pond 6P: 1-48" Culvert Crossing Golf Cart Path

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 1.15" for 2 YEAR event
Inflow = 66.47 cfs @ 12.89 hrs, Volume= 17.661 af
Outflow = 61.46 cfs @ 13.39 hrs, Volume= 17.564 af, Atten= 8%, Lag= 30.1 min
Primary = 61.46 cfs @ 13.39 hrs, Volume= 17.564 af
Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 99.06' @ 13.39 hrs Surf.Area= 22,689 sf Storage= 35,702 cf

Plug-Flow detention time= 9.2 min calculated for 17.564 af (99% of inflow) Center-of-Mass det. time= 7.5 min (897.8 - 890.2)

Volume	Inv	ert Ava	il.Storage	Storage D	escription			
#1	96.	00' 2	80,448 cf	Custom 9	Stage Data (P	Prismatic)Listed below (Recalc)		
Elevation (fee		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)			
96.0	00	1,580		0	0			
98.0	00	14,434		16,014	16,014			
100.0	00	30,000	•	44,434	60,448			
102.0	00	40,000	•	70,000	130,448			
105.0	00	60,000	1:	50,000	280,448			
Device	Routing	In	vert Out	et Devices				
#1	Primary	96	5.00' 48.0	" Round (Culvert			
	,		L= 3	L= 30.0' RCP, sq.cut end projecting, Ke= 0.500				
			Inle	t / Outlet Inv	/ert= 96.00' / 9	95.00' S= 0.0333 '/' Cc= 0.900		

Primary OutFlow Max=61.45 cfs @ 13.39 hrs HW=99.06' (Free Discharge)
—1=Culvert (Inlet Controls 61.45 cfs @ 5.96 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 7P: 1-24" Culvert at Greely Middle School

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 1.56" for 2 YEAR event

Inflow = 19.44 cfs @ 12.12 hrs, Volume= 1.427 af

Outflow = 1.21 cfs @ 14.58 hrs, Volume= 0.776 af, Atten= 94%, Lag= 147.2 min

Primary = 1.21 cfs @ 14.58 hrs, Volume= 0.776 af Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 121.90' @ 14.58 hrs Surf.Area= 21,586 sf Storage= 38,151 cf

Plug-Flow detention time= 238.2 min calculated for 0.776 af (54% of inflow)

Center-of-Mass det. time= 158.6 min (952.3 - 793.7)

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	214,248 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	18,593	0	0
122.00	21,745	40,338	40,338
124.00	25,131	46,876	87,214
126.00	32,605	57,736	144,950
128.00	36,693	69,298	214,248

Device	Routing	Invert	Outlet Devices
#1	Primary	120.00'	24.0" Round Culvert
	-		L= 80.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 120.00' / 119.00' S= 0.0125 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Secondary	127.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63
#3	Device 1	120.00'	6.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	126.00'	24.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Primary OutFlow Max=1.21 cfs @ 14.58 hrs HW=121.90' (Free Discharge)

1=Culvert (Passes 1.21 cfs of 14.46 cfs potential flow)

3=Orifice/Grate (Orifice Controls 1.21 cfs @ 6.18 fps)

-4=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=120.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 10P: 1-30" Culvert

Inflow Area =	111.340 ac, 22	38% Impervious, Inflov	v Depth > 0.96" for	2 YEAR event
Inflow =	45.72 cfs @ 1	13.07 hrs, Volume=	8.881 af	
Outflow =	36.86 cfs @ 1	I3.41 hrs, Volume=	8.705 af, Atten= ²	19%, Lag= 20.9 min
Primary =	32.64 cfs @ 1	I3.41 hrs, Volume=	8.577 af	
Secondary =	4.22 cfs @ 1	I3.41 hrs, Volume=	0.128 af	

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 71.16' @ 13.41 hrs Surf.Area= 38,177 sf Storage= 52,867 cf

Plug-Flow detention time= 22.6 min calculated for 8.705 af (98% of inflow)

Center-of-Mass det. time= 16.4 min (888.8 - 872.4)

Volume	Inve	rt Avail.Sto	rage	Storage I	Description	
#1	68.00)' 211,0 ₄	48 cf	Custom	Stage Data (P	rismatic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)		c.Store c-feet)	Cum.Store (cubic-feet)	
68.0		8,000	(CUDI	0	0	
70.0	00	14,434		22,434	22,434	
72.0	00	55,480	(59,914	92,348	
74.0	00	63,220	11	18,700	211,048	
Device	Routing	Invert	Outl	et Devices	;	
#1	Primary	68.00'	30.0	" Round	Culvert	
#2 Secondary 71.00'		Inlet n= 0 25.0 Hea	:/Outlet In 0.011 Con 0.011 Con 0.1 Iong x 2 0 (feet) 0.	overt= 68.00' / 6 crete pipe, stra 25.0' breadth B 20 0.40 0.60	ojecting, Ke= 0.500 67.00' S= 0.0333 '/' Cc= 0.900 ight & clean, Flow Area= 4.91 sf road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 70 2.64 2.63 2.64 2.64 2.63	

Primary OutFlow Max=32.63 cfs @ 13.41 hrs HW=71.16' (Free Discharge) 1=Culvert (Inlet Controls 32.63 cfs @ 6.65 fps)

Secondary OutFlow Max=4.13 cfs @ 13.41 hrs HW=71.16' (Free Discharge) **-2=Broad-Crested Rectangular Weir** (Weir Controls 4.13 cfs @ 1.06 fps)

Summary for Pond 15P: FocalPoint 60sf

Inflow Area =	0.550 ac, 67.27% Impervious, Inflow I	Depth > 1.95" for 2 YEAR event
Inflow =	1.45 cfs @ 12.02 hrs, Volume=	0.090 af
Outflow =	1.44 cfs @ 12.03 hrs, Volume=	0.090 af, Atten= 0%, Lag= 0.4 min
Primary =	0.14 cfs @ 11.55 hrs, Volume=	0.058 af
Secondary =	1.31 cfs @ 12.03 hrs, Volume=	0.032 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 100.69' @ 12.03 hrs Surf.Area= 60 sf Storage= 112 cf

Plug-Flow detention time= (not calculated: outflow precedes inflow) Center-of-Mass det. time= 2.2 min (774.2 - 771.9)

Volume	Invert	Avail.Storage	Storage Description
#1	97.75'	27 cf	3.00'W x 20.00'L x 2.25'H FocalPoint
			135 cf Overall x 20.0% Voids
#2	100.00'	133 cf	Custom Stage Data (Prismatic)Listed below (Recalc) -Impervious
		160 cf	Total Available Storage

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
100.00	60	0	0
100.50	157	54	54
101.00	157	79	133

Device	Routing	Invert	Outlet Devices	
#1	Primary	97.75'	100.000 in/hr Exfiltration over Surface area Phase-In= 0.10'	
#2	Secondary	100.50'	18.0" Horiz. Orifice/Grate C= 0.600	
			Limited to weir flow at low heads	

Primary OutFlow Max=0.14 cfs @ 11.55 hrs HW=97.97' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.14 cfs)

Secondary OutFlow Max=1.24 cfs @ 12.03 hrs HW=100.69' (Free Discharge) 2=Orifice/Grate (Weir Controls 1.24 cfs @ 1.41 fps)

Summary for Pond 16P: Arctic Fox WET POND

Inflow Area =	4.210 ac, 26.13% Impervious, Inflow D	epth > 1.20" for 2 YEAR event
Inflow =	2.55 cfs @ 12.83 hrs, Volume=	0.420 af
Outflow =	0.24 cfs @ 17.25 hrs, Volume=	0.089 af, Atten= 91%, Lag= 265.5 min
Primary =	0.24 cfs @ 17.25 hrs, Volume=	0.089 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 77.00' Surf.Area= 4,505 sf Storage= 18,632 cf Peak Elev= 78.80' @ 17.25 hrs Surf.Area= 9,245 sf Storage= 33,441 cf (14,810 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 204.2 min (1,049.8 - 845.6)

Volume	Invert	Avail.Storage	Storage	Description	
#1	71.00'	82,315 cf	Custon	n Stage Data (Pris	matic)Listed below (Recalc)
Elevation	Surf.Ar		.Store	Cum.Store	
(feet)	(sq	-ft) (cubi	ic-feet)	(cubic-feet)	
71.00	1,8	52	0	0	

(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
71.00	1,852	0	0
72.00	2,232	2,042	2,042
73.00	2,636	2,434	4,476
74.00	3,065	2,851	7,327
75.00	3,520	3,293	10,619
76.00	4,000	3,760	14,379
77.00	4,505	4,253	18,632
77.10	7,408	596	19,227
78.00	8,400	7,114	26,341
79.00	9,450	8,925	35,266
80.00	10,557	10,004	45,269
81.00	11,720	11,139	56,408
82.00	12,940	12,330	68,738
83.00	14,215	13,578	82,315

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Device	Routing	Invert	Outlet Devices
#1	Primary	74.00'	18.0" Round Culvert
			L= 58.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 74.00' / 70.00' S= 0.0690 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	78.50'	6.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	81.00'	48.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	81.50'	10.0' long x 10.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.24 cfs @ 17.25 hrs HW=78.80' (Free Discharge)

1=Culvert (Passes 0.24 cfs of 17.13 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.24 cfs @ 1.88 fps)

3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=77.00' (Free Discharge)

4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 17P: Mallard Way WET POND

Inflow Area =	7.260 ac, 33.06% Impervious, Inflow Depth > 1.32" for 2 YEAR event
Inflow =	4.88 cfs @ 12.82 hrs, Volume= 0.801 af
Outflow =	0.66 cfs @ 15.80 hrs, Volume= 0.320 af, Atten= 86%, Lag= 178.7 min
Primary =	0.66 cfs @ 15.80 hrs, Volume= 0.320 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 88.00' Surf.Area= 5,558 sf Storage= 23,438 cf

Peak Elev= 90.24' @ 15.80 hrs Surf.Area= 12,217 sf Storage= 47,283 cf (23,845 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 159.6 min (1,000.4 - 840.8)

Volume	Invert	Avail.Storage	Storage Description
#1	81.00'	70,904 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
81.00	1,346	0	0
82.00	1,867	1,607	1,607
83.00	2,419	2,143	3,750
84.00	2,996	2,708	6,457
85.00	3,599	3,298	9,755
86.00	4,226	3,913	13,667
87.00	4,879	4,553	18,220
88.00	5,558	5,219	23,438
88.10	9,325	744	24,182
89.00	10,578	8,956	33,139
90.00	11,887	11,233	44,371
91.00	13,252	12,570	56,941
92.00	14,675	13,964	70,904
Device Routing	Invert	Outlet Devices	

Device	Routing	Invert	Outlet Devices
#1	Primary	86.00'	18.0" Round Culvert
			L= 31.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 86.00' / 85.50' S= 0.0161 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	89.50'	6.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	90.50'	48.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	91.00'	10.0' long x 10.0' breadth Broad-Crested Rectangular Weir
	-		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.66 cfs @ 15.80 hrs HW=90.24' (Free Discharge)

-1=Culvert (Passes 0.66 cfs of 15.90 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.66 cfs @ 3.38 fps)
3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=88.00' (Free Discharge)

4=Broad-Crested Rectangular Wair (Controls 0.00 efc) -4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 18P: 24" CULVERT

8.390 ac, 28.61% Impervious, Inflow Depth > 0.56" for 2 YEAR event Inflow Area = Inflow 0.74 cfs @ 15.36 hrs, Volume= 0.393 af 0.74 cfs @ 15.44 hrs, Volume= 0.387 af, Atten= 0%, Lag= 4.6 min Outflow = 0.74 cfs @ 15.44 hrs, Volume= Primary 0.387 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 85.35' @ 15.44 hrs Surf.Area= 1,040 sf Storage= 319 cf

Plug-Flow detention time= 7.7 min calculated for 0.386 af (98% of inflow) Center-of-Mass det. time= 4.3 min (978.5 - 974.1)

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Volume	Inv	ert Avail.Sto	rage Stora	ge Description	
#1	85.0	00' 15,8	69 cf Cust	om Stage Data (Prismatic)Lis	ted below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.0	00	788	0	0	
86.0	00	1,512	1,150	1,150	
87.0	00	3,898	2,705	3,855	
88.0	00	5,621	4,760	8,615	
89.0	00	8,888	7,255	15,869	
Device	Routing	Invert	Outlet Dev		
#1	Primary	85.00'		nd Culvert	0.500
			Inlet / Outle	RCP, sq.cut end projecting, Ke et Invert= 85.00' / 84.50' S= 0. Concrete pipe, straight & clean,	.0100 '/' Cc= 0.900

Primary OutFlow Max=0.74 cfs @ 15.44 hrs HW=85.35' (Free Discharge) 1=Culvert (Inlet Controls 0.74 cfs @ 2.01 fps)

Summary for Pond 20P: Arch Culvert 1

Inflow Area =	96.890 ac, 2	24.53% Impervious, Ir	nflow Depth > 0.99'	for 2 YEAR event
Inflow =	44.21 cfs @	12.85 hrs, Volume=	8.024 af	
Outflow =	44.17 cfs @	12.86 hrs, Volume=	8.018 af, A	tten= 0%, Lag= 0.7 min
Primary =	44.17 cfs @	12.86 hrs, Volume=	8.018 af	-
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 83.92' @ 12.86 hrs Surf.Area= 1,574 sf Storage= 1,818 cf

Plug-Flow detention time= 0.8 min calculated for 7.992 af (100% of inflow) Center-of-Mass det. time= 0.6 min (864.2 - 863.7)

Volume	Inv	ert Avail	.Storage	Storage D	escription	
#1	82.	00' 8	35,094 cf	Custom S	Stage Data (Pi	rismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)	_	.Store c-feet)	Cum.Store (cubic-feet)	
82.0	00	320		0	0	
86.0	00	2,932		6,504	6,504	
87.0	00	7,643		5,288	11,792	
88.0	00	11,989		9,816	21,608	
89.0	00	18,865	1	5,427	37,035	
90.0	00	23,627	2	1,246	58,281	
91.0	00	30,000	2	6,814	85,094	
Device	Routing	Inv	vert Outle	et Devices		
#1	Primary	82.			•	126.0" Pipe Arch RCP_Arch 88x54 onforming to fill, Ke= 0.500

L= 70.0' RCP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 82.00' / 81.50' S= 0.0071 '/' Cc= 0.900

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n= 0.022 Earth, clean & straight, Flow Area= 25.69 sf #2 Secondary 90.00'

25.0' long x 25.0' breadth Broad-Crested Rectangular Weir

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=44.13 cfs @ 12.86 hrs HW=83.92' (Free Discharge)

1=RCP Arch 88x54 (Barrel Controls 44.13 cfs @ 5.05 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=82.00' (Free Discharge) -2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 21P: Arch Culvert 2

Inflow Area = 190.110 ac, 29.46% Impervious, Inflow Depth > 1.13" for 2 YEAR event

62.31 cfs @ 13.35 hrs, Volume= Inflow 17.912 af

62.30 cfs @ 13.39 hrs, Volume= Outflow = 17.832 af, Atten= 0%, Lag= 2.4 min

62.30 cfs @ 13.39 hrs, Volume= 17.832 af Primary 0.00 cfs @ 5.00 hrs, Volume= Secondary = 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 93.98' @ 13.39 hrs Surf.Area= 6.980 sf Storage= 11.863 cf

Plug-Flow detention time= 4.1 min calculated for 17.832 af (100% of inflow) Center-of-Mass det. time= 2.8 min (899.7 - 896.9)

Volume	Invert	Avail.Storage	Storage Description
#1	92.00'	200,953 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
92.00	5,000	0	0
93.00	6,000	5,500	5,500
94.00	7,000	6,500	12,000
95.00	8,390	7,695	19,695
96.00	12,267	10,329	30,024
97.00	23,771	18,019	48,043
98.00	31,886	27,829	75,871
99.00	67,139	49,513	125,384
100.00	84,000	75,570	200,953

Device	Routing	Invert	Outlet Devices
#1	Primary	92.00'	122.0" W x 77.3" H, R=62.0"/218.0" Pipe Arch RCP_Arch 122x78
	•		L= 70.0' RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 92.00' / 91.50' S= 0.0071 '/' Cc= 0.900
			n= 0.022 Earth, clean & straight, Flow Area= 51.67 sf
#2	Secondary	99.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

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Primary OutFlow Max=62.28 cfs @ 13.39 hrs HW=93.98' (Free Discharge)
1=RCP Arch 122x78 (Barrel Controls 62.28 cfs @ 5.19 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=92.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 24P: Cultec Recharger 150XLHD

Inflow Area =	0.550 ac, 67.27% Impervious, Inflow De	epth > 1.95" for 2 YEAR event
Inflow =	1.44 cfs @ 12.03 hrs, Volume=	0.090 af
Outflow =	0.31 cfs @ 12.43 hrs, Volume=	0.089 af, Atten= 79%, Lag= 24.0 min
Primary =	0.31 cfs @ 12.43 hrs, Volume=	0.089 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 95.81' @ 12.43 hrs Surf.Area= 0.025 ac Storage= 0.028 af

Plug-Flow detention time= 43.6 min calculated for 0.089 af (99% of inflow) Center-of-Mass det. time= 39.0 min (813.2 - 774.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	94.00'	0.018 af	14.50'W x 74.50'L x 2.54'H Field A
			0.063 af Overall - 0.018 af Embedded = 0.045 af x 40.0% Voids
#2A	94.50'	0.018 af	Cultec R-150XLHD x 28 Inside #1
			Effective Size= 29.8"W x 18.0"H => 2.65 sf x 10.25'L = 27.2 cf
			Overall Size= 33.0"W x 18.5"H x 11.00'L with 0.75' Overlap
			Row Length Adjustment= +0.75' x 2.65 sf x 4 rows
#3	96.50'	0.001 af	4.00'D x 4.00'H Vertical Cone/Cylinder
		0.037 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	94.00'	18.0" Round Culvert
			L= 30.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 94.00' / 93.00' S= 0.0333 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	94.00'	3.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	96.50'	18.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	96.50'	4.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=0.31 cfs @ 12.43 hrs HW=95.81' (Free Discharge)

1=Culvert (Passes 0.31 cfs of 8.77 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.31 cfs @ 6.25 fps)

3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=94.00' (Free Discharge)
4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 51P: 54 ROOF DRIPLINE BMP'S

Inflow Area = 3.220 ac,100.00% Impervious, Inflow Depth > 2.68" for 2 YEAR event

Inflow = 7.24 cfs @ 12.21 hrs, Volume= 0.719 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 100.09' @ 20.00 hrs Surf.Area= 867,510 sf Storage= 31,305 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Storage	e Storage Description
#1	100.00'	13,187 c	f 3.00'W x 105.00'L x 2.00'H Prismatoid x 54
#2	100.00'	1,051 c	34,020 cf Overall - 1,051 cf Embedded = 32,969 cf x 40.0% Voids 6.0" Round Pipe Storage x 51 Inside #1 L= 105.0' S= 0.0050 '/'
		14,239 c	f x 51.00 = 726,182 cf Total Available Storage
Device	Routing	Invert Ou	utlet Devices
#1	Primary	He	0.0' long x 10.0' breadth Broad-Crested Rectangular Weir X 51.00 ead (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 pef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=100.00' (Free Discharge) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Subcatchment 1S:

Runoff = 90.59 cfs @ 12.81 hrs, Volume= 14.836 af, Depth> 2.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac) (CN D	escription		
*	43.	440	70 W	OODS / FIE	LD HSG C	
*	18.	400	98 E	XISTING IM	PERVIOUS	AREA
*	23.	400	74 E	XISTING LA	WN C	
*	0.	100	74 N	IEW LAWN (
	85.	340	77 W	Veighted Ave	rage	
	66.	940	78	8.44% Pervi	ous Area	
	18.400		2	1.56% Imper	vious Area	
	Tc	Length	Slop	pe Velocity	Capacity	Description
_	(min)	(feet)	(ft/	ft) (ft/sec)	(cfs)	
	28.8	100	0.040	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.040	0.50		Shallow Concentrated Flow, BC
						Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Total			

Summary for Subcatchment 2S:

Runoff = 77.76 cfs @ 12.71 hrs, Volume= 11.685 af, Depth> 2.09"

	Area	(ac)	CN	Desc	cription		
*	22.	010	70	WOO	DDS / FIEL	D HSG C	
*	13.	000	98	EXIS	STING IMP	ERVIOUS	AREA
*	30.	000	74	EXIS	STING LAV	VN C	
*	1.	850	74	NEW	/ LAWN C		
*	0.	000	98	NEV	/ IMPERV	IOUS BUIL	DING AREA (see 51S)
*	0.	130	98	New	Trails		
	66.	990	77	Weig	hted Aver	age	
	53.	860		80.4	0% Pervio	us Area	
	13.	130		19.6	0% Imperv	ious Area	
	Tc	Length		Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.	.0400	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	21.7	650	0.	.0400	0.50		Shallow Concentrated Flow, BC
_							Forest w/Heavy Litter Kv= 2.5 fps
	50.5	750) T	otal			

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Summary for Subcatchment 3S:

Runoff = 29.25 cfs @ 12.85 hrs, Volume= 4.910 af, Depth> 1.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac)	CN	Desc	cription		
*	31.	320	70	WOO	DDS / FIEL	D HSG C	
*	0.	000	98	EXIS	STING IMP	ERVIOUS	AREA
*	4.	000	74	EXIS	STING LAV	VN C	
*	0.	210	74	NEW	LAWN C		
*	0.	410	70	NEW	/ FILL SLC	PE	
*	0.	000	98	NEW	/ IMPERV	IOUS BUIL	DING AREA (See 51s)
*	0.	100	98	NEV	/ Trails		
	36.	040	71	Weig	ghted Aver	age	
	35.	940		99.7	2% Pervio	us Area	
	0.	100		0.28	% Impervi	ous Area	
	Тс	Length		Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.	0400	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	15.0	450	0.	0400	0.50		Shallow Concentrated Flow, BC
			_				Forest w/Heavy Litter Kv= 2.5 fps
	16.5	75	5 0.	0900	0.08		Sheet Flow,
_							Woods: Dense underbrush n= 0.800 P2= 3.10"
	60.3	625	5 To	otal			

Summary for Subcatchment 4S:

Runoff = 12.23 cfs @ 12.83 hrs, Volume= 2.009 af, Depth> 1.85"

	Area (ac)	CN	Description
*	5.000	70	WOODS / FIELD HSG C
*	1.000	98	EXISTING IMPERVIOUS AREA
*	7.000	74	EXISTING LAWN C
*	0.000	98	NEW IMPERVIOUS PAVED AREA
*	0.000	74	NEW LAWN C
	13.000	74	Weighted Average
	12.000		92.31% Pervious Area
	1.000		7.69% Impervious Area

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	Tc	Length	Slope	,		Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC
_						Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Total			

Summary for Subcatchment 5S: drains to 48" culvert

Runoff = 91.32 cfs @ 13.48 hrs, Volume= 22.409 af, Depth> 2.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac) C	N Des	cription			
*	47.	000	70 WO	ODS / FIEI	D HSG C		
*	36.	000	98 EXIS	STING IMF	PERVIOUS	AREA	
*	35.	000	74 EXIS	STING LAV	VN C		
	118.	000	80 Wei	ghted Aver	age		
	82.	000	69.4	69.49% Pervious Area			
	36.000		30.5	1% Imperv	ious Area		
	Tc	Length	Slope	Velocity	Capacity	Description	
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)		
	38.0	100	0.0200	0.04		Sheet Flow, AB	
						Woods: Dense underbrush n= 0.800 P2= 3.10"	
	60.0	900	0.0100	0.25		Shallow Concentrated Flow, BC	
						Forest w/Heavy Litter Kv= 2.5 fps	
	14.8	2,671	0.0400	3.00		Shallow Concentrated Flow, CD	
_						Grassed Waterway Kv= 15.0 fps	
	112.8	3,671	Total				

Summary for Subcatchment 6S: drains to 48" culvert

Runoff = 103.57 cfs @ 12.52 hrs, Volume= 13.387 af, Depth> 2.43"

	Area (ac)	CN	Description
*	6.000	70	WOODS / FIELD HSG C
*	20.000	98	EXISTING IMPERVIOUS AREA
*	40.000	74	EXISTING LAWN C
	66.000	81	Weighted Average
	46.000		69.70% Pervious Area
	20.000		30.30% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	28.8	100	0.0400	0.06		Sheet Flow, AB
	5.0	900	0.0400	3.00		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, BC Crossed Weterway, Kyz 15 0 fee
	3.7	2,500	0.0400	11.41	182.56	Grassed Waterway Kv= 15.0 fps Trap/Vee/Rect Channel Flow, CD Pet W=4.00', D=2.00', Z= 2.0 '/', Tep W=12.00'
_						Bot.W=4.00' D=2.00' Z= 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
	37.5	3 500	Total			

Summary for Subcatchment 7S:

Runoff = 34.68 cfs @ 12.12 hrs, Volume= 2.580 af, Depth> 2.81"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

