

From: [Carla Nixon](#)
To: [Whitney Miller](#)
Subject: FW: Cumberland Rusty Lantern C-Store & Bank Development - Section 7 Submittal
Date: Tuesday, February 20, 2024 2:38:16 PM
Attachments: [image001.png](#)
[image002.png](#)
[Site-Stormwater PLans.pdf](#)
[SW MaintMan.pdf](#)
[I&M.pdf](#)
[22-RLM-004 SMP 2-5-24.pdf](#)
[22-004 Sidewalks.pdf](#)
[Sidewalk Memorandum Signed.pdf](#)
[AADT Calcs.pdf](#)
[image003.png](#)
[image004.png](#)
[image005.png](#)
[image006.png](#)

Will you please upload this email and attachments to Agenda Item #6?



Carla Nixon

Director of Planning, Town of Cumberland

[207-829-2206](tel:207-829-2206)

www.cumberlandmaine.com

290 Tuttle Road, Cumberland, Maine 04021



From: Diane Morabito <mordi@sewall.com>
Sent: Tuesday, February 20, 2024 12:06 PM
To: Illian, Randy <Randy.Illian@maine.gov>; vanLuling, Robert <Robert.vanLuling@maine.gov>
Cc: Carla Nixon <cnixon@cumberlandmaine.com>; William Shane <wshane@cumberlandmaine.com>; Curt Neufeld <cneufeld@priorityrealestategroup.com>; Jim Howard <jhoward@priorityrealestategroup.com>; Randy Dunton <rdunton@gorrillpalmer.com>
Subject: RE: Cumberland Rusty Lantern C-Store & Bank Development - Section 7 Submittal

This message's attachments contains at least one web link. This is often used for phishing attempts. Please only interact with this attachment if you know its source and that the content is safe. If in doubt, confirm the legitimacy with the sender by phone.

WARNING: This is an external email that originated outside of our email system. DO NOT CLICK links or open attachments unless you recognize the sender and know that the content is safe!

Hi Randy,

The additional information you requested below is attached:

1. Include drainage plans and drainage study – showing no net increase for the 50 year storm - Attached you will find the Stormwater Plans, Stormwater Maintenance Plan, Site Inspection

Form & Drainage Study

2. Concept plans must have approximate existing ROW and cut/fill lines – Attached you will find concept plans for the sidewalk showing existing ROW and cut/fill lines, as well as a signed agreement allowing regrading of an adjacent property.
3. Concept plans must show a sidewalk connection (and crosswalk) to the proposed sidewalk on Route 100 – towards Faraday Drive – The sidewalk plans show the requested crosswalk.
4. Based upon the HCL calculation for the intersection – include estimated increase in AADT, due to the development, for each direction and each approach (8 AADTs) – The AADT calculations are attached.

As always, let me know if you have any questions on these materials.

Thanks,
Diane

Diane W. Morabito, PE, PTOE

Vice President Traffic Engineering

T: +1. 207.817.5440 | **F:** +1. 207.827.3641 | **E:** diane.morabito@sewall.com

14 York Street | Portland, Maine 04101 | www.sewall.com



From: Illian, Randy <Randy.Illian@maine.gov>

Sent: Monday, December 4, 2023 2:32 PM

To: Diane Morabito <mordi@sewall.com>; vanLuling, Robert <Robert.vanLuling@maine.gov>

Cc: Carla Nixon <cnixon@cumberlandmaine.com>; wshane <wshane@cumberlandmaine.com>; cneufeld@priorityrealestategroup.com; Jim Howard <jhoward@priorityrealestategroup.com>; Randy Dunton <rdunton@gorrillpalmer.com>

Subject: RE: Cumberland Rusty Lantern C-Store & Bank Development - Section 7 Submittal

Diane,

I just got off the phone with our Safety Office. I misunderstood. They do not have a recent formal Safety Assessment. Please ignore that requirement.

Thank you,

Randy Illian, P.E.
Southern Region Traffic Engineer
Maine Department of Transportation
Scarborough, ME
Office: (207)885-7041
he / him

From: Diane Morabito <mordi@sewall.com>
Sent: Monday, December 4, 2023 2:04 PM
To: Illian, Randy <Randy.Illian@maine.gov>; vanLuling, Robert <Robert.vanLuling@maine.gov>
Cc: Carla Nixon <cnixon@cumberlandmaine.com>; wshane <wshane@cumberlandmaine.com>;
cneufeld@priorityrealestategroup.com; Jim Howard <jhoward@priorityrealestategroup.com>;
Randy Dunton <rdunton@gorrillpalmer.com>
Subject: RE: Cumberland Rusty Lantern C-Store & Bank Development - Section 7 Submittal

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Thanks Randy. We will pull these materials together and resubmit.

Can you provide the MaineDOT Safety Office Assessment so that I may review it? I did review the current Gorrill Palmer recommendations for intersection signage/safety improvements and included that in the study.

Diane

Diane W. Morabito, PE, PTOE

Vice President Traffic Engineering

T: +1. 207.817.5440 | **F:** +1. 207.827.3641 | **E:** diane.morabito@sewall.com

14 York Street | Portland, Maine 04101 | www.sewall.com



From: Illian, Randy <Randy.Illian@maine.gov>
Sent: Monday, December 4, 2023 1:35 PM
To: Diane Morabito <mordi@sewall.com>; vanLuling, Robert <Robert.vanLuling@maine.gov>
Cc: Carla Nixon <cnixon@cumberlandmaine.com>; wshane <wshane@cumberlandmaine.com>;
cneufeld@priorityrealestategroup.com; Jim Howard <jhoward@priorityrealestategroup.com>;
Randy Dunton <rdunton@gorrillpalmer.com>
Subject: RE: Cumberland Rusty Lantern C-Store & Bank Development - Section 7 Submittal

Diane,

I have reviewed the submittal. I have found it incomplete. Based upon Scoping Meeting discussions, please make the following revisions and resubmit.

1. Include a review of the MaineDOT Safety Office Roadway Safety Assessment and include and relevant third-party analysis and recommendations
2. Include drainage plans and drainage study – showing no net increase for the 50 year storm

Please note, we will also need the following addressed/submitted before issuing a Draft TMP:

1. Concept plans must have approximate existing ROW and cut/fill lines
2. Concept plans must show a sidewalk connection (and crosswalk) to the proposed sidewalk on Route 100 – towards Faraday Drive
3. Based upon the HCL calculation for the intersection – include estimated increase in AADT, due to the development, for each direction and each approach (8 AADTs)

Please feel free to call or write with any questions.

Sincerely,

Randy Illian, P.E.
Southern Region Traffic Engineer
Maine Department of Transportation
Scarborough, ME
Office: (207)885-7041
he / him

From: Diane Morabito <mordi@sewall.com>

Sent: Wednesday, November 22, 2023 12:17 PM

To: Illian, Randy <Randy.Illian@maine.gov>; vanLuling, Robert <Robert.vanLuling@maine.gov>

Cc: Carla Nixon <cnixon@cumberlandmaine.com>; wshane <wshane@cumberlandmaine.com>;
cneufeld@priorityrealestategroup.com; Jim Howard <jhoward@priorityrealestategroup.com>;

Randy Dunton <rdunton@gorrillpalmer.com>

Subject: Cumberland Rusty Lantern C-Store & Bank Development - Section 7 Submittal

EXTERNAL: This email originated from outside of the State of Maine Mail System. Do not click links or open attachments unless you recognize the sender and know the content is safe.

Hi Randy,

Attached please find Section 7 for the proposed Rusty Lantern Convenience store and bank development in Cumberland.

A check was mailed to you at your office this morning for the remaining \$ 1,500 application fee. Hopefully, you will have it the first of next week.

As always, do not hesitate to contact me if you have any questions or need any additional information regarding the study or our findings or recommendations.

Best Wishes for a Happy Thanksgiving!

Thanks,
Diane

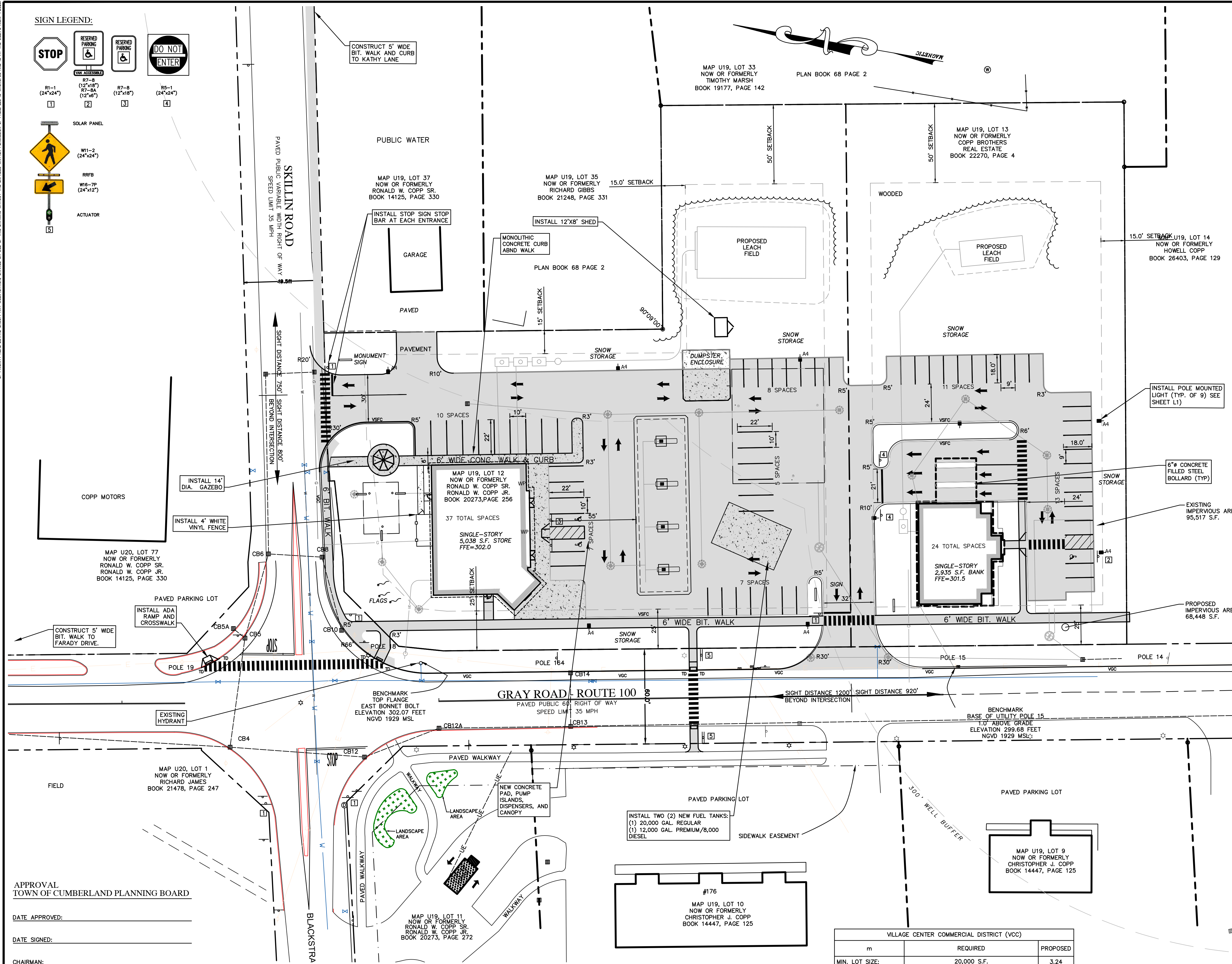
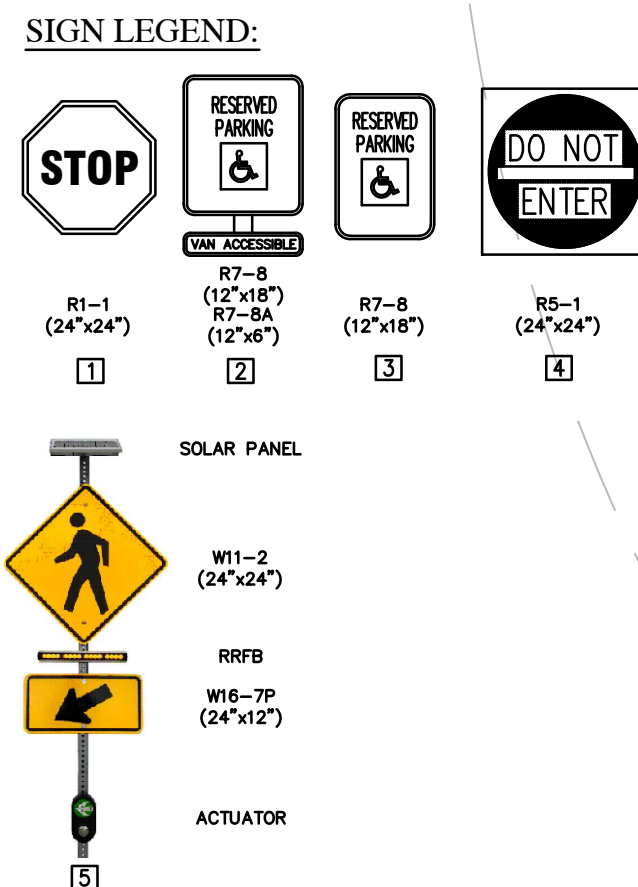
Diane W. Morabito, PE, PTOE

Vice President Traffic Engineering

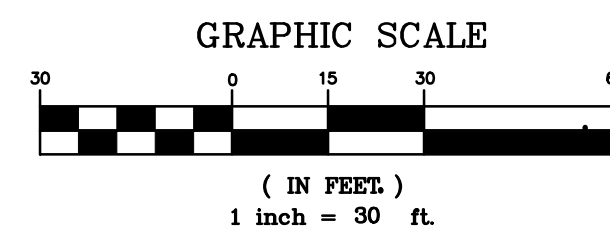
T: +1. 207.817.5440 | **F:** +1. 207.827.3641 | **E:** diane.morabito@sewall.com

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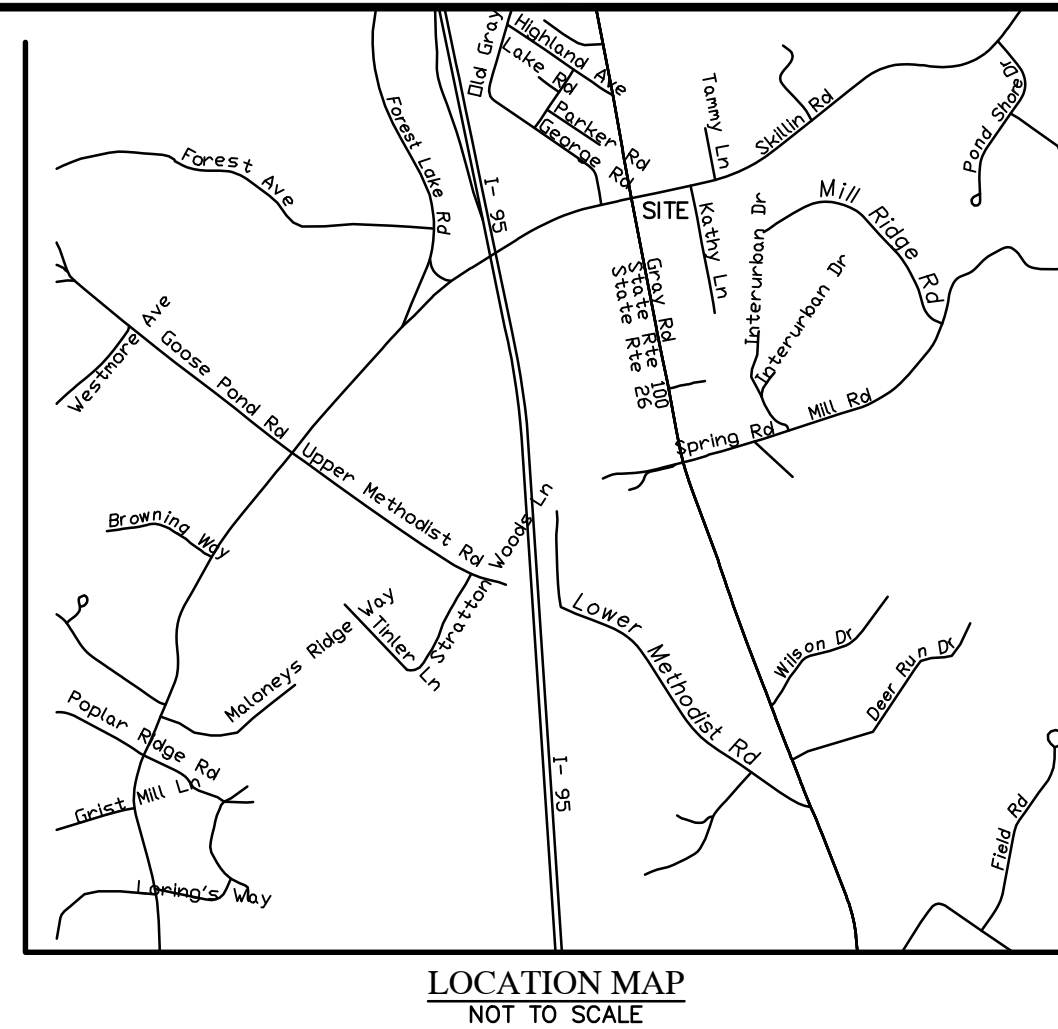




VILLAGE CENTER COMMERCIAL DISTRICT (VCC)		
m	REQUIRED	PROPOSED
MIN. LOT SIZE:	20,000 S.F.	3.24
MIN. LOT FRONTAGE:	75'	370'
MINIMUM SETBACKS:		
FRONT:	25'	25'
REAR:	50'	50'
SIDE:	15'	15'
MAX. HEIGHT:	40'	<40'
PARKING	BUS. SVC. - 1 PER 250 S.F. = 12 RETAIL - 1 PER 250 S.F. = 22 TOTAL = 34	37 24 61