_	Area	(ac) (CN E)esc	ription		
*	0.	000	70 V	VOC	DS / FIEL	D HSG C	
*	5.	000	98 E	EXIS	TING IMP	PERVIOUS	AREA
*	6.	000	74 E	XIS	TING LAV	VN C	
	11.	000	85 V	Veig	hted Aver	age	
	6.	000	5	4.55	% Pervio	us Area	
	5.	000	4	5.45	5% Imperv	vious Area	
_	Tc (min)	Length (feet)		pe /ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	7.5	100	0.04	00	0.22		Sheet Flow, AB
	1.1	200	0.04	00	3.00		Grass: Short n= 0.150 P2= 3.10" Shallow Concentrated Flow, BC Grassed Waterway Kv= 15.0 fps
	8.6	300	Tota	1		·	

Summary for Subcatchment 14S: 550 ROAD, 22' ROAD, 5' WALK to Forest Buffer

Runoff = 1.44 cfs @ 12.26 hrs, Volume= 0.149 af, Depth> 3.59"

	Area (ac)	CN	Description
*	0.400	98	NEW IMPERVIOUS PAVED AREA
*	0.100	74	NEW LAWN C
	0.500	93	Weighted Average
	0.100		20.00% Pervious Area
	0.400		80.00% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.2	11	0.0300	1.02		Sheet Flow, AB
	1.2	250	0.0300	3.52		Smooth surfaces n= 0.011 P2= 3.10" Shallow Concentrated Flow, BC
	40.0	7.5	0.0700	0.07		Paved Kv= 20.3 fps
	18.3	75	0.0700	0.07		Sheet Flow, Woods: Dense underbrush n= 0.800 P2= 3.10"
_	19 7	336	Total			

Summary for Subcatchment 15S: 600' ROAD, 22' ROAD, 5' WALK to Focal Points

Runoff = 2.39 cfs @ 12.02 hrs, Volume= 0.151 af, Depth> 3.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac) (ON Des	cription		
*	0.	370	98 NEV	V IMPERV	IOUS PAVI	ED AREA
*	0.	180	74 NEV	V LAWN C		
	0.	550	90 Wei	ghted Aver	age	
	0.	180	32.7	3% Pervio	us Area	
	0.	370	67.2	7% Imperv	ious Area	
	Тс	Length	•	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	0.2	11	0.0300	1.02		Sheet Flow, AB
						Smooth surfaces n= 0.011 P2= 3.10"
	1.2	250	0.0300	3.52		Shallow Concentrated Flow, BC
_						Paved Kv= 20.3 fps
	1.4	261	Total			

Summary for Subcatchment 16S: Arctic Fox Pond Watershed

Runoff = 4.99 cfs @ 12.80 hrs, Volume= 0.818 af, Depth> 2.33"

	Area (ac)	CN	Description
*	0.570	70	WOODS / FIELD HSG C
*	0.000	98	EXISTING IMPERVIOUS AREA
*	0.000	74	EXISTING LAWN C
*	1.100	98	NEW IMPERVIOUS PAVED AREA
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (see 51s)
*	2.540	74	NEW LAWN C
	4.210	80	Weighted Average
	3.110		73.87% Pervious Area
	1.100		26.13% Impervious Area

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	Tc	Length	Slope	,		Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC
_						Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Total			

Summary for Subcatchment 17S: Mallard Lane Pond Watershed

Runoff = 9.21 cfs @ 12.79 hrs, Volume= 1.513 af, Depth> 2.50"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area (ac) CN		Desc	cription						
*	0.	0.220 70 WO				_D HSG C				
*	0.	000	98	EXIS	STING IMF	PERVIOUS	AREA			
*	0.	000	74	EXIS	STING LAV	VN C				
*	2.	400	98	NEV	NEW IMPERVIOUS PAVED AREA					
*	0.	000	98	NEV	NEW IMPERVIOUS BUILDING AREA (see 51s)					
*	4.	640	74	NEV	V LAWN C					
	7.	260	82	Weig	ghted Aver	age				
	4.	860		66.9	4% Pervio	us Area				
	2.	400		33.0	6% Imperv	ious Area				
	Tc	Length	ı S	lope	Velocity	Capacity	Description			
	(min)	(feet))	(ft/ft)	(ft/sec)	(cfs)				
	28.8	100	0.0	0400	0.06		Sheet Flow, AB			
							Woods: Dense underbrush n= 0.800 P2= 3.10"			
	30.0	900	0.0	0400	0.50		Shallow Concentrated Flow, BC			
_							Forest w/Heavy Litter Kv= 2.5 fps			
	58.8	1,000	To	tal						

Summary for Subcatchment 18S:

Runoff = 1.07 cfs @ 12.72 hrs, Volume= 0.161 af, Depth> 1.71"

	Area (ac)	CN	Description
*	0.450	70	WOODS / FIELD HSG C
*	0.680	74	NEW LAWN C
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (see 51s)
	1.130	72	Weighted Average
	1.130		100.00% Pervious Area

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>
28.8	100	0.0400	0.06		Sheet Flow, AB
					Woods: Dense underbrush n= 0.800 P2= 3.10"
21.7	650	0.0400	0.50		Shallow Concentrated Flow, BC
					Forest w/Heavy Litter Kv= 2.5 fps
50.5	750	Total			

Summary for Subcatchment 19S:

Runoff = 26.82 cfs @ 12.14 hrs, Volume= 2.027 af, Depth> 1.74"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac)	CN	Desc	cription		
*	* 10.660 70			WOO	DDS / FIEL	D HSG C	
*	0.	600	98	EXIS	STING IMP	PERVIOUS	AREA
*	1.	600	74	EXIS	STING LAV	VN C	
*	0.	940	74	NEV	LAWN C		
*	0.	150	98	NEV	/ IMPERV	IOUS PAVI	ED AREA
*	0.	000	98	NEV	/ IMPERV	<u>IOUS BUIL</u>	DING AREA (See 51s)
	13.	950	72	Weig	ghted Aver	age	
	13.	200		94.6	2% Pervio	us Area	
	0.	750		5.38	% Impervio	ous Area	
	Tc	Length	ı S	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	7.5	100	0.0	0400	0.22		Sheet Flow, AB
							Grass: Short n= 0.150 P2= 3.10"
	1.7	300	0.0	0400	3.00		Shallow Concentrated Flow, BC
_							Grassed Waterway Kv= 15.0 fps
	9.2	400	To	otal			

Summary for Subcatchment 20S:

Runoff = 6.33 cfs @ 12.52 hrs, Volume= 0.806 af, Depth> 1.58"

	Area (ac)	CN	Description
*	5.820	70	WOODS / FIELD HSG C
*	0.000	98	EXISTING IMPERVIOUS AREA
*	0.000	74	EXISTING LAWN C
*	0.290	74	NEW LAWN C
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (See 51s)
	6.110	70	Weighted Average
	6.110		100.00% Pervious Area

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>
28.8	100	0.0400	0.06		Sheet Flow, AB
					Woods: Dense underbrush n= 0.800 P2= 3.10"
6.7	200	0.0400	0.50		Shallow Concentrated Flow, BC
					Forest w/Heavy Litter Kv= 2.5 fps
35.5	300	Total			

Summary for Subcatchment 51S: NEW Cottage Roof Areas

Runoff = 10.82 cfs @ 12.21 hrs, Volume= 1.087 af, Depth> 4.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 10 YEAR Rainfall=4.60"

	Area	(ac) C	N Desc	cription		
*	3.	220 9	98 52 C	ottage Ro	ofs + Comr	nunity Buildings
	3.220 100.00% Impervious Area					l
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.1	20	0.4000	3.25		Sheet Flow, AB
	2.5	25	0.0400	0.17		Smooth surfaces n= 0.011 P2= 3.10" Sheet Flow, BC
	2.5	25	0.0400	0.17		Grass: Short n= 0.150 P2= 3.10"
	13.1	75	0.1600	0.10		Sheet Flow, CD
_						Woods: Dense underbrush n= 0.800 P2= 3.10"
	15.7	120	Total			

Summary for Reach 3R: Stream @ Property Line

Inflow Area = 111.340 ac, 22.38% Impervious, Inflow Depth > 1.95" for 10 YEAR event

Inflow = 95.74 cfs @ 12.90 hrs, Volume= 18.084 af

Outflow = 95.42 cfs @ 12.99 hrs, Volume= 17.974 af, Atten= 0%, Lag= 5.4 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.49 fps, Min. Travel Time= 3.2 min Avg. Velocity = 1.70 fps, Avg. Travel Time= 8.4 min

Peak Storage= 18,298 cf @ 12.94 hrs Average Depth at Peak Storage= 1.57'

Bank-Full Depth= 3.00' Flow Area= 45.0 sf, Capacity= 287.21 cfs

12.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 1.0 '/' Top Width= 18.00' Length= 860.0' Slope= 0.0058 '/'

Inlet Invert= 77.00', Outlet Invert= 72.00'

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Summary for Reach 4R: Stream below RR crossing

Inflow Area = 96.890 ac, 24.53% Impervious, Inflow Depth > 1.98" for 10 YEAR event

Inflow = 91.80 cfs @ 12.83 hrs, Volume= 15.992 af

Outflow = 91.53 cfs @ 12.91 hrs, Volume= 15.908 af, Atten= 0%, Lag= 5.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.95 fps, Min. Travel Time= 2.9 min Avg. Velocity = 2.02 fps, Avg. Travel Time= 7.1 min

Peak Storage= 15,917 cf @ 12.86 hrs Average Depth at Peak Storage= 2.24'

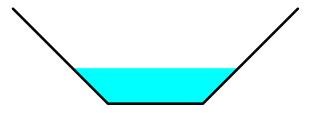
Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 582.42 cfs

6.00' x 6.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 860.0' Slope= 0.0058 '/'

Inlet Invert= 82.00', Outlet Invert= 77.00'



Summary for Reach 6R: Stream below Site @ PL

Inflow Area = 272.920 ac, 27.79% Impervious, Inflow Depth > 2.13" for 10 YEAR event

Inflow = 180.46 cfs @ 12.90 hrs, Volume= 48.484 af

Outflow = 180.21 cfs @ 12.94 hrs, Volume= 48.392 af, Atten= 0%, Lag= 2.2 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity = 6.13 fps, Min. Travel Time = 1.2 min Avg. Velocity = 3.48 fps, Avg. Travel Time = 2.2 min

Peak Storage= 13,236 cf @ 12.91 hrs Average Depth at Peak Storage= 2.74'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 538.97 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 61.00', Outlet Invert= 58.00'

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Summary for Reach 7R: Stream Through Site

Inflow Area = 257.100 ac, 26.89% Impervious, Inflow Depth > 2.20" for 10 YEAR event

Inflow = 179.35 cfs @ 12.84 hrs, Volume= 47.101 af

Outflow = 178.99 cfs @ 12.89 hrs, Volume= 46.963 af, Atten= 0%, Lag= 3.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 9.67 fps, Min. Travel Time= 1.9 min Avg. Velocity = 5.31 fps, Avg. Travel Time= 3.5 min

Peak Storage= 20,372 cf @ 12.86 hrs Average Depth at Peak Storage= 1.88'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 683.45 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,100.0' Slope= 0.0245 '/'

Inlet Invert= 88.00', Outlet Invert= 61.00'



Summary for Reach 14R: Swale from School and Neighborhood

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 1.26" for 10 YEAR event

Inflow = 1.70 cfs @ 15.15 hrs, Volume= 1.156 af

Outflow = 1.70 cfs @ 16.05 hrs, Volume= 1.014 af, Atten= 0%, Lag= 53.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity = 1.75 fps, Min. Travel Time = 32.1 min Avg. Velocity = 1.27 fps, Avg. Travel Time = 44.3 min

Peak Storage= 3,268 cf @ 15.51 hrs

Average Depth at Peak Storage= 0.23'

Bank-Full Depth= 3.00' Flow Area= 21.0 sf, Capacity= 147.12 cfs

4.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 10.00'

Length= 3,366.0' Slope= 0.0100 '/'

Inlet Invert= 117.66', Outlet Invert= 84.00'

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Summary for Reach 17R:

Inflow Area = 8.390 ac, 28.61% Impervious, Inflow Depth > 1.58" for 10 YEAR event

Inflow = 6.44 cfs @ 13.33 hrs, Volume= 1.102 af

Outflow = 6.41 cfs @ 13.40 hrs, Volume= 1.094 af, Atten= 0%, Lag= 3.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 5.32 fps, Min. Travel Time= 2.2 min Avg. Velocity = 2.69 fps, Avg. Travel Time= 4.3 min

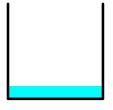
Peak Storage= 846 cf @ 13.36 hrs Average Depth at Peak Storage= 0.40'

Bank-Full Depth= 3.00' Flow Area= 9.0 sf, Capacity= 102.76 cfs

3.00' x 3.00' deep channel, n= 0.022 Earth, clean & straight

Length= 700.0' Slope= 0.0286 '/'

Inlet Invert= 81.00', Outlet Invert= 61.00'



Summary for Reach 18R: Stream Through Site

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 2.28" for 10 YEAR event

Inflow = 137.41 cfs @ 12.64 hrs, Volume= 35.006 af

Outflow = 137.06 cfs @ 12.71 hrs, Volume= 34.868 af, Atten= 0%, Lag= 4.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.79 fps, Min. Travel Time= 2.6 min Avg. Velocity = 3.99 fps, Avg. Travel Time= 5.0 min

Avg. velocity = 3.99 lps, Avg. Havei Time= 5

Peak Storage= 21,119 cf @ 12.67 hrs Average Depth at Peak Storage= 1.80'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 563.18 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,200.0' Slope= 0.0167 '/'

Inlet Invert= 125.00', Outlet Invert= 105.00'

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Summary for Reach 55R: Wetland below Site @ PL

Inflow Area = 36.040 ac, 0.28% Impervious, Inflow Depth > 1.63" for 10 YEAR event

Inflow = 29.25 cfs @ 12.85 hrs, Volume= 4.910 af

Outflow = 29.20 cfs @ 12.91 hrs, Volume= 4.890 af, Atten= 0%, Lag= 3.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 3.47 fps, Min. Travel Time= 2.2 min Avg. Velocity = 1.68 fps, Avg. Travel Time= 4.5 min

Peak Storage= 3,793 cf @ 12.87 hrs Average Depth at Peak Storage= 0.94'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 540.76 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 63.02', Outlet Invert= 60.00'



Summary for Pond 1P: 1-30" and 1-24" Culvert at Tuttle Road

Inflow Area = 111.340 ac, 22.38% Impervious, Inflow Depth > 1.91" for 10 YEAR event

Inflow = 90.43 cfs @ 13.15 hrs, Volume= 17.733 af

Outflow = 90.39 cfs @ 13.16 hrs, Volume= 17.704 af, Atten= 0%, Lag= 0.9 min

Primary = 58.61 cfs @ 13.16 hrs, Volume= 16.092 af Secondary = 31.78 cfs @ 13.16 hrs, Volume= 1.612 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 71.38' @ 13.16 hrs Surf.Area= 7,119 sf Storage= 18,233 cf

Plug-Flow detention time= 3.6 min calculated for 17.704 af (100% of inflow) Center-of-Mass det. time= 3.0 min (870.8 - 867.7)

Volume	Invert	Avail.Storage	Storage Description
#1	68.00'	31,683 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)				
68.0	00	3,850	0	0				
70.0	00	5,600	9,450	9,450				
72.0	00	7,800	13,400	22,850				
73.0	00	9,865	8,833	31,683				
Device	Routing	Invert	Outlet Devices					
#1	Primary	67.50'	30.0" Round C	ulvert				
,		L= 50.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf						
#2 Primary		67.50'	24.0" Round C	ulvert				
			L= 50.0' CPP, projecting, no headwall, Ke= 0.900					
			Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.9					
116		-,	•		or, Flow Area= 3.14 sf			
#3	Seconda	ry 71.00'			road-Crested Rectangular Weir			
			Head (feet) 0.2	U U.4U 0.60 I	0.80 1.00 1.20 1.40 1.60			

Primary OutFlow Max=58.60 cfs @ 13.16 hrs HW=71.38' (Free Discharge)

-1=Culvert (Inlet Controls 38.33 cfs @ 7.81 fps)

-2=Culvert (Inlet Controls 20.27 cfs @ 6.45 fps)

Secondary OutFlow Max=31.64 cfs @ 13.16 hrs HW=71.38' (Free Discharge) -3=Broad-Crested Rectangular Weir (Weir Controls 31.64 cfs @ 1.66 fps)

Summary for Pond 2P: Two 30" Culverts at Crossing Brook Road

Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.63

Inflow Area =	272.920 ac, 27.79% Impervious, Inflo	w Depth > 2.13" for 10 YEAR event
Inflow =	180.21 cfs @ 12.94 hrs, Volume=	48.392 af
Outflow =	88.83 cfs @ 15.03 hrs, Volume=	44.518 af, Atten= 51%, Lag= 125.9 min
Primary =	88.83 cfs @ 15.03 hrs, Volume=	44.518 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 51.40' @ 15.03 hrs Surf.Area= 148,024 sf Storage= 727,780 cf

Plug-Flow detention time= 106.3 min calculated for 44.370 af (92% of inflow) Center-of-Mass det. time= 84.2 min (961.5 - 877.3)

Volume	Invert	Avail.Storage	Storage Description
#1	44.00'	2,030,000 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
44.00	60,000	0	0
46.00	80,000	140,000	140,000
48.00	100,000	180,000	320,000
50.00	120,000	220,000	540,000
52.00	160,000	280,000	820,000
54.00	180,000	340,000	1,160,000
56.00	220,000	400,000	1,560,000
58.00	250,000	470,000	2,030,000

Device	Routing	Invert	Outlet Devices
#1	Primary	44.00'	30.0" Round Culvert
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 44.00' / 42.00' S= 0.0400 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf
#2	Primary	44.00'	24.0" Round Culvert
			L= 50.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 44.00' / 42.00' S= 0.0400 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
#3	Secondary	56.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=88.83 cfs @ 15.03 hrs HW=51.40' (Free Discharge)

1=Culvert (Inlet Controls 58.62 cfs @ 11.94 fps)

2=Culvert (Inlet Controls 30.21 cfs @ 9.62 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=44.00' (Free Discharge) 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 3P: 24" CULVERT

Inflow Area =	36.040 ac,	0.28% Impervious, Inflow D	Depth > 1.63" for 10 YEAR event
Inflow =	29.20 cfs @	12.91 hrs, Volume=	4.890 af
Outflow =	24.24 cfs @	13.21 hrs, Volume=	4.852 af, Atten= 17%, Lag= 18.2 min
Primary =	24.24 cfs @	13.21 hrs, Volume=	4.852 af
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 57.57' @ 13.21 hrs Surf.Area= 9,350 sf Storage= 22,161 cf

Plug-Flow detention time= 12.5 min calculated for 4.852 af (99% of inflow) Center-of-Mass det. time= 9.9 min (864.4 - 854.6)

Volume	Invert	Avail.Storage	Storage Description
#1	54.00'	56.342 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation		Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
54.0	00	2,362	0	0	
56.0	00	6,990	9,352	9,352	
58.0	00	10,000	16,990	26,342	
60.0	00	20,000	30,000	56,342	
Device	Routing	Invert	Outlet Devices		
#1	Primary	54.00'	24.0" Round C	Culvert	
	-		L= 50.0' RCP,	sq.cut end pro	ojecting, Ke= 0.500
			Inlet / Outlet Inv	/ert= 54.00' / 5	3.00' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Conc	rete pipe, strai	ight & clean, Flow Area= 3.14 sf
#2	Seconda	ry 59.00'	25.0' long x 25	5.0' breadth B	road-Crested Rectangular Weir
			Head (feet) 0.2	0.40 0.60	0.80 1.00 1.20 1.40 1.60

Primary OutFlow Max=24.23 cfs @ 13.21 hrs HW=57.57' (Free Discharge) 1=Culvert (Inlet Controls 24.23 cfs @ 7.71 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=54.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 4P: 18" CULVERT

Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Inflow Area =	13.000 ac,	7.69% Impervious, Inflow I	Depth > 1.85" for 10 YEAR event
Inflow =	12.23 cfs @	12.83 hrs, Volume=	2.009 af
Outflow =	8.95 cfs @	13.22 hrs, Volume=	1.973 af, Atten= 27%, Lag= 23.6 min
Primary =	8.95 cfs @	13.22 hrs, Volume=	1.973 af
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 86.86' @ 13.22 hrs Surf.Area= 13,049 sf Storage= 15,074 cf

Plug-Flow detention time= 26.6 min calculated for 1.973 af (98% of inflow) Center-of-Mass det. time= 20.5 min (864.1 - 843.6)

Volume	Inver	t Avail.Sto	rage Storag	e Description	
#1	85.00)' 82,7	55 cf Custo	m Stage Data (Prismatio)Listed below (Recalc)
Elevatio	-	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.0	00	3,343	0	0	
86.0	00	8,410	5,877	5,877	
88.0	00	19,234	27,644	33,521	
90.0	00	30,000	49,234	82,755	
Device	Routing	Invert	Outlet Devi	es	
#1	Primary	85.00'	18.0" Rou	nd Culvert	
				CP, sq.cut end projecting,	
				Invert= 85.00' / 84.00' S	
40	0			oncrete pipe, straight & cl	
#2	Secondar	y 89.00'	25.0 long	k 25.0' breadth Broad-Cr	ested Rectangular Weir

Volume

Invert

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Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.63

Primary OutFlow Max=8.95 cfs @ 13.22 hrs HW=86.86' (Free Discharge)
1=Culvert (Inlet Controls 8.95 cfs @ 5.06 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=85.00' (Free Discharge)

2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 5P: 4'x3' Oval and 30" Overflow Culvert

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 2.33" for 10 YEAR event Inflow = 137.73 cfs @ 12.61 hrs, Volume= 35.796 af

Outflow = 137.41 cfs @ 12.64 hrs, Volume= 35.006 af, Atten= 0%, Lag= 1.8 min 40.18 cfs @ 12.64 hrs, Volume= 20.895 af

Secondary = 97.23 cfs @ 12.64 hrs, Volume= 14.111 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 137.72' @ 12.64 hrs Surf.Area= 19,152 sf Storage= 92,199 cf

Plug-Flow detention time= 22.3 min calculated for 34.889 af (97% of inflow) Center-of-Mass det. time= 15.2 min (865.6 - 850.5)

Avail Storage Storage Description

volunie	IIIVEIL	Avaii.Siu	rage Storage	Description	
#1	129.00'	142,73	35 cf Custom	Stage Data (Pr	ismatic)Listed below (Recalc)
Elevation		urf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
129.0	00	4,441	0	0	
130.0	00	6,196	5,319	5,319	
132.0	00	8,225	14,421	19,740	
134.0	00	10,880	19,105	38,845	
136.0	00	14,005	24,885	63,730	
138.0	00	20,000	34,005	97,735	
140.0	00	25,000	45,000	142,735	
Device	Routing	Invert	Outlet Devices	S	
#1	Primary	129.00'	4.0" W x 3.0"	H, R=3.0" Ellip	tical Culvert
	,				jecting, Ke= 0.500
			Inlet / Outlet In	nvert= 129.00' / 3	128.00' S= 0.0333 '/' Cc= 0.900
			n= 0.011 Cor	ncrete pipe, straig	ght & clean, Flow Area= 0.07 sf
#2	Primary	132.00'	30.0" Round	Culvert	
	•		L= 50.0' CPF	P, projecting, no	headwall, Ke= 0.900
			Inlet / Outlet I	nvert= 132.00' / '	128.00' S= 0.0800 '/' Cc= 0.900
			n= 0.010 PV0	C, smooth interio	r, Flow Area= 4.91 sf
#3	Secondary	137.00'	60.0' long x	30.0' breadth Br	oad-Crested Rectangular Weir
	•				0.80 1.00 1.20 1.40 1.60
			Coef. (English	n) 2.68 2.70 2.7	70 2.64 2.63 2.64 2.64 2.63

Volume

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Primary OutFlow Max=40.17 cfs @ 12.64 hrs HW=137.72' (Free Discharge)

1=Culvert (Barrel Controls 0.74 cfs @ 10.99 fps)
2=Culvert (Inlet Controls 39.44 cfs @ 8.03 fps)

Secondary OutFlow Max=96.98 cfs @ 12.64 hrs HW=137.72' (Free Discharge)

3=Broad-Crested Rectangular Weir (Weir Controls 96.98 cfs @ 2.26 fps)

Summary for Pond 6P: 1-48" Culvert Crossing Golf Cart Path

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 2.27" for 10 YEAR event
Inflow = 137.06 cfs @ 12.71 hrs, Volume= 34.868 af
Outflow = 115.80 cfs @ 13.58 hrs, Volume= 34.715 af, Atten= 16%, Lag= 51.8 min

Primary = 115.80 cfs @ 13.58 hrs, Volume= 34.715 af Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 101.66' @ 13.58 hrs Surf.Area= 38,314 sf Storage= 117,247 cf

Avail Storage Storage Description

Plug-Flow detention time= 12.5 min calculated for 34.599 af (99% of inflow)

Center-of-Mass det. time= 11.1 min (881.4 - 870.3)