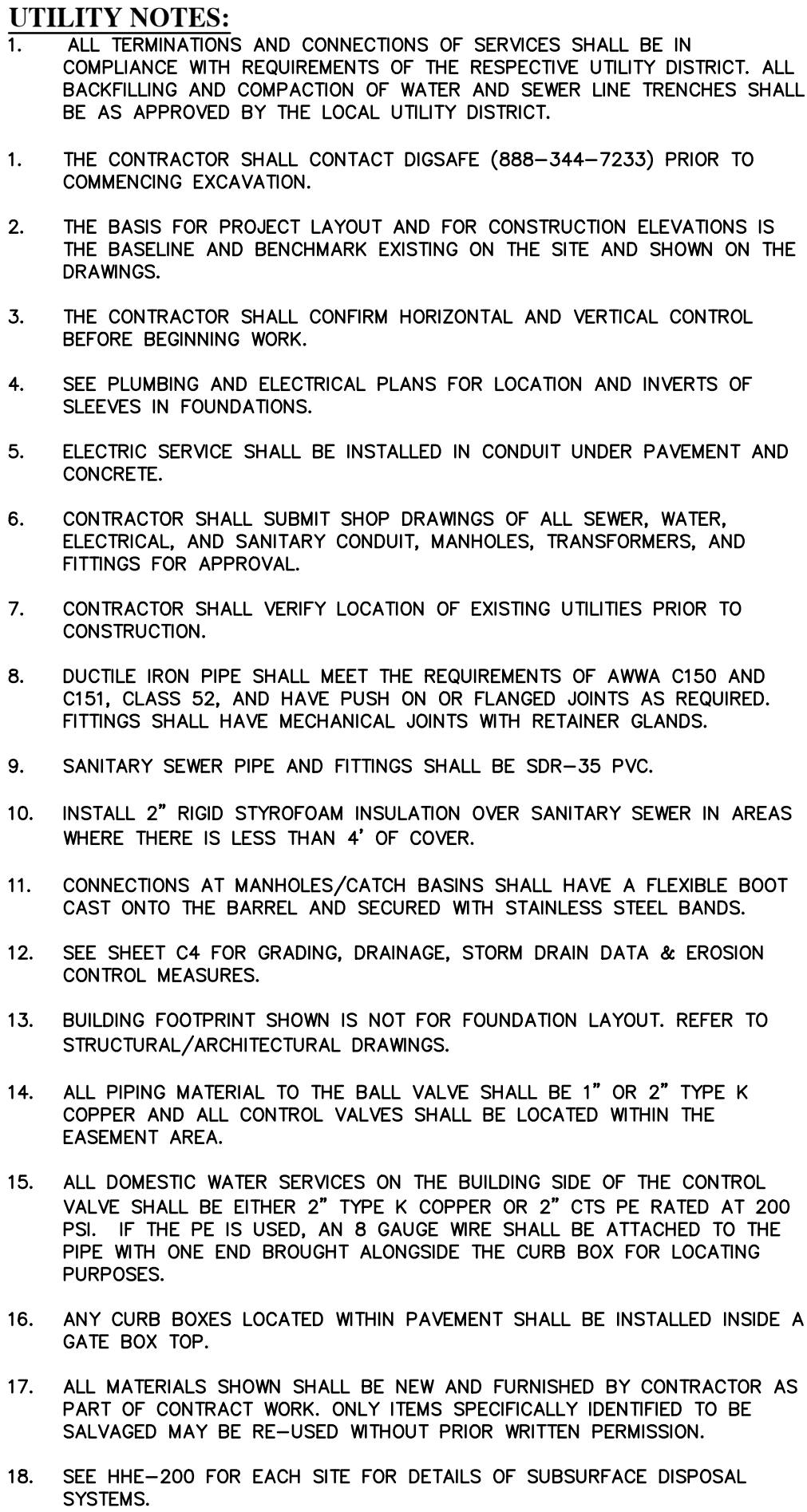


ISSUED FOR:
PERMITTING



- GENERAL NOTES:
- TITLE REFERENCE FOR SURVEYED PARCEL:
BK 20273, PG 256 (U19-12)
BK 34640, PG 209 (U19-13)
 - PLAN REFERENCE(S):
(1) EXISTING CONDITIONS SURVEY FOR PRIORITY REAL ESTATE GROUP OF 181 GRAY ROAD, CUMBERLAND, MAINE 04021, PREPARED BY BOUNDARY POINTS, NOT RECORDED.
 - AREA INFORMATION:
LOT 12: 81,259 S.F. (1.87 ACRES)
LOT 13: 59,857 S.F. (1.37 ACRES)
TOTAL AREA:141,116 S.F. (3.24 ACRES)
 - TAX MAP REFERENCE:
TAX MAP U19, LOT 12 & 13.
 - BASIS OF BEARINGS:
BEARINGS ARE MAINE STATE PLANE, WEST ZONE, NAD 83.
 - ELEVATION DATUM:
NGVD 1929 MSL
 - FLOOD ZONE INFORMATION:
PARCEL IS LOCATED WITHIN ZONE C (AREAS OF MINIMAL FLOODING) OF THE FLOOD INSURANCE RATE MAPS FOR CUMBERLAND COUNTY, MAINE. THE PROJECT IS LOCATED ON PANEL 15 OF 25 (COMMUNITY PANEL 230162 0015 B, EFF. DATE MAY 19, 1981)
 - IMPERVIOUS AREA:
EXISTING IMPERVIOUS AREA: 95,517 S.F. (2.18 AC)
PROPOSED IMPERVIOUS AREA: 68,117 S.F. (1.57 AC)
NET CHANGE IN IMPERVIOUS AREA: -27,400 S.F. (0.63 AC)
- UTILITY NOTES:
1. INFORMATION REGARDING THE LOCATION OF EXISTING UNDERGROUND UTILITIES IS A COMPILED OF THAT FOUND IN THE FIELD AND THAT SHOWN ON A PREVIOUS PLANS, AND SHALL NOT BE CONSIDERED AN AS-BUILT PLAN. CONTRACTOR SHALL BE RESPONSIBLE FOR FIELD VERIFYING UTILITY LOCATIONS PRIOR TO COMMENCING WORK. NOTIFY ENGINEER OF ANY DISCREPANCY BETWEEN UTILITIES AS SHOWN AND AS FOUND. CONTRACTOR SHALL NOTIFY DIG-SAFE PRIOR TO EXCAVATION.
1-888-344-7233
- LAYOUT NOTES:
1. ALL DIMENSIONING, UNLESS NOTED OTHERWISE, IS TO THE FACE OF CURB OR FOUNDATION.
 2. BOUNDARY INFORMATION ON LAYOUT PLAN IS FOR REFERENCE ONLY. REFER TO CERTIFIED BOUNDARY PLANS FOR BOUNDARY INFORMATION.
 3. ALL HANDICAP ACCESSIBLE PARKING SPACES, RAMPS AND SIDEWALKS SHALL BE CONSTRUCTED IN CONFORMANCE WITH THE AMERICANS WITH DISABILITIES ACT (ADA).
 4. ALL SITE SIGNAGE AND PAVEMENT MARKINGS SHALL CONFORM TO THE MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES. (MUTCD)
 5. BUILDING FOUNDATION SHOWN IS NOT FOR FOUNDATION LAYOUT. COORDINATE SITE WORK WITH ARCHITECTURAL DRAWINGS INCLUDING BUILDING FEATURES AND FOUNDATION PLAN.
 6. REFER TO SHEET C4 FOR GRADING AND DRAINAGE INFORMATION.
 7. REFER TO SHEET L1 FOR LANDSCAPE INFORMATION.
 8. REFER TO SHEET L2 FOR LIGHTING INFORMATION.

[illegible]



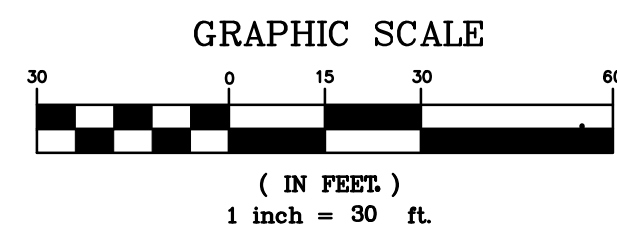
```
SEWER STRUCTURE DATA:
GT
RIM: 300.25
INV.IN: 295.76 (FROM STORE)
INV.OUT: 295.51 (TO ST#1)

ST1
RIM: 300.25
INV.IN: 295.50 (FROM GT)
INV.IN: 295.50 (FROM STORE)
INV.OUT: 295.25 (TO ST#2)

ST2
RIM: 300.25
INV.IN: 295.10 (FROM ST#1)
INV.OUT: 294.85 (TO PUMP STATION)

ST3
RIM: 301.00
INV.IN: 296.40 (FROM BANK)
INV.OUT: 296.15 (TO PUMP STATION)
```

P1: 6" SDR35 L=62' S=0.020
P2: 6" SDR35 L=62' S=0.024



ISSUED FOR:
PERMITTING

NOT FOR CONSTRUCTION

THIS PLAN IS ISSUED FOR REVIEW AND INFORMATION PURPOSES ONLY. THIS PLAN WILL CHANGE AND IS NOT INTENDED FOR PRICING OR CONSTRUCTION.

PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.

UTILITY PLAN

RUSTY LANTERN CONVENIENCE STORE

OR: CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

PRIORITY

2 MAIN STREET
TOPSHAM, MAINE 04086

SUBJECT.

U.

FIELD WK: CYN

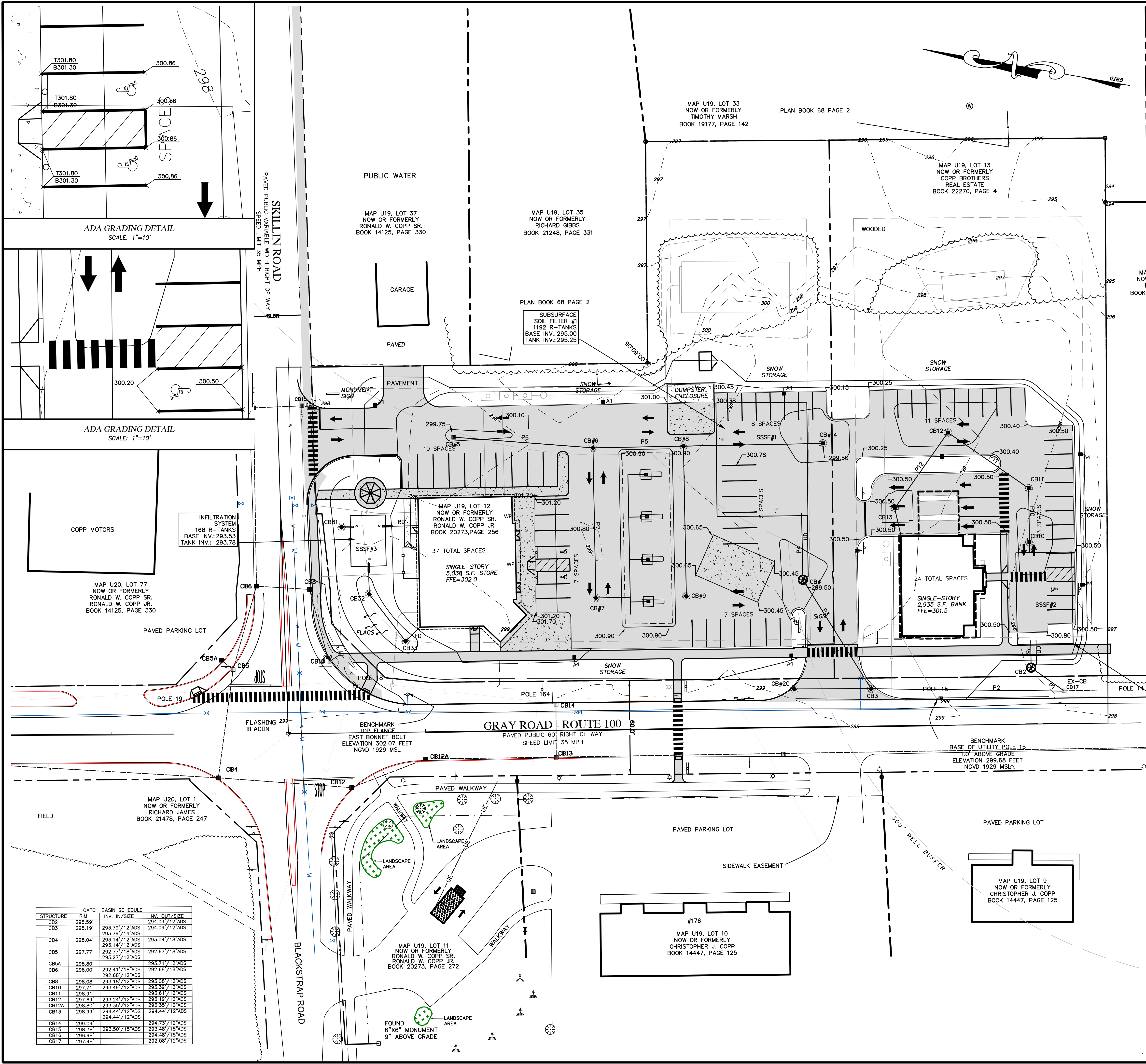
DRN BY: CYN

CH'D BY: CYN
DATE: 11-22-23

CH'D BY: CYN
DATE: 11-22-23

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C:\USERS\CURT NEUFELD\DOCUMENTS\PROJECTS\22-RLM-004 CUMBERLAND\DWG\22-004 SITE.DWG, CS GRADING, 05/22/2024 9:40 AM, CURT NEUFELD



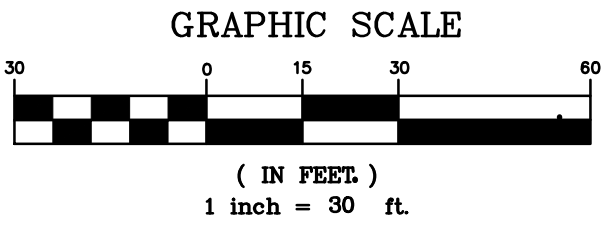
GRADING AND DRAINAGE NOTES:

1. THE CONTRACTOR SHALL PHASE GRADING EFFORTS SUCH THAT TOTAL SITE DISTURBANCE IS MINIMIZED. TEMPORARY EROSION CONTROL MEASURES SHALL BE INSTALLED PRIOR TO GRADING EFFORTS OR WITHOUT DELAY UPON THEIR COMPLETION, DEPENDENT UPON THE SITUATION.
2. ALL FILL SLOPES SHALL BE A MINIMUM OF 3:1 HORIZONTAL TO VERTICAL UNLESS OTHERWISE NOTED OR DIRECTED.
3. THE LIMITS OF DISTURBANCE SHALL GENERALLY BE THE MINIMAL EXTENT NECESSARY ONLY TO PERFORM THE GRADING EFFORTS SHOWN ON THE DRAWINGS. SPECIAL CARE SHALL BE TAKEN TO AVOID DISTURBANCE OF OBJECTS AND AREAS NOT SPECIFICALLY IDENTIFIED FOR MODIFICATION OR REMOVAL.
4. ALL DISTURBED AREAS SHALL BE LOAMED AND SEEDING IN ACCORDANCE WITH THE DRAWINGS, UNLESS INTENDED FOR OTHER SURFACE COVER.
5. STORM DRAINS SHALL BE CONSTRUCTED CONCURRENTLY WITH GRADING EFFORTS TO PROVIDE ADEQUATE CONVEYANCE FOR ANY SITE RUNOFF CONDITIONS.
6. WHERE FINAL GRADING HAS BEEN COMPLETED, SURFACE RESTORATION FOR DISTURBED AREAS WILL BE COMPLETED AS SOON AS PRACTICABLE. FOR VEGETATIVE AREAS, VEGETATION WILL BE PROGRESSIVELY ESTABLISHED.
7. UNLESS OTHERWISE NOTED, ALL STORM DRAIN PIPE SHALL BE IN ACCORDANCE WITH MDOT SPECIFICATIONS SECTION 603. PIPE CULVERTS AND STORM DRAINS, LATEST REVISION WITH ACCEPTABLE TYPES OF PIPE ARE AS FOLLOWS:
SMOOTH BORE POLYETHYLENE PIPE - HDPE N-12 ADS
8. BENCHMARK INFORMATION: SEE PLAN
9. THE CONTRACTOR SHALL SUBMIT SHOP DRAWINGS OF ALL DRAINAGE STRUCTURES AND PIPING PRIOR TO ORDERING.
10. RIM ELEVATIONS OF PROPOSED DRAINAGE STRUCTURES ARE APPROXIMATE. FINAL ELEVATIONS ARE TO BE SET FLUSH AND CONSISTENT WITH THE GRADING PLANS.
11. TRANSITIONS BETWEEN SLOPES ARE TO BE GENERALLY GRADUAL AND RESULT IN A SMOOTH, ROUNDED APPEARANCE.

STORM DRAIN PIPE TABLE									
NAME	SIZE (IN)	LENGTH	MATERIAL	SLOPE (%)	UP STR.	DN STR.	UP INV.	DOWN INV.	
P19	18.0	122.25	HDPE	0.500	CB#3	EX-CB	293.71	293.09	
P1	18.0	25.06	HDPE	0.500	CB#2	EX-CB	292.38	292.25	
P20	18.0	49.10	HDPE	0.500	CB#20	CB#3	294.05	293.81	
P3	18.0	81.90	HDPE	0.500	CB#4	CB#3	294.21	293.81	
P4	18.0	39.19	HDPE	0.001	SSSF1-Out	CB#4	294.32	294.31	
SSSF1	18.0	82.63	HDPE	0.001	SSSF1-IN	SSSF1-Out	294.42	294.42	
P8	18.0	6.33	HDPE	0.500	CB#6	SSSF1-IN	294.55	294.52	
P9	18.0	97.58	HDPE	0.500	CB#6	CB#8	294.94	294.65	
P9	12.0	95.54	HDPE	0.286	CB#9	CB#8	294.92	294.65	
P7	18.0	95.54	HDPE	0.294	CB#7	CB#6	295.32	295.04	
P6	12.0	88.49	HDPE	0.500	CB#5	CB#6	295.48	295.04	
P8	18.0	17.22	HDPE	0.500	SSSF2-Out	CB#2	292.56	292.48	
SSSF2	12.0	56.00	HDPE	0.001	SSSF2-IN	SSSF2-Out	292.56	292.56	
P9	12.0	6.82	HDPE	0.500	CB#10	SSSF2-IN	292.80	292.56	
P10	12.0	34.15	HDPE	0.500	CB#11	CB#10	292.87	292.70	
P11	12.0	62.43	HDPE	0.500	CB#12	CB#11	293.28	292.97	
P12	12.0	58.90	HDPE	0.500	CB#13	CB#12	293.67	293.38	
P14	12.0	9.94	HDPE	0.531	SSSF1-IN	CB#14	294.42	294.90	
P33	12.0	19.81	HDPE	0.500	CB#32	INF	293.90	293.90	
P34	12.0	37.83	Concrete	0.500	CB#33	CB#32	294.09	293.90	
P32	12.0	8.06	HDPE	0.971	CB#31	INF1	293.90	293.82	

STORM DRAIN STRUCTURE TABLE				
NAME	RIM ELEV	INV.-IN (1)	INV.-IN (2)	INV.-OUT
EX-CB	298.00	293.09	292.25	N/A
CB#3	298.83	293.81	293.81	293.71
CB#20	298.98	N/A	N/A	294.05
CB#4	299.50	294.31	N/A	294.21
SSSF1-Out	300.46	294.42	N/A	294.32
SSSF1-IN	300.79	294.52	N/A	294.42
CB#8	300.84	294.65	294.65	294.55
CB#6	300.25	295.04	295.04	294.94
CB#7	300.25	N/A	N/A	295.32
CB#5	299.85	N/A	N/A	295.48
CB#9	300.77	N/A	N/A	294.92
CB#2	298.00	292.48	N/A	292.38
SSSF2-Out	300.42	292.56	N/A	292.56
SSSF2-IN	299.67	292.56	N/A	292.56
CB#10	299.50	292.70	N/A	292.60
CB#11	300.39	292.97	N/A	292.87
CB#12	299.50	293.38	N/A	293.28
CB#13	299.50	N/A	N/A	293.67
CB#14	299.31	294.90	N/A	N/A
SSSF1-IN	299.28	N/A	N/A	294.42
INF	299.38	293.80	N/A	N/A
CB#32	299.52	293.90	N/A	293.90
CB#33	299.50	N/A	N/A	294.09
INF1	298.89	293.82	N/A	N/A
CB#31	298.88	N/A	N/A	293.90

SUBSURFACE SOIL FILTER #2
554 R-TANKS
BASE INV.: 292.47
TANK INV.: 292.72



ISSUED FOR:
PERMITTING

PRIORITY
REAL ESTATE GROUP

PRIORITY
REAL ESTATE GROUP

GRADING PLAN
RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME 04021

PROJECT:

PREPARED FOR:
CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

01-29-24

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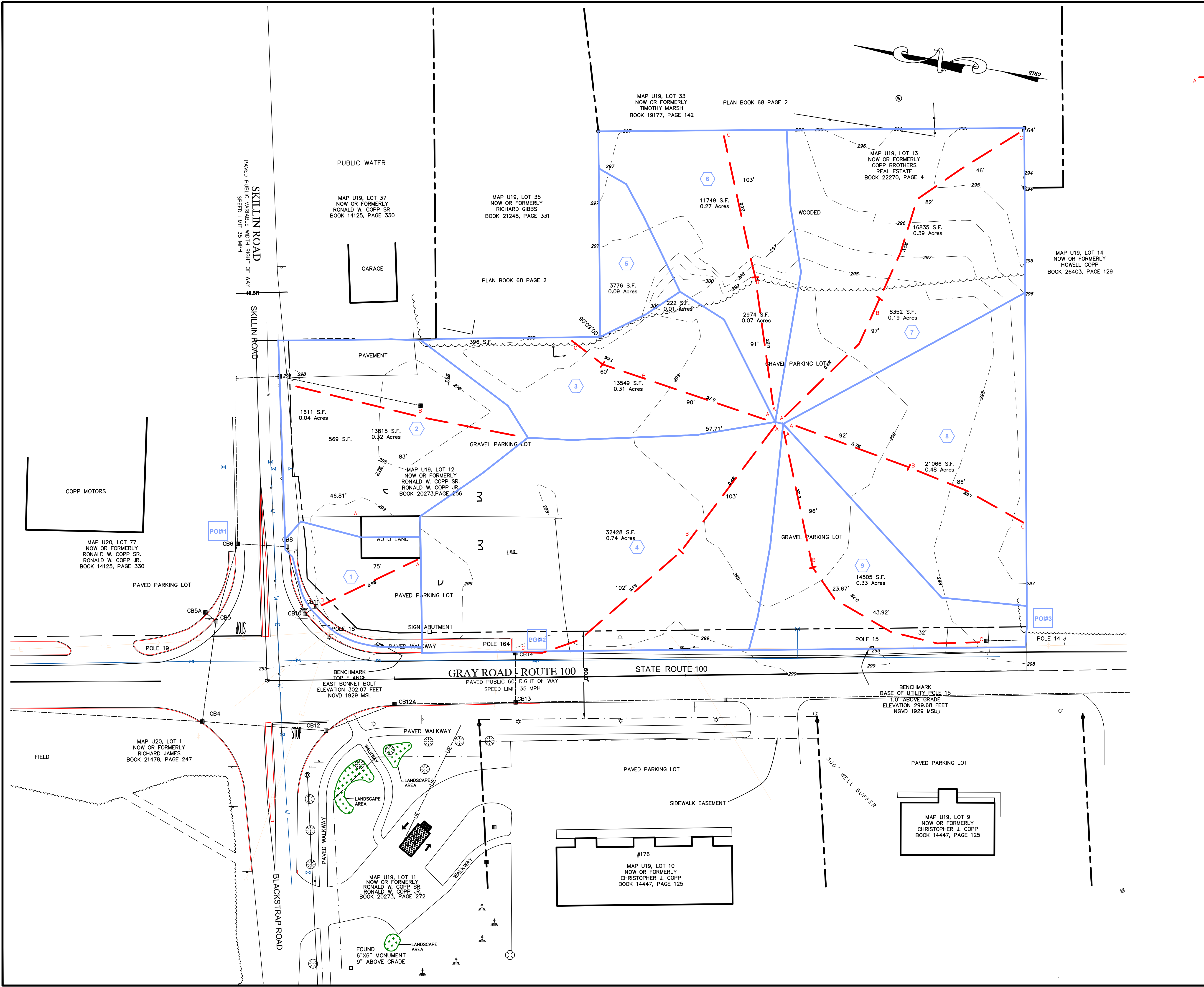
01-29-24

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C:\USERS\CURT NEUFELD\ONE DRIVE\DOCUMENTS\PROJECTS\22-RLM-004 CUMBERLAND\DWG\22-004 SITE.DWG, DRI PRE, 21/02/2024 9:40 AM, CURT NEUFELD

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LEGEND:

- SUBCATCHMENT AREA
- POINT OF INTEREST
- TIME OF CONCENTRATION

GRAPHIC SCALE

(IN FEET)

1 inch = 30 ft.

ISSUED FOR:

PERMITTING

PRIORITY REAL ESTATE GROUP

PRIORITY

2 MAIN STREET
TOPSHAM, MAINE 04086
(207) 837-6198

PRE-DEVELOPMENT DRAINAGE PLAN

PROJECT: RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME 04021

PREPARED FOR: CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

NOT FOR CONSTRUCTION

THIS PLAN IS ISSUED FOR REVIEW AND INFORMATION PURPOSES ONLY. THIS PLAN WILL CHANGE AND IS NOT INTENDED FOR PRICING OR CONSTRUCTION. PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.

DR1

SCALE: 1"=30'

JOB #: 22-RLM-004
MAP/LOT: U-19 12&13
FILE:

FIELD WK: CYN
DRN BY: CYN
CHD BY: CYN
DATE: 11-22-23

PROFESSIONAL SEAL

CURTIS NEUFELD
19779
LICENSED PROFESSIONAL ENGINEER
MAINE

01-29-24

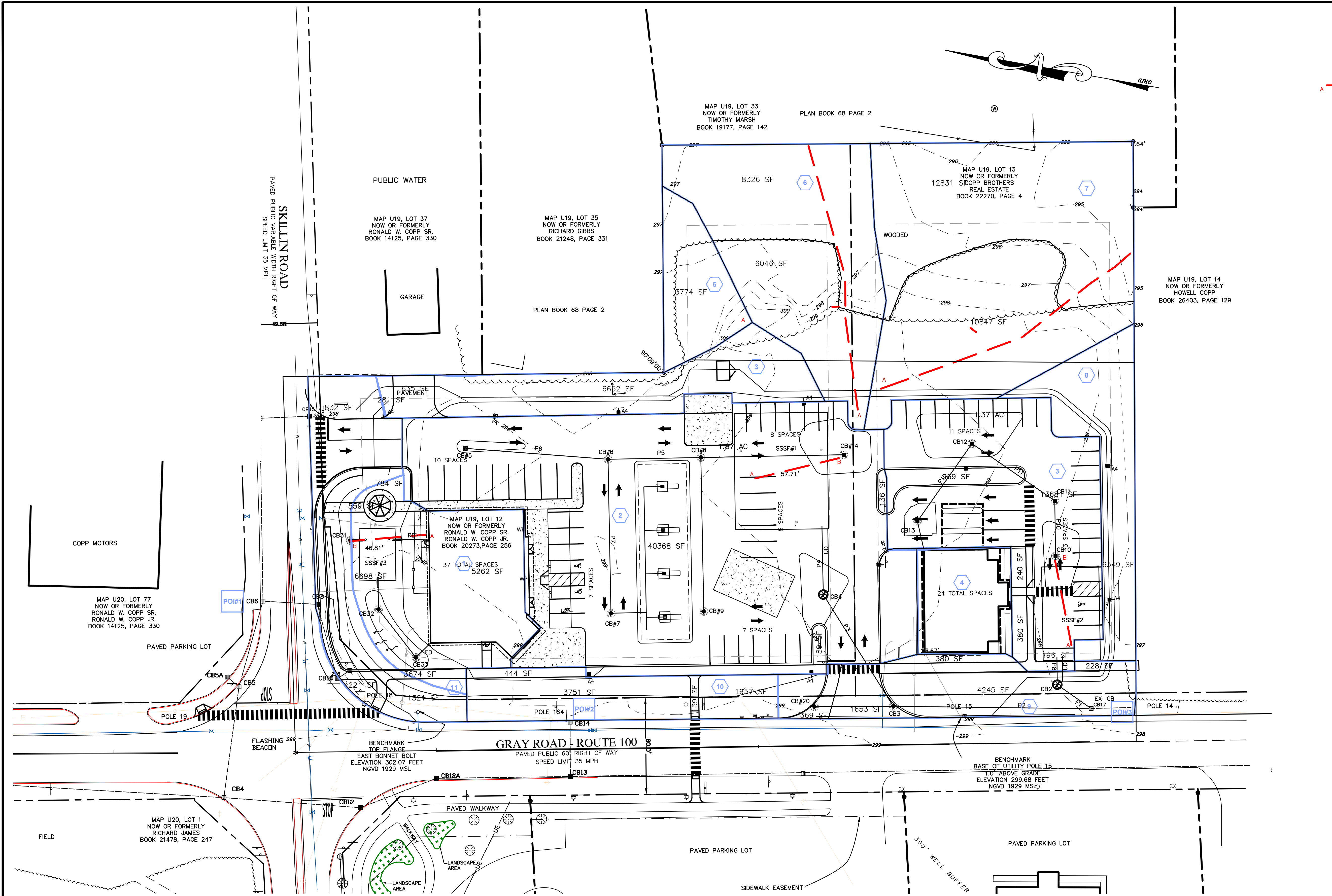
1. 08-11-23 SUBMITTED FOR WAREDOT REVIEW

2. 01-29-24 SUBMITTED TO TOWN OF CUMBERLAND FOR REVIEW

CYN CYN

C:\USERS\CURT NEUFELD\WORK\PROJECTS\22-RLM-004 CUMBERLAND\DWG\22-004 SITE.DWG, DR2 POST, 2/12/2024 9:40 AM, CURT NEUFELD

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LEGEND:

SUBCATCHMENT AREA

POINT OF INTEREST

TIME OF CONCENTRATION

GRAPHIC SCALE

(IN FEET)

1 inch = 30 ft.

ISSUED FOR:

PERMITTING

STORMWATER TREATMENT METHOD SIZING - SUBSURFACE SAND FILTERS							
	(A)	(B)	(C)	(D)	(E)	(F)	(G)
SUBCATCHMENT	IMPERVIOUS AREA (S.F.) (FROM PLAN)	REQUIRED STORAGE (C.F.) (A) X 0.083'	LANDSCAPED AREA (S.F.) (FROM PLAN)	REQUIRED STORAGE (C.F.) (C) X 0.033'	TOTAL STORAGE REQUIRED/PROVIDED (C.F.) (B) + (D)	FILTER AREA REQUIRED/PROVIDED (S.F.) [(A)X0.05] + [(C)X0.02]	TREATMENT METHOD
2	40638	3387	325	11	3397	7417	SSSF#1
3,4	17592	1466	1785	60	1526	2424	SSSF#2
1	5262	439	1447	48	487	1192	SSSF#3

PRIORITY REAL ESTATE GROUP

POST-DEVELOPMENT DRAINAGE PLAN

PROJECT: RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME 04021

PREPARED FOR: CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

DATE: 11-22-23

LEGEND:

SUBCATCHMENT AREA

POINT OF INTEREST

TIME OF CONCENTRATION

NOT FOR CONSTRUCTION

THIS PLAN IS ISSUED FOR REVIEW AND INFORMATION PURPOSES ONLY. THIS PLAN WILL CHANGE AND IS NOT INTENDED FOR PRICING OR CONSTRUCTION. PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.

DR2

SCALE: 1"=30'

JOB #: 22-RLM-004

MAP/LOT: U-19 12&13

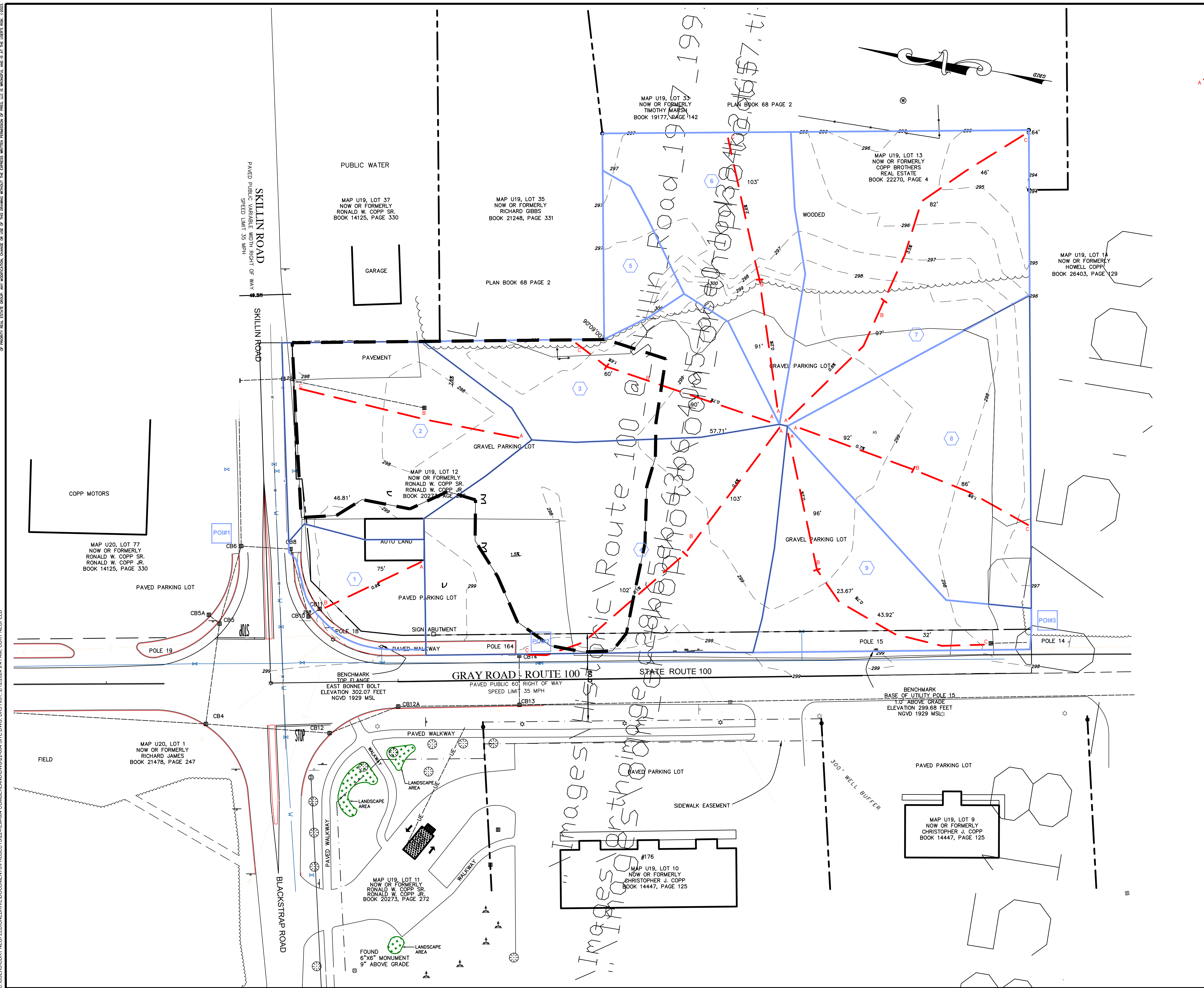
FILE:

FIELD WK: CYN

DRN BY: CYN

CHD BY: CYN

DATE: 11-22-23



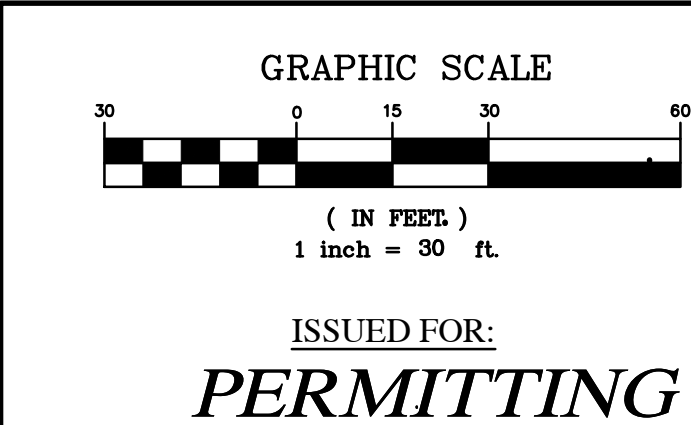
TIME OF CONCENTRATION

ISSUED FOR:

ISSUED FOR:
PERMITTING

01-29-24

PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.



NOT FOR CONSTRUCTION

THIS PLAN IS ISSUED FOR REVIEW AND INFORMATION PURPOSES ONLY. THIS PLAN WILL CHANGE AND IS NOT INTENDED FOR PRICING OR CONSTRUCTION.

PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND SHOULD BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.

PRE/POST DEVELOPMENT IMPERVIOUS AREA COMPARISON

RUSTY LANTERN CONVENIENCE STORE

FOR: CUMBERLAND REAL ESTATE GROUP, LLC

PRIORITY

2 MAIN STREET
TOPSHAM, MAINE 04086
(207) 837-6198

IA

**PRIORITY
REAL ESTATE
GROUP**

FIELD WK:	
DRN BY: CYN	
CH'D BY: CYN	

STORMWATER MANAGEMENT INSPECTION AND MAINTENANCE PLAN

1.0 GENERAL

This stormwater management maintenance plan has been prepared in support of the Maine Department of Environmental Protection Site Law Permit amendment for the Lakeside Concrete Cutting and Abatement Professional commercial building and offices in Cumberland, Maine. The requirements of this plan shall be incorporated into the efforts associated with the development including construction and ongoing operations.

This plan was prepared by:

Curt Neufeld, P.E. #9779
Sitelines, PA
119 Purinton Road, Suite A
Brunswick, Maine 04011
207-725-1200 x18

2.0 BEST MANAGEMENT PRACTICES

2.1 Best Management Practices

During Construction, a stabilized construction entrance, sediment barrier, and/or erosion control mix, seeding, and mulching practices will be used in accordance with the Maine Department of Environmental Protection Best Management Practices (BMP) manual during construction and until a stabilized condition exists.

After Construction, stormwater BMPs will include housekeeping and physical measures described herein, including the grassed underdrained soil filters, sweeping of paved surfaces, and maintenance of storm drain pipes and outfalls.

The stormwater maintenance management for this project will be performed consistent with the two references listed below and as amended in this manual. Where standards are not consistent, the more stringent requirement shall apply.

2.2 References

The primary references for the maintenance of the BMPs were as follows:

- 1 "Stormwater Management for Maine", Maine Department of Environmental Protection No. DEPLW0738, Volume 3, May 2016.
- 2 "Maine Erosion and Sedimentation Best Management Practices", Maine Department of Environmental Protection, current edition on-line.
- 3 "Maine Erosion and Sediment Control Field Guide for Contractors", Maine Department of Environmental Protection, 2014 Revision.

This information is provided as guidance if the Owner/would like to learn more about the BMPs. Also, maintenance for these BMPs may change over time. It is not expected the Owner will have the references readily available, however, they may be available through the DEP website.

3.0 MAINTENANCE OF STORMWATER FEATURES

3.1 General Responsibilities

The Contractor will be responsible for inspecting and maintaining the stormwater features until the construction phase of the project is complete. These efforts shall include maintenance of erosion and sedimentation control measures, temporary and permanent stormwater features, and addressing interim site conditions as necessary. After completion of construction, the Applicant will be responsible for inspecting and maintaining the permanent stormwater features as shown on the plan.

The Point of Contact for the Applicant is as follows:

Mr. James Howard
Cumberland Real Estate Holdings, LLC
2 Main Street
Topsham, Maine 04086
(207) 837-6198

3.2 General Requirements

The general requirements for this stormwater maintenance management manual will meet the standards of Reference No.1, specific to the water quality feature concerned. Additional maintenance requirements are identified in the following narratives.

3.3 Specific Maintenance Requirements

The following specific maintenance requirements apply to stormwater features as follows:

3.3.1 R-Tanks

- The maintenance of the R-Tanks shall be in accordance with the manufacturer's recommendations. A copy of the Operation and Maintenance Guidelines for the Separator Row and Stormwater Management System are attached.
- Maintenance shall be performed by an appropriate service company with equipment designed for the purpose.

3.3.2 Outlet Control Structures

- The maintenance of outlet control structures shall be performed bi-annually to ensure proper function.
- Debris and trash shall be removed from the structure sump when present.
- Sediment build-up in the sump should be removed when accumulation is within 1 foot of the invert of the outlet pipe and/or snout hood is observed.

3.3.3 Storm Drain Pipes & Drainage Manholes

- Piped drainage systems shall be inspected in spring and late fall, and after heavy rains to remove any obstructions to flow; remove accumulated sediments and debris at the inlet, at the outlet, and within the conduit; and to repair any erosion damage at the culvert's inlet and outlet. Sediment should be removed when its level exceeds 20% of the pipe diameter. Hydraulic flushing or any mechanical means may accomplish sediment removal. Care shall be taken to contain the sediment at the pipe outlet.

3.3.4 Paved Surfaces

- Accumulations of winter sand along impervious areas shall be cleared at least once a year, preferably in the spring. Accumulations on pavement may be removed by pavement vacuum sweeping, or mechanical sweeping (e.g. "street-sweeper"). Accumulations of sand along the edge of paved areas may be removed by grading excess sand to the pavement edge and removing it manually or by a front-end loader.

3.3.5 Vegetative Surfaces

- For most vegetative surfaces, grass should be mowed on a regular basis so that grass height does not exceed 6 inches. Any erosion rills, gullies, or bare spots should be seeded or sodded to re-establish the turf cover.
- Buffer, screening, and decorative landscaping should be inspected for health on a regular basis. Pruning, weeding, feeding, and mulching.
- Fertilizers will only be applied once yearly, to occur in the spring, and at the lowest recommended concentration. Herbicides and pesticides will only be used in accordance with DEP recommendations.

3.3.6 Drainage Structures

- Inspect for sediment in traps/sump/bed of basin. Remove sediment if within 1 foot of outlet invert.
- Inspect frame and grate to verify grate is flush with finish grade.
- Inspect for damaged or missing pavement around frame and grate.
- Inspect structure for presence of trash or debris.
- Inspect for oil and oil adsorbent material if present.
- If applicable, inspect oil absorbent pad. Replace if necessary.

4.0 CONSTRUCTION INSPECTION AND MAINTENANCE

4.1 Maintenance Frequency

Inspections of the erosion and sedimentation control measures, and temporary and permanent stormwater features during the construction process shall be performed at least once per week and before and after each significant rainfall event. For the purposes of the inspection schedule, a significant rainfall event shall be any storm event that produces more than 0.5 inches of rainfall in a 24-hour period.

During winter construction, in the months from November to March, inspections shall be performed after each rainfall, snowstorm, or thawing, and at least once per week.

4.2 Inspection Scope

The scope of construction inspections shall include disturbed and impervious areas, material storage areas, and vehicle access points in addition to the erosion and sedimentation control measures, and temporary and permanent stormwater features.

4.3 Inspection and Maintenance Checklist

All inspection forms and documentation of corrective actions during construction shall be maintained for a minimum of three (3) years after permanent stabilization has been achieved.

4.4 Corrective Action Timeline

As part of the inspection and maintenance process, if any corrective action is warranted, it shall be started by the end of the next workday and completed within seven (7) days or before the next storm event, whichever comes first.

All required corrective actions shall be documented and maintained with the inspection forms.

4.5 Qualifications of Inspector

The person(s) responsible for inspection during construction and post-construction shall be conducted by someone with knowledge or erosion and stormwater control, including the standards and conditions of the approvals.

5.0 POST-CONSTRUCTION INSPECTION AND MAINTENANCE

5.1 Maintenance Frequency

Notwithstanding any other schedule noted, general inspections post-construction shall be conducted monthly during wet weather conditions from March to November. Inspections shall also be conducted following any significant storm events. For the purposes of the inspection schedule, a significant rainfall event shall be any storm event that produces more than 0.5 inches of rainfall in a 24-hour period. Specifically, inspections of the vegetated soil filters and pond shall be conducted following any significant storm event during the first year after construction to ensure that they drain dry within 24 to 48 hours.

5.2 Inspection and Maintenance Checklist

An inspection and maintenance log specific to this project is appended. All post-construction inspection forms and documentation of corrective actions shall be maintained for a minimum of five (5) years.

5.3 Corrective Action Timeline

As part of the inspection and maintenance process, if any corrective action is warranted, it shall be started by the end of the next workday and completed within seven (7) days or before the next storm event, whichever comes first.

All required corrective actions shall be documented and maintained with the inspection forms.

5.4 Qualifications of Inspector

The person(s) responsible for inspection during construction and post-construction shall be conducted by someone with knowledge or erosion and stormwater control, including the standards and conditions of the approvals.

6.0 RECERTIFICATION

6.1 Recertification requirement

Within three months of the expiration of each five-year interval from the date of issuance of the permit, the permittee shall certify the following to the department.

- 1) All areas of the project site have been inspected for areas of erosion, and appropriate steps have been taken to permanently stabilize these areas.
- 2) All aspects of the stormwater control system are operating as approved, have been inspected for damage, wear, and malfunction, and appropriate steps have been taken to repair or replace the system, or portions of the system, as necessary.
- 3) The stormwater maintenance plan for the site is being implemented as approved by the Department, and the maintenance log is being maintained.
- 4) All proprietary systems have been maintained according to the manufacturer's recommendations. Where required by the Department, the permittee shall execute a 5-year maintenance contract with a qualified professional for the coming 5-year interval. The maintenance contract must include provisions for routine inspections, cleaning and general maintenance.
- 5) The Department may waive some or all of these recertification requirements on a case-by-case basis for permittees subject to the Department's Multi-Sector General Permit ("MSGP") and/or Maine Pollutant Discharge Elimination System ("MEPDES") programs where it is demonstrated that these programs are providing stormwater control that is at least as effective as required pursuant to this Chapter.

A circular professional engineer seal for the State of Maine. The outer ring contains the text "STATE OF MAINE" at the top and "PROFESSIONAL ENGINEER" at the bottom, separated by two stars. The inner circle contains the text "CURTIS Y. NEUFELD" and "9779 LICENSED" arranged in a circular pattern.

PROJECT: RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME 04021

PREPARED FOR: CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

FIELD WK:	SCALE: 1"=30'	
DRN BY: CYN	JOB #: 22-RLM-004	
CH'D BY: CYN	MAP/LOT: U-19 12&13	
DATE: 11-22-23	FILE:	



February 13, 2024

22-RLT-004

Mr. Ronald Copp, Sr.
187 Gray Road
Cumberland, Maine 04021

Re: **Memorandum of Understanding**
PROPOSED CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME
Tax Map U19, Lot 12 & 13

Dear Mr. Copp,

As per our recent discussions, this memorandum to formalize and confirm our mutual understandings regarding the construction of a sidewalk along the frontage of your property located at 5 Skillin Road (Tax Map U19, Lot 37).