Invert

#1 96.00' 280,448 cf Custom Stage Data (Prismatic)Listed below (R Elevation (feet) Surf.Area Inc.Store (cubic-feet) (cubic-feet) 96.00 1,580 0 0 98.00 14,434 16,014 16,014 100.00 30,000 44,434 60,448 102.00 40,000 70,000 130,448 105.00 60,000 150,000 280,448	VOIGITIC	IIIVCIL	Avail.C	norage	Otorage	Description			
(feet) (sq-ft) (cubic-feet) (cubic-feet) 96.00 1,580 0 0 98.00 14,434 16,014 16,014 100.00 30,000 44,434 60,448 102.00 40,000 70,000 130,448	#1	96.00'	280	,448 cf	Custon	n Stage Data (Pi	ismatic) Liste	ed below (F	Recalc)
96.00 1,580 0 0 98.00 14,434 16,014 16,014 100.00 30,000 44,434 60,448 102.00 40,000 70,000 130,448									
100.00 30,000 44,434 60,448 102.00 40,000 70,000 130,448		,) dabo	<u> </u>	0			
102.00 40,000 70,000 130,448			,		,	- / -			
105.00 60,000 150,000 280,448	102.00	40	0,000	7	0,000	130,448			
	105.00	60	0,000	15	0,000	280,448			

Device	Routing	Invert	Outlet Devices
#1	Primary	96.00'	48.0" Round Culvert
	•		L= 30.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 96.00' / 95.00' S= 0.0333 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 12.57 sf
#2	Secondary	103.00'	20.0' long x 20.0' breadth Broad-Crested Rectangular Weir
	•		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=115.79 cfs @ 13.58 hrs HW=101.66' (Free Discharge)
1=Culvert (Inlet Controls 115.79 cfs @ 9.21 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=96.00' (Free Discharge)
2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Pond 7P: 1-24" Culvert at Greely Middle School

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 2.81" for 10 YEAR event

Inflow = 34.68 cfs @ 12.12 hrs, Volume= 2.580 af

Outflow = 1.70 cfs @ 15.15 hrs, Volume= 1.156 af, Atten= 95%, Lag= 181.6 min

Primary = $1.70 \text{ cfs } \boxed{0}$ 15.15 hrs, Volume= 1.156 af Secondary = $0.00 \text{ cfs } \boxed{0}$ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 123.47' @ 15.15 hrs Surf.Area= 24,239 sf Storage= 74,205 cf

Peak Elev= 123.47 @ 15.15 fils Sun.Area= 24,239 St Storage= 74,205 C

Plug-Flow detention time= 249.6 min calculated for 1.156 af (45% of inflow) Center-of-Mass det. time= 162.9 min (942.8 - 780.0)

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	214,248 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	18,593	0	0
122.00	21,745	40,338	40,338
124.00	25,131	46,876	87,214
126.00	32,605	57,736	144,950
128.00	36,693	69,298	214,248

<u>Device</u>	Routing	Invert	Outlet Devices
#1	Primary	120.00'	24.0" Round Culvert L= 80.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 120.00' / 119.00' S= 0.0125 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Secondary	127.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63
#3	Device 1	120.00'	6.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	126.00'	24.0" Horiz. Orifice/Grate C= 0.600 Limited to weir flow at low heads

Primary OutFlow Max=1.70 cfs @ 15.15 hrs HW=123.47' (Free Discharge)

1=Culvert (Passes 1.70 cfs of 23.79 cfs potential flow)

3=Orifice/Grate (Orifice Controls 1.70 cfs @ 8.64 fps)

-4=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=120.00' (Free Discharge)

2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 10P: 1-30" Culvert

Inflow Area =	111.340 ac, 22.38% Impervious, Inflow	Depth > 1.94"	for 10 YEAR event
Inflow =	95.42 cfs @ 12.99 hrs, Volume=	17.974 af	
Outflow =	90.43 cfs @ 13.15 hrs, Volume=	17.733 af, Atte	en= 5%, Lag= 9.4 min
Primary =	38.16 cfs @ 13.15 hrs, Volume=	13.705 af	
Secondary =	52.27 cfs @ 13.15 hrs, Volume=	4.028 af	

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 71.86' @ 13.15 hrs Surf.Area= 52,533 sf Storage= 84,592 cf

Plug-Flow detention time= 19.8 min calculated for 17.674 af (98% of inflow)

Center-of-Mass det. time= 15.3 min (867.7 - 852.4)

Volume	Inve	rt Avail.Sto	rage	Storage	Description	
#1	68.0	0' 211,04	48 cf	Custom	Stage Data (Pi	rismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)	
68.0		8,000	(Cabi	0	0	
70.0 72.0	00	14,434 55,480		22,434 89,914	22,434 92,348	
74.0		63,220		18,700	211,048	
Device	Routing	Invert	Outl	et Device	S	
#1	Primary	68.00'	30.0	" Round	Culvert	
#2	Secondar	y 71.00'	Inlet n= 0 25.0 Hea	/ Outlet In .011 Cor ' long x 2 d (feet) 0	nvert= 68.00' / 6 ncrete pipe, strai 25.0' breadth B .20 0.40 0.60	ojecting, Ke= 0.500 7.00' S= 0.0333 '/' Cc= 0.900 ight & clean, Flow Area= 4.91 sf road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=38.16 cfs @ 13.15 hrs HW=71.86' (Free Discharge) 1=Culvert (Inlet Controls 38.16 cfs @ 7.77 fps)

Secondary OutFlow Max=52.24 cfs @ 13.15 hrs HW=71.86' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 52.24 cfs @ 2.44 fps)

Summary for Pond 15P: FocalPoint 60sf

Inflow Area =	0.550 ac, 67.27% Impervious, Inflow I	Depth > 3.30" for 10 YEAR event
Inflow =	2.39 cfs @ 12.02 hrs, Volume=	0.151 af
Outflow =	2.38 cfs @ 12.03 hrs, Volume=	0.151 af, Atten= 0%, Lag= 0.4 min
Primary =	0.14 cfs @ 11.10 hrs, Volume=	0.084 af
Secondary =	2.24 cfs @ 12.03 hrs, Volume=	0.067 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 100.78' @ 12.03 hrs Surf.Area= 60 sf Storage= 125 cf

Plug-Flow detention time= 2.4 min calculated for 0.151 af (100% of inflow) Center-of-Mass det. time= 2.4 min (761.9 - 759.5)

Volume	Invert	Avail.Storage	Storage Description
#1	97.75'	27 cf	3.00'W x 20.00'L x 2.25'H FocalPoint
			135 cf Overall x 20.0% Voids
#2	100.00'	133 cf	Custom Stage Data (Prismatic)Listed below (Recalc) -Impervious
		160 cf	Total Available Storage

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
100.00	60	0	0
100.50	157	54	54
101.00	157	79	133

Device	Routing	Invert	Outlet Devices	
#1	Primary	97.75'	100.000 in/hr Exfiltration over Surface area	Phase-In= 0.10'
#2	Secondary	100.50'	18.0" Horiz. Orifice/Grate C= 0.600	
	•		Limited to weir flow at low heads	

Primary OutFlow Max=0.14 cfs @ 11.10 hrs HW=97.90' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.14 cfs)

Secondary OutFlow Max=2.14 cfs @ 12.03 hrs HW=100.77' (Free Discharge) 2=Orifice/Grate (Weir Controls 2.14 cfs @ 1.69 fps)

Summary for Pond 16P: Arctic Fox WET POND

Inflow Area =	4.210 ac, 26.13% Impervious, Inflow D	epth > 2.33" for 10 YEAR event
Inflow =	4.99 cfs @ 12.80 hrs, Volume=	0.818 af
Outflow =	0.87 cfs @ 14.84 hrs, Volume=	0.426 af, Atten= 83%, Lag= 122.2 min
Primary =	0.87 cfs @ 14.84 hrs, Volume=	0.426 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 77.00' Surf.Area= 4,505 sf Storage= 18,632 cf Peak Elev= 79.60' @ 14.84 hrs Surf.Area= 10,110 sf Storage= 41,095 cf (22,463 cf above start)

Plug-Flow detention time= (not calculated: initial storage exceeds outflow) Center-of-Mass det. time= 149.0 min (980.4 - 831.5)

Volume	Invert	Avail.Storage	Storage Description	
#1	71.00'	82,315 cf	Custom Stage Data (Prismatic)Listed below (Recalc)	
Elevation (feet)	Surf.Aı (sq		nc.Store Cum.Store pic-feet) (cubic-feet)	

Suii.Aiea	1110.51016	Culli.Sible
(sq-ft)	(cubic-feet)	(cubic-feet)
1,852	0	0
2,232	2,042	2,042
2,636	2,434	4,476
3,065	2,851	7,327
3,520	3,293	10,619
4,000	3,760	14,379
4,505	4,253	18,632
7,408	596	19,227
8,400	7,114	26,341
9,450	8,925	35,266
10,557	10,004	45,269
11,720	11,139	56,408
12,940	12,330	68,738
14,215	13,578	82,315
	(sq-ft) 1,852 2,232 2,636 3,065 3,520 4,000 4,505 7,408 8,400 9,450 10,557 11,720 12,940	(sq-ft) (cubic-feet) 1,852 0 2,232 2,042 2,636 2,434 3,065 2,851 3,520 3,293 4,000 3,760 4,505 4,253 7,408 596 8,400 7,114 9,450 8,925 10,557 10,004 11,720 11,139 12,940 12,330

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Device	Routing	Invert	Outlet Devices				
#1	Primary	74.00'	18.0" Round Culvert				
			L= 58.0' RCP, square edge headwall, Ke= 0.500				
			Inlet / Outlet Invert= 74.00' / 70.00' S= 0.0690 '/' Cc= 0.900				
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf				
#2	Device 1	78.50'	6.0" Vert. Orifice/Grate C= 0.600				
#3	Device 1	81.00'	48.0" Horiz. Orifice/Grate C= 0.600				
			Limited to weir flow at low heads				
#4	Secondary	81.50'	10.0' long x 10.0' breadth Broad-Crested Rectangular Weir				
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60				
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64				

Primary OutFlow Max=0.87 cfs @ 14.84 hrs HW=79.60' (Free Discharge)

1=Culvert (Passes 0.87 cfs of 18.73 cfs potential flow)

-2=Orifice/Grate (Orifice Controls 0.87 cfs @ 4.43 fps)

3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=77.00' (Free Discharge)

4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 17P: Mallard Way WET POND

Inflow Area =	7.260 ac, 33.06% Impervious, Inflow De	epth > 2.50" for 10 YEAR event
Inflow =	9.21 cfs @ 12.79 hrs, Volume=	1.513 af
Outflow =	5.98 cfs @ 13.28 hrs, Volume=	0.948 af, Atten= 35%, Lag= 29.3 min
Primary =	5.98 cfs @ 13.28 hrs, Volume=	0.948 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 88.00' Surf.Area= 5,558 sf Storage= 23,438 cf

Peak Elev= 90.74' @ 13.28 hrs Surf.Area= 12,902 sf Storage= 53,590 cf (30,152 cf above start)

Plug-Flow detention time= 303.7 min calculated for 0.410 af (27% of inflow) Center-of-Mass det. time= 82.8 min (909.8 - 827.1)

Volume	Invert	Avail.Storage	Storage Description
#1	81.00'	70,904 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
81.00	1,346	0	0
82.00	1,867	1,607	1,607
83.00	2,419	2,143	3,750
84.00	2,996	2,708	6,457
85.00	3,599	3,298	9,755
86.00	4,226	3,913	13,667
87.00	4,879	4,553	18,220
88.00	5,558	5,219	23,438
88.10	9,325	744	24,182
89.00	10,578	8,956	33,139
90.00	11,887	11,233	44,371
91.00	13,252	12,570	56,941
92.00	14,675	13,964	70,904

Device	Routing	Invert	Outlet Devices
#1	Primary	86.00'	18.0" Round Culvert L= 31.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 86.00' / 85.50' S= 0.0161 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	89.50'	6.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	90.50'	48.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	91.00'	10.0' long x 10.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=5.87 cfs @ 13.28 hrs HW=90.74' (Free Discharge)

-1=Culvert (Passes 5.87 cfs of 17.00 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.94 cfs @ 4.80 fps)
3=Orifice/Grate (Weir Controls 4.93 cfs @ 1.61 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=88.00' (Free Discharge)

4=Broad-Crested Rectangular Wair (Controls 0.00 afc) -4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 18P: 24" CULVERT

Inflow Area	=	8.390 ac, 2	28.61% Imp	ervious,	Inflow	Depth >	1.59"	for 10	YEAR event
Inflow =	=	6.58 cfs @	13.27 hrs,	Volume	=	1.109 a	af		
Outflow =	=	6.44 cfs @	13.33 hrs,	Volume	=	1.102 a	af, Att	en= 2%,	Lag= 4.0 min
Primary =	=	6.44 cfs @	13.33 hrs,	Volume	=	1.102 a	af		

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 86.14' @ 13.33 hrs Surf.Area= 1,850 sf Storage= 1,388 cf

Plug-Flow detention time= 5.0 min calculated for 1.102 af (99% of inflow) Center-of-Mass det. time= 3.1 min (902.9 - 899.8)

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Volume	Inv	ert Avail.Sto	rage Storage	e Description	
#1	85.	00' 15,8	69 cf Custor	n Stage Data (Prismatic)List	ed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.0	00	788	0	0	
86.0	00	1,512	1,150	1,150	
87.0	00	3,898	2,705	3,855	
88.0	00	5,621	4,760	8,615	
89.0	00	8,888	7,255	15,869	
Device	Routing	Invert	Outlet Devic	es	
#1	Primary	85.00'	24.0" Roun	d Culvert	
			Inlet / Outlet	P, sq.cut end projecting, Ke- Invert= 85.00' / 84.50' S= 0.0 ncrete pipe, straight & clean,	0100 '/' Cc= 0.900

Primary OutFlow Max=6.42 cfs @ 13.33 hrs HW=86.14' (Free Discharge) 1=Culvert (Barrel Controls 6.42 cfs @ 5.01 fps)

Summary for Pond 20P: Arch Culvert 1

Inflow Area =	96.890 ac, 24.53%	Impervious, Inflow	Depth > 1.98"	for 10 YEAR event
Inflow =	91.80 cfs @ 12.81	hrs, Volume=	16.001 af	
Outflow =	91.80 cfs @ 12.83	hrs, Volume=	15.992 af, Att	en= 0%, Lag= 0.6 min
Primary =	91.80 cfs @ 12.83	hrs, Volume=	15.992 af	_
Secondary =	0.00 cfs @ 5.00	hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 85.05' @ 12.83 hrs Surf.Area= 2,314 sf Storage= 4,023 cf

Plug-Flow detention time= 0.8 min calculated for 15.939 af (100% of inflow) Center-of-Mass det. time= 0.6 min (846.7 - 846.1)

Volume	Inv	ert Avai	I.Storage	Storage D	escription	
#1	82.	00'	85,094 cf	Custom S	Stage Data (Pr	rismatic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)	
82.0	00	320		0	0	
86.0	00	2,932		6,504	6,504	
87.0	00	7,643		5,288	11,792	
88.0	00	11,989		9,816	21,608	
89.0	00	18,865	1	5,427	37,035	
90.0	00	23,627	2	1,246	58,281	
91.0	00	30,000	2	6,814	85,094	
Device	Routing	In	vert Outle	et Devices		
#1	Primary	82			•	26.0" Pipe Arch RCP_Arch 88x54
			L= 7	0.0' RCP.	end-section c	onforming to fill, Ke= 0.500

Inlet / Outlet Invert= 82.00' / 81.50' S= 0.0071 '/' Cc= 0.900

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n= 0.022 Earth, clean & straight, Flow Area= 25.69 sf #2 Secondary 90.00' **25.0' long x 25.0' breadth Broad-Crested Rectangul**

25.0' long x 25.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60

Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=91.68 cfs @ 12.83 hrs HW=85.05' (Free Discharge) 1=RCP Arch 88x54 (Barrel Controls 91.68 cfs @ 6.19 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=82.00' (Free Discharge)

2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 21P: Arch Culvert 2

Inflow Area = 190.110 ac, 29.46% Impervious, Inflow Depth > 2.24" for 10 YEAR event

Inflow = 117.28 cfs @ 13.54 hrs, Volume= 35.520 af

Outflow = 117.26 cfs @ 13.58 hrs, Volume= 35.416 af, Atten= 0%, Lag= 2.0 min

Primary = 117.26 cfs @ 13.58 hrs, Volume= 35.416 af Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 94.90' @ 13.58 hrs Surf.Area= 8,247 sf Storage= 18,840 cf

Plug-Flow detention time= 3.3 min calculated for 35.416 af (100% of inflow)

Center-of-Mass det. time= 2.4 min (882.7 - 880.3)

Volume	Invert	Avail.Storage	Storage Description
#1	92.00'	200,953 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
92.00	5,000	0	0
93.00	6,000	5,500	5,500
94.00	7,000	6,500	12,000
95.00	8,390	7,695	19,695
96.00	12,267	10,329	30,024
97.00	23,771	18,019	48,043
98.00	31,886	27,829	75,871
99.00	67,139	49,513	125,384
100.00	84,000	75,570	200,953

Device	Routing	Invert	Outlet Devices
#1	Primary	92.00'	122.0" W x 77.3" H, R=62.0"/218.0" Pipe Arch RCP_Arch 122x78
	•		L= 70.0' RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 92.00' / 91.50' S= 0.0071 '/' Cc= 0.900
			n= 0.022 Earth, clean & straight, Flow Area= 51.67 sf
#2	Secondary	99.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

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Primary OutFlow Max=117.25 cfs @ 13.58 hrs HW=94.90' (Free Discharge)
1=RCP_Arch 122x78 (Barrel Controls 117.25 cfs @ 6.18 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=92.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 24P: Cultec Recharger 150XLHD

Inflow Area =	0.550 ac, 67.27% Impervious, Inflo	ow Depth > 3.30" for 10 YEAR event	
Inflow =	2.38 cfs @ 12.03 hrs, Volume=	0.151 af	
Outflow =	2.93 cfs @ 12.10 hrs, Volume=	0.150 af, Atten= 0%, Lag= 4.3 min	
Primary =	1.86 cfs @ 12.10 hrs, Volume=	0.142 af	
Secondary =	1.08 cfs @ 12.10 hrs, Volume=	0.008 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.71' @ 12.10 hrs Surf.Area= 0.025 ac Storage= 0.036 af

Plug-Flow detention time= 41.2 min calculated for 0.150 af (99% of inflow) Center-of-Mass det. time= 37.5 min (799.3 - 761.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	94.00'	0.018 af	14.50'W x 74.50'L x 2.54'H Field A
			0.063 af Overall - 0.018 af Embedded = 0.045 af x 40.0% Voids
#2A	94.50'	0.018 af	Cultec R-150XLHD x 28 Inside #1
			Effective Size= 29.8"W x 18.0"H => 2.65 sf x 10.25'L = 27.2 cf
			Overall Size= 33.0"W x 18.5"H x 11.00'L with 0.75' Overlap
			Row Length Adjustment= +0.75' x 2.65 sf x 4 rows
#3	96.50'	0.001 af	4.00'D x 4.00'H Vertical Cone/Cylinder
		0.037 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	94.00'	18.0" Round Culvert
			L= 30.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 94.00' / 93.00' S= 0.0333 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	94.00'	3.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	96.50'	18.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	96.50'	4.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=1.84 cfs @ 12.10 hrs HW=96.71' (Free Discharge)

1=Culvert (Passes 1.84 cfs of 11.91 cfs potential flow)

—2=Orifice/Grate (Orifice Controls 0.38 cfs @ 7.74 fps) **—3=Orifice/Grate** (Weir Controls 1.46 cfs @ 1.49 fps)

Secondary OutFlow Max=1.07 cfs @ 12.10 hrs HW=96.71' (Free Discharge)
4=Broad-Crested Rectangular Weir (Weir Controls 1.07 cfs @ 1.28 fps)

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Summary for Pond 51P: 54 ROOF DRIPLINE BMP'S

Inflow Area = 3.220 ac,100.00% Impervious, Inflow Depth > 4.05" for 10 YEAR event

Inflow = 10.82 cfs @ 12.21 hrs, Volume= 1.087 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume = 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 100.13' @ 20.00 hrs Surf.Area= 867,510 sf Storage= 47,341 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume Invert A		Avail.Storag	e Storage Description
#1	100.00'	13,187	of 3.00'W x 105.00'L x 2.00'H Prismatoid x 54
#2	100.00'	1,051 (34,020 cf Overall - 1,051 cf Embedded = 32,969 cf x 40.0% Voids 6.0" Round Pipe Storage x 51 Inside #1 L= 105.0' S= 0.0050 '/'
		14,239	cf x 51.00 = 726,182 cf Total Available Storage
Device	Routing	Invert O	utlet Devices
#1	Primary	H	00.0' long x 10.0' breadth Broad-Crested Rectangular Weir X 51.00 ead (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 pef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=100.00' (Free Discharge)
1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Subcatchment 1S:

Runoff = 131.34 cfs @ 12.79 hrs, Volume= 21.542 af, Depth> 3.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac)	CN	Desc	cription					
*	43.	440	70	WOO	DDS / FIEL	D HSG C				
*	18.	400	98	EXIS	EXISTING IMPERVIOUS AREA					
*	23.	400	74	EXIS	STING LAV	VN C				
*	0.	100	74	NEV	LAWN C					
	85.340 77			Weig	ghted Aver	age				
	66.940			78.4	4% Pervio	us Area				
	18.	400		21.5	6% Imperv	ious Area				
	Tc	Lengtl		Slope	Velocity	Capacity	Description			
_	(min)	(feet	:)	(ft/ft)	(ft/sec)	(cfs)				
	28.8	100	0.	0400	0.06		Sheet Flow, AB			
							Woods: Dense underbrush n= 0.800 P2= 3.10"			
	30.0	900	0.	0400	0.50		Shallow Concentrated Flow, BC			
_							Forest w/Heavy Litter Kv= 2.5 fps			
	58.8	1.000) To	otal						

Summary for Subcatchment 2S:

Runoff = 112.64 cfs @ 12.69 hrs, Volume= 16.962 af, Depth> 3.04"

	Area	(ac)	CN	Desc	cription					
*	22.	010	70	WOODS / FIELD HSG C						
*	13.	000	98	EXIS	STING IMP	PERVIOUS	AREA			
*	30.	000	74	EXIS	STING LAV	VN C				
*	1.	850	74	NEV	LAWN C					
*	0.	000	98	NEV	/ IMPERV	IOUS BUIL	DING AREA (see 51S)			
*	0.	130	98	New	Trails					
	66.	990	77	Weig	ghted Aver	age				
	53.	860		80.4	0% Pervio	us Area				
	13.	130		19.6	0% Imperv	ious Area				
	Tc	Length	ı S	Slope	Velocity	Capacity	Description			
_	(min)	(feet))	(ft/ft)	(ft/sec)	(cfs)				
	28.8	100	0.0	0400	0.06		Sheet Flow, AB			
							Woods: Dense underbrush n= 0.800 P2= 3.10"			
	21.7	650	0.0	0400	0.50		Shallow Concentrated Flow, BC			
							Forest w/Heavy Litter Kv= 2.5 fps			
	50.5	750) To	otal						

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Summary for Subcatchment 3S:

Runoff = 45.00 cfs @ 12.82 hrs, Volume= 7.460 af, Depth> 2.48"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac)	CN	Desc	cription					
*	31.	320	70	70 WOODS / FIELD HSG C						
*	0.	000	98	EXIS	EXISTING IMPERVIOUS AREA					
*	4.	000	74	EXIS	STING LAV	VN C				
*	0.	210	74	NEW	/ LAWN C					
*	0.	410	70	NEW	/ FILL SLC	PE				
*	0.	000	98	NEW	/ IMPERVI	OUS BUIL	DING AREA (See 51s)			
*	0.	100	98	NEV	/ Trails					
	36.	040	71	Weig	hted Aver	age				
	35.	940		99.7	2% Pervio	us Area				
	0.	100		0.28	% Impervio	ous Area				
	Тс	Length		Slope	Velocity	Capacity	Description			
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	28.8	100	0.	0400	0.06		Sheet Flow, AB			
							Woods: Dense underbrush n= 0.800 P2= 3.10"			
	15.0	450	0.	0400	0.50		Shallow Concentrated Flow, BC			
			_				Forest w/Heavy Litter Kv= 2.5 fps			
	16.5	7	5 0.	0900	0.08		Sheet Flow,			
_							Woods: Dense underbrush n= 0.800 P2= 3.10"			
	60.3	628	5 To	otal						

Summary for Subcatchment 4S:

Runoff = 18.21 cfs @ 12.81 hrs, Volume= 2.982 af, Depth> 2.75"

	Area (ac)	CN	Description
*	5.000	70	WOODS / FIELD HSG C
*	1.000	98	EXISTING IMPERVIOUS AREA
*	7.000	74	EXISTING LAWN C
*	0.000	98	NEW IMPERVIOUS PAVED AREA
*	0.000	74	NEW LAWN C
	13.000	74	Weighted Average
	12.000		92.31% Pervious Area
	1.000		7.69% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC
_						Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Total			