Priority Real Estate Group, LLC, is currently in the process of securing local and state permits for the development of a new convenience store and gas station at the intersection of Gray Road and Skillin Road, which is situated on a parcel of land owned by you. A sidewalk is mandated as part of the permit requirements set forth by MaineDOT, extending from the project site to Kathy Lane. This sidewalk will be constructed behind and adjacent to the existing curb. Given that the public right-of-way (ROW) spans 49.5 feet (3 rods) in width and does not include sufficient width to install the sidewalk and associated grading within the ROW, grading work outside the ROW will be necessary, extending slightly beyond the ROW limits and onto your property. Notably, the construction activities may impact mature trees and other vegetation along the frontage.

We understand from our discussions that you do not object to removing the vegetation, including the large oak tree if it is necessary for the project.

It is our understanding that a physical barrier shall be installed on the back side of the new walk as consideration for granting a grading easement. The barrier could be a fence (preferred) or plantings with year-round vegetation (e.g., hydrangea).

It is our understanding that the maintenance of the walk will be the responsibility of the Town of Cumberland.


We understand that the amount of vegetation impacted by the work will be determined by a detailed design and shared with you before the work.

If these understandings align with your expectations, I kindly request that you signify your agreement by signing below and returning a copy of this letter to me. Your signed agreement will be included in our application to MaineDOT as documentation of our coordination.

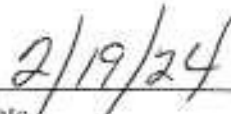
Thank you for your attention to this matter. Please do not hesitate to contact me if you have any questions or require further clarification.

Agreement

I have read and concur with the understandings above and will grant a temporary grading easement for the exclusive purpose of the construction of a sidewalk along the entire frontage of our land at 5 Skillin Road.

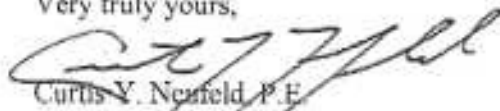


Ronald W. Copp, Sr.



Date

Very truly yours,


Curtis V. Newfield, P.E.
Vice-President

Enclosures



General Site Inspection Maintenance & Housekeeping Form			
General Information			
Project Name:	Rusty Lantern Market	Inspection Date	
Project Location:	181 Gray Road	Current Weather	
	Cumberland ME 04021	Date / Amount Last Percip.	
BMP Owner:	Cumberland Real Estate Holdings, LLC	Company Inspection:	
Owner Mailing Address:	2 Main Street	Company Mailing Address:	
	Topsham, ME 04086		
Owner Phone #:		Company Phone #:	
Owner Email:		Inspector Name	
		Inspector Email	
BMP Element	Suggested Maintenance & Recommended	Observations	Inspection Notes/Recommended
Vegetated Areas	Inspect slopes/embankments for erosion (annually)		
	Replant bare areas or areas of sparse growth (annually)		
Paved Surfaces	Clear accumulated winter sand (annually)		
	Remove sediment along edges of parking and within low spots / pockets (annually)		
Ditches/Swales	Remove obstructions/debris/sediment (monthly)		
	Inspect for erosion/repair as needed (annually)		
	Mow vegetated ditches (annually)		
Catch Basins	Remove sediment/debris from sump (annually)		
	Remove sediment/debris from inlet/outlet aprons (annually)		
Culverts	Inspect inlet/outlet aprons for erosion, repair as needed (annually)		
	Inspect, repair as needed, riprap aprons for dislodged/sparse coverage (annually)		
	Remove sediment/debris from outlet aprons (annually)		
Pipe Outlets	Inspect outlet aprons for erosion, repair as needed (annually)		
	Inspect, repair as needed, riprap aprons for dislodged/sparse coverage (annually)		
Additional Notes/Observations:			

Subsurface Sand Filter Inspection Maintenance & Housekeeping Form			
General Information			
Project Name:	Rusty Lantern Market	Inspection Date	
Project Location:	181 Gray Road	Current Weather	
	Cumberland ME 04021	Date / Amount Last Percip.	
BMP Owner:	Cumberland Real Estate Holdings, LLC	Company Inspection:	
Owner Mailing Address:	2 Main Street	Company Mailing Address:	
	Topsham, ME 04086		
Owner Phone #:		Company Phone #:	
Owner Email:		Inspector Name	
		Inspector Email	
BMP Element	Suggested Maintenance & Recommended Frequency	Observations	Inspection Notes/Recommended Action
Pre-Treatment Chamber Row	Inspect pre-treatment chamber row for presence of sediment via inspection port with a flashlight and stadia rod (annually)		
Subsurface Sand Filters	Inspect for evidence of excessive sediment deposits (annually)		
	Inspect overflow for presence of sediment and/or trash (annually)		
Catch Basins & Outlet Control Structures	Inspect for presence of sediment and/or trash (annually)		
	Inspect frame and grate to verify grate is flush with finish grade (annually)		
	Inspect for presence of trash and debris (annually)		
	Inspect oil adsorbent material (Smart Sponge). Replace per manufacturer's recommendations (annually)		
Additional Notes/Observations:			

AADT INCREASES DUE TO PROPOSED CUMBERLAND CONVENIENCE STORE DEVELOPMENT

AADT INCREASE CALCULATIONS

Existing AADTS for the four legs of the intersection are as follows:

- Skillin Road – 2,850
- Blackstrap Road – 2,952
- Route 26 – Southern Leg – 5,560
- Route 26 – Northern Leg – 5,610

No Build peak hour volumes for each of the approach and departure lanes are as follows:

Skillin Road – approaching Gray Road – 100 AM, 141 PM
Skillin Road – departing Gray Road – 144 AM, 156 PM
Blackstrap Road – approaching Gray Road - 162 AM, 122 PM
Blackstrap Road – departing Gray Road – 95 AM, 178 PM
Gray Road NB – approaching intersection – 152 AM, 395 PM
Gray Road NB – departing intersection – 151 AM, 337 PM
Gray Road SB, approaching intersection – 271 AM, 194 PM
Gray Road SB, departing intersection 292 AM, 180 PM

Percent increases for each of the approaches & departing lanes, based upon the primary trip assignments, are as follows:

Skillin Road – approaching Gray Road – 8 % AM, 5 % PM – 6.5 % average
Skillin Road – departing Gray Road – 3 % AM, 3 % PM – 3 % average
Blackstrap Road – approaching Gray Road – 5 % AM, 8 % PM, 6.5 % average
Blackstrap Road – departing Gray Road – 1 % AM, 6 % PM, 3.5 % average
Gray Road NB – approaching intersection – 8 % AM, 5 % PM, 6.5 % average
Gray Road NB – departing intersection – 7 % AM, 4 % PM, 5.5 % average
Gray Road SB, approaching intersection – 4 % AM, 8 % PM, 6 % average
Gray Road SB, departing intersection – 1 % AM, 3 % PM, 2 % average

Applying the average peak hour increases to the AADT for each lane results in the following:

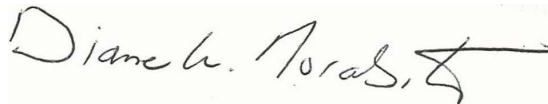
Skillin Road – approaching Gray Road – 6.5 % = 93 vehicles
Skillin Road – departing Gray Road – 3 % = 43 vehicles
Blackstrap Road – approaching Gray Road – 6.5 % = 96 vehicles
Blackstrap Road – departing Gray Road – 3.5 % = 52 vehicles
Gray Road NB – approaching intersection – 6.5 % = 181 vehicles
Gray Road NB – departing intersection – 5.5 % = 154 vehicles
Gray Road SB, approaching intersection – 6 % = 168 vehicles
Gray Road SB, departing intersection – 2 % = 56 vehicles

Total vehicle increases above = 843

As always, let me know if you have any questions or concerns regarding these calculations or results.



Sincerely,

A handwritten signature in black ink that reads "Diane W. Morabito" followed by a stylized flourish.

Diane W. Morabito, P.E. PTOE
Vice President Traffic Engineering

STORMWATER MANAGEMENT PLAN

Rusty Lantern Market 181 Gray Road, Cumberland, Maine

Introduction

Cumberland Real Estate Group, LLC (herein referred to as Applicant) is proposing the construction of a single-story, 5,038 s.f. convenience store building, gasoline pumps, canopy, associated parking, infrastructure, and landscaping situated on a site with frontage on Gray Road (U.S. Route 26) and Skillin Road in Cumberland, Maine. The proposed development will result in approximately 67,548 s.f. (1.55 acres) of impervious area. The increased runoff from the paved areas of site will be directed to one of two Subsurface Soil Filters for water quality treatment and water quantity mitigation. Currently the site has approximately 94,592 s.f. (2.17 acres) of impervious area, comprised of the existing building and pavement, and extensive gravel surfaced area compacted from years of use. The proposed project will result in a reduction of 27,044 s.f. (0.62 acres) of impervious area.

Available historical photographs were reviewed to determine when the existing parcels were previously developed. Most of the development had occurred by 1997, which is before the implementation of the Stormwater Law. The amount of undeveloped area was estimated from the aerial photograph to be approximately 34656 s.f. (0.80 acres). Per Maine Department of Environmental Protection (DEP) rules, only the area developed since 1997 would be required to meet the requirements of Chapter 500; however, since it is less than 1-acre, it does not meet the criteria for a Stormwater Law application. As the project results in less than an acre of new impervious area, it does not require a Stormwater Law permit from the DEP; however, a Stormwater Law Permit-by-Rule will be filed.

In accordance with the Town's ordinances, it is required to conform to Basic, General, and Flooding Standards in accordance with Chapter 500 of the DEP rules.

Study Methodology

Topographical data was obtained from an on-the-ground survey completed by Boundary Points, a division Main-Land. Hydrologic boundaries were generated using the topographic mapping, and the drainage patterns were verified by a site reconnaissance visit.

Surficial soils located in the vicinity of the site were obtained from the United States Department of Agriculture Natural Resources Conservation Service Soil Survey Geographic (SSURGO) Database. The Applicant's parcel includes the soil classifications listed below. Soil units found in the development area are primarily Hinkley Loamy Sand. Flycatcher, LLC, observed test pits to evaluate the seasonal high groundwater table at locations where stormwater best management practices (BMPs) are proposed. The Flycatcher report confirmed the soils were similar to Hinkley; with the observation that some imported fill was evident.

SOIL TYPES IN LOCAL STUDY AREA

Soils Series	Symbol(s)	Hydrologic Group (HSG) **
Hinckley Loamy Sand	HIB	A

**Hydrologic Soils Group taken from SCS TR-55 Manual

Test pits were completed at the site by Summit Geoengineering. A copy of the geotechnical investigation has been enclosed with this submission.

Basic Standards

Erosion control BMPs are shown on the project drawings, and notes and details on implementing them are included on separate drawings in the set. The Contractor will be responsible for maintaining the BMPs throughout construction. After the site is stabilized and accepted by the owner, the owner will be responsible for maintaining the permanent BMPs.

Disturbed area will be minimized by clearing only the amount of land required for the construction of each building, which will not be constructed concurrently.

Major site work activities and their sequence follow:

1. Install a stabilized construction entrance.
2. Cut and remove trees around area of work, as necessary, leaving the duff layer in place.
3. Set sediment barrier and erosion control measures around the perimeter of the limits of work. Stumps shall be ground onsite and used for sediment barrier and/or mulch.
4. Clear and grub the work site as needed to execute plans using caution not to overexpose the site. Topsoil salvaged shall be stockpiled and protected against erosion.
5. Install storm drainage and infrastructure, including access.
6. Construct buildings.
7. Construct pavement.
8. Loam, seed, and mulch disturbed areas.
9. Monitor the site for signs of erosion monthly and after major storm events.
10. Removal of temporary erosion control measures. Ninety (90) days post-construction or upon satisfactory establishment of vegetation has been obtained.
11. Inspect the site semi-annually for any sign of erosion or area requiring additional seeding.

The contractor shall monitor the disturbed area for signs of erosion or sediment transport off-site and take corrective action immediately. Inspections shall be logged using the form supplied in the stormwater facilities maintenance plan and kept on file. Completed logs shall be maintained by the Applicant after construction.

Flooding Standard

The project area is located in Zone C (Areas of Minimal Flooding) of the Flood Insurance Rate Maps (FIRMs) for Cumberland County, Maine. The project area is located on Panel 18 of 25 (Community Panel 230162-0015-B, Effective May 19, 1981). An excerpt of the applicable FIRM is enclosed with the supporting graphics. There is no impact from flooding anticipated for this project.

Off-Site Watersheds

There are no off-site watersheds that were reviewed as part of the stormwater analysis. The project area has little variation in elevation and adjacent roads and developed areas serve as hydrologic boundaries.

On-Site Subcatchments

Pre-Development Conditions

The pre-development hydrologic analysis is based on the existing site condition, which is mostly undeveloped and comprised of paved and unpaved areas. The development area is relatively flat and drains from a high point near the middle to the perimeter of the graveled area. Runoff from the front portion of the site is conveyed into the existing storm drain system in Gray Road.

- | | |
|----------------|--|
| Subcatchment 1 | represents the area immediately adjacent to the intersection of Gray and Skillin Roads. The area drains to existing catch basins connected to the storm drains in the ROW. |
| Subcatchment 2 | represents 0.32-acres that drains internally to a catch basin connected to the storm drain in the Skillin Road ROW. |
| Subcatchment 3 | represents approximately 0.31-acres that drains to the abutting land to the east. |
| Subcatchment 4 | represents approximately 0.74-acres that drains toward Gray Road, where it is collected at a catch basin. |
| Subcatchment 5 | represents a small area that drains to the abutting property. |
| Subcatchment 6 | represents an approximately 0.27-acre area of gravel and woods that drains to the east. |
| Subcatchment 7 | represents an approximately 0.39-acre area of gravel and woods that drains to the southeast. |
| Subcatchment 8 | represents an approximately 0.48-acre area of gravel surface that drains to the parcel to the south of the site. |
| Subcatchment 9 | represents an approximately 0.33-acre area of gravel surface that drains to the Gray Road ROW. |

Post-Development Conditions

Under post-development conditions, the commercial buildings will be constructed with associated paved access, landscaping, and infrastructure. Stormwater runoff from the new impervious area will be directed to one of two Subsurface Soil Filters, with the exception of the roofs, which will drain an infiltration basin or stone drip edge. A summary of the subcatchments is provided below:

- | | |
|----------------|---|
| Subcatchment 1 | represents the convenience store and lawn areas between it and the intersection of the roads. These areas drain to an infiltration gallery. |
|----------------|---|

- Subcatchment 2 represents the parking area, fueling pumps, and entrance from Gray Road. This area is collected by catch basins and conveyed to Subsurface Soil Filter #1 (SSSF#1).
- Subcatchment 3 represents the parking area and drive-thru lanes for the bank. This area is collected by catch basins and conveyed to SSSF#2.
- Subcatchment 4 represents the bank building, which will drain to a drip edge filter BMP.
- Subcatchment 6 represents an approximately 0.27-acre area of gravel surface and woods that drains to the east.
- Subcatchment 7 represents an approximately 0.39-acre area of gravel surface and woods that drains to the southeast.
- Subcatchment 8 represents an approximately 0.48-acre area of gravel surface that drains to the parcel to the south of the site.
- Subcatchment 9 represents an approximately 0.15-acre area of lawn and walk that drains to the Gray Road ROW.
- Subcatchment 10 represents an approximately 0.15-acre area of lawn and walk that drains to the Gray Road ROW.
- Subcatchment 11 represents an approximately 0.14-acre area of lawn and walk that drains to the Gray Road ROW.

Results

A comparison of pre-development and post-development peak rates of stormwater runoff at the Analysis Points is presented in the following tables. Peak runoff rates were estimated for the 2-, 10-, 25, and 50-year 24-hour storm events.

Analysis Point 1 (POI#1)	Peak Runoff Rate (cfs)		
Design Storm	Pre-Development	Post-Development	Difference
2-Year	1.05	0.45	-0.60
10-Year	1.50	0.60	-0.90
25-Year	2.00	0.73	-1.27
50-Year	2.39	0.90	-1.49

Analysis Point 1 (POI#2)	Peak Runoff Rate (cfs)		
Design Storm	Pre-Development	Post-Development	Difference
2-Year	3.70	0.17	-3.53
10-Year	5.34	0.37	-4.97
25-Year	7.06	0.63	-6.43
50-Year	8.44	0.90	-7.54

As shown in the tables above, the total net peak rate of flow leaving the site is reduced for all storm events.

General Standard

An analysis of the pre-development and post-development areas shows that the runoff from 96% of the proposed impervious area and 81% of the proposed developed area on the parcel will be directed to the Subsurface Soil Filters for treatment and detention. The results are presented in the following table.

The proposed project will create approximately 67,548 (1.55 acres) of new impervious area. Runoff from approximately 63,190 s.f. (1.36 acres), or 94%, of the impervious area will be conveyed to the Subsurface Soil Filters for treatment and detention. In the post-development condition, the site will include approximately 30,829 s.f. (0.71 acres) of landscaped area, for a total of 85,825 s.f. (1.97 acres) of developed area. Runoff from approximately 18,355 s.f. (0.42 acres) of the landscaped area will be conveyed to the Filter, resulting in 70,678 s.f. (1.62 acres), or 82.4%, of the developed areas directed to the SSF for treatment and detention.

Water Quality

The project is required to provide stormwater treatment for 95% of the impervious area and 80% of the developed area. This goal for water quality treatment is achieved using two (2) Subsurface Soil Filters for the paved areas, and infiltration system for the convenience store building, and drip-edge treatment BMPs for the bank building.

Subsurface Soil Filters

Two Subsurface Soil Filters with underdrains and liners are proposed for the treatment and detention of the runoff from the proposed paved areas, including the developed landscaped area, paved parking and access aisles. The filter has been sized so that the surface area of the filter is greater than 5% of the impervious tributary area plus 2% of the landscaped tributary area. The media is 18" thick and designed to store a treatment volume greater than 1.0 inch over the impervious area and 0.4 inches over the landscaped area, and filter at a rate of 2.41 inches per hour. Separation is provided between the bottom of the filter media and the high seasonal water table and liners are proposed for the bottoms of the systems. The maximum depth of stored runoff is less than 18 inches. Overflows have been included in the design to allow for detention within the subsurface soil filter footprint.

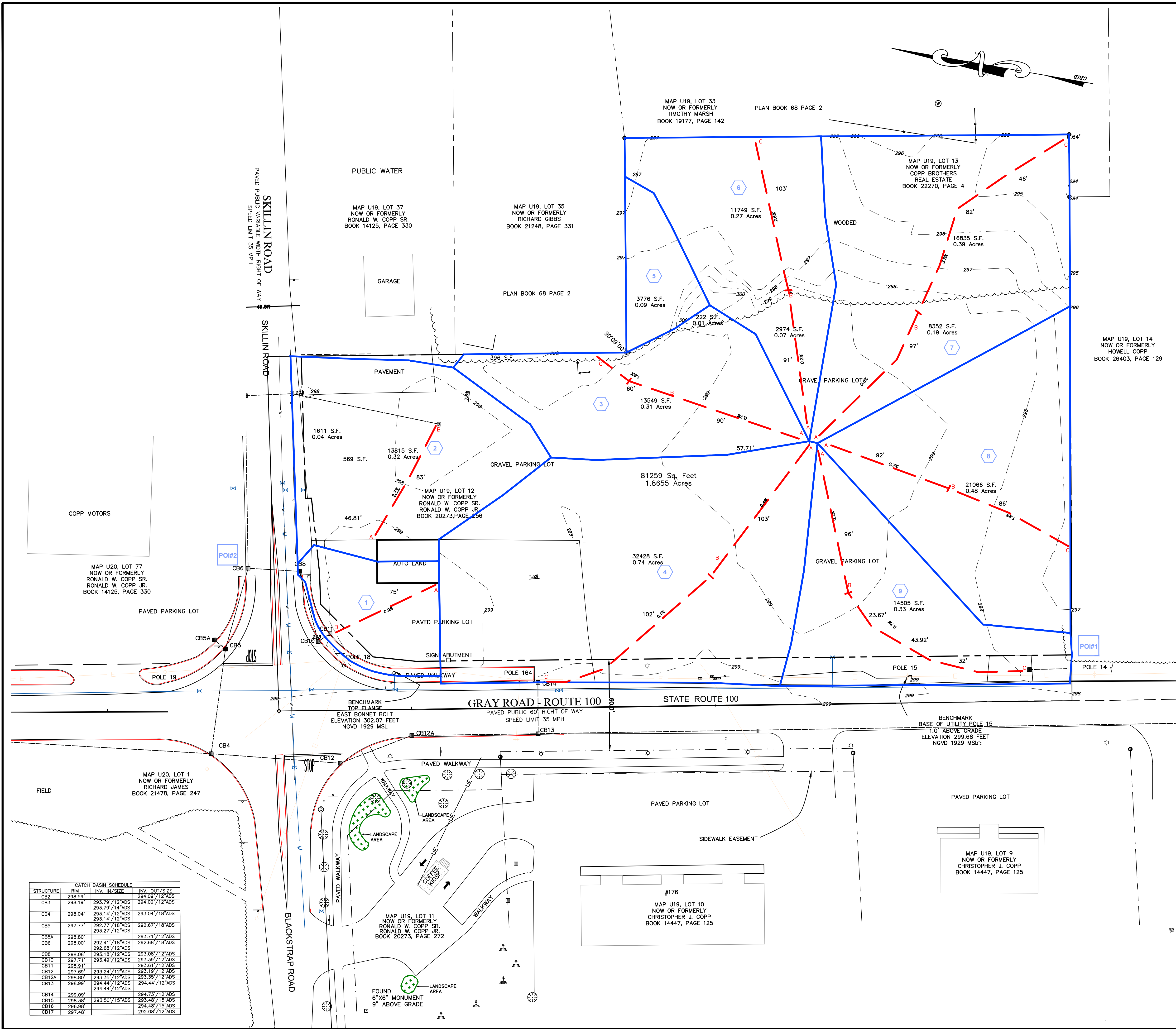
Conclusion

Through the implementation of erosion and sedimentation control measures and best management practices,

the project complies with the requirements of the Basic Standard.