Summary for Subcatchment 5S: drains to 48" culvert

Runoff = 129.65 cfs @ 13.46 hrs, Volume= 31.922 af, Depth> 3.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac) (CN De	escription					
*	47.	000	70 W	OODS / FIE	LD HSG C				
*	36.	000	98 EX	CISTING IMP	PERVIOUS	AREA			
*	35.	000	74 EX	(ISTING LA	WN C				
	118.	000	80 W	Weighted Average					
	82.	000	69	.49% Pervio	us Area				
	36.	000	30	.51% Imper	vious Area				
	_					-			
	Тс	Length			Capacity	Description			
_	(min)	(feet)	(ft/fi	t) (ft/sec)	(cfs)				
	38.0	100	0.020	0.04		Sheet Flow, AB			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	60.0	900	0.010	0 0.25		Shallow Concentrated Flow, BC			
						Forest w/Heavy Litter Kv= 2.5 fps			
	14.8	2,671	0.040	0 3.00		Shallow Concentrated Flow, CD			
_						Grassed Waterway Kv= 15.0 fps			
	112.8	3,671	Total						

Summary for Subcatchment 6S: drains to 48" culvert

Runoff = 145.08 cfs @ 12.51 hrs, Volume= 18.906 af, Depth> 3.44"

	Area (ac)	CN	Description
*	6.000	70	WOODS / FIELD HSG C
*	20.000	98	EXISTING IMPERVIOUS AREA
*	40.000	74	EXISTING LAWN C
	66.000	81	Weighted Average
	46.000		69.70% Pervious Area
	20.000		30.30% Impervious Area

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Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
28.8	100	0.0400	0.06		Sheet Flow, AB
					Woods: Dense underbrush n= 0.800 P2= 3.10"
5.0	900	0.0400	3.00		Shallow Concentrated Flow, BC
					Grassed Waterway Kv= 15.0 fps
3.7	2,500	0.0400	11.41	182.56	Trap/Vee/Rect Channel Flow, CD
					Bot.W=4.00' D=2.00' Z= 2.0 '/' Top.W=12.00'
					n= 0.030 Earth, grassed & winding
37.5	3 500	Total			

Summary for Subcatchment 7S:

Runoff = 47.09 cfs @ 12.12 hrs, Volume= 3.550 af, Depth> 3.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac) (CN De	escription				
*	0.	000	70 W	OODS / FIE	LD HSG C			
*	5.	000	98 EX	(ISTING IMF	PERVIOUS	AREA		
*	6.	000	74 EX	(ISTING LA	WN C			
11.000 85 Weighted Average								
	6.	000	54	.55% Pervio	us Area			
	5.	000	45	45.45% Impervious Area				
	Tc (min)	Length (feet)			Capacity (cfs)	Description		
	7.5	100	0.0400	0 0.22		Sheet Flow, AB		
	1.1	200	0.0400	0 3.00		Grass: Short n= 0.150 P2= 3.10" Shallow Concentrated Flow, BC Grassed Waterway Kv= 15.0 fps		
	8.6	300	Total	·	·	<u> </u>		

Summary for Subcatchment 14S: 550 ROAD, 22' ROAD, 5' WALK to Forest Buffer

Runoff = 1.86 cfs @ 12.26 hrs, Volume= 0.196 af, Depth> 4.69"

	Area (ac)	CN	Description
*	0.400	98	NEW IMPERVIOUS PAVED AREA
*	0.100	74	NEW LAWN C
	0.500	93	Weighted Average
	0.100		20.00% Pervious Area
	0.400		80.00% Impervious Area

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
0.2	11	0.0300	1.02		Sheet Flow, AB
					Smooth surfaces n= 0.011 P2= 3.10"
1.2	250	0.0300	3.52		Shallow Concentrated Flow, BC
					Paved Kv= 20.3 fps
18.3	75	0.0700	0.07		Sheet Flow,
					Woods: Dense underbrush n= 0.800 P2= 3.10"
19 7	336	Total			

Summary for Subcatchment 15S: 600' ROAD, 22' ROAD, 5' WALK to Focal Points

Runoff = 3.14 cfs @ 12.02 hrs, Volume= 0.202 af, Depth> 4.40"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac) (CN Des	cription		
*	0.	370	98 NEV	V IMPERV	IOUS PAVI	ED AREA
*	0.	180	74 NEV	V LAWN C		
	0.	550	90 Wei	ghted Aver	age	
	0.	180	32.7	3% Pervio	us Area	
	0.	370	67.2	7% Imper	ious Area	
	_					
	Tc	Length	Slope	Velocity	Capacity	Description
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	0.2	11	0.0300	1.02		Sheet Flow, AB
						Smooth surfaces n= 0.011 P2= 3.10"
	1.2	250	0.0300	3.52		Shallow Concentrated Flow, BC
						Paved Kv= 20.3 fps
	1.4	261	Total			

Summary for Subcatchment 16S: Arctic Fox Pond Watershed

Runoff = 7.06 cfs @ 12.78 hrs, Volume= 1.163 af, Depth> 3.32"

	Area (ac)	CN	Description
*	0.570	70	WOODS / FIELD HSG C
*	0.000	98	EXISTING IMPERVIOUS AREA
*	0.000	74	EXISTING LAWN C
*	1.100	98	NEW IMPERVIOUS PAVED AREA
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (see 51s)
*	2.540	74	NEW LAWN C
	4.210	80	Weighted Average
	3.110		73.87% Pervious Area
	1.100		26.13% Impervious Area

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	Tc	Length	Slope	,		Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC
_						Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Total			

Summary for Subcatchment 17S: Mallard Lane Pond Watershed

Runoff = 12.83 cfs @ 12.78 hrs, Volume= 2.124 af, Depth> 3.51"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac)	CN	Desc	cription		
* 0.220 70 WOODS / FIELD HSG C							
*	0.	000	98	EXIS	STING IMP	PERVIOUS	AREA
*	0.	000	74	EXIS	STING LAV	VN C	
*	2.	400	98	NEV	/ IMPERV	IOUS PAVI	ED AREA
*	0.	000	98	NEV	/ IMPERV	IOUS BUIL	DING AREA (see 51s)
*	4.	640	74	NEV	LAWN C		
	7.	260	82	Weig	ghted Aver	age	
	4.	860		66.9	4% Pervio	us Area	
	2.	400		33.0	6% Imperv	vious Area	
	Тс	Length	1 5	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.	0400	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.	0400	0.50		Shallow Concentrated Flow, BC
							Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000) To	otal			

Summary for Subcatchment 18S:

Runoff = 1.62 cfs @ 12.71 hrs, Volume= 0.243 af, Depth> 2.58"

	Area (ac)	CN	Description
*	0.450	70	WOODS / FIELD HSG C
*	0.680	74	NEW LAWN C
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (see 51s)
	1.130	72	Weighted Average
	1.130		100.00% Pervious Area

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>
28.8	100	0.0400	0.06		Sheet Flow, AB
					Woods: Dense underbrush n= 0.800 P2= 3.10"
21.7	650	0.0400	0.50		Shallow Concentrated Flow, BC
					Forest w/Heavy Litter Kv= 2.5 fps
50.5	750	Total			

Summary for Subcatchment 19S:

Runoff = 40.63 cfs @ 12.14 hrs, Volume= 3.049 af, Depth> 2.62"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac)	CN	Desc	cription						
*	10.000 /0 WOODS / FIELD HSG C										
*	0.	600	98	EXIS	XISTING IMPERVIOUS AREA						
*	1.	600	74	EXIS	XISTING LAWN C						
*	0.	0.940 74 NEW LAWN C									
*	0.	150	98	NEW	/ IMPERV	IOUS PAVI	ED AREA				
*	0.	000	98	NEW	/ IMPERV	IOUS BUIL	DING AREA (See 51s)				
	13.950 72 Weighted Average				hted Aver	age					
	13.200 94.62% Pervious Area										
	0.750 5.38% Impervious Area				% Impervi	ous Area					
					•						
	Tc	Lengt	h	Slope	Velocity	Capacity	Description				
	(min)	(feet	t)	(ft/ft)	(ft/sec)	(cfs)	·				
	7.5	10	0 0	.0400	0.22		Sheet Flow, AB				
							Grass: Short n= 0.150 P2= 3.10"				
	1.7	30	0 0	.0400	3.00		Shallow Concentrated Flow, BC				
							Grassed Waterway Kv= 15.0 fps				
	9.2	40	0 T	otal			·				

Summary for Subcatchment 20S:

Runoff = 9.81 cfs @ 12.51 hrs, Volume= 1.233 af, Depth> 2.42"

	Area (ac)	CN	Description
*	5.820	70	WOODS / FIELD HSG C
*	0.000	98	EXISTING IMPERVIOUS AREA
*	0.000	74	EXISTING LAWN C
*	0.290	74	NEW LAWN C
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (See 51s)
_	6.110	70	Weighted Average
	6.110		100.00% Pervious Area

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	·
28.8	100	0.0400	0.06		Sheet Flow, AB
					Woods: Dense underbrush n= 0.800 P2= 3.10"
6.7	200	0.0400	0.50		Shallow Concentrated Flow, BC
					Forest w/Heavy Litter Kv= 2.5 fps
35.5	300	Total			

Summary for Subcatchment 51S: NEW Cottage Roof Areas

Runoff = 13.68 cfs @ 12.21 hrs, Volume= 1.381 af, Depth> 5.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 25 YEAR Rainfall=5.80"

	Area	(ac) C	N Desc	cription		
*	3.	220 9	98 52 C	ottage Ro	ofs + Comn	nunity Buildings
	3.	220	100.	00% Impe	rvious Area	
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.1	20	0.4000	3.25		Sheet Flow, AB
	2.5	25	0.0400	0.17		Smooth surfaces n= 0.011 P2= 3.10" Sheet Flow, BC
	2.0	25	0.0400	0.17		Grass: Short n= 0.150 P2= 3.10"
	13.1	75	0.1600	0.10		Sheet Flow, CD
_						Woods: Dense underbrush n= 0.800 P2= 3.10"
	15.7	120	Total			

Summary for Reach 3R: Stream @ Property Line

Inflow Area = 111.340 ac, 22.38% Impervious, Inflow Depth > 2.82" for 25 YEAR event

Inflow = 138.49 cfs @ 12.88 hrs, Volume= 26.128 af

Outflow = 138.13 cfs @ 12.96 hrs, Volume= 25.998 af, Atten= 0%, Lag= 4.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 5.07 fps, Min. Travel Time= 2.8 min Avg. Velocity = 1.97 fps, Avg. Travel Time= 7.3 min

Peak Storage= 23,439 cf @ 12.92 hrs Average Depth at Peak Storage= 1.95'

Bank-Full Depth= 3.00' Flow Area= 45.0 sf, Capacity= 287.21 cfs

12.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 1.0 '/' Top Width= 18.00' Length= 860.0' Slope= 0.0058 '/' Inlet Invert= 77.00', Outlet Invert= 72.00'

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Summary for Reach 4R: Stream below RR crossing

Inflow Area = 96.890 ac, 24.53% Impervious, Inflow Depth > 2.85" for 25 YEAR event

Inflow = 132.89 cfs @ 12.82 hrs, Volume= 22.983 af

Outflow = 132.44 cfs @ 12.89 hrs, Volume= 22.883 af, Atten= 0%, Lag= 4.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 5.49 fps, Min. Travel Time= 2.6 min Avg. Velocity = 2.30 fps, Avg. Travel Time= 6.2 min

Peak Storage= 20,778 cf @ 12.85 hrs Average Depth at Peak Storage= 2.76'

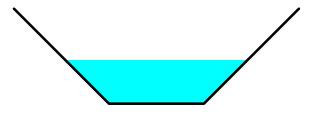
Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 582.42 cfs

6.00' x 6.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 860.0' Slope= 0.0058 '/'

Inlet Invert= 82.00', Outlet Invert= 77.00'



Summary for Reach 6R: Stream below Site @ PL

Inflow Area = 272.920 ac, 27.79% Impervious, Inflow Depth > 3.07" for 25 YEAR event

Inflow = 250.46 cfs @ 12.91 hrs, Volume= 69.911 af

Outflow = 250.22 cfs @ 12.96 hrs, Volume= 69.799 af, Atten= 0%, Lag= 2.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity = 6.73 fps, Min. Travel Time = 1.1 min

Avg. Velocity = 3.75 fps, Avg. Travel Time= 2.0 min

Peak Storage= 16,730 cf @ 12.93 hrs Average Depth at Peak Storage= 3.29'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf. Capacity= 538.97 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

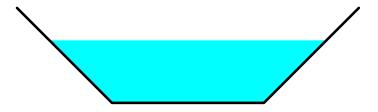
Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 61.00', Outlet Invert= 58.00'

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Summary for Reach 7R: Stream Through Site

Inflow Area = 257.100 ac, 26.89% Impervious, Inflow Depth > 3.16" for 25 YEAR event

Inflow = 243.08 cfs @ 12.80 hrs, Volume= 67.667 af

Outflow = 242.73 cfs @ 12.85 hrs, Volume= 67.501 af, Atten= 0%, Lag= 3.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 10.61 fps, Min. Travel Time= 1.7 min Avg. Velocity = 5.75 fps, Avg. Travel Time= 3.2 min

Peak Storage= 25,194 cf @ 12.82 hrs Average Depth at Peak Storage= 2.24'

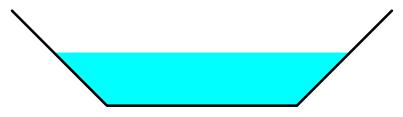
Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 683.45 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,100.0' Slope= 0.0245 '/'

Inlet Invert= 88.00', Outlet Invert= 61.00'



Summary for Reach 14R: Swale from School and Neighborhood

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 1.54" for 25 YEAR event

Inflow = 2.00 cfs @ 15.48 hrs, Volume= 1.411 af

Outflow = 2.00 cfs @ 16.31 hrs, Volume= 1.251 af, Atten= 0%, Lag= 49.8 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 1.85 fps, Min. Travel Time= 30.3 min Avg. Velocity = 1.32 fps, Avg. Travel Time= 42.6 min

Peak Storage= 3,624 cf @ 15.80 hrs

Average Depth at Peak Storage= 0.25'

Bank-Full Depth= 3.00' Flow Area= 21.0 sf, Capacity= 147.12 cfs

4.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 10.00'

Length= 3,366.0' Slope= 0.0100 '/'

Inlet Invert= 117.66', Outlet Invert= 84.00'

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Summary for Reach 17R:

Inflow Area = 8.390 ac, 28.61% Impervious, Inflow Depth > 2.52" for 25 YEAR event

Inflow = 12.30 cfs @ 13.09 hrs, Volume= 1.764 af

Outflow = 12.26 cfs @ 13.14 hrs, Volume= 1.757 af, Atten= 0%, Lag= 3.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.60 fps, Min. Travel Time= 1.8 min Avg. Velocity = 2.89 fps, Avg. Travel Time= 4.0 min

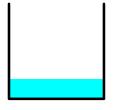
Peak Storage= 1,304 cf @ 13.11 hrs Average Depth at Peak Storage= 0.62'

Bank-Full Depth= 3.00' Flow Area= 9.0 sf, Capacity= 102.76 cfs

3.00' x 3.00' deep channel, n= 0.022 Earth, clean & straight

Length= 700.0' Slope= 0.0286 '/'

Inlet Invert= 81.00', Outlet Invert= 61.00'



Summary for Reach 18R: Stream Through Site

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 3.26" for 25 YEAR event

Inflow = 195.61 cfs @ 12.62 hrs, Volume= 49.959 af

Outflow = 195.00 cfs @ 12.69 hrs, Volume= 49.794 af, Atten= 0%, Lag= 4.3 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 8.68 fps, Min. Travel Time= 2.3 min

Avg. Velocity = 4.33 fps, Avg. Travel Time= 4.6 min

Peak Storage= 26,999 cf @ 12.65 hrs

Average Depth at Peak Storage= 2.20'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 563.18 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,200.0' Slope= 0.0167 '/'

Inlet Invert= 125.00', Outlet Invert= 105.00'

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Summary for Reach 55R: Wetland below Site @ PL

36.040 ac, 0.28% Impervious, Inflow Depth > 2.48" for 25 YEAR event Inflow Area =

45.00 cfs @ 12.82 hrs, Volume= Inflow 7.460 af

Outflow 44.85 cfs @ 12.89 hrs, Volume= 7.436 af, Atten= 0%, Lag= 3.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.01 fps, Min. Travel Time= 1.9 min Avg. Velocity = 1.86 fps, Avg. Travel Time= 4.0 min

Peak Storage= 5,048 cf @ 12.85 hrs Average Depth at Peak Storage= 1.22'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 540.76 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 63.02', Outlet Invert= 60.00'



Summary for Pond 1P: 1-30" and 1-24" Culvert at Tuttle Road

111.340 ac, 22.38% Impervious, Inflow Depth > 2.77" for 25 YEAR event Inflow Area =

132.69 cfs @ 13.10 hrs, Volume= Inflow 25.710 af

132.66 cfs @ 13.11 hrs, Volume= 25.668 af, Atten= 0%, Lag= 0.7 min Outflow

Primary 61.50 cfs @ 13.11 hrs, Volume= 20.586 af 71.16 cfs @ 13.11 hrs, Volume= Secondary = 5.083 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 71.66' @ 13.11 hrs Surf.Area= 7,421 sf Storage= 20,226 cf

Plug-Flow detention time= 3.3 min calculated for 25.668 af (100% of inflow)

Center-of-Mass det. time= 2.8 min (859.2 - 856.4)

Volume	Invert	Avail.Storage	Storage Description
#1	68.00'	31,683 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

#3

Secondary

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Elevation (feet)		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
68.0	00	3,850	0	0	
70.0	00	5,600	9,450 9,450		
72.0	00	7,800	13,400	22,850	
73.0	00	9,865	8,833	31,683	
Device	Routing	Invert	Outlet Devices		
	<u> </u>	07.50		_	
#1	Primary	67.50'	30.0" Round C	ulvert	
#1	Primary	67.50	L= 50.0' RCP, Inlet / Outlet Inv	sq.cut end pro ert= 67.50' / 6	jecting, Ke= 0.500 6.50' S= 0.0200 '/' Cc= 0.900 ght & clean, Flow Area= 4.91 sf
#1 #2	Primary	67.50'	L= 50.0' RCP, Inlet / Outlet Inv	sq.cut end pro ert= 67.50' / 6 rete pipe, strai	6.50' S= 0.0200 '/' Cc= 0.900
	•		L= 50.0' RCP, Inlet / Outlet Inv n= 0.011 Concr 24.0" Round C L= 50.0' CPP,	sq.cut end pro ert= 67.50' / 6 rete pipe, strai ulvert projecting, no	5.50' S= 0.0200 '/' Cc= 0.900 ght & clean, Flow Area= 4.91 sf headwall, Ke= 0.900
	•		L= 50.0' RCP, Inlet / Outlet Inv n= 0.011 Concr 24.0" Round C L= 50.0' CPP, Inlet / Outlet Inv	sq.cut end pro ert= 67.50' / 6 rete pipe, strai ulvert projecting, no ert= 67.50' / 6	6.50' S= 0.0200 '/' Cc= 0.900 ght & clean, Flow Area= 4.91 sf

Primary OutFlow Max=61.49 cfs @ 13.11 hrs HW=71.65' (Free Discharge)

1=Culvert (Inlet Controls 40.28 cfs @ 8.21 fps)

71.00'

-2=Culvert (Inlet Controls 21.21 cfs @ 6.75 fps)

Secondary OutFlow Max=71.03 cfs @ 13.11 hrs HW=71.65' (Free Discharge)

3=Broad-Crested Rectangular Weir (Weir Controls 71.03 cfs @ 2.17 fps)

Summary for Pond 2P: Two 30" Culverts at Crossing Brook Road

50.0' long x 50.0' breadth Broad-Crested Rectangular Weir Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

272.920 ac, 27.79% Impervious, Inflow Depth > 3.07" for 25 YEAR event Inflow Area = Inflow 250.22 cfs @ 12.96 hrs, Volume= 69.799 af Outflow 107.16 cfs @ 15.42 hrs, Volume= 59.718 af, Atten= 57%, Lag= 147.8 min Primary = 107.16 cfs @ 15.42 hrs, Volume= 59.718 af 5.00 hrs, Volume= 0.000 af Secondary = 0.00 cfs @

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 54.24' @ 15.42 hrs Surf.Area= 184,784 sf Storage= 1,203,628 cf

Plug-Flow detention time= 133.7 min calculated for 59.718 af (86% of inflow) Center-of-Mass det. time= 96.8 min (965.7 - 868.9)

Volume	Invert	Avail.Storage	Storage Description
#1	44.00'	2,030,000 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
44.00	60,000	0	0
46.00	80,000	140,000	140,000
48.00	100,000	180,000	320,000
50.00	120,000	220,000	540,000
52.00	160,000	280,000	820,000
54.00	180,000	340,000	1,160,000
56.00	220,000	400,000	1,560,000
58.00	250,000	470,000	2,030,000

Device	Routing	Invert	Outlet Devices
#1	Primary	44.00'	30.0" Round Culvert
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 44.00' / 42.00' S= 0.0400 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf
#2	Primary	44.00'	24.0" Round Culvert
			L= 50.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 44.00' / 42.00' S= 0.0400 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
#3	Secondary	56.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=107.16 cfs @ 15.42 hrs HW=54.24' (Free Discharge)

1=Culvert (Inlet Controls 70.86 cfs @ 14.44 fps)

2=Culvert (Inlet Controls 36.30 cfs @ 11.55 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=44.00' (Free Discharge) 3=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 3P: 24" CULVERT

Inflow Area =	36.040 ac,	0.28% Impervious, Inflow D	Depth > 2.48" for 25 YEAR event
Inflow =	44.85 cfs @	12.89 hrs, Volume=	7.436 af
Outflow =	38.26 cfs @	13.17 hrs, Volume=	7.390 af, Atten= 15%, Lag= 16.9 min
Primary =	31.09 cfs @	13.17 hrs, Volume=	7.225 af
Secondary =	7.16 cfs @	13.17 hrs, Volume=	0.165 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 59.23' @ 13.17 hrs Surf.Area= 16,126 sf Storage= 42,346 cf

Plug-Flow detention time= 15.0 min calculated for 7.390 af (99% of inflow) Center-of-Mass det. time= 12.8 min (858.2 - 845.4)

Volume	Invert	Avail.Storage	Storage Description
#1	54.00'	56.342 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	on	Surf.Area	Inc.Store	Cum.Store		
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)		
54.0	00	2,362	0	0		
56.0	00	6,990	9,352	9,352		
58.0	00	10,000	16,990	26,342		
60.0	00	20,000	30,000	56,342		
Device	Routing	Invert	Outlet Devices			
#1	Primary	54.00'	24.0" Round C	ulvert		
			L= 50.0' RCP,	sq.cut end pro	ojecting, Ke= 0.500	
			Inlet / Outlet Invert= 54.00' / 53.00' S= 0.0200 '/' Cc= 0.900			
			n= 0.011 Concr	rete pipe, strai	ight & clean, Flow Area= 3.14 sf	
#2	Seconda	ry 59.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir			

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.63

Primary OutFlow Max=31.08 cfs @ 13.17 hrs HW=59.22' (Free Discharge) 1=Culvert (Inlet Controls 31.08 cfs @ 9.89 fps)

Secondary OutFlow Max=7.02 cfs @ 13.17 hrs HW=59.22' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 7.02 cfs @ 1.26 fps)

Summary for Pond 4P: 18" CULVERT

Inflow Area =	13.000 ac,	7.69% Impervious, Inflow D	Depth > 2.75" for 25 YEAR event
Inflow =	18.21 cfs @	12.81 hrs, Volume=	2.982 af
Outflow =	11.61 cfs @	13.31 hrs, Volume=	2.938 af, Atten= 36%, Lag= 30.1 min
Primary =	11.61 cfs @	13.31 hrs, Volume=	2.938 af
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 87.61' @ 13.31 hrs Surf.Area= 17,137 sf Storage= 26,474 cf

Plug-Flow detention time= 30.0 min calculated for 2.938 af (99% of inflow) Center-of-Mass det. time= 24.9 min (860.1 - 835.2)

Volume	Inve	rt Avail.Sto	rage Storage	e Description	
#1	85.00	0' 82,7	55 cf Custor	n Stage Data (Prism	atic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.0	00	3,343	0	0	
86.0	00	8,410	5,877	5,877	
88.0	00	19,234	27,644	33,521	
90.0	00	30,000	49,234	82,755	
Device	Routing	Invert	Outlet Device	es	
#1	Primary	85.00'	18.0" Roun	d Culvert	
				P, sq.cut end project	
					o' S= 0.0200 '/' Cc= 0.900
					& clean, Flow Area= 1.77 sf
#2	Secondar	y 89.00'	25.0' long x	25.0' breadth Broad	d-Crested Rectangular Weir

Volume

Invert

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Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.63

Primary OutFlow Max=11.61 cfs @ 13.31 hrs HW=87.61' (Free Discharge)
1=Culvert (Inlet Controls 11.61 cfs @ 6.57 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=85.00' (Free Discharge)

2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 5P: 4'x3' Oval and 30" Overflow Culvert