By collecting and treating runoff from new impervious area, 96% of the new impervious area will be treated in accordance with Chapter 500. Similarly, 81% of the developed area will be treated prior to discharge from the site. The runoff from the development will not adversely impact the existing storm drains in Route 26 or the adjacent parcels. By capturing and treating runoff from the impervious surfaces and developed areas the project likewise meets the applicable portions of the General Standard. The General Standard is met and exceeded. By providing detention in the proposed stormwater management BMPs, the peak runoff rates of the post-development condition are reduced to below the pre-development peak runoff rates; the project is not subject to the requirements of the Flooding Standard, but the development has been designed so that the project complies with the requirements of the Flooding Standard.

Attachment 1 – Pre-Development HydroCAD Report
Attachment 2 – Pre-Development Watershed Map
Attachment 3 – Post-Development HydroCAD Report
Attachment 4 – Post-Development Watershed Map



CATCH BASIN SCHEDULE				
STRUCTURE	RM	IN	IN/ SIZE	OUT/ SIZE
CB1	298'19"	293'79"	12" AD	294.09' / 12" AD
CB3	298'19"	293'79"	12" AD	294.09' / 12" AD
CB4	298'04"	293'14"	12" AD	293.04' / 18" AD
CB5	297'77"	293'77"	18" AD	292.67' / 18" AD
CB5A	298'80"	293'27"	12" AD	293.71' / 12" AD
CB6	298'80"	292'41"	18" AD	292.68' / 18" AD
CB8	298'08"	293'18"	12" AD	293.08' / 12" AD
CB10	297'71"	293'49"	12" AD	293.39' / 12" AD
CB11	298'91"	293'35"	12" AD	293.61' / 12" AD
CB12	298'69"	293'24"	12" AD	293.54' / 12" AD
CB12A	298'80"	293'25"	12" AD	293.35' / 12" AD
CB13	298'99"	294'44"	12" AD	294.44' / 12" AD
CB14	299'09"			294.73' / 12" AD
CB15	298'36"	293'50"	15" AD	294.48' / 15" AD
CB16	298'91"	293'48"	12" AD	293.48' / 12" AD
CB17	297'48"			292.08' / 12" AD

LEGEND:

The diagram shows a vertical stack of shapes: a hexagon labeled '1S' at the top, followed by a rectangle labeled 'POI#1' below it. To the right of these shapes are the labels 'SUBCATCHMENT AREA' and 'POINT OF INTEREST' respectively. Below the shapes is a horizontal red line with 'A' at the left end and 'B' at the right end. To the right of this line is the label 'TIME OF CONCENTRATION'.

PRIORITY
2 MAIN STREET
TOPSHAM, MAINE 04086

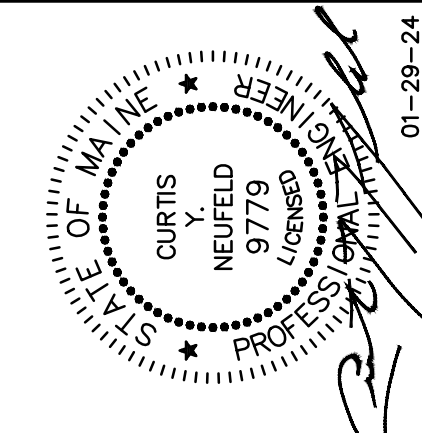
DR1

FIELD WK:	SCALE: 1"=30'	SHEET: DR
DRN BY: CYN	JOB #: 22-RLM-004	
CHD BY: CYN	MAP/LOT: U-19 12&13	
DATE: 11-22-23	FILE:	

PRE-DEVELOPMENT DRAINAGE PLAN

RUSTY LANTERN CONVENIENCE STORE

PR: CUMBERLAND REAL ESTATE GROUP, LLC



NOT FOR CONSTRUCTION

THIS PLAN IS ISSUED FOR REVIEW AND INFORMATION PURPOSES ONLY. THIS PLAN WILL CHANGE AND IS NOT INTENDED FOR PRICING OR CONSTRUCTION.

PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.

GRAPHIC SCALE

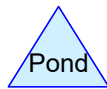
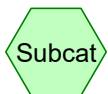
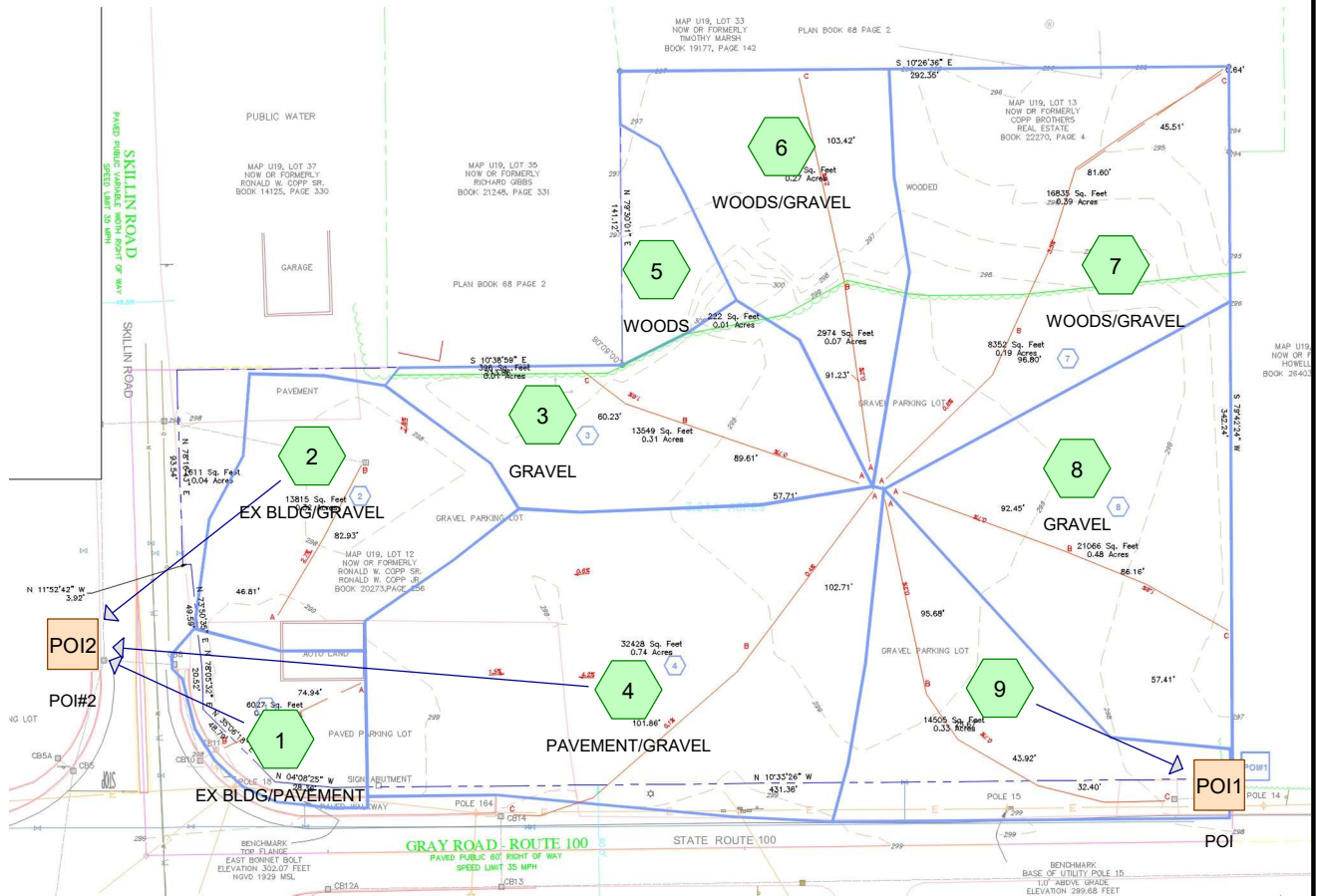
0 15 30

(IN FEET)

1 inch = 30 ft.

ISSUED FOR:

PERMITTING



Routing Diagram for Cumberland PreDev
 Prepared by Priority Real Estate Group LLC, Printed 2/5/2024
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Cumberland PreDev

Prepared by Priority Real Estate Group LLC

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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-yr	Cumberland 24-hr S1	2-yr	Default	24.00	1	3.10	2
2	5-Year	Type III 24-hr		Default	24.00	1	3.66	2
3	10-Year	Type III 24-hr		Default	24.00	1	4.60	2
4	25-yr	Cumberland 24-hr S1	25-yr	Default	24.00	1	5.80	2
5	50-Year	Type III 24-hr		Default	24.00	1	6.27	2

Cumberland PreDev

Prepared by Priority Real Estate Group LLC

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
2.449	0.000	0.000	0.000	0.000	2.449	Gravel surface	2, 3, 4, 6, 7, 8, 9
0.138	0.000	0.000	0.000	0.000	0.138	Paved parking	1
0.743	0.000	0.000	0.000	0.000	0.743	Woods, Good	5, 6, 7
3.330	0.000	0.000	0.000	0.000	3.330	TOTAL AREA	

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: EX BLDG/PAVEMENT Runoff Area=6,027 sf 100.00% Impervious Runoff Depth=2.87"
Flow Length=75' Slope=0.0090 '/' Tc=5.0 min CN=98 Runoff=0.45 cfs 0.033 af

Subcatchment 2: EX BLDG/GRAVEL Runoff Area=13,815 sf 0.00% Impervious Runoff Depth=2.65"
Flow Length=83' Slope=0.0270 '/' Tc=5.0 min CN=96 Runoff=1.00 cfs 0.070 af

Subcatchment 3: GRAVEL Runoff Area=13,549 sf 0.00% Impervious Runoff Depth=2.65"
Flow Length=150' Tc=5.0 min CN=96 Runoff=0.98 cfs 0.069 af

Subcatchment 4: PAVEMENT/GRAVEL Runoff Area=32,428 sf 0.00% Impervious Runoff Depth=2.65"
Flow Length=202' Tc=5.7 min CN=96 Runoff=2.26 cfs 0.164 af

Subcatchment 5: WOODS Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.00"
Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af

Subcatchment 6: WOODS/GRAVEL Runoff Area=14,723 sf 0.00% Impervious Runoff Depth=0.01"
Flow Length=194' Tc=5.3 min CN=43 Runoff=0.00 cfs 0.000 af

Subcatchment 7: WOODS/GRAVEL Runoff Area=25,187 sf 0.00% Impervious Runoff Depth=0.15"
Flow Length=100' Slope=0.0080 '/' Tc=5.0 min CN=52 Runoff=0.01 cfs 0.007 af

Subcatchment 8: GRAVEL Runoff Area=21,066 sf 0.00% Impervious Runoff Depth=2.65"
Flow Length=186' Tc=5.0 min CN=96 Runoff=1.52 cfs 0.107 af

Subcatchment 9: Runoff Area=14,505 sf 0.00% Impervious Runoff Depth=2.65"
Flow Length=100' Slope=0.0020 '/' Tc=5.0 min CN=96 Runoff=1.05 cfs 0.074 af

Reach POI1: POI Inflow=1.05 cfs 0.074 af
Outflow=1.05 cfs 0.074 af

Reach POI2: POI#2 Inflow=3.70 cfs 0.268 af
Outflow=3.70 cfs 0.268 af

Total Runoff Area = 3.330 ac Runoff Volume = 0.524 af Average Runoff Depth = 1.89"
95.85% Pervious = 3.192 ac 4.15% Impervious = 0.138 ac

Summary for Subcatchment 1: EX BLDG/PAVEMENT

Runoff = 0.45 cfs @ 12.02 hrs, Volume= 0.033 af, Depth= 2.87"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
6,027	98	Paved parking, HSG A
6,027		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	75	0.0090	0.91		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.4	75	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 2: EX BLDG/GRAVEL

Runoff = 1.00 cfs @ 12.02 hrs, Volume= 0.070 af, Depth= 2.65"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
13,815	96	Gravel surface, HSG A
13,815		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	83	0.0270	1.45		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.0	83	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 3: GRAVEL

Runoff = 0.98 cfs @ 12.02 hrs, Volume= 0.069 af, Depth= 2.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
13,549	96	Gravel surface, HSG A
13,549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	90	0.0070	0.86		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	60	0.0160	2.04		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.3	150	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 4: PAVEMENT/GRAVEL

Runoff = 2.26 cfs @ 12.03 hrs, Volume= 0.164 af, Depth= 2.65"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
32,428	96	Gravel surface, HSG A
32,428		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	100	0.0040	0.70		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.3	102	0.0010	0.51		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
5.7	202	Total			

Summary for Subcatchment 5: WOODS

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 6: WOODS/GRAVEL

Runoff = 0.00 cfs @ 24.00 hrs, Volume= 0.000 af, Depth= 0.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
11,749	30	Woods, Good, HSG A
2,974	96	Gravel surface, HSG A
14,723	43	Weighted Average
14,723		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Summary for Subcatchment 7: WOODS/GRAVEL

Runoff = 0.01 cfs @ 13.24 hrs, Volume= 0.007 af, Depth= 0.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
16,835	30	Woods, Good, HSG A
8,352	96	Gravel surface, HSG A
25,187	52	Weighted Average
25,187		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.8	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 8: GRAVEL

Runoff = 1.52 cfs @ 12.02 hrs, Volume= 0.107 af, Depth= 2.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
21,066	96	Gravel surface, HSG A
21,066		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 9:

Runoff = 1.05 cfs @ 12.02 hrs, Volume= 0.074 af, Depth= 2.65"
 Routed to Reach POI1 : POI

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
14,505	96	Gravel surface, HSG A
14,505		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.1	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach POI1: POI

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.333 ac, 0.00% Impervious, Inflow Depth = 2.65" for 2-yr event
Inflow = 1.05 cfs @ 12.02 hrs, Volume= 0.074 af
Outflow = 1.05 cfs @ 12.02 hrs, Volume= 0.074 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, 11.53% Impervious, Inflow Depth = 2.68" for 2-yr event
Inflow = 3.70 cfs @ 12.03 hrs, Volume= 0.268 af
Outflow = 3.70 cfs @ 12.03 hrs, Volume= 0.268 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: EX BLDG/PAVEMENT Runoff Area=6,027 sf 100.00% Impervious Runoff Depth=3.43"
Flow Length=75' Slope=0.0090 '/' Tc=5.0 min CN=98 Runoff=0.50 cfs 0.040 af

Subcatchment 2: EX BLDG/GRAVEL Runoff Area=13,815 sf 0.00% Impervious Runoff Depth=3.20"
Flow Length=83' Slope=0.0270 '/' Tc=5.0 min CN=96 Runoff=1.12 cfs 0.085 af

Subcatchment 3: GRAVEL Runoff Area=13,549 sf 0.00% Impervious Runoff Depth=3.20"
Flow Length=150' Tc=5.0 min CN=96 Runoff=1.10 cfs 0.083 af

Subcatchment 4: PAVEMENT/GRAVEL Runoff Area=32,428 sf 0.00% Impervious Runoff Depth=3.20"
Flow Length=202' Tc=5.7 min CN=96 Runoff=2.58 cfs 0.199 af

Subcatchment 5: WOODS Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.00"
Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af

Subcatchment 6: WOODS/GRAVEL Runoff Area=14,723 sf 0.00% Impervious Runoff Depth=0.07"
Flow Length=194' Tc=5.3 min CN=43 Runoff=0.00 cfs 0.002 af

Subcatchment 7: WOODS/GRAVEL Runoff Area=25,187 sf 0.00% Impervious Runoff Depth=0.30"
Flow Length=100' Slope=0.0080 '/' Tc=5.0 min CN=52 Runoff=0.07 cfs 0.014 af

Subcatchment 8: GRAVEL Runoff Area=21,066 sf 0.00% Impervious Runoff Depth=3.20"
Flow Length=186' Tc=5.0 min CN=96 Runoff=1.71 cfs 0.129 af

Subcatchment 9: Runoff Area=14,505 sf 0.00% Impervious Runoff Depth=3.20"
Flow Length=100' Slope=0.0020 '/' Tc=5.0 min CN=96 Runoff=1.18 cfs 0.089 af

Reach POI1: POI Inflow=1.18 cfs 0.089 af
Outflow=1.18 cfs 0.089 af

Reach POI2: POI#2 Inflow=4.20 cfs 0.323 af
Outflow=4.20 cfs 0.323 af

Total Runoff Area = 3.330 ac Runoff Volume = 0.640 af Average Runoff Depth = 2.31"
95.85% Pervious = 3.192 ac 4.15% Impervious = 0.138 ac

Summary for Subcatchment 1: EX BLDG/PAVEMENT

Runoff = 0.50 cfs @ 12.07 hrs, Volume= 0.040 af, Depth= 3.43"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
6,027	98	Paved parking, HSG A
6,027		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	75	0.0090	0.91		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.4	75	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 2: EX BLDG/GRAVEL

Runoff = 1.12 cfs @ 12.07 hrs, Volume= 0.085 af, Depth= 3.20"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
13,815	96	Gravel surface, HSG A
13,815		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	83	0.0270	1.45		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.0	83	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 3: GRAVEL

Runoff = 1.10 cfs @ 12.07 hrs, Volume= 0.083 af, Depth= 3.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
13,549	96	Gravel surface, HSG A
13,549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	90	0.0070	0.86		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	60	0.0160	2.04		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.3	150	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 4: PAVEMENT/GRAVEL

Runoff = 2.58 cfs @ 12.08 hrs, Volume= 0.199 af, Depth= 3.20"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
32,428	96	Gravel surface, HSG A
32,428		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	100	0.0040	0.70		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.3	102	0.0010	0.51		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
5.7	202	Total			

Summary for Subcatchment 5: WOODS

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 6: WOODS/GRAVEL

Runoff = 0.00 cfs @ 14.96 hrs, Volume= 0.002 af, Depth= 0.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
11,749	30	Woods, Good, HSG A
2,974	96	Gravel surface, HSG A
14,723	43	Weighted Average
14,723		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Summary for Subcatchment 7: WOODS/GRAVEL

Runoff = 0.07 cfs @ 12.31 hrs, Volume= 0.014 af, Depth= 0.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
16,835	30	Woods, Good, HSG A
8,352	96	Gravel surface, HSG A
25,187	52	Weighted Average
25,187		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.8	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 8: GRAVEL

Runoff = 1.71 cfs @ 12.07 hrs, Volume= 0.129 af, Depth= 3.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
21,066	96	Gravel surface, HSG A
21,066		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 9:

Runoff = 1.18 cfs @ 12.07 hrs, Volume= 0.089 af, Depth= 3.20"
 Routed to Reach POI1 : POI

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
14,505	96	Gravel surface, HSG A
14,505		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.1	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach POI1: POI

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.333 ac, 0.00% Impervious, Inflow Depth = 3.20" for 5-Year event
Inflow = 1.18 cfs @ 12.07 hrs, Volume= 0.089 af
Outflow = 1.18 cfs @ 12.07 hrs, Volume= 0.089 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, 11.53% Impervious, Inflow Depth = 3.23" for 5-Year event
Inflow = 4.20 cfs @ 12.08 hrs, Volume= 0.323 af
Outflow = 4.20 cfs @ 12.08 hrs, Volume= 0.323 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: EX BLDG/PAVEMENT Runoff Area=6,027 sf 100.00% Impervious Runoff Depth=4.36"
Flow Length=75' Slope=0.0090 '/' Tc=5.0 min CN=98 Runoff=0.63 cfs 0.050 af

Subcatchment 2: EX BLDG/GRAVEL Runoff Area=13,815 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=83' Slope=0.0270 '/' Tc=5.0 min CN=96 Runoff=1.43 cfs 0.109 af

Subcatchment 3: GRAVEL Runoff Area=13,549 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=150' Tc=5.0 min CN=96 Runoff=1.40 cfs 0.107 af

Subcatchment 4: PAVEMENT/GRAVEL Runoff Area=32,428 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=202' Tc=5.7 min CN=96 Runoff=3.29 cfs 0.257 af

Subcatchment 5: WOODS Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.00"
Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af

Subcatchment 6: WOODS/GRAVEL Runoff Area=14,723 sf 0.00% Impervious Runoff Depth=0.25"
Flow Length=194' Tc=5.3 min CN=43 Runoff=0.03 cfs 0.007 af

Subcatchment 7: WOODS/GRAVEL Runoff Area=25,187 sf 0.00% Impervious Runoff Depth=0.63"
Flow Length=100' Slope=0.0080 '/' Tc=5.0 min CN=52 Runoff=0.27 cfs 0.030 af

Subcatchment 8: GRAVEL Runoff Area=21,066 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=186' Tc=5.0 min CN=96 Runoff=2.18 cfs 0.167 af

Subcatchment 9: Runoff Area=14,505 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=100' Slope=0.0020 '/' Tc=5.0 min CN=96 Runoff=1.50 cfs 0.115 af

Reach POI1: POI Inflow=1.50 cfs 0.115 af
Outflow=1.50 cfs 0.115 af

Reach POI2: POI#2 Inflow=5.34 cfs 0.416 af
Outflow=5.34 cfs 0.416 af

Total Runoff Area = 3.330 ac Runoff Volume = 0.842 af Average Runoff Depth = 3.03"
95.85% Pervious = 3.192 ac 4.15% Impervious = 0.138 ac

Summary for Subcatchment 1: EX BLDG/PAVEMENT

Runoff = 0.63 cfs @ 12.07 hrs, Volume= 0.050 af, Depth= 4.36"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
6,027	98	Paved parking, HSG A
6,027		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	75	0.0090	0.91		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.4	75	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 2: EX BLDG/GRAVEL

Runoff = 1.43 cfs @ 12.07 hrs, Volume= 0.109 af, Depth= 4.14"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
13,815	96	Gravel surface, HSG A
13,815		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	83	0.0270	1.45		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.0	83	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 3: GRAVEL

Runoff = 1.40 cfs @ 12.07 hrs, Volume= 0.107 af, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
13,549	96	Gravel surface, HSG A
13,549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	90	0.0070	0.86		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	60	0.0160	2.04		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.3	150	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 4: PAVEMENT/GRAVEL

Runoff = 3.29 cfs @ 12.08 hrs, Volume= 0.257 af, Depth= 4.14"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
32,428	96	Gravel surface, HSG A
32,428		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	100	0.0040	0.70		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.3	102	0.0010	0.51		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
5.7	202	Total			

Summary for Subcatchment 5: WOODS

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 6: WOODS/GRAVEL

Runoff = 0.03 cfs @ 12.40 hrs, Volume= 0.007 af, Depth= 0.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
11,749	30	Woods, Good, HSG A
2,974	96	Gravel surface, HSG A
14,723	43	Weighted Average
14,723		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Summary for Subcatchment 7: WOODS/GRAVEL

Runoff = 0.27 cfs @ 12.11 hrs, Volume= 0.030 af, Depth= 0.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
16,835	30	Woods, Good, HSG A
8,352	96	Gravel surface, HSG A
25,187	52	Weighted Average
25,187		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.8	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 8: GRAVEL

Runoff = 2.18 cfs @ 12.07 hrs, Volume= 0.167 af, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
21,066	96	Gravel surface, HSG A
21,066		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 9:

Runoff = 1.50 cfs @ 12.07 hrs, Volume= 0.115 af, Depth= 4.14"
 Routed to Reach POI1 : POI

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
14,505	96	Gravel surface, HSG A
14,505		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.1	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach POI1: POI

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.333 ac, 0.00% Impervious, Inflow Depth = 4.14" for 10-Year event
Inflow = 1.50 cfs @ 12.07 hrs, Volume= 0.115 af
Outflow = 1.50 cfs @ 12.07 hrs, Volume= 0.115 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, 11.53% Impervious, Inflow Depth = 4.16" for 10-Year event
Inflow = 5.34 cfs @ 12.08 hrs, Volume= 0.416 af
Outflow = 5.34 cfs @ 12.08 hrs, Volume= 0.416 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: EX BLDG/PAVEMENT Runoff Area=6,027 sf 100.00% Impervious Runoff Depth=5.56"
Flow Length=75' Slope=0.0090 '/' Tc=5.0 min CN=98 Runoff=0.84 cfs 0.064 af

Subcatchment 2: EX BLDG/GRAVEL Runoff Area=13,815 sf 0.00% Impervious Runoff Depth=5.33"
Flow Length=83' Slope=0.0270 '/' Tc=5.0 min CN=96 Runoff=1.91 cfs 0.141 af

Subcatchment 3: GRAVEL Runoff Area=13,549 sf 0.00% Impervious Runoff Depth=5.33"
Flow Length=150' Tc=5.0 min CN=96 Runoff=1.87 cfs 0.138 af

Subcatchment 4: PAVEMENT/GRAVEL Runoff Area=32,428 sf 0.00% Impervious Runoff Depth=5.33"
Flow Length=202' Tc=5.7 min CN=96 Runoff=4.33 cfs 0.331 af

Subcatchment 5: WOODS Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.05"
Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af

Subcatchment 6: WOODS/GRAVEL Runoff Area=14,723 sf 0.00% Impervious Runoff Depth=0.60"
Flow Length=194' Tc=5.3 min CN=43 Runoff=0.08 cfs 0.017 af

Subcatchment 7: WOODS/GRAVEL Runoff Area=25,187 sf 0.00% Impervious Runoff Depth=1.19"
Flow Length=100' Slope=0.0080 '/' Tc=5.0 min CN=52 Runoff=0.68 cfs 0.057 af

Subcatchment 8: GRAVEL Runoff Area=21,066 sf 0.00% Impervious Runoff Depth=5.33"
Flow Length=186' Tc=5.0 min CN=96 Runoff=2.91 cfs 0.215 af

Subcatchment 9: Runoff Area=14,505 sf 0.00% Impervious Runoff Depth=5.33"
Flow Length=100' Slope=0.0020 '/' Tc=5.0 min CN=96 Runoff=2.00 cfs 0.148 af

Reach POI1: POI Inflow=2.00 cfs 0.148 af
Outflow=2.00 cfs 0.148 af

Reach POI2: POI#2 Inflow=7.06 cfs 0.536 af
Outflow=7.06 cfs 0.536 af

Total Runoff Area = 3.330 ac Runoff Volume = 1.111 af Average Runoff Depth = 4.00"
95.85% Pervious = 3.192 ac 4.15% Impervious = 0.138 ac

Summary for Subcatchment 1: EX BLDG/PAVEMENT

Runoff = 0.84 cfs @ 12.02 hrs, Volume= 0.064 af, Depth= 5.56"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
6,027	98	Paved parking, HSG A
6,027		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	75	0.0090	0.91		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.4	75	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 2: EX BLDG/GRAVEL

Runoff = 1.91 cfs @ 12.02 hrs, Volume= 0.141 af, Depth= 5.33"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
13,815	96	Gravel surface, HSG A
13,815		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	83	0.0270	1.45		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.0	83	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 3: GRAVEL

Runoff = 1.87 cfs @ 12.02 hrs, Volume= 0.138 af, Depth= 5.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
13,549	96	Gravel surface, HSG A
13,549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	90	0.0070	0.86		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	60	0.0160	2.04		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.3	150	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 4: PAVEMENT/GRAVEL

Runoff = 4.33 cfs @ 12.03 hrs, Volume= 0.331 af, Depth= 5.33"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
32,428	96	Gravel surface, HSG A
32,428		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	100	0.0040	0.70		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.3	102	0.0010	0.51		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
5.7	202	Total			

Summary for Subcatchment 5: WOODS

Runoff = 0.00 cfs @ 23.96 hrs, Volume= 0.000 af, Depth= 0.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 6: WOODS/GRAVEL

Runoff = 0.08 cfs @ 12.08 hrs, Volume= 0.017 af, Depth= 0.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
11,749	30	Woods, Good, HSG A
2,974	96	Gravel surface, HSG A
14,723	43	Weighted Average
14,723		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Summary for Subcatchment 7: WOODS/GRAVEL

Runoff = 0.68 cfs @ 12.04 hrs, Volume= 0.057 af, Depth= 1.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
16,835	30	Woods, Good, HSG A
8,352	96	Gravel surface, HSG A
25,187	52	Weighted Average
25,187		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.8	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 8: GRAVEL

Runoff = 2.91 cfs @ 12.02 hrs, Volume= 0.215 af, Depth= 5.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
21,066	96	Gravel surface, HSG A
21,066		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 9:

Runoff = 2.00 cfs @ 12.02 hrs, Volume= 0.148 af, Depth= 5.33"
 Routed to Reach POI1 : POI

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
14,505	96	Gravel surface, HSG A
14,505		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.1	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach POI1: POI

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.333 ac, 0.00% Impervious, Inflow Depth = 5.33" for 25-yr event
Inflow = 2.00 cfs @ 12.02 hrs, Volume= 0.148 af
Outflow = 2.00 cfs @ 12.02 hrs, Volume= 0.148 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, 11.53% Impervious, Inflow Depth = 5.36" for 25-yr event
Inflow = 7.06 cfs @ 12.03 hrs, Volume= 0.536 af
Outflow = 7.06 cfs @ 12.03 hrs, Volume= 0.536 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: EX BLDG/PAVEMENT Runoff Area=6,027 sf 100.00% Impervious Runoff Depth=6.03"
Flow Length=75' Slope=0.0090 '/' Tc=5.0 min CN=98 Runoff=0.87 cfs 0.070 af

Subcatchment 2: EX BLDG/GRAVEL Runoff Area=13,815 sf 0.00% Impervious Runoff Depth=5.80"
Flow Length=83' Slope=0.0270 '/' Tc=5.0 min CN=96 Runoff=1.97 cfs 0.153 af

Subcatchment 3: GRAVEL Runoff Area=13,549 sf 0.00% Impervious Runoff Depth=5.80"
Flow Length=150' Tc=5.0 min CN=96 Runoff=1.93 cfs 0.150 af

Subcatchment 4: PAVEMENT/GRAVEL Runoff Area=32,428 sf 0.00% Impervious Runoff Depth=5.80"
Flow Length=202' Tc=5.7 min CN=96 Runoff=4.53 cfs 0.360 af

Subcatchment 5: WOODS Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.10"
Tc=5.0 min CN=30 Runoff=0.00 cfs 0.001 af

Subcatchment 6: WOODS/GRAVEL Runoff Area=14,723 sf 0.00% Impervious Runoff Depth=0.78"
Flow Length=194' Tc=5.3 min CN=43 Runoff=0.17 cfs 0.022 af

Subcatchment 7: WOODS/GRAVEL Runoff Area=25,187 sf 0.00% Impervious Runoff Depth=1.43"
Flow Length=100' Slope=0.0080 '/' Tc=5.0 min CN=52 Runoff=0.86 cfs 0.069 af

Subcatchment 8: GRAVEL Runoff Area=21,066 sf 0.00% Impervious Runoff Depth=5.80"
Flow Length=186' Tc=5.0 min CN=96 Runoff=3.00 cfs 0.234 af

Subcatchment 9: Runoff Area=14,505 sf 0.00% Impervious Runoff Depth=5.80"
Flow Length=100' Slope=0.0020 '/' Tc=5.0 min CN=96 Runoff=2.07 cfs 0.161 af

Reach POI1: POI Inflow=2.07 cfs 0.161 af
Outflow=2.07 cfs 0.161 af

Reach POI2: POI#2 Inflow=7.36 cfs 0.582 af
Outflow=7.36 cfs 0.582 af

Total Runoff Area = 3.330 ac Runoff Volume = 1.219 af Average Runoff Depth = 4.39"
95.85% Pervious = 3.192 ac 4.15% Impervious = 0.138 ac

Summary for Subcatchment 1: EX BLDG/PAVEMENT

Runoff = 0.87 cfs @ 12.07 hrs, Volume= 0.070 af, Depth= 6.03"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 50-Year Rainfall=6.27"

Area (sf)	CN	Description
6,027	98	Paved parking, HSG A
6,027		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	75	0.0090	0.91		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.4	75	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 2: EX BLDG/GRAVEL

Runoff = 1.97 cfs @ 12.07 hrs, Volume= 0.153 af, Depth= 5.80"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 50-Year Rainfall=6.27"

Area (sf)	CN	Description
13,815	96	Gravel surface, HSG A
13,815		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	83	0.0270	1.45		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.0	83	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 3: GRAVEL

Runoff = 1.93 cfs @ 12.07 hrs, Volume= 0.150 af, Depth= 5.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 50-Year Rainfall=6.27"

Area (sf)	CN	Description
13,549	96	Gravel surface, HSG A
13,549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	90	0.0070	0.86		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	60	0.0160	2.04		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.3	150	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 4: PAVEMENT/GRAVEL

Runoff = 4.53 cfs @ 12.08 hrs, Volume= 0.360 af, Depth= 5.80"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 50-Year Rainfall=6.27"

Area (sf)	CN	Description
32,428	96	Gravel surface, HSG A
32,428		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	100	0.0040	0.70		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.3	102	0.0010	0.51		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
5.7	202	Total			

Summary for Subcatchment 5: WOODS

Runoff = 0.00 cfs @ 15.14 hrs, Volume= 0.001 af, Depth= 0.10"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 50-Year Rainfall=6.27"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 6: WOODS/GRAVEL

Runoff = 0.17 cfs @ 12.13 hrs, Volume= 0.022 af, Depth= 0.78"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 50-Year Rainfall=6.27"

Area (sf)	CN	Description
11,749	30	Woods, Good, HSG A
2,974	96	Gravel surface, HSG A
14,723	43	Weighted Average
14,723		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Summary for Subcatchment 7: WOODS/GRAVEL

Runoff = 0.86 cfs @ 12.09 hrs, Volume= 0.069 af, Depth= 1.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 50-Year Rainfall=6.27"

Area (sf)	CN	Description
16,835	30	Woods, Good, HSG A
8,352	96	Gravel surface, HSG A
25,187	52	Weighted Average
25,187		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.8	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 8: GRAVEL

Runoff = 3.00 cfs @ 12.07 hrs, Volume= 0.234 af, Depth= 5.80"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 50-Year Rainfall=6.27"

Area (sf)	CN	Description
21,066	96	Gravel surface, HSG A
21,066		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 9:

Runoff = 2.07 cfs @ 12.07 hrs, Volume= 0.161 af, Depth= 5.80"
 Routed to Reach POI1 : POI

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 50-Year Rainfall=6.27"

Area (sf)	CN	Description
14,505	96	Gravel surface, HSG A
14,505		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.1	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach POI1: POI

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.333 ac, 0.00% Impervious, Inflow Depth = 5.80" for 50-Year event

Inflow = 2.07 cfs @ 12.07 hrs, Volume= 0.161 af

Outflow = 2.07 cfs @ 12.07 hrs, Volume= 0.161 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

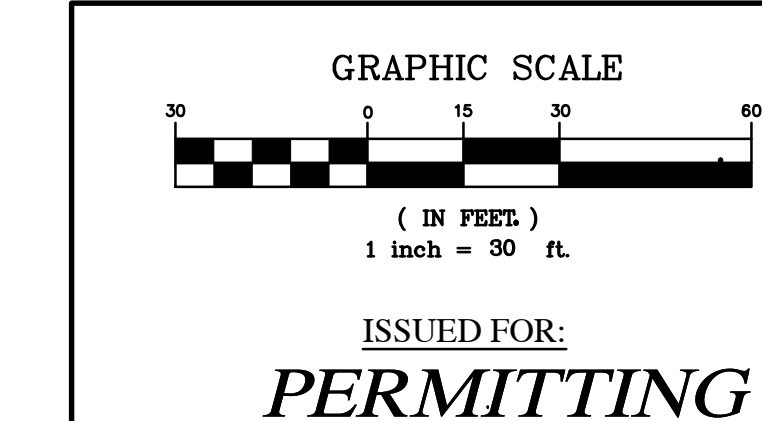
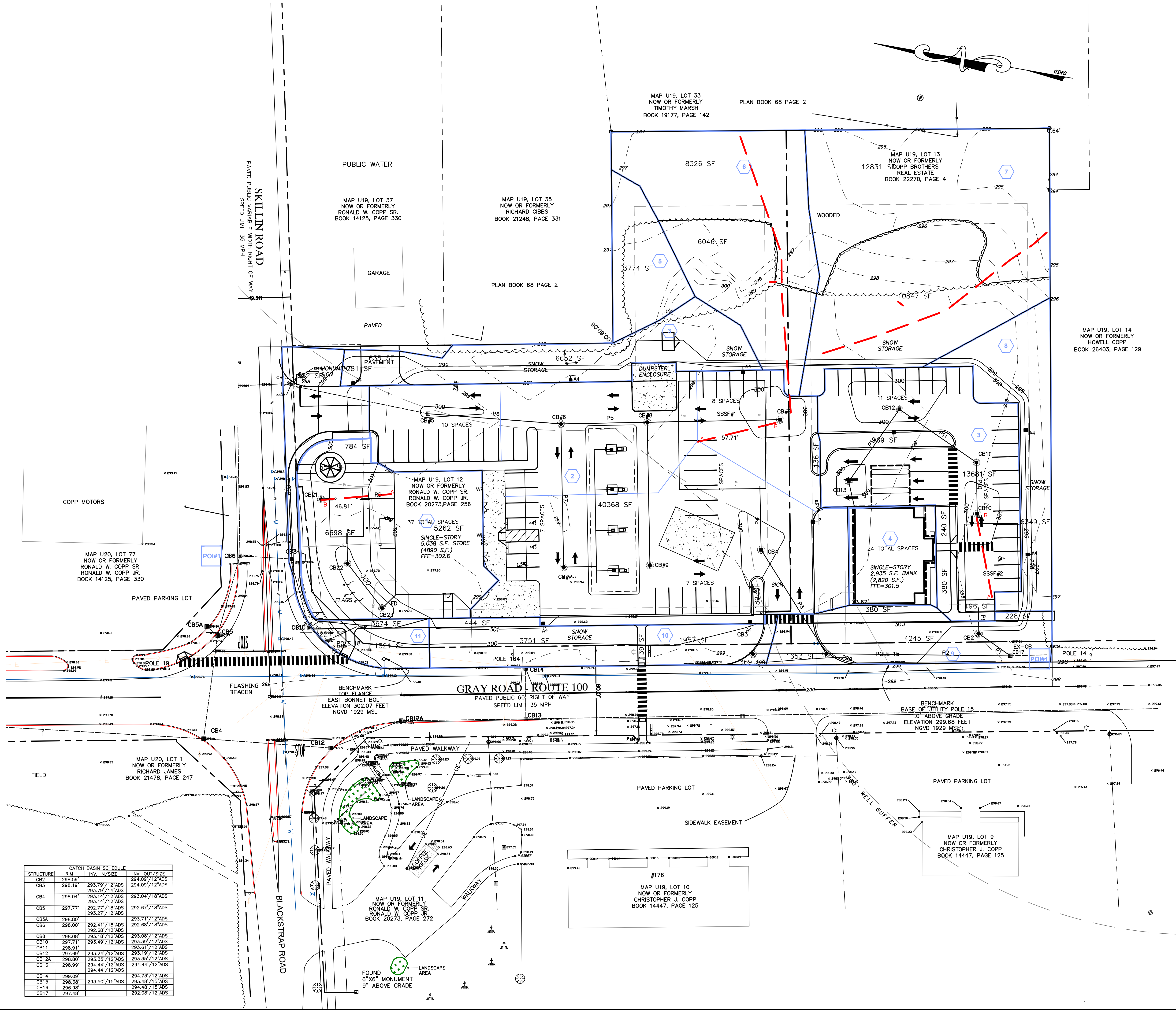
[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, 11.53% Impervious, Inflow Depth = 5.82" for 50-Year event
Inflow = 7.36 cfs @ 12.08 hrs, Volume= 0.582 af
Outflow = 7.36 cfs @ 12.08 hrs, Volume= 0.582 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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STRUCTURE	INVERT	INVERT	INVERT	INVERT
CB2	298.59'	293.79'/12"ADS	294.09'/12"ADS	
CB3	298.19'	293.79'/12"ADS	294.09'/12"ADS	
CB4	298.04'	293.14'/12"ADS	293.04'/18"ADS	
CB5	297.77'	292.77'/18"ADS	292.67'/18"ADS	
CB5A	298.80'	292.41'/18"ADS	293.71'/12"ADS	
CB6	298.00'	292.68'/12"ADS	292.68'/18"ADS	
CB8	298.08'	293.18'/12"ADS	293.08'/12"ADS	
CB10	297.71'	293.49'/12"ADS	293.39'/12"ADS	
CB11	298.91'	293.61'/12"ADS	293.61'/12"ADS	
CB12	297.69'	293.24'/12"ADS	293.19'/12"ADS	
CB12A	298.60'	293.35'/12"ADS	293.35'/12"ADS	
CB13	298.99'	294.44'/12"ADS	294.44'/12"ADS	
CB14	299.09'	294.73'/12"ADS	294.73'/12"ADS	
CB15	298.38'	293.50'/15"ADS	293.48'/15"ADS	
CB16	298.98'	294.48'/15"ADS	294.48'/15"ADS	
CB17	297.48'	292.08'/12"ADS	292.08'/12"ADS	



LEGEND:

1S SUBCATCHMENT AREA

POI#1 POINT OF INTEREST

A TIME OF CONCENTRATION

PRIORITY REAL ESTATE GROUP

POST-DEVELOPMENT DRAINAGE PLAN

RUSTY LANTERN CONVENIENCE STORE

181 GRAY ROAD, CUMBERLAND, ME 04021

PREPARED FOR: CUMBERLAND REAL ESTATE GROUP, LLC

2 MAIN STREET, TOPSHAM, ME 04086

NOT FOR CONSTRUCTION

THIS PLAN IS ISSUED FOR REVIEW AND INFORMATION PURPOSES ONLY. THIS PLAN WILL CHANGE AND IS NOT INTENDED FOR PRICING OR CONSTRUCTION.

PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.