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 3.31" for 25 YEAR event Inflow = 195.88 cfs @ 12.60 hrs, Volume= 50.828 af

Outflow = 195.61 cfs @ 12.62 hrs, Volume= 49.959 af, Atten= 0%, Lag= 1.4 min Primary = 41.35 cfs @ 12.62 hrs, Volume= 24.775 af

Secondary = 154.26 cfs @ 12.62 hrs, Volume= 25.185 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 137.98' @ 12.62 hrs Surf.Area= 19,954 sf Storage= 97,425 cf

Plug-Flow detention time= 18.5 min calculated for 49.959 af (98% of inflow) Center-of-Mass det. time= 12.7 min (855.8 - 843.0)

Avail Storage Storage Description

Volume	IIIVEIL	Avaii.0t0	rage Storage	Description	
#1	129.00'	142,73	35 cf Custom	Stage Data (Pri	ismatic)Listed below (Recalc)
Elevation (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
129.0		4,441	0	0	
130.0		6,196	5,319	5,319	
132.0		8,225	14,421	19,740	
134.0		10,880	19,105	38,845	
136.0		14,005	24,885	63,730	
138.0		20,000	34,005	97,735	
140.0		25,000	45,000	142,735	
		-,	-,	,	
Device	Routing	Invert	Outlet Devices	3	
#1	Primary	129.00'	4.0" W x 3.0"	H, R=3.0" Ellip	tical Culvert
	,				jecting, Ke= 0.500
			Inlet / Outlet Ir	nvert= 129.00' / 1	128.00' S= 0.0333 '/' Cc= 0.900
			n= 0.011 Con	icrete pipe, straiç	ght & clean, Flow Area= 0.07 sf
#2	Primary	132.00'	30.0" Round	Culvert	
			L= 50.0' CPF	P, projecting, no	headwall, Ke= 0.900
					128.00' S= 0.0800 '/' Cc= 0.900
				,	r, Flow Area= 4.91 sf
#3	Secondary	137.00'			oad-Crested Rectangular Weir
			` ,		0.80 1.00 1.20 1.40 1.60
			Coef. (English	i) 2.68 2.70 2.7	70 2.64 2.63 2.64 2.64 2.63

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Primary OutFlow Max=41.34 cfs @ 12.62 hrs HW=137.98' (Free Discharge)

1=Culvert (Barrel Controls 0.75 cfs @ 11.15 fps)
2=Culvert (Inlet Controls 40.59 cfs @ 8.27 fps)

Secondary OutFlow Max=153.85 cfs @ 12.62 hrs HW=137.98' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 153.85 cfs @ 2.61 fps)

Summary for Pond 6P: 1-48" Culvert Crossing Golf Cart Path

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 3.25" for 25 YEAR event

Inflow = 195.00 cfs @ 12.69 hrs, Volume= 49.794 af

Outflow = 167.75 cfs @ 13.40 hrs, Volume= 49.594 af, Atten= 14%, Lag= 42.0 min

Primary = 143.09 cfs @ 13.40 hrs, Volume= 47.792 af Secondary = 24.65 cfs @ 13.40 hrs, Volume= 1.802 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 103.59' @ 13.40 hrs Surf.Area= 50,620 sf Storage= 202,628 cf

Plug-Flow detention time= 15.7 min calculated for 49.429 af (99% of inflow)

Center-of-Mass det. time= 14.3 min (874.4 - 860.0)

Volume	Inv	<u>rert Avail.S</u>	torage Stora	ge Description	
#1	96.	00' 280	448 cf Cust	om Stage Data (Pr	ismatic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
96.0	00	1,580	0	0	
98.0	00	14,434	16,014	16,014	
100.0	00	30,000	44,434	60,448	
102.0	00	40,000	70,000	130,448	
105.0	00	60,000	150,000	280,448	
Device	Routing	Inve	t Outlet Devi	ces	
44.4	D.::	00.00	10 AU D	and Andrews	

Device	Routing	invert	Outlet Devices
#1	Primary	96.00'	48.0" Round Culvert
			L= 30.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 96.00' / 95.00' S= 0.0333 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 12.57 sf
#2	Secondary	103.00'	20.0' long x 20.0' breadth Broad-Crested Rectangular Weir
	•		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=143.09 cfs @ 13.40 hrs HW=103.59' (Free Discharge)
1=Culvert (Inlet Controls 143.09 cfs @ 11.39 fps)

Secondary OutFlow Max=24.65 cfs @ 13.40 hrs HW=103.59' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 24.65 cfs @ 2.08 fps)

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Summary for Pond 7P: 1-24" Culvert at Greely Middle School

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 3.87" for 25 YEAR event

Inflow = 47.09 cfs @ 12.12 hrs, Volume= 3.550 af

Outflow = 2.00 cfs @ 15.48 hrs, Volume= 1.411 af, Atten= 96%, Lag= 201.4 min

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 124.71' @ 15.48 hrs Surf.Area= 27,778 sf Storage= 105,955 cf

Plug-Flow detention time= 256.5 min calculated for 1.411 af (40% of inflow)

Center-of-Mass det. time= 162.0 min (934.4 - 772.4)

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	214,248 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	18,593	0	0
122.00	21,745	40,338	40,338
124.00	25,131	46,876	87,214
126.00	32,605	57,736	144,950
128.00	36,693	69,298	214,248

Device	Routing	Invert	Outlet Devices
#1	Primary	120.00'	24.0" Round Culvert
			L= 80.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 120.00' / 119.00' S= 0.0125 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Secondary	127.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63
#3	Device 1	120.00'	6.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	126.00'	24.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Primary OutFlow Max=2.00 cfs @ 15.48 hrs HW=124.71' (Free Discharge)

1=Culvert (Passes 2.00 cfs of 29.13 cfs potential flow)

3=Orifice/Grate (Orifice Controls 2.00 cfs @ 10.17 fps)

-4=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=120.00' (Free Discharge)

2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 10P: 1-30" Culvert

Inflow Area =	111.340 ac, 2	2.38% Impervious,	Inflow Depth > 2.8	30" for 25 YEAR event
Inflow =	138.13 cfs @	12.96 hrs, Volume	= 25.998 af	
Outflow =	132.69 cfs @	13.10 hrs, Volume	= 25.710 af,	Atten= 4%, Lag= 8.1 min
Primary =	40.91 cfs @	13.10 hrs, Volume	= 17.100 af	
Secondary =	91.79 cfs @	13.10 hrs, Volume	= 8.610 af	

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 72.25' @ 13.10 hrs Surf.Area= 56,431 sf Storage= 106,101 cf

Plug-Flow detention time= 18.1 min calculated for 25.710 af (99% of inflow)

Center-of-Mass det. time= 14.3 min (856.4 - 842.1)

Volume	Inve	rt Avail.Sto	rage	Storage	Description	
#1	68.0	0' 211,04	48 cf	Custom	Stage Data (Pi	rismatic)Listed below (Recalc)
Elevatio		Surf.Area (sq-ft)		:.Store c-feet)	Cum.Store (cubic-feet)	
68.0		8,000	(Cabi	0	0	
70.0 72.0	00	14,434 55,480		22,434 89,914	22,434 92,348	
74.0		63,220		18,700	211,048	
Device	Routing	Invert	Outl	et Device	S	
#1	Primary	68.00'	30.0	" Round	Culvert	
#2	Secondar	y 71.00'	Inlet n= 0 25.0 Hea	/ Outlet In .011 Cor ' long x 2 d (feet) 0	nvert= 68.00' / 6 ncrete pipe, strai 25.0' breadth B .20 0.40 0.60	ojecting, Ke= 0.500 7.00' S= 0.0333 '/' Cc= 0.900 ight & clean, Flow Area= 4.91 sf road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=40.91 cfs @ 13.10 hrs HW=72.25' (Free Discharge) 1=Culvert (Inlet Controls 40.91 cfs @ 8.33 fps)

Secondary OutFlow Max=91.76 cfs @ 13.10 hrs HW=72.25' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 91.76 cfs @ 2.95 fps)

Summary for Pond 15P: FocalPoint 60sf

Inflow Area =	0.550 ac, 67.27% Impervious, Inflow I	Depth > 4.40" for 25 YEAR event
Inflow =	3.14 cfs @ 12.02 hrs, Volume=	0.202 af
Outflow =	3.12 cfs @ 12.03 hrs, Volume=	0.202 af, Atten= 1%, Lag= 0.4 min
Primary =	0.14 cfs @ 10.50 hrs, Volume=	0.102 af
Secondary =	2.98 cfs @ 12.03 hrs, Volume=	0.100 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 100.83' @ 12.03 hrs Surf.Area= 60 sf Storage= 134 cf

Plug-Flow detention time= 2.6 min calculated for 0.201 af (100% of inflow) Center-of-Mass det. time= 2.6 min (755.9 - 753.3)

Volume	Invert	Avail.Storage	Storage Description
#1	97.75'	27 cf	3.00'W x 20.00'L x 2.25'H FocalPoint
			135 cf Overall x 20.0% Voids
#2	100.00'	133 cf	Custom Stage Data (Prismatic)Listed below (Recalc) -Impervious
		160 cf	Total Available Storage

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
100.00	60	0	0
100.50	157	54	54
101.00	157	79	133

Device	Routing	Invert	Outlet Devices	
#1	Primary	97.75'	100.000 in/hr Exfiltration over Surface area	Phase-In= 0.10'
#2	Secondary	100.50'	18.0" Horiz. Orifice/Grate C= 0.600	
			Limited to weir flow at low heads	

Primary OutFlow Max=0.14 cfs @ 10.50 hrs HW=97.89' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.14 cfs)

Secondary OutFlow Max=2.84 cfs @ 12.03 hrs HW=100.82' (Free Discharge) 2=Orifice/Grate (Weir Controls 2.84 cfs @ 1.86 fps)

Summary for Pond 16P: Arctic Fox WET POND

Inflow Area =	4.210 ac, 26.13% Impervious, Inflow D	epth > 3.32" for 25 YEAR event
Inflow =	7.06 cfs @ 12.78 hrs, Volume=	1.163 af
Outflow =	1.23 cfs @ 14.72 hrs, Volume=	0.654 af, Atten= 83%, Lag= 116.0 min
Primary =	1.23 cfs @ 14.72 hrs, Volume=	0.654 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 77.00' Surf.Area= 4,505 sf Storage= 18,632 cf Peak Elev= 80.45' @ 14.72 hrs Surf.Area= 11,085 sf Storage= 50,184 cf (31,552 cf above start)

Plug-Flow detention time= 416.3 min calculated for 0.225 af (19% of inflow) Center-of-Mass det. time= 153.5 min (977.2 - 823.7)

Volume	Invert	Avail.Storage	Storage Description
#1	71.00'	82,315 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
71.00	1,852	0	0
72.00	2,232	2,042	2,042
73.00	2,636	2,434	4,476
74.00	3,065	2,851	7,327
75.00	3,520	3,293	10,619
76.00	4,000	3,760	14,379
77.00	4,505	4,253	18,632
77.10	7,408	596	19,227
78.00	8,400	7,114	26,341
79.00	9,450	8,925	35,266
80.00	10,557	10,004	45,269
81.00	11,720	11,139	56,408
82.00	12,940	12,330	68,738
83.00	14,215	13,578	82,315

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Device	Routing	Invert	Outlet Devices
#1	Primary	74.00'	18.0" Round Culvert
			L= 58.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 74.00' / 70.00' S= 0.0690 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	78.50'	6.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	81.00'	48.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	81.50'	10.0' long x 10.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=1.23 cfs @ 14.72 hrs HW=80.45' (Free Discharge)

1=Culvert (Passes 1.23 cfs of 20.32 cfs potential flow)

2=Orifice/Grate (Orifice Controls 1.23 cfs @ 6.29 fps)

3=Orifice/Grate (Controls 0.00 cfs)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=77.00' (Free Discharge)

4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 17P: Mallard Way WET POND

Inflow Area =	7.260 ac, 33.06% Impervious, Inflov	w Depth > 3.51" for 25 YEAR event
Inflow =	12.83 cfs @ 12.78 hrs, Volume=	2.124 af
Outflow =	11.51 cfs @ 13.01 hrs, Volume=	1.529 af, Atten= 10%, Lag= 13.9 min
Primary =	11.51 cfs @ 13.01 hrs, Volume=	1.529 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 88.00' Surf.Area= 5,558 sf Storage= 23,438 cf

Peak Elev= 90.90' @ 13.01 hrs Surf.Area= 13,119 sf Storage= 55,655 cf (32,217 cf above start)

Plug-Flow detention time= 192.7 min calculated for 0.988 af (46% of inflow) Center-of-Mass det. time= 56.8 min (876.3 - 819.5)

Volume	Invert	Avail.Storage	Storage Description
#1	81.00'	70,904 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
81.00	1,346	0	0
82.00	1,867	1,607	1,607
83.00	2,419	2,143	3,750
84.00	2,996	2,708	6,457
85.00	3,599	3,298	9,755
86.00	4,226	3,913	13,667
87.00	4,879	4,553	18,220
88.00	5,558	5,219	23,438
88.10	9,325	744	24,182
89.00	10,578	8,956	33,139
90.00	11,887	11,233	44,371
91.00	13,252	12,570	56,941
92.00	14,675	13,964	70,904

Device	Routing	Invert	Outlet Devices
#1	Primary	86.00'	18.0" Round Culvert L= 31.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 86.00' / 85.50' S= 0.0161 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	89.50'	6.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	90.50'	48.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	91.00'	10.0' long x 10.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=11.49 cfs @ 13.01 hrs HW=90.90' (Free Discharge)

-1=Culvert (Passes 11.49 cfs of 17.34 cfs potential flow)

2=Orifice/Grate (Orifice Controls 1.01 cfs @ 5.17 fps)

-3=Orifice/Grate (Weir Controls 10.47 cfs @ 2.07 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=88.00' (Free Discharge)

4=Broad-Crested Rectangular Wair (Controls 0.00 efs) -4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 18P: 24" CULVERT

Inflow Area = 8.390 ac, 28.61% Impervious, Inflow Depth > 2.53" for 25 YEAR event

Inflow 12.79 cfs @ 12.99 hrs, Volume= 1.772 af 12.30 cfs @ 13.09 hrs, Volume= 1.764 af, Atten= 4%, Lag= 5.8 min Outflow =

12.30 cfs @ 13.09 hrs, Volume= Primary 1.764 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 86.74' @ 13.09 hrs Surf.Area= 3,272 sf Storage= 2,915 cf

Plug-Flow detention time= 4.5 min calculated for 1.758 af (99% of inflow) Center-of-Mass det. time= 3.1 min (873.3 - 870.2)

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Volume	Inv	ert Avail.Sto	rage Stora	ge Description	
#1	85.0	00' 15,8	69 cf Cust	om Stage Data (Prismatic)Lis	ted below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.0	00	788	0	0	
86.0	00	1,512	1,150	1,150	
87.0	00	3,898	2,705	3,855	
88.0	00	5,621	4,760	8,615	
89.0	00	8,888	7,255	15,869	
Device	Routing	Invert	Outlet Dev		
#1	Primary	85.00'		nd Culvert	0.500
			Inlet / Outle	RCP, sq.cut end projecting, Ke et Invert= 85.00' / 84.50' S= 0. Concrete pipe, straight & clean,	.0100 '/' Cc= 0.900

Primary OutFlow Max=12.29 cfs @ 13.09 hrs HW=86.74' (Free Discharge) 1=Culvert (Barrel Controls 12.29 cfs @ 5.67 fps)

Summary for Pond 20P: Arch Culvert 1

Inflow Area =	96.890 ac, 24	I.53% Impervious, In	flow Depth > 2.85"	for 25 YEAR event
Inflow =	132.88 cfs @	12.80 hrs, Volume=	22.993 af	
Outflow =	132.89 cfs @	12.82 hrs, Volume=	22.983 af, At	ten= 0%, Lag= 1.1 min
Primary =	132.89 cfs @	12.82 hrs, Volume=	22.983 af	-
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 85.98' @ 12.82 hrs Surf.Area= 2,917 sf Storage= 6,437 cf

Plug-Flow detention time= 0.8 min calculated for 22.906 af (100% of inflow) Center-of-Mass det. time= 0.6 min (837.3 - 836.7)

Volume	ln۱	vert Avail.	Storage	Storage D	escription	
#1	82.	.00' 8	5,094 cf	Custom S	Stage Data (Pr	rismatic)Listed below (Recalc)
Elevation (fee	et)	Surf.Area (sq-ft)	_	.Store c-feet)	Cum.Store (cubic-feet)	
82.0	_	320		0	0	
86.0	_	2,932		6,504	6,504	
87.0 88.0		7,643 11,989		5,288 9,816	11,792 21,608	
89.0		18,865	1	5,427	37,035	
90.0	00	23,627	2	21,246	58,281	
91.0	00	30,000	2	26,814	85,094	
Device	Routing	Inv	ert Outle	et Devices		
#1	Primary	82.			•	126.0" Pipe Arch RCP_Arch 88x54 onforming to fill, Ke= 0.500

Inlet / Outlet Invert= 82.00' / 81.50' S= 0.0071 '/' Cc= 0.900

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n= 0.022 Earth, clean & straight, Flow Area= 25.69 sf #2 Secondary 90.00'

25.0' long x 25.0' breadth Broad-Crested Rectangular Weir

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=132.70 cfs @ 12.82 hrs HW=85.97' (Free Discharge)

1=RCP Arch 88x54 (Barrel Controls 132.70 cfs @ 6.88 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=82.00' (Free Discharge) -2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 21P: Arch Culvert 2

Inflow Area = 190.110 ac, 29.46% Impervious, Inflow Depth > 3.21" for 25 YEAR event

170.34 cfs @ 13.37 hrs, Volume= Inflow 50.827 af

170.22 cfs @ 13.42 hrs, Volume= Outflow = 50.705 af, Atten= 0%, Lag= 2.9 min

170.22 cfs @ 13.42 hrs, Volume= 50.705 af Primary 0.00 cfs @ 5.00 hrs, Volume= Secondary = 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 95.68' @ 13.42 hrs Surf.Area= 11.009 sf Storage= 26.246 cf

Plug-Flow detention time= 3.1 min calculated for 50.705 af (100% of inflow)

Center-of-Mass det. time= 2.3 min (875.5 - 873.2)

Volume	Invert	Avail.Storage	Storage Description
#1	92.00'	200,953 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
92.00	5,000	0	0
93.00	6,000	5,500	5,500
94.00	7,000	6,500	12,000
95.00	8,390	7,695	19,695
96.00	12,267	10,329	30,024
97.00	23,771	18,019	48,043
98.00	31,886	27,829	75,871
99.00	67,139	49,513	125,384
100.00	84,000	75,570	200,953

Device	Routing	Invert	Outlet Devices
#1	Primary	92.00'	122.0" W x 77.3" H, R=62.0"/218.0" Pipe Arch RCP_Arch 122x78
	•		L= 70.0' RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 92.00' / 91.50' S= 0.0071 '/' Cc= 0.900
			n= 0.022 Earth, clean & straight, Flow Area= 51.67 sf
#2	Secondary	99.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

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Primary OutFlow Max=170.18 cfs @ 13.42 hrs HW=95.67' (Free Discharge) 1=RCP_Arch 122x78 (Barrel Controls 170.18 cfs @ 6.85 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=92.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 24P: Cultec Recharger 150XLHD

Inflow Area =	0.550 ac, 67.27% Impervious, Ir	nflow Depth > 4.40" for 25 YEAR event
Inflow =	3.12 cfs @ 12.03 hrs, Volume=	0.202 af
Outflow =	4.18 cfs @ 12.05 hrs, Volume=	0.200 af, Atten= 0%, Lag= 1.1 min
Primary =	2.57 cfs @ 12.05 hrs, Volume=	0.182 af
Secondary =	1.61 cfs @ 12.05 hrs, Volume=	0.018 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.77' @ 12.04 hrs Surf.Area= 0.025 ac Storage= 0.036 af

Plug-Flow detention time= 37.3 min calculated for 0.200 af (99% of inflow) Center-of-Mass det. time= 34.0 min (789.9 - 755.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	94.00'	0.018 af	14.50'W x 74.50'L x 2.54'H Field A
			0.063 af Overall - 0.018 af Embedded = 0.045 af x 40.0% Voids
#2A	94.50'	0.018 af	Cultec R-150XLHD x 28 Inside #1
			Effective Size= 29.8"W x 18.0"H => 2.65 sf x 10.25'L = 27.2 cf
			Overall Size= 33.0"W x 18.5"H x 11.00'L with 0.75' Overlap
			Row Length Adjustment= +0.75' x 2.65 sf x 4 rows
#3	96.50'	0.001 af	4.00'D x 4.00'H Vertical Cone/Cylinder
		0.037 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	94.00'	18.0" Round Culvert
			L= 30.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 94.00' / 93.00' S= 0.0333 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	94.00'	3.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	96.50'	18.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	96.50'	4.0' long x 0.5' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=2.41 cfs @ 12.05 hrs HW=96.76' (Free Discharge)

1=Culvert (Passes 2.41 cfs of 12.06 cfs potential flow)

2=Orifice/Grate (Orifice Controls 0.38 cfs @ 7.81 fps)

-3=Orifice/Grate (Weir Controls 2.03 cfs @ 1.66 fps)

Secondary OutFlow Max=1.50 cfs @ 12.05 hrs HW=96.76' (Free Discharge)
4=Broad-Crested Rectangular Weir (Weir Controls 1.50 cfs @ 1.44 fps)

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Summary for Pond 51P: 54 ROOF DRIPLINE BMP'S

Inflow Area = 3.220 ac,100.00% Impervious, Inflow Depth > 5.15" for 25 YEAR event

Inflow = 13.68 cfs @ 12.21 hrs, Volume= 1.381 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 100.17' @ 20.00 hrs Surf.Area= 867,510 sf Storage= 60,115 cf

Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Stora	Storage Description	
#1	100.00'	13,187	3.00'W x 105.00'L x 2.00'H	Prismatoid x 54
#2	100.00'	1,051	34,020 cf Overall - 1,051 cf & 6.0" Round Pipe Storage > L= 105.0' S= 0.0050 '/'	Embedded = 32,969 cf x 40.0% Voids x 51 Inside #1
		14,239	x 51.00 = 726,182 cf Tota	Available Storage
Device	Routing	Invert	et Devices	
#1	Primary		O' long x 10.0' breadth Broad (feet) 0.20 0.40 0.60 0.80 (English) 2.49 2.56 2.70 2	

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=100.00' (Free Discharge) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

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Summary for Subcatchment 1S:

Runoff = 212.84 cfs @ 12.77 hrs, Volume= 35.251 af, Depth> 4.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac)	CN	Desc	cription		
*	43.	440	70	WOO	DDS / FIEL	D HSG C	
*							AREA
*					STING LAV	VN C	
*	0.	100	74	NEV	/ LAWN C		
85.340 77 Weighted Average					hted Aver	age	
	66.940 78.44% Pervio			4% Pervio	us Area		
	18.400		21.5	6% Imperv	ious Area		
	_						
	Tc	Lengt		Slope	Velocity	Capacity	Description
_	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	10	0 (0.0400	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	90	0 (0.0400	0.50		Shallow Concentrated Flow, BC
							Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,00	0 -	Total			

Summary for Subcatchment 2S:

Runoff = 182.12 cfs @ 12.68 hrs, Volume= 27.748 af, Depth> 4.97"

	Area	(ac)	CN	Desc	cription		
*	22.	010	70	WOO	DDS / FIEL	D HSG C	
*	13.	000	98	EXIS	STING IMP	PERVIOUS	AREA
*	30.	000	74	EXIS	STING LAV	VN C	
*	1.	850	74	NEW	/ LAWN C		
*	0.	000	98	NEW	/ IMPERV	IOUS BUIL	DING AREA (see 51S)
*	0.	130	98	New	Trails		
	66.	990	77	Weig	hted Aver	age	
	53.860			80.4	0% Pervio	us Area	
	13.	130		19.6	0% Imperv	vious Area	
	_			_			
	Tc	Length		lope	Velocity	Capacity	Description
_	(min)	(feet)) ((ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0	400	0.06		Sheet Flow, AB
							Woods: Dense underbrush n= 0.800 P2= 3.10"
	21.7	650	0.0	400	0.50		Shallow Concentrated Flow, BC
_							Forest w/Heavy Litter Kv= 2.5 fps
	50.5	750	To	tal			

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Summary for Subcatchment 3S:

Runoff = 77.47 cfs @ 12.81 hrs, Volume= 12.844 af, Depth> 4.28"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac)	CN	Desc	cription						
*	31.	320	70	WOODS / FIELD HSG C							
*	0.	000	98	EXIS	EXISTING IMPERVIOUS AREA						
*	4.	4.000 74		EXIS	STING LAV	VN C					
*	0.	210	74	NEW	NEW LAWN C						
*	0.	410	70	NEW	NEW FILL SLOPE						
*	0.	000	98	NEW	NEW IMPERVIOUS BUILDING AREA (See 51s)						
*	0.	100	98	NEV	/ Trails						
	36.	040	71	Weig	ghted Aver	age					
	35.	940		99.7	2% Pervio	us Area					
	0.	100		0.28	% Impervio	ous Area					
	Tc	Length		Slope	Velocity	Capacity	Description				
_	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)					
	28.8	100	0.	0400	0.06		Sheet Flow, AB				
							Woods: Dense underbrush n= 0.800 P2= 3.10"				
	15.0	450	0.	0400	0.50		Shallow Concentrated Flow, BC				
							Forest w/Heavy Litter Kv= 2.5 fps				
	16.5	75	5 0.	0900	0.08		Sheet Flow,				
_							Woods: Dense underbrush n= 0.800 P2= 3.10"				
	60.3	625	5 To	otal							