DR2

SCALE: 1"=30'

JOB #: 22-RLM-004

MAP/LOT: U-19 12&13

DATE: 11-22-23

PRIORITY REAL ESTATE GROUP

CURTIS NEUFELD

REGISTERED PROFESSIONAL ENGINEER

MAINE 9779

Cumberland Post

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Project Notes

Copied 4 events from Cumberland 24-hr S1 storm

Rainfall events imported from "Atlas-14-Rain.txt" for 1365 ME Cumberland Nw

Cumberland Post*Cumberland 24-hr S1 2-yr Rainfall=3.10"*

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Page 3

Summary for Subcatchment 1: Store Roof

Runoff = 0.15 cfs @ 12.04 hrs, Volume= 0.014 af, Depth= 0.55"
Routed to Pond 5P : Roof Infiltration

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
5,262	98	Roofs, HSG A
784	39	>75% Grass cover, Good, HSG A
6,698	39	>75% Grass cover, Good, HSG A
559	98	Paved parking, HSG A
13,303	65	Weighted Average
7,482		56.24% Pervious Area
5,821		43.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Cumberland Post*Cumberland 24-hr S1 2-yr Rainfall=3.10"*

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Summary for Subcatchment 2: C-Store Parking

Runoff = 3.11 cfs @ 12.02 hrs, Volume= 0.223 af, Depth= 2.76"
Routed to Pond 3P : SSSF1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
40,368	98	Paved parking, HSG A
136	74	>75% Grass cover, Good, HSG C
1,560	74	>75% Grass cover, Good, HSG C
189	74	>75% Grass cover, Good, HSG C
42,253	97	Weighted Average
1,885		4.46% Pervious Area
40,368		95.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Cumberland Post*Cumberland 24-hr S1 2-yr Rainfall=3.10"*

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Summary for Subcatchment 3:[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 0.00 cfs @ 23.96 hrs, Volume= 0.000 af, Depth= 0.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
281	39	>75% Grass cover, Good, HSG A
635	98	Paved parking, HSG A
6,652	39	>75% Grass cover, Good, HSG A
7,568	44	Weighted Average
6,933		91.61% Pervious Area
635		8.39% Impervious Area

Cumberland Post*Cumberland 24-hr S1 2-yr Rainfall=3.10"*

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Summary for Subcatchment 4: (new Subcat)

Runoff = 0.22 cfs @ 12.02 hrs, Volume= 0.016 af, Depth= 2.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
2,935	98	Roofs, HSG A
2,935		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Cumberland Post*Cumberland 24-hr S1 2-yr Rainfall=3.10"*

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Summary for Subcatchment 5: Woods/Lawn

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Cumberland Post*Cumberland 24-hr S1 2-yr Rainfall=3.10"*

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Summary for Subcatchment 6: Woods/Lawn

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
8,326	30	Woods, Good, HSG A
6,046	39	>75% Grass cover, Good, HSG A
14,372	34	Weighted Average
14,372		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Cumberland Post*Cumberland 24-hr S1 2-yr Rainfall=3.10"*

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Summary for Subcatchment 7: Woods/Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
12,831	30	Woods, Good, HSG A
10,847	39	>75% Grass cover, Good, HSG A
23,678	34	Weighted Average
23,678		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.00"

Cumberland Post*Cumberland 24-hr S1 2-yr Rainfall=3.10"*

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Summary for Subcatchment 8: Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
6,349	39	>75% Grass cover, Good, HSG A
6,349		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces $n=0.011$ $P2=3.00"$
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved $K_v=16.1$ fps
2.5	186	Total			

Cumberland Post*Cumberland 24-hr S1 2-yr Rainfall=3.10"*

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Summary for Subcatchment 9:[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.01 cfs @ 12.12 hrs, Volume= 0.003 af, Depth= 0.25"
 Routed to Reach POI1 : POI#1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
 Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
4,245	39	>75% Grass cover, Good, HSG A
1,652	98	Paved parking, HSG A
380	39	>75% Grass cover, Good, HSG A
228	98	Paved parking, HSG A
6,505	56	Weighted Average
4,625		71.10% Pervious Area
1,880		28.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B Smooth surfaces $n=0.011$ $P2=3.00"$

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Summary for Subcatchment 10:

Runoff = 0.00 cfs @ 23.24 hrs, Volume= 0.001 af, Depth= 0.06"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
3,751	39	>75% Grass cover, Good, HSG A
1,957	39	>75% Grass cover, Good, HSG A
444	98	Paved parking, HSG A
139	98	Paved parking, HSG A
369	98	Paved parking, HSG A
6,660	47	Weighted Average
5,708		85.71% Pervious Area
952		14.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 11: Drive Entrance

Runoff = 0.17 cfs @ 12.03 hrs, Volume= 0.012 af, Depth= 1.03"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
832	39	>75% Grass cover, Good, HSG A
1,321	39	>75% Grass cover, Good, HSG A
221	39	>75% Grass cover, Good, HSG A
3,674	98	Paved parking, HSG A
6,048	75	Weighted Average
2,374		39.25% Pervious Area
3,674		60.75% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 30: Bank Parking

Runoff = 0.96 cfs @ 12.03 hrs, Volume= 0.064 af, Depth= 2.16"
Routed to Pond 6P : SSSF2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
13,681	98	Paved parking, HSG A
969	39	>75% Grass cover, Good, HSG A
240	39	>75% Grass cover, Good, HSG A
380	39	>75% Grass cover, Good, HSG A
196	39	>75% Grass cover, Good, HSG A
15,466	91	Weighted Average
1,785		11.54% Pervious Area
13,681		88.46% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Reach POI1: POI#1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.474 ac, 87.08% Impervious, Inflow Depth = 2.36" for 2-yr event
Inflow = 0.45 cfs @ 12.52 hrs, Volume= 0.290 af
Outflow = 0.45 cfs @ 12.52 hrs, Volume= 0.290 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.292 ac, 36.40% Impervious, Inflow Depth = 0.52" for 2-yr event
Inflow = 0.17 cfs @ 12.03 hrs, Volume= 0.013 af
Outflow = 0.17 cfs @ 12.03 hrs, Volume= 0.013 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Summary for Pond 3P: SSSF1

Inflow Area = 0.970 ac, 95.54% Impervious, Inflow Depth = 2.76" for 2-yr event
 Inflow = 3.11 cfs @ 12.02 hrs, Volume= 0.223 af
 Outflow = 0.32 cfs @ 12.62 hrs, Volume= 0.223 af, Atten= 90%, Lag= 35.7 min
 Primary = 0.32 cfs @ 12.62 hrs, Volume= 0.223 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 10.76' @ 12.62 hrs Surf.Area= 4,163 sf Storage= 2,303 cf

Plug-Flow detention time= 43.4 min calculated for 0.223 af (100% of inflow)
 Center-of-Mass det. time= 43.4 min (816.0 - 772.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	10.00'	2,374 cf	74.87'W x 55.61'L x 2.69'H Field A 11,214 cf Overall - 5,279 cf Embedded = 5,934 cf x 40.0% Voids
#2A	10.25'	5,015 cf	ACF R-Tank HD 1 x 1188 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 1188 Chambers in 54 Rows
7,389 cf			Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	10.00'	2.410 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 8.00'

Primary OutFlow Max=0.32 cfs @ 12.62 hrs HW=10.76' (Free Discharge)
 ↑ **1=Exfiltration** (Controls 0.32 cfs)

Pond 3P: SSSF1 - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

22 Chambers/Row x 2.35' Long = 51.61' Row Length +24.0" End Stone x 2 = 55.61' Base Length

54 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 74.87' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

1,188 Chambers x 4.2 cf = 5,015.5 cf Chamber Storage

1,188 Chambers x 4.4 cf = 5,279.5 cf Displacement

11,213.7 cf Field - 5,279.5 cf Chambers = 5,934.2 cf Stone x 40.0% Voids = 2,373.7 cf Stone Storage

Chamber Storage + Stone Storage = 7,389.2 cf = 0.170 af

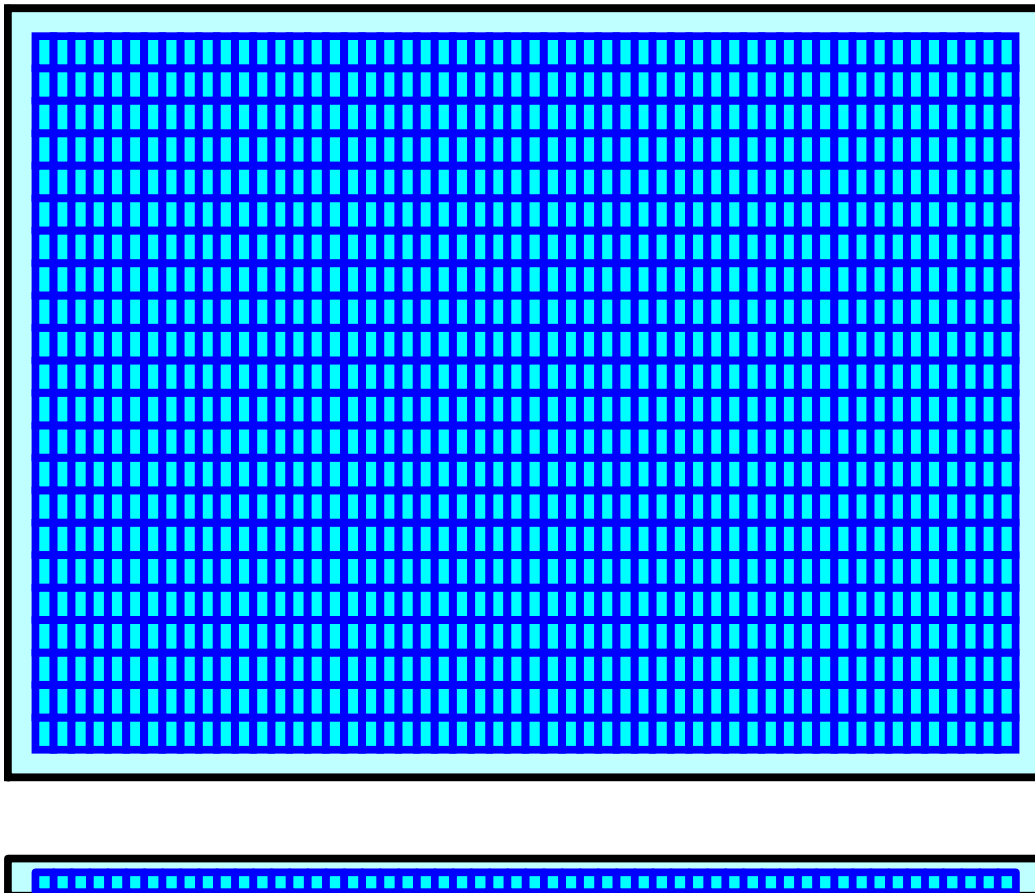
Overall Storage Efficiency = 65.9%

Overall System Size = 55.61' x 74.87' x 2.69'

1,188 Chambers

415.3 cy Field

219.8 cy Stone



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Cumberland 24-hr S1 2-yr Rainfall=3.10"

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Summary for Pond 5P: Roof Infiltration

Inflow Area = 0.305 ac, 43.76% Impervious, Inflow Depth = 0.55" for 2-yr event
 Inflow = 0.15 cfs @ 12.04 hrs, Volume= 0.014 af
 Outflow = 0.05 cfs @ 12.00 hrs, Volume= 0.014 af, Atten= 69%, Lag= 0.0 min
 Discarded = 0.05 cfs @ 12.00 hrs, Volume= 0.014 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 295.16' @ 12.28 hrs Surf.Area= 862 sf Storage= 56 cf

Plug-Flow detention time= 6.2 min calculated for 0.014 af (100% of inflow)
 Center-of-Mass det. time= 6.2 min (959.0 - 952.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	295.00'	559 cf	25.00'W x 34.50'L x 2.69'H Field A 2,323 cf Overall - 924 cf Embedded = 1,398 cf x 40.0% Voids
#2A	295.25'	878 cf	ACF R-Tank HD 1 x 208 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 208 Chambers in 16 Rows
		1,437 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	295.00'	2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.05 cfs @ 12.00 hrs HW=295.04' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Pond 5P: Roof Infiltration - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

13 Chambers/Row x 2.35' Long = 30.50' Row Length +24.0" End Stone x 2 = 34.50' Base Length

16 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 25.00' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

208 Chambers x 4.2 cf = 878.1 cf Chamber Storage

208 Chambers x 4.4 cf = 924.4 cf Displacement

2,322.7 cf Field - 924.4 cf Chambers = 1,398.3 cf Stone x 40.0% Voids = 559.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,437.5 cf = 0.033 af

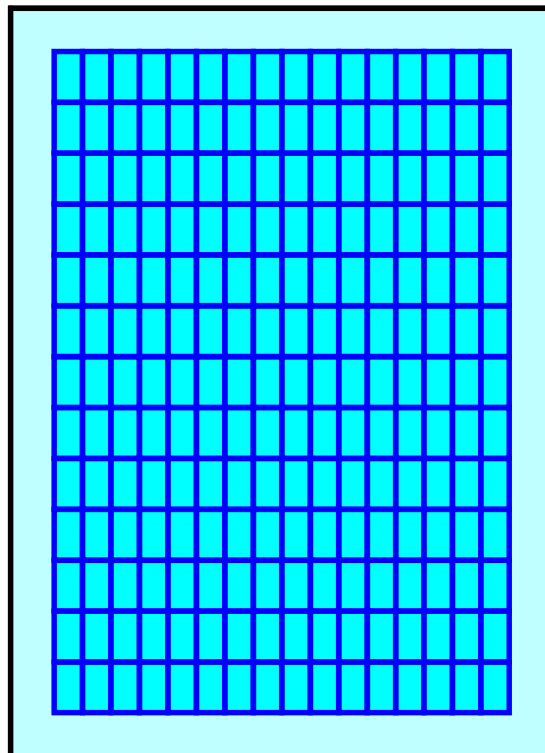
Overall Storage Efficiency = 61.9%

Overall System Size = 34.50' x 25.00' x 2.69'

208 Chambers

86.0 cy Field

51.8 cy Stone



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Cumberland 24-hr S1 2-yr Rainfall=3.10"

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Summary for Pond 6P: SSSF2

Inflow Area = 0.355 ac, 88.46% Impervious, Inflow Depth = 2.16" for 2-yr event
 Inflow = 0.96 cfs @ 12.03 hrs, Volume= 0.064 af
 Outflow = 0.13 cfs @ 11.76 hrs, Volume= 0.064 af, Atten= 87%, Lag= 0.0 min
 Primary = 0.13 cfs @ 11.76 hrs, Volume= 0.064 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 294.42' @ 12.51 hrs Surf.Area= 2,299 sf Storage= 561 cf

Plug-Flow detention time= 23.0 min calculated for 0.064 af (100% of inflow)
 Center-of-Mass det. time= 23.0 min (846.0 - 823.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	294.00'	1,268 cf	38.12'W x 60.30'L x 2.04'H Field A 4,683 cf Overall - 1,513 cf Embedded = 3,171 cf x 40.0% Voids
#2A	294.25'	1,437 cf	ACF R-Tank SD 1 x 624 Inside #1 Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf 624 Chambers in 26 Rows
		2,705 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	294.00'	2.410 in/hr Exfiltration over Surface area

Primary OutFlow Max=0.13 cfs @ 11.76 hrs HW=294.02' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.13 cfs)

Pond 6P: SSSF2 - Chamber Wizard Field A

Chamber Model = ACF R-Tank SD 1 (ACF Environmental R-Tank SD)

Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf

Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf

24 Chambers/Row x 2.35' Long = 56.30' Row Length +24.0" End Stone x 2 = 60.30' Base Length

26 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 38.12' Base Width

3.0" Stone Base + 9.4" Chamber Height + 12.0" Stone Cover = 2.04' Field Height

624 Chambers x 2.3 cf = 1,436.9 cf Chamber Storage

624 Chambers x 2.4 cf = 1,512.6 cf Displacement

4,683.3 cf Field - 1,512.6 cf Chambers = 3,170.7 cf Stone x 40.0% Voids = 1,268.3 cf Stone Storage

Chamber Storage + Stone Storage = 2,705.2 cf = 0.062 af

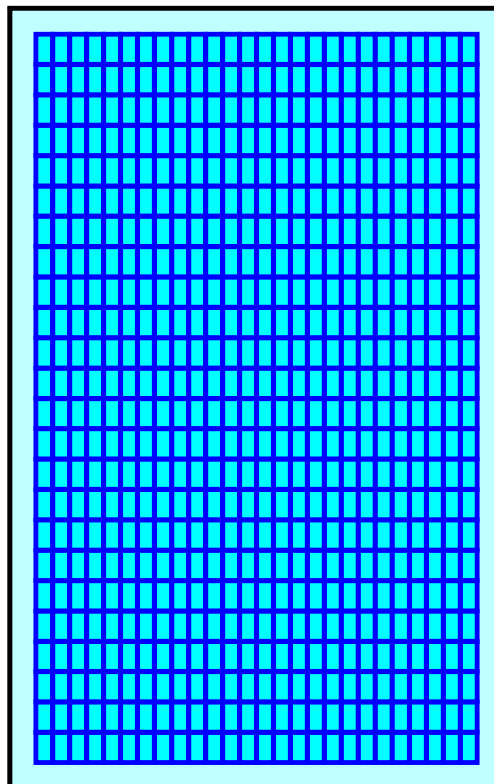
Overall Storage Efficiency = 57.8%

Overall System Size = 60.30' x 38.12' x 2.04'

624 Chambers

173.5 cy Field

117.4 cy Stone



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Summary for Pond 7P: CB

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.325 ac, 93.64% Impervious, Inflow Depth = 2.60" for 2-yr event
Inflow = 0.45 cfs @ 12.62 hrs, Volume= 0.287 af
Primary = 0.45 cfs @ 12.62 hrs, Volume= 0.287 af, Atten= 0%, Lag= 0.0 min
Routed to Reach POI1 : POI#1

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 1: Store Roof

Runoff = 0.48 cfs @ 12.09 hrs, Volume= 0.035 af, Depth= 1.39"
Routed to Pond 5P : Roof Infiltration

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
5,262	98	Roofs, HSG A
784	39	>75% Grass cover, Good, HSG A
6,698	39	>75% Grass cover, Good, HSG A
559	98	Paved parking, HSG A
13,303	65	Weighted Average
7,482		56.24% Pervious Area
5,821		43.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 2: C-Store Parking

Runoff = 4.41 cfs @ 12.07 hrs, Volume= 0.343 af, Depth= 4.25"
Routed to Pond 3P : SSSF1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
40,368	98	Paved parking, HSG A
136	74	>75% Grass cover, Good, HSG C
1,560	74	>75% Grass cover, Good, HSG C
189	74	>75% Grass cover, Good, HSG C
42,253	97	Weighted Average
1,885		4.46% Pervious Area
40,368		95.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 3:

[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 0.02 cfs @ 12.29 hrs, Volume= 0.004 af, Depth= 0.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
281	39	>75% Grass cover, Good, HSG A
635	98	Paved parking, HSG A
6,652	39	>75% Grass cover, Good, HSG A
7,568	44	Weighted Average
6,933		91.61% Pervious Area
635		8.39% Impervious Area

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Summary for Subcatchment 4: (new Subcat)

Runoff = 0.31 cfs @ 12.07 hrs, Volume= 0.025 af, Depth= 4.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
2,935	98	Roofs, HSG A
2,935		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 5: Woods/Lawn

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 6: Woods/Lawn

Runoff = 0.00 cfs @ 20.90 hrs, Volume= 0.001 af, Depth= 0.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
8,326	30	Woods, Good, HSG A
6,046	39	>75% Grass cover, Good, HSG A
14,372	34	Weighted Average
14,372		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 7: Woods/Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.00 cfs @ 20.87 hrs, Volume= 0.001 af, Depth= 0.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
12,831	30	Woods, Good, HSG A
10,847	39	>75% Grass cover, Good, HSG A
23,678	34	Weighted Average
23,678		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.00"

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 8: Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.00 cfs @ 14.53 hrs, Volume= 0.002 af, Depth= 0.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
6,349	39	>75% Grass cover, Good, HSG A
6,349		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total			

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 9:[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.12 cfs @ 12.07 hrs, Volume= 0.010 af, Depth= 0.84"
 Routed to Reach POI1 : POI#1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
 Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
4,245	39	>75% Grass cover, Good, HSG A
1,652	98	Paved parking, HSG A
380	39	>75% Grass cover, Good, HSG A
228	98	Paved parking, HSG A
6,505	56	Weighted Average
4,625		71.10% Pervious Area
1,880		28.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B Smooth surfaces $n=0.011$ $P2=3.00"$

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 10:

Runoff = 0.03 cfs @ 12.29 hrs, Volume= 0.005 af, Depth= 0.40"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
3,751	39	>75% Grass cover, Good, HSG A
1,957	39	>75% Grass cover, Good, HSG A
444	98	Paved parking, HSG A
139	98	Paved parking, HSG A
369	98	Paved parking, HSG A
6,660	47	Weighted Average
5,708		85.71% Pervious Area
952		14.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 11: Drive Entrance

Runoff = 0.35 cfs @ 12.08 hrs, Volume= 0.025 af, Depth= 2.13"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
832	39	>75% Grass cover, Good, HSG A
1,321	39	>75% Grass cover, Good, HSG A
221	39	>75% Grass cover, Good, HSG A
3,674	98	Paved parking, HSG A
6,048	75	Weighted Average
2,374		39.25% Pervious Area
3,674		60.75% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 30: Bank Parking

Runoff = 1.47 cfs @ 12.07 hrs, Volume= 0.106 af, Depth= 3.59"
Routed to Pond 6P : SSSF2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
13,681	98	Paved parking, HSG A
969	39	>75% Grass cover, Good, HSG A
240	39	>75% Grass cover, Good, HSG A
380	39	>75% Grass cover, Good, HSG A
196	39	>75% Grass cover, Good, HSG A
15,466	91	Weighted Average
1,785		11.54% Pervious Area
13,681		88.46% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Reach POI1: POI#1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.474 ac, 87.08% Impervious, Inflow Depth = 3.75" for 10-Year event
Inflow = 0.60 cfs @ 12.09 hrs, Volume= 0.460 af
Outflow = 0.60 cfs @ 12.09 hrs, Volume= 0.460 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.292 ac, 36.40% Impervious, Inflow Depth = 1.22" for 10-Year event
Inflow = 0.37 cfs @ 12.08 hrs, Volume= 0.030 af
Outflow = 0.37 cfs @ 12.08 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Pond 3P: SSSF1

Inflow Area = 0.970 ac, 95.54% Impervious, Inflow Depth = 4.25" for 10-Year event
 Inflow = 4.41 cfs @ 12.07 hrs, Volume= 0.343 af
 Outflow = 0.43 cfs @ 12.83 hrs, Volume= 0.343 af, Atten= 90%, Lag= 45.5 min
 Primary = 0.43 cfs @ 12.83 hrs, Volume= 0.343 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 11.68' @ 12.83 hrs Surf.Area= 4,163 sf Storage= 5,666 cf

Plug-Flow detention time= 111.4 min calculated for 0.343 af (100% of inflow)
 Center-of-Mass det. time= 111.3 min (867.9 - 756.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	10.00'	2,374 cf	74.87'W x 55.61'L x 2.69'H Field A 11,214 cf Overall - 5,279 cf Embedded = 5,934 cf x 40.0% Voids
#2A	10.25'	5,015 cf	ACF R-Tank HD 1 x 1188 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 1188 Chambers in 54 Rows
		7,389 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	10.00'	2.410 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 8.00'

Primary OutFlow Max=0.43 cfs @ 12.83 hrs HW=11.68' (Free Discharge)
 ↑ **1=Exfiltration** (Controls 0.43 cfs)