Summary for Subcatchment 4S:

Runoff = 30.35 cfs @ 12.78 hrs, Volume= 5.001 af, Depth> 4.62"

	Area (ac)	CN	Description
*	5.000	70	WOODS / FIELD HSG C
*	1.000	98	EXISTING IMPERVIOUS AREA
*	7.000	74	EXISTING LAWN C
*	0.000	98	NEW IMPERVIOUS PAVED AREA
*	0.000	74	NEW LAWN C
	13.000	74	Weighted Average
	12.000		92.31% Pervious Area
	1.000		7.69% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	28.8	100	0.0400	0.06	, ,	Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC
_						Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Total			

Summary for Subcatchment 5S: drains to 48" culvert

Runoff = 205.17 cfs @ 13.43 hrs, Volume= 51.121 af, Depth> 5.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac) (CN Des	scription					
*	47.	47.000 70		WOODS / FIELD HSG C					
*	36.000 98		98 EX	EXISTING IMPERVIOUS AREA					
*	35.	000	74 EX	EXISTING LAWN C					
-	118.	000	80 We	Weighted Average					
	82.	000	69.	49% Pervio	us Area				
	36.	000	30.	51% Imper	vious Area				
	Тс	Length	•	•	Capacity	Description			
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)				
	38.0	100	0.0200	0.04		Sheet Flow, AB			
						Woods: Dense underbrush n= 0.800 P2= 3.10"			
	60.0	900	0.0100	0.25		Shallow Concentrated Flow, BC			
						Forest w/Heavy Litter Kv= 2.5 fps			
	14.8	2,671	0.0400	3.00		Shallow Concentrated Flow, CD			
_						Grassed Waterway Kv= 15.0 fps			
	112.8	3,671	Total						

Summary for Subcatchment 6S: drains to 48" culvert

Runoff = 226.05 cfs @ 12.51 hrs, Volume= 29.982 af, Depth> 5.45"

	Area (ac)	CN	Description
*	6.000	70	WOODS / FIELD HSG C
*	20.000	98	EXISTING IMPERVIOUS AREA
*	40.000	74	EXISTING LAWN C
	66.000	81	Weighted Average
	46.000		69.70% Pervious Area
	20.000		30.30% Impervious Area

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	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
-	28.8	100	0.0400	0.06		Sheet Flow, AB
	5.0	900	0.0400	3.00		Woods: Dense underbrush n= 0.800 P2= 3.10" Shallow Concentrated Flow, BC Crossed Weterway, Kyz 15 0 fee
	3.7	2,500	0.0400	11.41	182.56	Grassed Waterway Kv= 15.0 fps Trap/Vee/Rect Channel Flow, CD Pet W=4.00', D=2.00', Z= 2.0 '/', Tep W=12.00'
_						Bot.W=4.00' D=2.00' Z= 2.0 '/' Top.W=12.00' n= 0.030 Earth, grassed & winding
	37.5	3 500	Total			

Summary for Subcatchment 7S:

Runoff = 70.86 cfs @ 12.12 hrs, Volume= 5.462 af, Depth> 5.96"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

_	Area	(ac) (CN E)esc	ription		
*	0.	000	70 V	VOC	DS / FIEL	D HSG C	
*	5.	000	98 E	EXIS	TING IMP	PERVIOUS	AREA
*	6.	000	74 E	XIS	TING LAV	VN C	
	11.	000	85 V	Veig	hted Aver	age	
6.000 54.55% Pervious Area						us Area	
	5.000 4			5.45	5% Imperv	vious Area	
_	Tc (min)	Length (feet)		pe /ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	7.5	100	0.04	00	0.22		Sheet Flow, AB
	1.1	200	0.04	00	3.00		Grass: Short n= 0.150 P2= 3.10" Shallow Concentrated Flow, BC Grassed Waterway Kv= 15.0 fps
	8.6	300	Tota	1		·	

Summary for Subcatchment 14S: 550 ROAD, 22' ROAD, 5' WALK to Forest Buffer

Runoff = 2.66 cfs @ 12.26 hrs, Volume= 0.284 af, Depth> 6.81"

	Area (ac)	CN	Description
*	0.400	98	NEW IMPERVIOUS PAVED AREA
*	0.100	74	NEW LAWN C
	0.500	93	Weighted Average
	0.100		20.00% Pervious Area
	0.400		80.00% Impervious Area

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	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	0.2	11	0.0300	1.02		Sheet Flow, AB
						Smooth surfaces n= 0.011 P2= 3.10"
	1.2	250	0.0300	3.52		Shallow Concentrated Flow, BC
						Paved Kv= 20.3 fps
	18.3	75	0.0700	0.07		Sheet Flow,
_						Woods: Dense underbrush n= 0.800 P2= 3.10"
	19 7	336	Total			

Summary for Subcatchment 15S: 600' ROAD, 22' ROAD, 5' WALK to Focal Points

Runoff = 4.55 cfs @ 12.02 hrs, Volume= 0.299 af, Depth> 6.52"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac) C	N Desc	cription		
*	* 0.370 98 NEW IMPERVIOUS PAVED AREA					
*	0.	180	74 NEV	V LAWN C		
0.550 90 Weighted Average						
	0.	180		3% Pervio	•	
0.370 67.27% Impervious Area						
•			•			
	Tc	Length	Slope	Velocity	Capacity	Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	0.2	11	0.0300	1.02		Sheet Flow, AB
						Smooth surfaces n= 0.011 P2= 3.10"
	1.2	250	0.0300	3.52		Shallow Concentrated Flow, BC
_						Paved Kv= 20.3 fps
	14	261	Total			

Summary for Subcatchment 16S: Arctic Fox Pond Watershed

Runoff = 11.13 cfs @ 12.77 hrs, Volume= 1.859 af, Depth> 5.30"

	Area (ac)	CN	Description			
*	0.570	70	WOODS / FIELD HSG C			
*	0.000	98	EXISTING IMPERVIOUS AREA			
*	0.000	74	EXISTING LAWN C			
*	1.100	98	NEW IMPERVIOUS PAVED AREA			
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (see 51s)			
*	2.540	74	NEW LAWN C			
	4.210	80	Weighted Average			
	3.110		73.87% Pervious Area			
	1.100		26.13% Impervious Area			

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	Tc	Length	Slope	,		Description
	(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	
	28.8	100	0.0400	0.06		Sheet Flow, AB
						Woods: Dense underbrush n= 0.800 P2= 3.10"
	30.0	900	0.0400	0.50		Shallow Concentrated Flow, BC
_						Forest w/Heavy Litter Kv= 2.5 fps
	58.8	1,000	Total			

Summary for Subcatchment 17S: Mallard Lane Pond Watershed

Runoff = 19.89 cfs @ 12.77 hrs, Volume= 3.346 af, Depth> 5.53"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac)	CN	Desc	cription					
*	0.	220	70	WOO	WOODS / FIELD HSG C					
*	0.	000	98	EXIS	EXISTING IMPERVIOUS AREA					
*	0.	000	74	EXIS	EXISTING LAWN C					
*	2.	400	98	NEW	NEW IMPERVIOUS PAVED AREA					
*	0.	000	98	NEW	NEW IMPERVIOUS BUILDING AREA (see 51s)					
*	4.	640	74	NEW	/ LAWN C		, , , , , , , , , , , , , , , , , , ,			
	7.	260	82	Weig	hted Aver	age				
4.860 66.94% Pervious Area										
	2.	400		33.0	6% Imperv	ious Area				
					-					
	Тс	Lengt	h	Slope	Velocity	Capacity	Description			
	(min)	(fee	t)	(ft/ft)	(ft/sec)	(cfs)				
	28.8	10	0 0	0.0400	0.06		Sheet Flow, AB			
							Woods: Dense underbrush n= 0.800 P2= 3.10"			
	30.0	90	0 0	0.0400	0.50		Shallow Concentrated Flow, BC			
							Forest w/Heavy Litter Kv= 2.5 fps			
	58.8	1,00	0 T	otal						

Summary for Subcatchment 18S:

Runoff = 2.75 cfs @ 12.69 hrs, Volume= 0.415 af, Depth> 4.40"

	Area (ac)	CN	Description
*	0.450	70	WOODS / FIELD HSG C
*	0.680	74	NEW LAWN C
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (see 51s)
	1.130	72	Weighted Average
	1.130		100.00% Pervious Area

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>
28.8	100	0.0400	0.06		Sheet Flow, AB
					Woods: Dense underbrush n= 0.800 P2= 3.10"
21.7	650	0.0400	0.50		Shallow Concentrated Flow, BC
					Forest w/Heavy Litter Kv= 2.5 fps
50.5	750	Total			

Summary for Subcatchment 19S:

Runoff = 68.81 cfs @ 12.13 hrs, Volume= 5.192 af, Depth> 4.47"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac)	CN	Desc	cription		
*	10.	660	70	WO	DDS / FIEL	D HSG C	
*	0.	600	98	EXIS	STING IMP	PERVIOUS	AREA
*	1.	600	74	EXIS	STING LAV	VN C	
*	0.	940	74	NEV	LAWN C		
*	0.	150	98	NEV	/ IMPERV	IOUS PAVI	ED AREA
*	0.	000	98	NEV	/ IMPERV	IOUS BUIL	DING AREA (See 51s)
	13.	950	72	Weig	hted Aver	age	
13.200 94.62% Pervious Area							
0.750 5.38% Impervious Area				5.38	% Impervio	ous Area	
					•		
	Tc	Length	1 5	Slope	Velocity	Capacity	Description
	(min)	(feet))	(ft/ft)	(ft/sec)	(cfs)	
	7.5	100	0.	0400	0.22		Sheet Flow, AB
							Grass: Short n= 0.150 P2= 3.10"
	1.7	300	0.	0400	3.00		Shallow Concentrated Flow, BC
							Grassed Waterway Kv= 15.0 fps
	9.2	400) To	otal			

Summary for Subcatchment 20S:

Runoff = 17.02 cfs @ 12.50 hrs, Volume= 2.140 af, Depth> 4.20"

	Area (ac)	CN	Description			
*	5.820	70	WOODS / FIELD HSG C			
*	0.000	98	EXISTING IMPERVIOUS AREA			
*	0.000	74	XISTING LAWN C			
*	0.290	74	NEW LAWN C			
*	0.000	98	NEW IMPERVIOUS BUILDING AREA (See 51s)			
_	6.110	70	Weighted Average			
	6.110		100.00% Pervious Area			

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Tc	Length	Slope	Velocity	Capacity	Description
(min)	(feet)	(ft/ft)	(ft/sec)	(cfs)	<u> </u>
28.8	100	0.0400	0.06		Sheet Flow, AB
					Woods: Dense underbrush n= 0.800 P2= 3.10"
6.7	200	0.0400	0.50		Shallow Concentrated Flow, BC
					Forest w/Heavy Litter Kv= 2.5 fps
35.5	300	Total			

Summary for Subcatchment 51S: NEW Cottage Roof Areas

Runoff = 19.15 cfs @ 12.21 hrs, Volume= 1.941 af, Depth> 7.23"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Type III 24-hr 100 YEAR Rainfall=8.10"

	Area	(ac) C	N Desc	cription		
* 3.220 98 52 Cottage Roofs + Community Buildings						nunity Buildings
	3.	220	220 100.00% Impe			l
	Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
	0.1	20	0.4000	3.25		Sheet Flow, AB
	2.5	25	0.0400	0.17		Smooth surfaces n= 0.011 P2= 3.10" Sheet Flow, BC
	2.5	25	0.0400	0.17		Grass: Short n= 0.150 P2= 3.10"
	13.1	75	0.1600	0.10		Sheet Flow, CD
_						Woods: Dense underbrush n= 0.800 P2= 3.10"
	15.7	120	Total			

Summary for Reach 3R: Stream @ Property Line

Inflow Area = 111.340 ac, 22.38% Impervious, Inflow Depth > 4.64" for 100 YEAR event

Inflow = 217.93 cfs @ 12.95 hrs, Volume= 43.053 af

Outflow = 217.18 cfs @ 13.02 hrs, Volume= 42.893 af, Atten= 0%, Lag= 4.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity = 5.86 fps, Min. Travel Time = 2.4 min Avg. Velocity = 2.44 fps, Avg. Travel Time = 5.9 min

Peak Storage= 31,916 cf @ 12.98 hrs Average Depth at Peak Storage= 2.55'

Bank-Full Depth= 3.00' Flow Area= 45.0 sf, Capacity= 287.21 cfs

12.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 860.0' Slope= 0.0058 '/'

Inlet Invert= 77.00', Outlet Invert= 72.00'

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Summary for Reach 4R: Stream below RR crossing

Inflow Area = 96.890 ac, 24.53% Impervious, Inflow Depth > 4.67" for 100 YEAR event

Inflow = 209.77 cfs @ 12.89 hrs, Volume= 37.702 af

Outflow = 209.03 cfs @ 12.96 hrs, Volume= 37.577 af, Atten= 0%, Lag= 4.1 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 6.21 fps, Min. Travel Time= 2.3 min Avg. Velocity = 2.77 fps, Avg. Travel Time= 5.2 min

Peak Storage= 28,997 cf @ 12.92 hrs Average Depth at Peak Storage= 3.54'

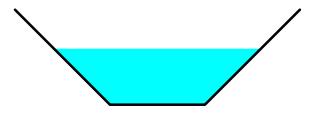
Bank-Full Depth= 6.00' Flow Area= 72.0 sf, Capacity= 582.42 cfs

6.00' x 6.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 860.0' Slope= 0.0058 '/'

Inlet Invert= 82.00', Outlet Invert= 77.00'



Summary for Reach 6R: Stream below Site @ PL

Inflow Area = 272.920 ac, 27.79% Impervious, Inflow Depth > 4.98" for 100 YEAR event

Inflow = 462.85 cfs @ 12.91 hrs, Volume= 113.295 af

Outflow = 462.13 cfs @ 12.94 hrs, Volume= 113.148 af, Atten= 0%, Lag= 1.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.96 fps, Min. Travel Time= 0.9 min

Avg. Velocity = 4.13 fps, Avg. Travel Time= 1.8 min

Peak Storage= 26,152 cf @ 12.92 hrs Average Depth at Peak Storage= 4.61'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf. Capacity= 538.97 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 61.00', Outlet Invert= 58.00'

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Summary for Reach 7R: Stream Through Site

257.100 ac, 26.89% Impervious, Inflow Depth > 5.10" for 100 YEAR event Inflow Area =

Inflow 443.48 cfs @ 12.86 hrs, Volume= 109.195 af

Outflow 442.48 cfs @ 12.91 hrs, Volume= 108.975 af, Atten= 0%, Lag= 2.7 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 12.62 fps. Min. Travel Time= 1.5 min Avg. Velocity = 6.37 fps, Avg. Travel Time= 2.9 min

Peak Storage= 38,590 cf @ 12.88 hrs Average Depth at Peak Storage= 3.15'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 683.45 cfs

8.00' x 4.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00'

Length= 1,100.0' Slope= 0.0245 '/'

Inlet Invert= 88.00', Outlet Invert= 61.00'



Summary for Reach 14R: Swale from School and Neighborhood

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 2.53" for 100 YEAR event

5.29 cfs @ 13.59 hrs, Volume= Inflow 2.323 af

5.15 cfs @ 14.25 hrs, Volume= Outflow 2.167 af, Atten= 3%, Lag= 40.0 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 2.59 fps, Min. Travel Time= 21.7 min

Avg. Velocity = 1.53 fps, Avg. Travel Time= 36.7 min

Peak Storage= 6,698 cf @ 13.89 hrs Average Depth at Peak Storage= 0.45'

Bank-Full Depth= 3.00' Flow Area= 21.0 sf, Capacity= 147.12 cfs

4.00' x 3.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 10.00'

Length= 3,366.0' Slope= 0.0100 '/'

Inlet Invert= 117.66', Outlet Invert= 84.00'

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Summary for Reach 17R:

Inflow Area = 8.390 ac, 28.61% Impervious, Inflow Depth > 4.48" for 100 YEAR event

Inflow = 20.11 cfs @ 13.06 hrs, Volume= 3.131 af

Outflow = 20.09 cfs @ 13.10 hrs, Volume= 3.123 af, Atten= 0%, Lag= 2.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 7.68 fps, Min. Travel Time= 1.5 min Avg. Velocity = 3.18 fps, Avg. Travel Time= 3.7 min

Peak Storage= 1,832 cf @ 13.08 hrs Average Depth at Peak Storage= 0.87'

Bank-Full Depth= 3.00' Flow Area= 9.0 sf, Capacity= 102.76 cfs

3.00' x 3.00' deep channel, n= 0.022 Earth, clean & straight Length= 700.0' Slope= 0.0286 '/' Inlet Invert= 81.00', Outlet Invert= 61.00'

| |



Summary for Reach 18R: Stream Through Site

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 5.22" for 100 YEAR event

Inflow = 310.32 cfs @ 12.61 hrs, Volume= 79.993 af

Outflow = 309.46 cfs @ 12.67 hrs, Volume= 79.772 af, Atten= 0%, Lag= 3.6 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity = 9.93 fps, Min. Travel Time = 2.0 min Avg. Velocity = 4.83 fps, Avg. Travel Time = 4.1 min

Peak Storage= 37,431 cf @ 12.64 hrs Average Depth at Peak Storage= 2.87'

Bank-Full Depth= 4.00' Flow Area= 48.0 sf, Capacity= 563.18 cfs

 $8.00' \times 4.00'$ deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 16.00' Length= 1,200.0' Slope= 0.0167 '/'

Inlet Invert= 125.00', Outlet Invert= 105.00'

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Summary for Reach 55R: Wetland below Site @ PL

Inflow Area = 36.040 ac, 0.28% Impervious, Inflow Depth > 4.28" for 100 YEAR event

Inflow = 77.47 cfs @ 12.81 hrs, Volume= 12.844 af

Outflow = 77.22 cfs @ 12.86 hrs, Volume= 12.813 af, Atten= 0%, Lag= 2.9 min

Routing by Stor-Ind+Trans method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Max. Velocity= 4.77 fps, Min. Travel Time= 1.6 min Avg. Velocity = 2.12 fps, Avg. Travel Time= 3.5 min

Peak Storage= 7,300 cf @ 12.83 hrs Average Depth at Peak Storage= 1.68'

Bank-Full Depth= 5.00' Flow Area= 65.0 sf, Capacity= 540.76 cfs

8.00' x 5.00' deep channel, n= 0.030 Stream, clean & straight

Side Slope Z-value= 1.0 '/' Top Width= 18.00'

Length= 450.0' Slope= 0.0067 '/'

Inlet Invert= 63.02', Outlet Invert= 60.00'



Summary for Pond 1P: 1-30" and 1-24" Culvert at Tuttle Road

Inflow Area = 111.340 ac, 22.38% Impervious, Inflow Depth > 4.58" for 100 YEAR event

Inflow = 212.26 cfs @ 13.12 hrs, Volume= 42.524 af

Outflow = 212.20 cfs @ 13.13 hrs, Volume= 42.462 af, Atten= 0%, Lag= 0.6 min

Primary = 65.67 cfs @ 13.13 hrs, Volume= 28.273 af Secondary = 146.54 cfs @ 13.13 hrs, Volume= 14.190 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 72.07' @ 13.13 hrs Surf.Area= 7,952 sf Storage= 23,430 cf

Plug-Flow detention time= 2.9 min calculated for 42.462 af (100% of inflow)

Center-of-Mass det. time= 2.4 min (844.8 - 842.4)

Volume	Invert	Avail.Storage	Storage Description
#1	68.00'	31,683 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation		on	Surf.Area	Inc.Store Cum.Store					
(feet)		et)	(sq-ft)	(cubic-feet)	(cubic-feet)				
68.00		00	3,850	0	0				
	70.0	00	5,600	9,450	9,450				
	72.0	00	7,800	13,400	22,850				
	73.0	00	9,865	8,833	31,683				
	Device	Routing	Invert	Outlet Devices					
	#1	Primary	67.50'	30.0" Round C	ulvert				
				L= 50.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900					
				n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf					
	#2	Primary	67.50'	24.0" Round Culvert					
				L= 50.0' CPP,	= 50.0' CPP, projecting, no headwall, Ke= 0.900				
				Inlet / Outlet Invert= 67.50' / 66.50' S= 0.0200 '/' Cc= 0.900					
						or, Flow Area= 3.14 sf			
	#3	Seconda	ry 71.00'			Broad-Crested Rectangular Weir			
				Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60					

Primary OutFlow Max=65.66 cfs @ 13.13 hrs HW=72.07' (Free Discharge)

1=Culvert (Inlet Controls 43.08 cfs @ 8.78 fps)

-2=Culvert (Inlet Controls 22.57 cfs @ 7.19 fps)

Secondary OutFlow Max=146.32 cfs @ 13.13 hrs HW=72.07' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 146.32 cfs @ 2.73 fps)

Summary for Pond 2P: Two 30" Culverts at Crossing Brook Road

Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

272.920 ac, 27.79% Impervious, Inflow Depth > 4.98" for 100 YEAR event Inflow Area = Inflow 462.13 cfs @ 12.94 hrs, Volume= 113.148 af 234.77 cfs @ 14.42 hrs, Volume= Outflow = 91.982 af, Atten= 49%, Lag= 89.0 min Primary = 124.48 cfs @ 14.42 hrs, Volume= 76.018 af 110.29 cfs @ 14.42 hrs, Volume= Secondary = 15.963 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 57.41' @ 14.42 hrs Surf.Area= 241,122 sf Storage= 1,884,664 cf

Plug-Flow detention time= 133.1 min calculated for 91.676 af (81% of inflow) Center-of-Mass det. time= 88.0 min (942.1 - 854.1)

Volume	Invert	Avail.Storage	Storage Description
#1	44.00'	2,030,000 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
44.00	60,000	0	0
46.00	80,000	140,000	140,000
48.00	100,000	180,000	320,000
50.00	120,000	220,000	540,000
52.00	160,000	280,000	820,000
54.00	180,000	340,000	1,160,000
56.00	220,000	400,000	1,560,000
58.00	250,000	470,000	2,030,000

Device	Routing	Invert	Outlet Devices
#1	Primary	44.00'	30.0" Round Culvert
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 44.00' / 42.00' S= 0.0400 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 4.91 sf
#2	Primary	44.00'	24.0" Round Culvert
			L= 50.0' CPP, projecting, no headwall, Ke= 0.900
			Inlet / Outlet Invert= 44.00' / 42.00' S= 0.0400 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 3.14 sf
#3	Secondary	56.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=124.48 cfs @ 14.42 hrs HW=57.41' (Free Discharge)

1=Culvert (Inlet Controls 82.41 cfs @ 16.79 fps)

2=Culvert (Inlet Controls 42.07 cfs @ 13.39 fps)

Secondary OutFlow Max=110.18 cfs @ 14.42 hrs HW=57.41' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 110.18 cfs @ 3.13 fps)

Summary for Pond 3P: 24" CULVERT

Inflow Area =	36.040 ac,	0.28% Impervious, Inflow	Depth > 4.27"	for 100 YEAR event
Inflow =	77.22 cfs @	12.86 hrs, Volume=	12.813 af	
Outflow =	76.14 cfs @	12.94 hrs, Volume=	12.751 af, Att	en= 1%, Lag= 4.6 min
Primary =	32.97 cfs @	12.94 hrs, Volume=	10.338 af	•
Secondary =	43.17 cfs @	12.94 hrs. Volume=	2.413 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 59.75' @ 12.94 hrs Surf.Area= 18,753 sf Storage= 51,510 cf

Plug-Flow detention time= 13.6 min calculated for 12.709 af (99% of inflow) Center-of-Mass det. time= 11.8 min (845.1 - 833.3)

Volume	Invert	Avail.Storage	Storage Description
#1	54.00'	56.342 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	on	Surf.Area	Inc.Store	Cum.Store	
(fee	et)	(sq-ft)	(cubic-feet)	(cubic-feet)	
54.0	00	2,362	0	0	
56.0	00	6,990	9,352	9,352	
58.0	00	10,000	16,990	26,342	
60.0	00	20,000	30,000	56,342	
Device	Routing	Invert	Outlet Devices		
#1	Primary	54.00'	24.0" Round C	Culvert	
	-		L= 50.0' RCP,	sq.cut end pro	ojecting, Ke= 0.500
			Inlet / Outlet Inv	/ert= 54.00' / 5	3.00' S= 0.0200 '/' Cc= 0.900
			n= 0.011 Conc	rete pipe, strai	ght & clean, Flow Area= 3.14 sf
#2	Seconda	ry 59.00'	25.0' long x 25	5.0' breadth B	road-Crested Rectangular Weir
			Head (feet) 0.2	0.40 0.60	0.80 1.00 1.20 1.40 1.60

Primary OutFlow Max=32.97 cfs @ 12.94 hrs HW=59.75' (Free Discharge) 1=Culvert (Inlet Controls 32.97 cfs @ 10.49 fps)

Secondary OutFlow Max=43.07 cfs @ 12.94 hrs HW=59.75' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 43.07 cfs @ 2.30 fps)

Summary for Pond 4P: 18" CULVERT

Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Inflow Area =	13.000 ac,	7.69% Impervious, Inflow D	epth > 4.62" for 100 YEAR event
Inflow =	30.35 cfs @	12.78 hrs, Volume=	5.001 af
Outflow =	15.83 cfs @	13.43 hrs, Volume=	4.943 af, Atten= 48%, Lag= 39.0 min
Primary =	15.41 cfs @	13.43 hrs, Volume=	4.937 af
Secondary =	0.43 cfs @	13.43 hrs, Volume=	0.006 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 89.03' @ 13.43 hrs Surf.Area= 24,770 sf Storage= 56,147 cf

Plug-Flow detention time= 40.7 min calculated for 4.943 af (99% of inflow) Center-of-Mass det. time= 36.5 min (860.4 - 823.9)

Volume	Inver	t Avail.Sto	rage Storag	e Description	
#1	85.00)' 82,7	55 cf Custo	m Stage Data (Prismatio)Listed below (Recalc)
Elevatio	-	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.0	00	3,343	0	0	
86.0	00	8,410	5,877	5,877	
88.0	00	19,234	27,644	33,521	
90.0	00	30,000	49,234	82,755	
Device	Routing	Invert	Outlet Devi	es	
#1	Primary	85.00'	18.0" Rou	nd Culvert	
				CP, sq.cut end projecting,	
				Invert= 85.00' / 84.00' S	
40	0			oncrete pipe, straight & cl	
#2	Secondar	y 89.00'	25.0 long	k 25.0' breadth Broad-Cr	ested Rectangular Weir

Volume

Invert

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Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.63

Primary OutFlow Max=15.40 cfs @ 13.43 hrs HW=89.03' (Free Discharge)
1=Culvert (Inlet Controls 15.40 cfs @ 8.72 fps)

Secondary OutFlow Max=0.31 cfs @ 13.43 hrs HW=89.03' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 0.31 cfs @ 0.45 fps)

Summary for Pond 5P: 4'x3' Oval and 30" Overflow Culvert

Inflow Area =	184.000 ac, 3	30.43% Impervious,	Inflow Depth > 5.2	29" for 100 YEAR event
Inflow =	310.62 cfs @	12.59 hrs, Volume	= 81.103 af	
Outflow =	310.32 cfs @	12.61 hrs, Volume	= 79.993 af,	Atten= 0%, Lag= 1.3 min
Primary =	43.18 cfs @	12.61 hrs, Volume	= 30.794 af	
Secondary =	267.14 cfs @	12.61 hrs, Volume	= 49.198 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 138.42' @ 12.61 hrs Surf.Area= 21,043 sf Storage= 106,292 cf

Plug-Flow detention time= 14.3 min calculated for 79.727 af (98% of inflow) Center-of-Mass det. time= 9.6 min (842.4 - 832.8)

Avail Storage Storage Description

Volume	IIIVEIL	Avaii.0t0	rage Storage	Description		
#1	129.00'	142,73	35 cf Custom	Stage Data (Pri	ismatic)Listed below (Recalc)	
Elevation (fee		urf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)		
129.0		4,441	0	0		
130.0		6,196	5,319	5,319		
132.0		8,225	14,421	19,740		
134.0		10,880	19,105	38,845		
136.0		14,005	24,885	63,730		
138.0		20,000	34,005	97,735		
140.0		25,000	45,000	142,735		
		-,	-,	,		
Device	Routing	Invert	Outlet Devices	3		
#1	Primary	129.00'	4.0" W x 3.0"	H, R=3.0" Ellip	tical Culvert	
	,				jecting, Ke= 0.500	
			Inlet / Outlet Ir	nvert= 129.00' / 1	128.00' S= 0.0333 '/' Cc= 0.900	
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 0.07 sf			
#2	Primary	132.00'	30.0" Round	Culvert		
			L= 50.0' CPF	P, projecting, no	headwall, Ke= 0.900	
					128.00' S= 0.0800 '/' Cc= 0.900	
				,	r, Flow Area= 4.91 sf	
#3	Secondary	137.00'			oad-Crested Rectangular Weir	
			` ,		0.80 1.00 1.20 1.40 1.60	
			Coef. (English	i) 2.68 2.70 2.7	70 2.64 2.63 2.64 2.64 2.63	

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Primary OutFlow Max=43.17 cfs @ 12.61 hrs HW=138.42' (Free Discharge)

1=Culvert (Barrel Controls 0.77 cfs @ 11.39 fps)
2=Culvert (Inlet Controls 42.41 cfs @ 8.64 fps)

Secondary OutFlow Max=266.71 cfs @ 12.61 hrs HW=138.42' (Free Discharge) 3=Broad-Crested Rectangular Weir (Weir Controls 266.71 cfs @ 3.14 fps)

Summary for Pond 6P: 1-48" Culvert Crossing Golf Cart Path

Inflow Area = 184.000 ac, 30.43% Impervious, Inflow Depth > 5.20" for 100 YEAR event

Inflow = 309.46 cfs @ 12.67 hrs, Volume= 79.772 af

Outflow = 285.90 cfs @ 12.94 hrs, Volume= 79.464 af, Atten= 8%, Lag= 16.1 min

Primary = 157.89 cfs @ 12.94 hrs, Volume= 64.473 af Secondary = 128.01 cfs @ 12.94 hrs, Volume= 14.991 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 104.81' @ 12.94 hrs Surf.Area= 58,728 sf Storage= 269,120 cf

Plug-Flow detention time= 15.3 min calculated for 79.200 af (99% of inflow)

Center-of-Mass det. time= 13.9 min (860.1 - 846.2)

Volume	Invert	Avail.Storage	Storage	Description	
#1	96.00' 280,448 cf		Custom Stage Data (Prismatic)Listed below (Recalc)		
Elevation			c.Store	Cum.Store	

Elevation	Suri.Area	inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
96.00	1,580	0	0
98.00	14,434	16,014	16,014
100.00	30,000	44,434	60,448
102.00	40,000	70,000	130,448
105.00	60,000	150,000	280,448

Device	Routing	Invert	Outlet Devices
#1	Primary	96.00'	48.0" Round Culvert
	•		L= 30.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 96.00' / 95.00' S= 0.0333 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 12.57 sf
#2	Secondary	103.00'	20.0' long x 20.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=157.88 cfs @ 12.94 hrs HW=104.81' (Free Discharge)
1=Culvert (Inlet Controls 157.88 cfs @ 12.56 fps)

Secondary OutFlow Max=127.90 cfs @ 12.94 hrs HW=104.81' (Free Discharge) 2=Broad-Crested Rectangular Weir (Weir Controls 127.90 cfs @ 3.54 fps)

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Summary for Pond 7P: 1-24" Culvert at Greely Middle School

Inflow Area = 11.000 ac, 45.45% Impervious, Inflow Depth > 5.96" for 100 YEAR event Inflow

70.86 cfs @ 12.12 hrs, Volume= 5.462 af

5.29 cfs @ 13.59 hrs, Volume= Outflow 2.323 af, Atten= 93%, Lag= 88.0 min

5.29 cfs @ 13.59 hrs, Volume= 2.323 af Primary Secondary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

Peak Elev= 126.27' @ 13.59 hrs Surf.Area= 33,165 sf Storage= 153,967 cf

Plug-Flow detention time= 234.9 min calculated for 2.323 af (43% of inflow)

Center-of-Mass det. time= 139.3 min (901.6 - 762.3)

Volume	Invert	Avail.Storage	Storage Description
#1	120.00'	214,248 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
120.00	18,593	0	0
122.00	21,745	40,338	40,338
124.00	25,131	46,876	87,214
126.00	32,605	57,736	144,950
128.00	36,693	69,298	214,248

Device	Routing	Invert	Outlet Devices
#1	Primary	120.00'	24.0" Round Culvert
			L= 80.0' RCP, sq.cut end projecting, Ke= 0.500
			Inlet / Outlet Invert= 120.00' / 119.00' S= 0.0125 '/' Cc= 0.900
			n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf
#2	Secondary	127.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
	•		Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63
#3	Device 1	120.00'	6.0" Vert. Orifice/Grate C= 0.600
#4	Device 1	126.00'	24.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads

Primary OutFlow Max=5.27 cfs @ 13.59 hrs HW=126.27' (Free Discharge)

-1=Culvert (Passes 5.27 cfs of 34.74 cfs potential flow)

-3=Orifice/Grate (Orifice Controls 2.32 cfs @ 11.82 fps)

-4=Orifice/Grate (Weir Controls 2.95 cfs @ 1.71 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=120.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 10P: 1-30" Culvert

Inflow Area =	111.340 ac, 2	2.38% Impervious,	Inflow Depth > 4.6	32" for 100 YEAR event
Inflow =	217.18 cfs @	13.02 hrs, Volume:	= 42.893 af	
Outflow =	212.26 cfs @	13.12 hrs, Volume:	= 42.524 af,	Atten= 2%, Lag= 6.2 min
Primary =	44.93 cfs @	13.12 hrs, Volume:	= 22.888 af	•
Secondary =	167.33 cfs @	13.12 hrs, Volume:	= 19.636 af	

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Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 72.86' @ 13.12 hrs Surf.Area= 58.824 sf Storage= 141.729 cf

Plug-Flow detention time= 16.2 min calculated for 42.524 af (99% of inflow)

Center-of-Mass det. time= 13.1 min (842.4 - 829.3)

Volume	Inve	rt Avail.Sto	rage	Storage	Description	
#1	68.0	0' 211,04	48 cf	Custom	Stage Data (P	rismatic)Listed below (Recalc)
Elevation		Surf.Area		:.Store	Cum.Store	
(fee		(sq-ft)	(Cubi	c-feet)	(cubic-feet)	
68.0		8,000		0	0	
70.0		14,434		22,434	22,434	
72.0	00	55,480	6	69,914	92,348	
74.0	00	63,220	11	18,700	211,048	
Device	Routing	Invert	Outl	et Devices	3	
#1	Primary	68.00'	30.0	" Round	Culvert	
#2	Seconda	ry 71.00'	Inlet n= 0 25.0 Hea	/ Outlet In 0.011 Cor ' long x 2 d (feet) 0	nvert= 68.00' / 6 acrete pipe, strai 2 5.0' breadth B .20 0.40 0.60	ojecting, Ke= 0.500 67.00' S= 0.0333 '/' Cc= 0.900 ight & clean, Flow Area= 4.91 sf road-Crested Rectangular Weir 0.80 1.00 1.20 1.40 1.60 70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=44.92 cfs @ 13.12 hrs HW=72.86' (Free Discharge) 1=Culvert (Inlet Controls 44.92 cfs @ 9.15 fps)

Secondary OutFlow Max=167.12 cfs @ 13.12 hrs HW=72.86' (Free Discharge) **-2=Broad-Crested Rectangular Weir** (Weir Controls 167.12 cfs @ 3.59 fps)

Summary for Pond 15P: FocalPoint 60sf

Inflow Area =	0.550 ac, 67.27% Impervious, Inflow D	epth > 6.52" for 100 YEAR event
Inflow =	4.55 cfs @ 12.02 hrs, Volume=	0.299 af
Outflow =	4.52 cfs @ 12.03 hrs, Volume=	0.299 af, Atten= 1%, Lag= 0.3 min
Primary =	0.14 cfs @ 9.45 hrs, Volume=	0.126 af
Secondary =	4.38 cfs @ 12.03 hrs, Volume=	0.173 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 100.93' @ 12.03 hrs Surf.Area= 60 sf Storage= 149 cf

Plug-Flow detention time= 2.6 min calculated for 0.299 af (100% of inflow) Center-of-Mass det. time= 2.6 min (748.6 - 746.0)

Volume	Invert	Avail.Storage	Storage Description
#1	97.75'	27 cf	3.00'W x 20.00'L x 2.25'H FocalPoint
			135 cf Overall x 20.0% Voids
#2	100.00'	133 cf	Custom Stage Data (Prismatic)Listed below (Recalc) -Impervious
		160 cf	Total Available Storage

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
100.00	60	0	0
100.50	157	54	54
101.00	157	79	133

Device	Routing	Invert	Outlet Devices	
#1	Primary	97.75'	100.000 in/hr Exfiltration over Surface area Phase-In= 0.10'	
#2	Secondary	100.50'	18.0" Horiz. Orifice/Grate C= 0.600	
			Limited to weir flow at low heads	

Primary OutFlow Max=0.14 cfs @ 9.45 hrs HW=97.91' (Free Discharge) 1=Exfiltration (Exfiltration Controls 0.14 cfs)

Secondary OutFlow Max=4.19 cfs @ 12.03 hrs HW=100.92' (Free Discharge) 2=Orifice/Grate (Weir Controls 4.19 cfs @ 2.12 fps)

Summary for Pond 16P: Arctic Fox WET POND

Inflow Area =	4.210 ac, 26.13% Impervious, Inflow	v Depth > 5.30" for 100 YEAR event
Inflow =	11.13 cfs @ 12.77 hrs, Volume=	1.859 af
Outflow =	6.50 cfs @ 13.33 hrs, Volume=	1.197 af, Atten= 42%, Lag= 33.8 min
Primary =	6.50 cfs @ 13.33 hrs, Volume=	1.197 af
Secondary =	0.00 cfs @ 5.00 hrs, Volume=	0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 77.00' Surf.Area= 4,505 sf Storage= 18,632 cf Peak Elev= 81.24' @ 13.33 hrs Surf.Area= 12,016 sf Storage= 59,284 cf (40,653 cf above start)

Plug-Flow detention time= 275.3 min calculated for 0.766 af (41% of inflow) Center-of-Mass det. time= 113.6 min (926.6 - 813.0)

Volume	Invert	Avail.Storage	Storage Description
#1	71.00'	82,315 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation (feet)	Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)
(ieet)		(Cubic-leet)	(Cubic-leet)
71.00	1,852	0	0
72.00	2,232	2,042	2,042
73.00	2,636	2,434	4,476
74.00	3,065	2,851	7,327
75.00	3,520	3,293	10,619
76.00	4,000	3,760	14,379
77.00	4,505	4,253	18,632
77.10	7,408	596	19,227
78.00	8,400	7,114	26,341
79.00	9,450	8,925	35,266
80.00	10,557	10,004	45,269
81.00	11,720	11,139	56,408
82.00	12,940	12,330	68,738
83.00	14,215	13,578	82,315

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Device	Routing	Invert	Outlet Devices
#1	Primary	74.00'	18.0" Round Culvert
			L= 58.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 74.00' / 70.00' S= 0.0690 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	78.50'	6.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	81.00'	48.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	81.50'	10.0' long x 10.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=6.38 cfs @ 13.33 hrs HW=81.24' (Free Discharge)

1=Culvert (Passes 6.38 cfs of 21.68 cfs potential flow)

2=Orifice/Grate (Orifice Controls 1.49 cfs @ 7.60 fps)

3=Orifice/Grate (Weir Controls 4.89 cfs @ 1.61 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=77.00' (Free Discharge)

4=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 17P: Mallard Way WET POND

Inflow Area =	7.260 ac, 33.06% Impervious, In	nflow Depth > 5.53" for 100 YEAR event
Inflow =	19.89 cfs @ 12.77 hrs, Volume=	3.346 af
Outflow =	18.97 cfs @ 12.91 hrs, Volume=	2.725 af, Atten= 5%, Lag= 8.7 min
Primary =	17.80 cfs @ 12.91 hrs, Volume=	2.689 af
Secondary =	1.17 cfs @ 12.91 hrs, Volume=	0.036 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Starting Elev= 88.00' Surf.Area= 5,558 sf Storage= 23,438 cf

Peak Elev= 91.13' @ 12.91 hrs Surf.Area= 13,435 sf Storage= 58,656 cf (35,218 cf above start)

Plug-Flow detention time= 131.6 min calculated for 2.179 af (65% of inflow) Center-of-Mass det. time= 41.5 min (850.5 - 809.0)

Volume	Invert	Avail.Storage	Storage Description
#1	81.00'	70,904 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

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Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
81.00	1,346	0	0
82.00	1,867	1,607	1,607
83.00	2,419	2,143	3,750
84.00	2,996	2,708	6,457
85.00	3,599	3,298	9,755
86.00	4,226	3,913	13,667
87.00	4,879	4,553	18,220
88.00	5,558	5,219	23,438
88.10	9,325	744	24,182
89.00	10,578	8,956	33,139
90.00	11,887	11,233	44,371
91.00	13,252	12,570	56,941
92.00	14,675	13,964	70,904

Device	Routing	Invert	Outlet Devices
#1	Primary	86.00'	18.0" Round Culvert L= 31.0' RCP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 86.00' / 85.50' S= 0.0161 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	89.50'	6.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	90.50'	48.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	91.00'	10.0' long x 10.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=17.80 cfs @ 12.91 hrs HW=91.13' (Free Discharge)

-1=Culvert (Inlet Controls 17.80 cfs @ 10.07 fps)

2=Orifice/Grate (Passes < 1.11 cfs potential flow)
3=Orifice/Grate (Passes < 20.44 cfs potential flow)

Secondary OutFlow Max=1.14 cfs @ 12.91 hrs HW=91.13' (Free Discharge) **-4=Broad-Crested Rectangular Weir** (Weir Controls 1.14 cfs @ 0.89 fps)

Summary for Pond 18P: 24" CULVERT

Inflow Area = 8.390 ac, 28.61% Impervious, Inflow Depth > 4.49" for 100 YEAR event

Inflow 21.43 cfs @ 12.87 hrs, Volume= 3.139 af

20.11 cfs @ 13.06 hrs, Volume= Outflow = 3.131 af, Atten= 6%, Lag= 11.5 min

20.11 cfs @ 13.06 hrs, Volume= Primary 3.131 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 87.77' @ 13.06 hrs Surf.Area= 5,221 sf Storage= 7,357 cf

Plug-Flow detention time= 4.9 min calculated for 3.121 af (99% of inflow) Center-of-Mass det. time= 4.0 min (850.5 - 846.6)

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Volume	Inv	ert Avail.Sto	rage Storag	e Description	
#1	85.	00' 15,8	69 cf Custor	n Stage Data (Prismatic)և	isted below (Recalc)
Elevation (fee		Surf.Area (sq-ft)	Inc.Store (cubic-feet)	Cum.Store (cubic-feet)	
85.0	00	788	0	0	
86.0	00	1,512	1,150	1,150	
87.0	00	3,898	2,705	3,855	
88.0	00	5,621	4,760	8,615	
89.0	00	8,888	7,255	15,869	
Device	Routing	Invert	Outlet Devic	es	
#1	Primary	85.00'	24.0" Roun	d Culvert	
			L= 50.0' RCP, sq.cut end projecting, Ke= 0.500 Inlet / Outlet Invert= 85.00' / 84.50' S= 0.0100 '/' Cc= 0.900 n= 0.011 Concrete pipe, straight & clean, Flow Area= 3.14 sf		

Primary OutFlow Max=20.10 cfs @ 13.06 hrs HW=87.77' (Free Discharge) 1=Culvert (Inlet Controls 20.10 cfs @ 6.40 fps)

Summary for Pond 20P: Arch Culvert 1

Inflow Area =	96.890 ac, 2	4.53% Impervious, I	nflow Depth > 4.6	7" for 100 YEAR event
Inflow =	214.82 cfs @	12.78 hrs, Volume=	37.715 af	
Outflow =	209.77 cfs @	12.89 hrs, Volume=	37.702 af,	Atten= 2%, Lag= 6.6 min
Primary =	209.77 cfs @	12.89 hrs, Volume=	37.702 af	-
Secondary =	0.00 cfs @	5.00 hrs, Volume=	0.000 af	

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 88.24' @ 12.89 hrs Surf.Area= 13,654 sf Storage= 24,713 cf

Plug-Flow detention time= 1.0 min calculated for 37.702 af (100% of inflow) Center-of-Mass det. time= 0.9 min (825.6 - 824.7)

Volume	In	vert Avai	l.Storage	Storage	Description	
#1	82	.00'	35,094 cf	Custom	Stage Data (Pr	rismatic)Listed below (Recalc)
Elevation (fee		Surf.Area (sq-ft)		.Store c-feet)	Cum.Store (cubic-feet)	
82.0	00	320		0	0	
86.0	00	2,932		6,504	6,504	
87.0	00	7,643		5,288	11,792	
88.0	00	11,989		9,816	21,608	
89.0	00	18,865	1	5,427	37,035	
90.0	00	23,627	2	21,246	58,281	
91.0	00	30,000	2	26,814	85,094	
Device	Routing	g Inv	vert Outle	et Devices	3	
#1	Primary	82.			•	26.0" Pipe Arch RCP_Arch 88x54 onforming to fill, Ke= 0.500

L= 70.0' RCP, end-section conforming to fill, Ke= 0.500 Inlet / Outlet Invert= 82.00' / 81.50' S= 0.0071 '/' Cc= 0.900

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n= 0.022 Earth, clean & straight, Flow Area= 25.69 sf #2 Secondary 90.00'

25.0' long x 25.0' breadth Broad-Crested Rectangular Weir

Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 Coef. (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

Primary OutFlow Max=209.49 cfs @ 12.89 hrs HW=88.24' (Free Discharge)

1=RCP Arch 88x54 (Barrel Controls 209.49 cfs @ 8.16 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=82.00' (Free Discharge) -2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 21P: Arch Culvert 2

Inflow Area = 190.110 ac, 29.46% Impervious, Inflow Depth > 5.15" for 100 YEAR event

Inflow 295.09 cfs @ 12.92 hrs, Volume= 81.604 af

290.85 cfs @ 13.04 hrs, Volume= Outflow = 81.447 af, Atten= 1%, Lag= 7.4 min

290.85 cfs @ 13.04 hrs, Volume= 81.447 af Primary 0.00 cfs @ 5.00 hrs, Volume= Secondary = 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 97.31' @ 13.04 hrs Surf.Area= 26,283 sf Storage= 55,790 cf

Plug-Flow detention time= 3.1 min calculated for 81.176 af (99% of inflow)

Center-of-Mass det. time= 2.4 min (861.2 - 858.8)

Volume	Invert	Avail.Storage	Storage Description
#1	92.00'	200,953 cf	Custom Stage Data (Prismatic)Listed below (Recalc)

Elevation	Surf.Area	Inc.Store	Cum.Store
(feet)	(sq-ft)	(cubic-feet)	(cubic-feet)
92.00	5,000	0	0
93.00	6,000	5,500	5,500
94.00	7,000	6,500	12,000
95.00	8,390	7,695	19,695
96.00	12,267	10,329	30,024
97.00	23,771	18,019	48,043
98.00	31,886	27,829	75,871
99.00	67,139	49,513	125,384
100.00	84,000	75,570	200,953

Device	Routing	Invert	Outlet Devices
#1	Primary	92.00'	122.0" W x 77.3" H, R=62.0"/218.0" Pipe Arch RCP_Arch 122x78
	•		L= 70.0' RCP, end-section conforming to fill, Ke= 0.500
			Inlet / Outlet Invert= 92.00' / 91.50' S= 0.0071 '/' Cc= 0.900
			n= 0.022 Earth, clean & straight, Flow Area= 51.67 sf
#2	Secondary	99.00'	25.0' long x 25.0' breadth Broad-Crested Rectangular Weir
			Head (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60
			Coef (English) 2.68 2.70 2.70 2.64 2.63 2.64 2.64 2.63

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Primary OutFlow Max=290.75 cfs @ 13.04 hrs HW=97.31' (Free Discharge)
1=RCP Arch 122x78 (Barrel Controls 290.75 cfs @ 8.00 fps)

Secondary OutFlow Max=0.00 cfs @ 5.00 hrs HW=92.00' (Free Discharge) 2=Broad-Crested Rectangular Weir (Controls 0.00 cfs)

Summary for Pond 24P: Cultec Recharger 150XLHD

Inflow Area =	0.550 ac, 67.27% Impervious, Inflow	Depth > 6.52" for 100 YEAR event
Inflow =	4.52 cfs @ 12.03 hrs, Volume=	0.299 af
Outflow =	4.98 cfs @ 12.01 hrs, Volume=	0.297 af, Atten= 0%, Lag= 0.0 mir
Primary =	3.02 cfs @ 12.01 hrs, Volume=	0.256 af
Secondary =	1.96 cfs @ 12.01 hrs, Volume=	0.041 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs Peak Elev= 96.81' @ 12.01 hrs Surf.Area= 0.025 ac Storage= 0.036 af

Plug-Flow detention time= 33.8 min calculated for 0.297 af (99% of inflow) Center-of-Mass det. time= 30.9 min (779.5 - 748.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	94.00'	0.018 af	14.50'W x 74.50'L x 2.54'H Field A
			0.063 af Overall - 0.018 af Embedded = 0.045 af x 40.0% Voids
#2A	94.50'	0.018 af	Cultec R-150XLHD x 28 Inside #1
			Effective Size= 29.8"W x 18.0"H => 2.65 sf x 10.25'L = 27.2 cf
			Overall Size= 33.0"W x 18.5"H x 11.00'L with 0.75' Overlap
			Row Length Adjustment= +0.75' x 2.65 sf x 4 rows
#3	96.50'	0.001 af	4.00'D x 4.00'H Vertical Cone/Cylinder
		0.037 af	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	94.00'	18.0" Round Culvert
			L= 30.0' CPP, square edge headwall, Ke= 0.500
			Inlet / Outlet Invert= 94.00' / 93.00' S= 0.0333 '/' Cc= 0.900
			n= 0.010 PVC, smooth interior, Flow Area= 1.77 sf
#2	Device 1	94.00'	3.0" Vert. Orifice/Grate C= 0.600
#3	Device 1	96.50'	18.0" Horiz. Orifice/Grate C= 0.600
			Limited to weir flow at low heads
#4	Secondary	96.50'	4.0' long x 0.5' breadth Broad-Crested Rectangular Weir
	•		Head (feet) 0.20 0.40 0.60 0.80 1.00
			Coef. (English) 2.80 2.92 3.08 3.30 3.32

Primary OutFlow Max=2.83 cfs @ 12.01 hrs HW=96.79' (Free Discharge)

1=Culvert (Passes 2.83 cfs of 12.16 cfs potential flow)

—2=Orifice/Grate (Orifice Controls 0.39 cfs @ 7.86 fps)
—3=Orifice/Grate (Weir Controls 2.44 cfs @ 1.77 fps)

Secondary OutFlow Max=1.81 cfs @ 12.01 hrs HW=96.79' (Free Discharge)
4=Broad-Crested Rectangular Weir (Weir Controls 1.81 cfs @ 1.55 fps)

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Summary for Pond 51P: 54 ROOF DRIPLINE BMP'S

Inflow Area = 3.220 ac,100.00% Impervious, Inflow Depth > 7.23" for 100 YEAR event

Inflow = 19.15 cfs @ 12.21 hrs, Volume= 1.941 af

Outflow = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af, Atten= 100%, Lag= 0.0 min

Primary = 0.00 cfs @ 5.00 hrs, Volume= 0.000 af

Routing by Stor-Ind method, Time Span= 5.00-20.00 hrs, dt= 0.05 hrs

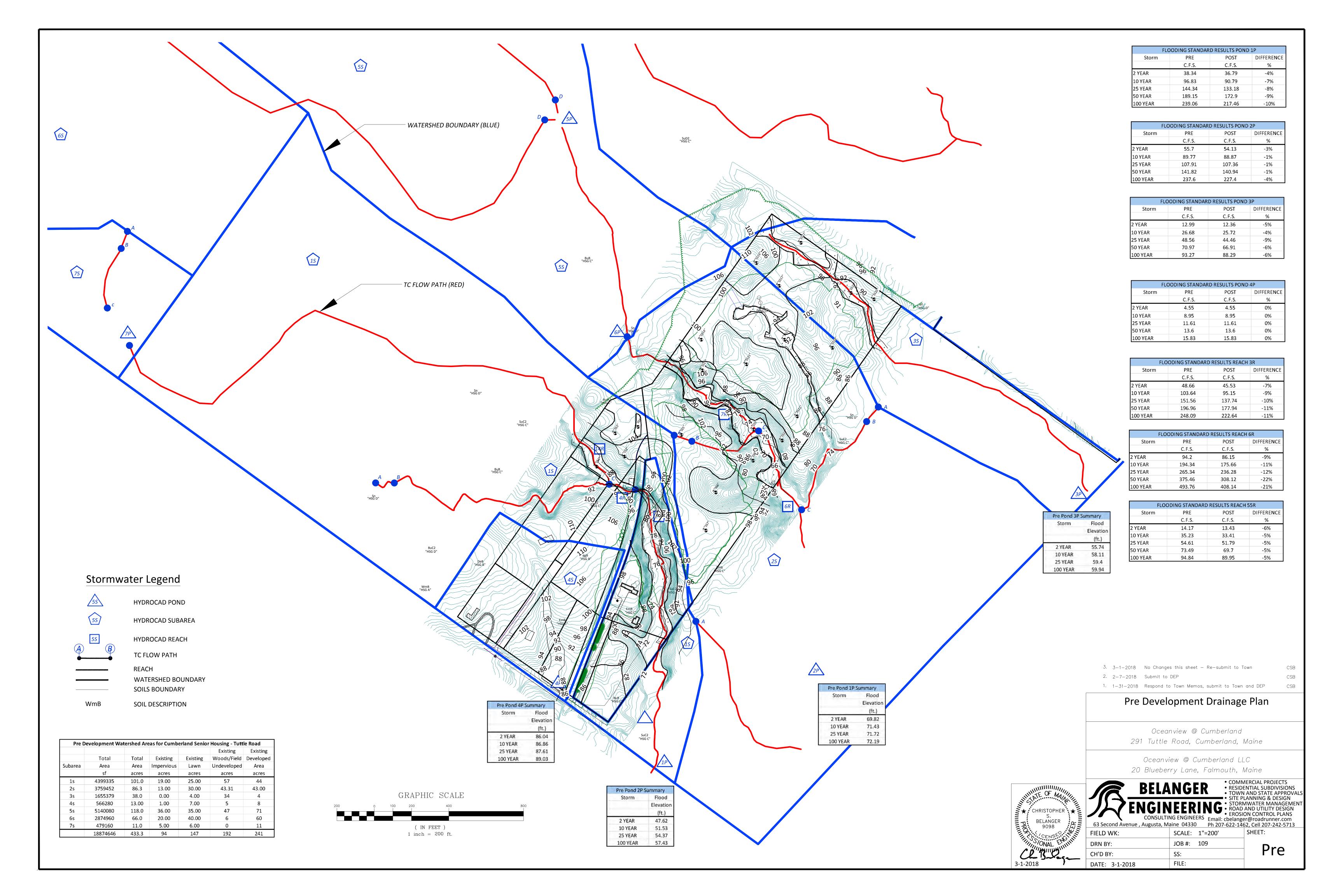
Peak Elev= 100.24' @ 20.00 hrs Surf.Area= 867,510 sf Storage= 84,525 cf

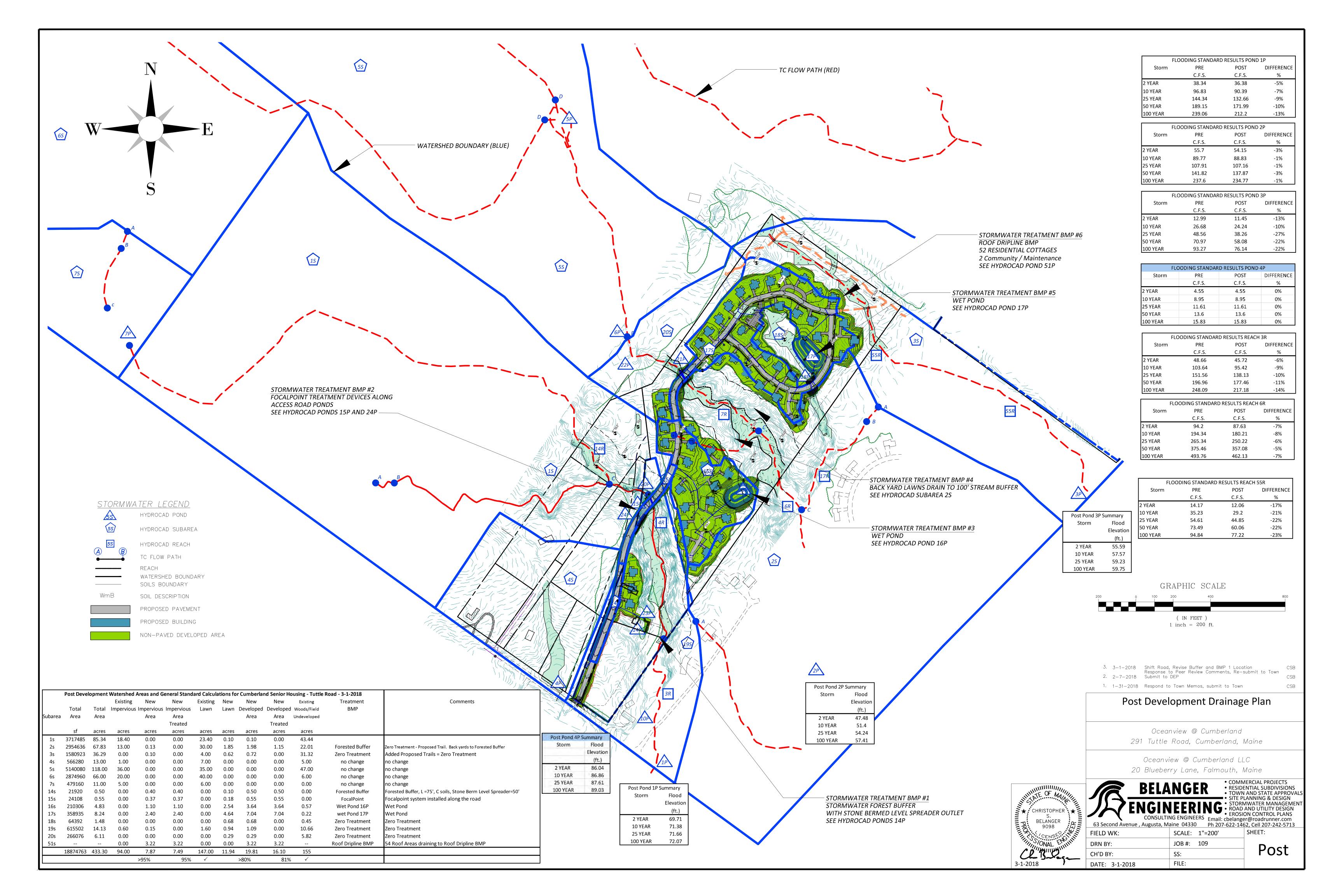
Plug-Flow detention time= (not calculated: initial storage exceeds outflow)

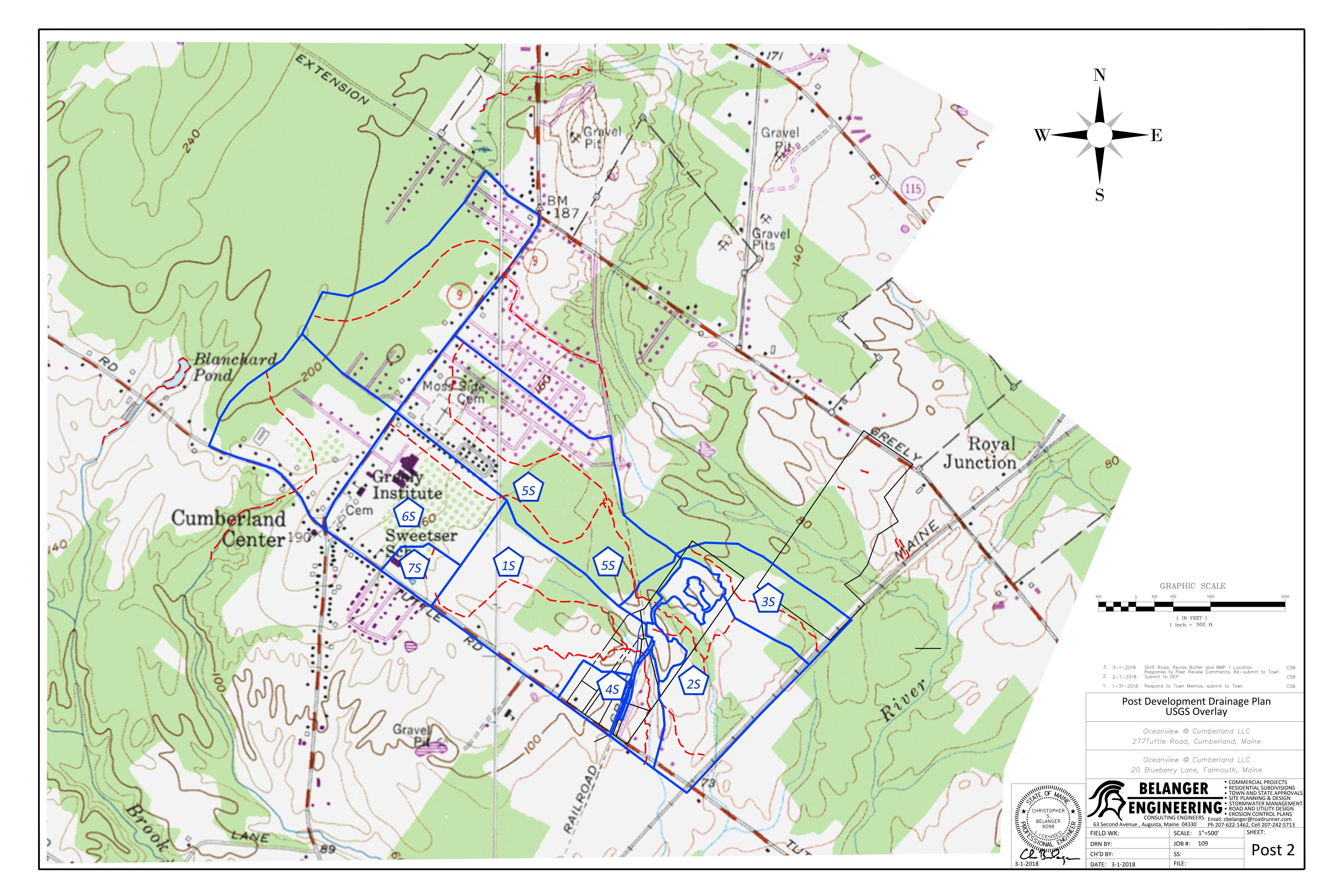
Center-of-Mass det. time= (not calculated: no outflow)

Volume	Invert	Avail.Stor	age	Storage Description
#1	100.00'	13,18	7 cf	3.00'W x 105.00'L x 2.00'H Prismatoid x 54
#2	100.00'	1,05	1 cf	34,020 cf Overall - 1,051 cf Embedded = 32,969 cf x 40.0% Voids 6.0" Round Pipe Storage x 51 Inside #1 L= 105.0' S= 0.0050 '/'
		14,23	9 cf	x 51.00 = 726,182 cf Total Available Storage
Device	Routing	Invert	Outle	et Devices
#1	Primary	101.50'	Head	0' long x 10.0' breadth Broad-Crested Rectangular Weir X 51.00 d (feet) 0.20 0.40 0.60 0.80 1.00 1.20 1.40 1.60 f. (English) 2.49 2.56 2.70 2.69 2.68 2.69 2.67 2.64

Primary OutFlow Max=0.00 cfs @ 5.00 hrs HW=100.00' (Free Discharge) 1=Broad-Crested Rectangular Weir (Controls 0.00 cfs)









May 4, 2018

Ms. Christine Woodruff
Department of Environmental Protection
312 Canco Road
Portland, Maine 04103

Subject: Ben Viola Response # 1

OceanView At Cumberland

277 Tuttle Road, Cumberland, Maine

Dear Ms. Woodruff:

The following responds to Ben Viola's email dated April 17, 2018. Mr. Viola's original comments are underlined.

The following are my comments regarding the OceanView at Cumberland site location of development application currently being reviewed by the Department.

• <u>The Treatment Table on sheet "POST" appears to incorrectly calls out Treatment</u> BMP of subcatchment 17.

We have updated the chart on the post plan as suggested. Subareas 17S drains to pond 17P which is a wet pond. Subarea 18S models the wetland area beside the pond that does not receives treatment.

• Wet pond P16 does not appear to meet the 3 to 1 length to width requirement.

Please correct this.

We have updated the pond shape to be 3:1 as required.

• Boardwalk crossings are considered wetland impacts. Were they counted as wetland impacts?

Yes. We have added notes on sheets C2, C3, C4, and C5 referring the impacts and the NRPA application.

• Which plan (plans) best shows the locations of forested buffers?

We have shaded the buffer areas brown on the "post stormwater" plan.



June 18, 2018

Ms. Christine Woodruff
Department of Environmental Protection
312 Canco Road
Portland, Maine 04103

Subject: Ben Viola Response # 2

OceanView At Cumberland

277 Tuttle Road, Cumberland, Maine

Dear Ms. Woodruff:

The following responds to Ben Viola's comments to Rick Licht by email dated June 6, 2018. Mr. Viola's original comments are underlined.

The following are issues that need to be resolved with the Oceanview site location of development application.

• Sheet C24 – The emergency spillway in the location proposed forces water from the spillway to make a 90 degree turn at the end of the spillway. Please investigate moving the emergency spillway to the other side of the principal outlet. In that location there would not be the abrupt change in direction.

We have moved the emergency spillway as requested. See Sheet C24.

• Sheet C20 – The end view is of Box Culvert #2 not Box Culvert #1.

We have updated the end view on sheet C20.

• The Focal Point systems need to be moved out of the stream crossing. I will leave this up to you Chris to work out the details with Rick.

We have revised the road profile and grading to move the low point back 100'. We will install a couple of catch basins at the low point and will pipe the stormwater to the pond and focal point system at Sta 19+50 right for treatment. This will move the system out of the wetland as required.



• <u>I also asked Rick to update the application form for any changes that have been or will be made.</u>

Rick Licht will update the application. The project creates 7.87 acres of impervious area and 19.81 acres of developed area.

Should you have questions, please call.

Very truly yours,

CLRQ.

Christopher S. Belanger, P.E. Enclosures

cc: Rick Licht, Licht Environmental Design

Matt Teare, Seacoast Management Company Chris Wasileski, Seacoast Management Company

63 Second Avenue, Augusta, Maine 04330

From: rick licht

To: "Viola, Ben"; "Woodruff, Christine"

Cc: cbelanger@roadrunner.com; "Chris Wasileski"; "Christian Haynes"
Subject: RE: Oceanview At Cumberland DEP SW Review Comments

Date: Wednesday, June 6, 2018 2:44:43 PM

Thanks Ben and for the phone call. The changes are pretty minor and Chris B and I should turn around very quickly.

Christine- Ben discussed that the focal point units cannot go in the stream crossing area per NRPA rules. I will call to discuss so we understand why. The obvious low point of most stream crossings is somewhere near the stream which is where the drainage collects..

Best

Rick

Frederic (Rick) Licht, PE, LSE Licht Environmental Design, LLC

35 Fran Circle Gray, Maine 04039 (v) 207.749.4924 lichtenvironmentaldesign.com

From: Viola, Ben [mailto:Ben.Viola@maine.gov] Sent: Wednesday, June 6, 2018 1:07 PM

To: Woodruff, Christine

Cc: rick licht

Subject: Oceanview

Chris,

The following are issues that need to be resolved with the Oceanview site location of development application.

- Sheet C24 The emergency spillway in the location proposed forces water from the spillway to make a 90 degree turn at the end of the spillway. Please investigate moving the emergency spillway to the other side of the principal outlet. In that location there would not be the abrupt change in direction.
- Sheet C20 The end view is of Box Culvert #2 not Box Culvert #1.
- The Focal Point systems need to be moved out of the stream crossing. I will leave this up to

you Chris to work out the details with Rick.

• I also asked Rick to update the application form for any changes that have been or will be made.

I will continue my review when I receive a response to the above issues. As always please have the applicant explain how each comment is addressed in the cover accompanying the submittal.

If you or Rick have any questions please contact me.

Ben Viola, PE

Environmental Engineer in the Bureau of Land Resources Phone: 207-822-6365 (desk) 207-822-6300 (receptionist) 207-822-6303 (fax) www.maine.gov/dep



• Sheet "POST" – not sure how dripline filters are counted. Which houses use roof drip line filters?

Every house will have a roof drip edge and underdrain to provide treatment for the buildings. The chart on the post plan shows subarea 51S which includes the roof areas for 54 buildings (3.22 acres).

• <u>Sheets "C29" and "C30" appear to have problems with lettering on my copy.</u> <u>Please provide new copies.</u>

We have updated the focal point sheets and details. See sheets C27, C28, C29, C30, C31A, and C31B.

• Sheet "C29" bypass manifold appears to bypass separator row from Focal Point system. How is the 1 inch and 0.4 inch of runoff ensured to be treated in the separator row?

We have updated the details and outlet design. The focal point underdrain will drain into the treatment row. Once the treatment row is flooded, runoff will overflow to the R-tank storage chambers. The R-tank will outlet into an outlet structure. The outlet structure will contain a 4" concrete baffle with a 2" orifice to provide slow release of runoff to the stream.

Sheet "C26" & "C27" – Based on the plan, I'm not understanding Focal Point installation. Perhaps there is a better way of showing this.

We have updated the focal point sheets and details. See sheets C27, C28, C29, C30, C31A, and C31B.

• <u>I could not locate test pit information for Focal Points in the application. Where</u> is this information in the application?

The focal point system will be located adjacent to the road and is located in a fill condition. The bottom of the system is at elevation 85.0. Further Mark Hampton has provided test pits and high intensity soil survey plan. A separate test pit in the focal point area is not applicable in this condition.

63 Second Avenue, Augusta, Maine 04330



• <u>Need more information on dewatering of wet ponds during construction. Please</u> add dewatering details and show locations for dewatering silt sacks.

Construction dewatering notes is provided on Sheet C16. We have added a sediment trap and Geotextile filter bag location and note on the plans. See sheet C22 and C24. We have also added notes on C4 and C5 requiring the sediment basin be located a minimum 25' from the wetland.

<u>I have spoken with Rick Licht about these comments and he will be making the</u> appropriate changes. He should explain how each issue is addressed in the cover letter accompanying the response.

Should you have questions, please call.

Very truly yours,

Christopher S. Belanger, P.E.

Enclosures

cc: Matt Teare, Seacoast Management Company

Chris Wasileski, Seacoast Management Company

63 Second Avenue, Augusta, Maine 04330



SOIL EVALUATION • WETLAND DELINEATIONS • SOIL SURVEYS • WETLAND PERMITTING

4674

May 7, 2018

Mr. Rick Licht Licht Environmental Design LLC 35 Fran Circle Gray, ME 04039

Re: Soil Evaluation, Proposed Stormwater Buffer, Oceanview of Cumberland Cumberland, ME

Dear Rick,

I completed a soil evaluation for the proposed stormwater buffer on the Allen property for the Oceanview of Cumberland project Cumberland, ME. The soil evaluation was conducted in accordance with the Maine Subsurface Wastewater Disposal Rules dated August 2015, as amended. I evaluated one hand excavated soil test pit in the center of the proposed stormwater buffer. The soils found on the parcel are moderately well drained marine laucustrine soils. There is a seasonal high watertable at approximately 20 inches. There was no observed groundwater table in the soil test pit. The soil test pit log description is attached.

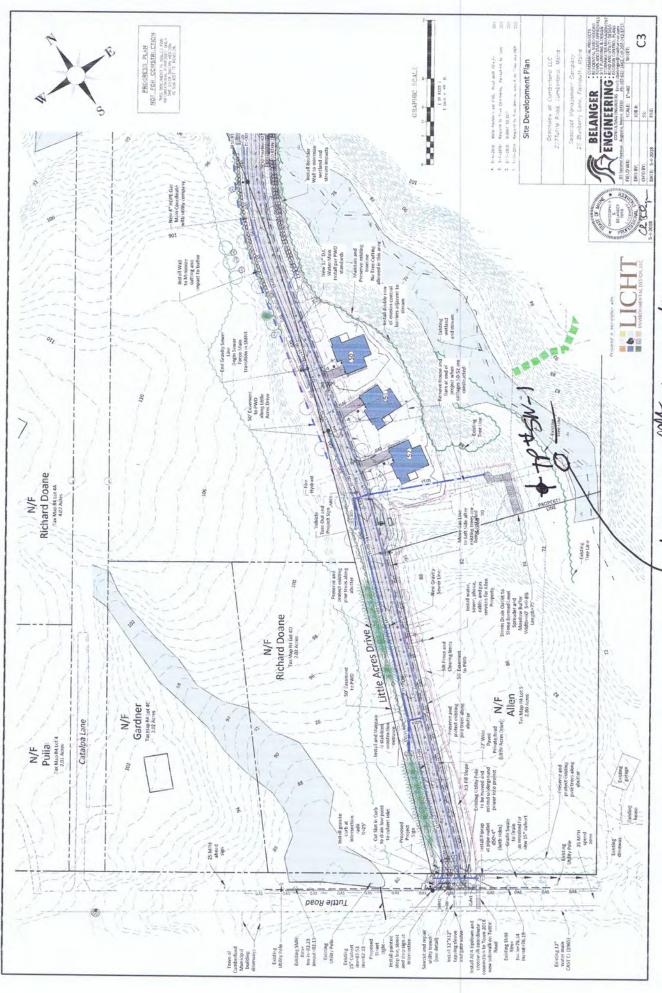
If you have any questions or require additional information, please contact me.

Sincerely,

Mark J. Hampton L.S.E., C.S.S. Licensed Site Evaluator #263

Certified Soil Scientist #216

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