Pond 3P: SSSF1 - Chamber Wizard Field A

Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

22 Chambers/Row x 2.35' Long = 51.61' Row Length +24.0" End Stone x 2 = 55.61' Base Length

54 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 74.87' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

1,188 Chambers x 4.2 cf = 5,015.5 cf Chamber Storage

1,188 Chambers x 4.4 cf = 5,279.5 cf Displacement

11,213.7 cf Field - 5,279.5 cf Chambers = 5,934.2 cf Stone x 40.0% Voids = 2,373.7 cf Stone Storage

Chamber Storage + Stone Storage = 7,389.2 cf = 0.170 af

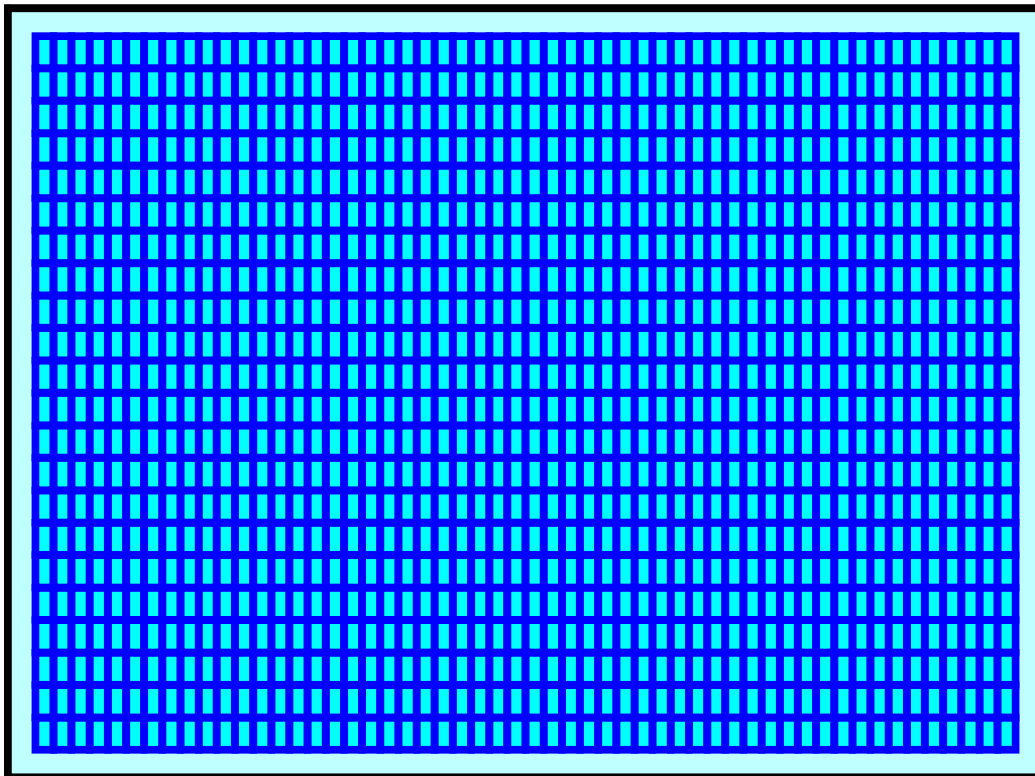
Overall Storage Efficiency = 65.9%

Overall System Size = 55.61' x 74.87' x 2.69'

1,188 Chambers

415.3 cy Field

219.8 cy Stone



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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Pond 5P: Roof Infiltration

Inflow Area = 0.305 ac, 43.76% Impervious, Inflow Depth = 1.39" for 10-Year event
 Inflow = 0.48 cfs @ 12.09 hrs, Volume= 0.035 af
 Outflow = 0.05 cfs @ 11.80 hrs, Volume= 0.035 af, Atten= 90%, Lag= 0.0 min
 Discarded = 0.05 cfs @ 11.80 hrs, Volume= 0.035 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 295.91' @ 13.46 hrs Surf.Area= 862 sf Storage= 548 cf

Plug-Flow detention time= 106.9 min calculated for 0.035 af (100% of inflow)
 Center-of-Mass det. time= 106.9 min (972.2 - 865.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	295.00'	559 cf	25.00'W x 34.50'L x 2.69'H Field A 2,323 cf Overall - 924 cf Embedded = 1,398 cf x 40.0% Voids
#2A	295.25'	878 cf	ACF R-Tank HD 1 x 208 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 208 Chambers in 16 Rows
		1,437 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	295.00'	2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.05 cfs @ 11.80 hrs HW=295.03' (Free Discharge)

↑ **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Pond 5P: Roof Infiltration - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

13 Chambers/Row x 2.35' Long = 30.50' Row Length +24.0" End Stone x 2 = 34.50' Base Length

16 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 25.00' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

208 Chambers x 4.2 cf = 878.1 cf Chamber Storage

208 Chambers x 4.4 cf = 924.4 cf Displacement

2,322.7 cf Field - 924.4 cf Chambers = 1,398.3 cf Stone x 40.0% Voids = 559.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,437.5 cf = 0.033 af

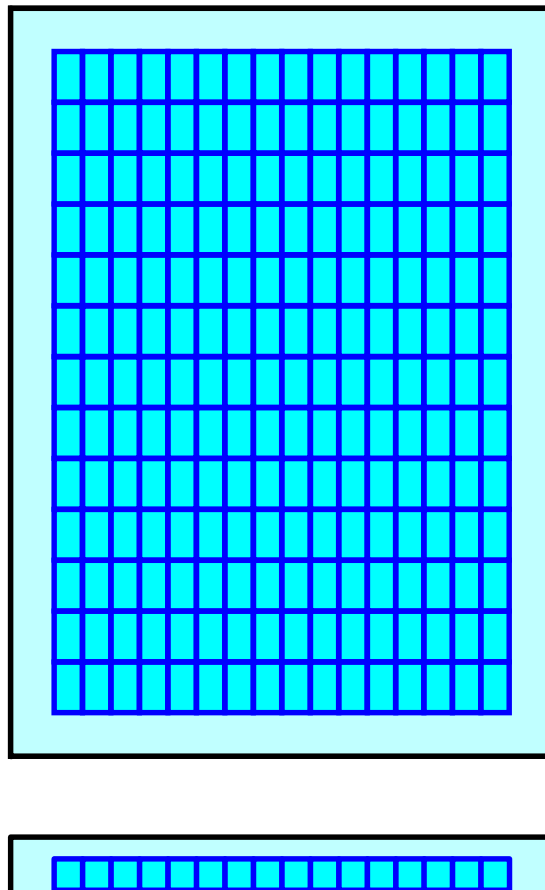
Overall Storage Efficiency = 61.9%

Overall System Size = 34.50' x 25.00' x 2.69'

208 Chambers

86.0 cy Field

51.8 cy Stone



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Summary for Pond 6P: SSSF2

Inflow Area = 0.355 ac, 88.46% Impervious, Inflow Depth = 3.59" for 10-Year event
 Inflow = 1.47 cfs @ 12.07 hrs, Volume= 0.106 af
 Outflow = 0.13 cfs @ 11.44 hrs, Volume= 0.106 af, Atten= 91%, Lag= 0.0 min
 Primary = 0.13 cfs @ 11.44 hrs, Volume= 0.106 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 295.01' @ 12.97 hrs Surf.Area= 2,299 sf Storage= 1,731 cf

Plug-Flow detention time= 103.5 min calculated for 0.106 af (100% of inflow)
 Center-of-Mass det. time= 103.5 min (892.2 - 788.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	294.00'	1,268 cf	38.12'W x 60.30'L x 2.04'H Field A 4,683 cf Overall - 1,513 cf Embedded = 3,171 cf x 40.0% Voids
#2A	294.25'	1,437 cf	ACF R-Tank SD 1 x 624 Inside #1 Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf 624 Chambers in 26 Rows
		2,705 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	294.00'	2.410 in/hr Exfiltration over Surface area

Primary OutFlow Max=0.13 cfs @ 11.44 hrs HW=294.02' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.13 cfs)

Pond 6P: SSSF2 - Chamber Wizard Field A**Chamber Model = ACF R-Tank SD 1 (ACF Environmental R-Tank SD)**

Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf

Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf

24 Chambers/Row x 2.35' Long = 56.30' Row Length +24.0" End Stone x 2 = 60.30' Base Length

26 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 38.12' Base Width

3.0" Stone Base + 9.4" Chamber Height + 12.0" Stone Cover = 2.04' Field Height

624 Chambers x 2.3 cf = 1,436.9 cf Chamber Storage

624 Chambers x 2.4 cf = 1,512.6 cf Displacement

4,683.3 cf Field - 1,512.6 cf Chambers = 3,170.7 cf Stone x 40.0% Voids = 1,268.3 cf Stone Storage

Chamber Storage + Stone Storage = 2,705.2 cf = 0.062 af

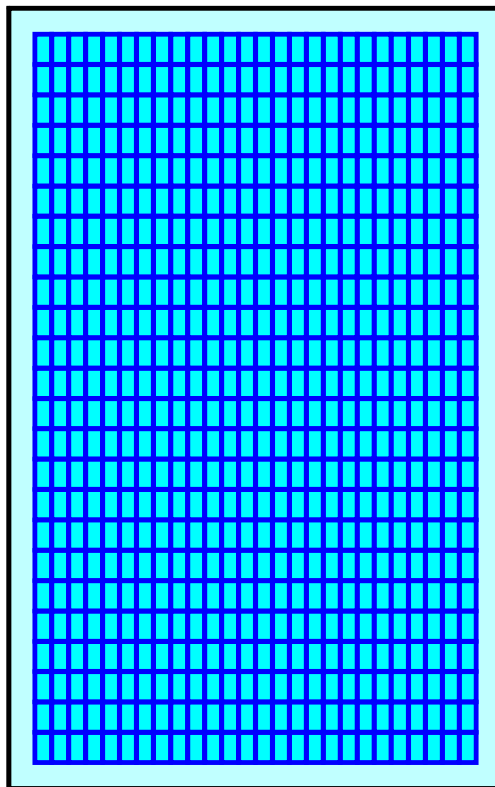
Overall Storage Efficiency = 57.8%

Overall System Size = 60.30' x 38.12' x 2.04'

624 Chambers

173.5 cy Field

117.4 cy Stone



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Summary for Pond 7P: CB

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.325 ac, 93.64% Impervious, Inflow Depth = 4.07" for 10-Year event
Inflow = 0.56 cfs @ 12.83 hrs, Volume= 0.450 af
Primary = 0.56 cfs @ 12.83 hrs, Volume= 0.450 af, Atten= 0%, Lag= 0.0 min
Routed to Reach POI1 : POI#1

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Summary for Subcatchment 1: Store Roof

Runoff = 0.81 cfs @ 12.03 hrs, Volume= 0.056 af, Depth= 2.21"
Routed to Pond 5P : Roof Infiltration

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
5,262	98	Roofs, HSG A
784	39	>75% Grass cover, Good, HSG A
6,698	39	>75% Grass cover, Good, HSG A
559	98	Paved parking, HSG A
13,303	65	Weighted Average
7,482		56.24% Pervious Area
5,821		43.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 2: C-Store Parking

Runoff = 5.87 cfs @ 12.02 hrs, Volume= 0.440 af, Depth= 5.44"
Routed to Pond 3P : SSSF1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
40,368	98	Paved parking, HSG A
136	74	>75% Grass cover, Good, HSG C
1,560	74	>75% Grass cover, Good, HSG C
189	74	>75% Grass cover, Good, HSG C
42,253	97	Weighted Average
1,885		4.46% Pervious Area
40,368		95.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 3:[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 0.07 cfs @ 11.99 hrs, Volume= 0.010 af, Depth= 0.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs*Cumberland 24-hr S1 25-yr Rainfall=5.80"*

Area (sf)	CN	Description
281	39	>75% Grass cover, Good, HSG A
635	98	Paved parking, HSG A
6,652	39	>75% Grass cover, Good, HSG A
7,568	44	Weighted Average
6,933		91.61% Pervious Area
635		8.39% Impervious Area

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Summary for Subcatchment 4: (new Subcat)

Runoff = 0.41 cfs @ 12.02 hrs, Volume= 0.031 af, Depth= 5.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
2,935	98	Roofs, HSG A
2,935		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 5: Woods/Lawn

Runoff = 0.00 cfs @ 23.96 hrs, Volume= 0.000 af, Depth= 0.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 6: Woods/Lawn

Runoff = 0.01 cfs @ 17.44 hrs, Volume= 0.005 af, Depth= 0.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
8,326	30	Woods, Good, HSG A
6,046	39	>75% Grass cover, Good, HSG A
14,372	34	Weighted Average
14,372		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

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Summary for Subcatchment 7: Woods/Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.01 cfs @ 17.40 hrs, Volume= 0.008 af, Depth= 0.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
12,831	30	Woods, Good, HSG A
10,847	39	>75% Grass cover, Good, HSG A
23,678	34	Weighted Average
23,678		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.00"

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Summary for Subcatchment 8: Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.01 cfs @ 12.32 hrs, Volume= 0.005 af, Depth= 0.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
6,349	39	>75% Grass cover, Good, HSG A
6,349		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces $n=0.011$ $P2=3.00"$
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved $K_v=16.1$ fps
2.5	186	Total			

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Summary for Subcatchment 9:[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.26 cfs @ 12.01 hrs, Volume= 0.018 af, Depth= 1.48"
Routed to Reach POI1 : POI#1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
4,245	39	>75% Grass cover, Good, HSG A
1,652	98	Paved parking, HSG A
380	39	>75% Grass cover, Good, HSG A
228	98	Paved parking, HSG A
6,505	56	Weighted Average
4,625		71.10% Pervious Area
1,880		28.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B Smooth surfaces $n=0.011$ $P2=3.00"$

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Summary for Subcatchment 10:

Runoff = 0.10 cfs @ 12.04 hrs, Volume= 0.011 af, Depth= 0.85"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
3,751	39	>75% Grass cover, Good, HSG A
1,957	39	>75% Grass cover, Good, HSG A
444	98	Paved parking, HSG A
139	98	Paved parking, HSG A
369	98	Paved parking, HSG A
6,660	47	Weighted Average
5,708		85.71% Pervious Area
952		14.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 11: Drive Entrance

Runoff = 0.54 cfs @ 12.03 hrs, Volume= 0.036 af, Depth= 3.11"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
832	39	>75% Grass cover, Good, HSG A
1,321	39	>75% Grass cover, Good, HSG A
221	39	>75% Grass cover, Good, HSG A
3,674	98	Paved parking, HSG A
6,048	75	Weighted Average
2,374		39.25% Pervious Area
3,674		60.75% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 30: Bank Parking

Runoff = 2.01 cfs @ 12.02 hrs, Volume= 0.141 af, Depth= 4.76"
Routed to Pond 6P : SSSF2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
13,681	98	Paved parking, HSG A
969	39	>75% Grass cover, Good, HSG A
240	39	>75% Grass cover, Good, HSG A
380	39	>75% Grass cover, Good, HSG A
196	39	>75% Grass cover, Good, HSG A
15,466	91	Weighted Average
1,785		11.54% Pervious Area
13,681		88.46% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Reach POI1: POI#1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.474 ac, 87.08% Impervious, Inflow Depth = 4.88" for 25-yr event
Inflow = 0.73 cfs @ 12.01 hrs, Volume= 0.599 af
Outflow = 0.73 cfs @ 12.01 hrs, Volume= 0.599 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.292 ac, 36.40% Impervious, Inflow Depth = 1.93" for 25-yr event
Inflow = 0.63 cfs @ 12.03 hrs, Volume= 0.047 af
Outflow = 0.63 cfs @ 12.03 hrs, Volume= 0.047 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Cumberland 24-hr S1 25-yr Rainfall=5.80"

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Summary for Pond 3P: SSSF1

Inflow Area = 0.970 ac, 95.54% Impervious, Inflow Depth = 5.44" for 25-yr event
 Inflow = 5.87 cfs @ 12.02 hrs, Volume= 0.440 af
 Outflow = 0.44 cfs @ 12.98 hrs, Volume= 0.440 af, Atten= 93%, Lag= 57.7 min
 Primary = 0.44 cfs @ 12.98 hrs, Volume= 0.440 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 11.75' @ 12.98 hrs Surf.Area= 4,163 sf Storage= 5,820 cf

Plug-Flow detention time= 107.6 min calculated for 0.440 af (100% of inflow)
 Center-of-Mass det. time= 107.5 min (862.2 - 754.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	10.00'	2,374 cf	74.87'W x 55.61'L x 2.69'H Field A 11,214 cf Overall - 5,279 cf Embedded = 5,934 cf x 40.0% Voids
#2A	10.25'	5,015 cf	ACF R-Tank HD 1 x 1188 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 1188 Chambers in 54 Rows
7,389 cf			Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	10.00'	2.410 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 8.00'

Primary OutFlow Max=0.44 cfs @ 12.98 hrs HW=11.75' (Free Discharge)
 ↑ **1=Exfiltration** (Controls 0.44 cfs)

Pond 3P: SSSF1 - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

22 Chambers/Row x 2.35' Long = 51.61' Row Length +24.0" End Stone x 2 = 55.61' Base Length

54 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 74.87' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

1,188 Chambers x 4.2 cf = 5,015.5 cf Chamber Storage

1,188 Chambers x 4.4 cf = 5,279.5 cf Displacement

11,213.7 cf Field - 5,279.5 cf Chambers = 5,934.2 cf Stone x 40.0% Voids = 2,373.7 cf Stone Storage

Chamber Storage + Stone Storage = 7,389.2 cf = 0.170 af

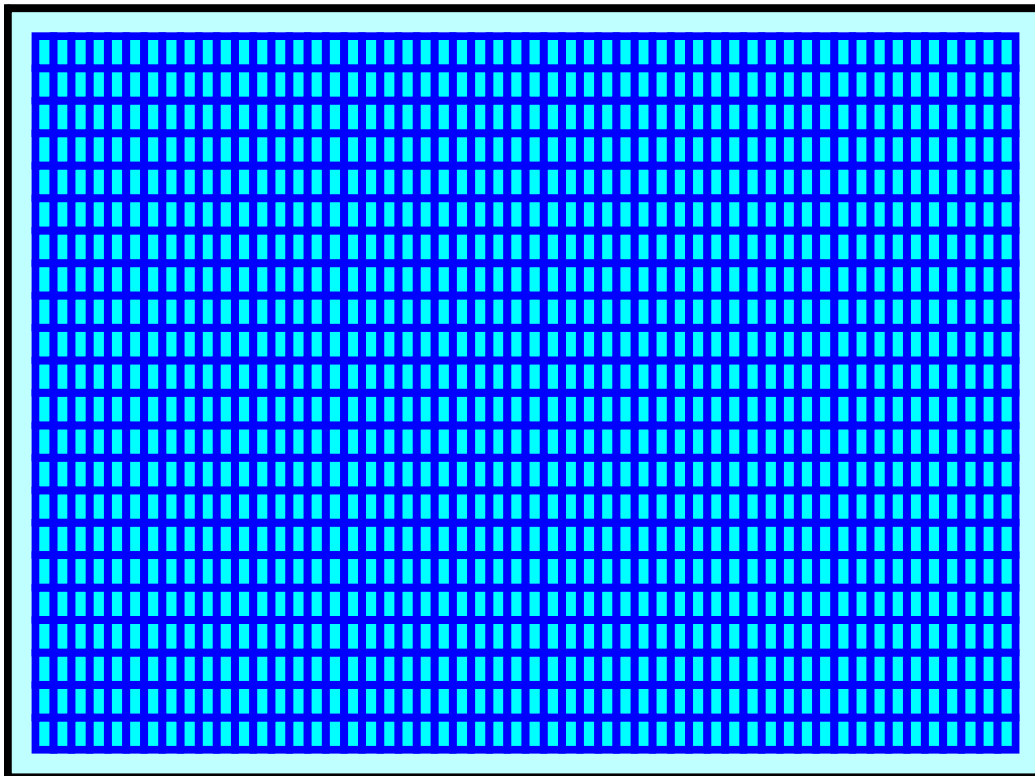
Overall Storage Efficiency = 65.9%

Overall System Size = 55.61' x 74.87' x 2.69'

1,188 Chambers

415.3 cy Field

219.8 cy Stone



Cumberland Post

Cumberland 24-hr S1 25-yr Rainfall=5.80"

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Summary for Pond 5P: Roof Infiltration

Inflow Area = 0.305 ac, 43.76% Impervious, Inflow Depth = 2.21" for 25-yr event
 Inflow = 0.81 cfs @ 12.03 hrs, Volume= 0.056 af
 Outflow = 0.05 cfs @ 11.52 hrs, Volume= 0.056 af, Atten= 94%, Lag= 0.0 min
 Discarded = 0.05 cfs @ 11.52 hrs, Volume= 0.056 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 296.31' @ 14.41 hrs Surf.Area= 862 sf Storage= 823 cf

Plug-Flow detention time= 175.2 min calculated for 0.056 af (100% of inflow)
 Center-of-Mass det. time= 175.1 min (1,066.3 - 891.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	295.00'	559 cf	25.00'W x 34.50'L x 2.69'H Field A 2,323 cf Overall - 924 cf Embedded = 1,398 cf x 40.0% Voids
#2A	295.25'	878 cf	ACF R-Tank HD 1 x 208 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 208 Chambers in 16 Rows
		1,437 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	295.00'	2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.05 cfs @ 11.52 hrs HW=295.03' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Pond 5P: Roof Infiltration - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

13 Chambers/Row x 2.35' Long = 30.50' Row Length +24.0" End Stone x 2 = 34.50' Base Length

16 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 25.00' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

208 Chambers x 4.2 cf = 878.1 cf Chamber Storage

208 Chambers x 4.4 cf = 924.4 cf Displacement

2,322.7 cf Field - 924.4 cf Chambers = 1,398.3 cf Stone x 40.0% Voids = 559.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,437.5 cf = 0.033 af

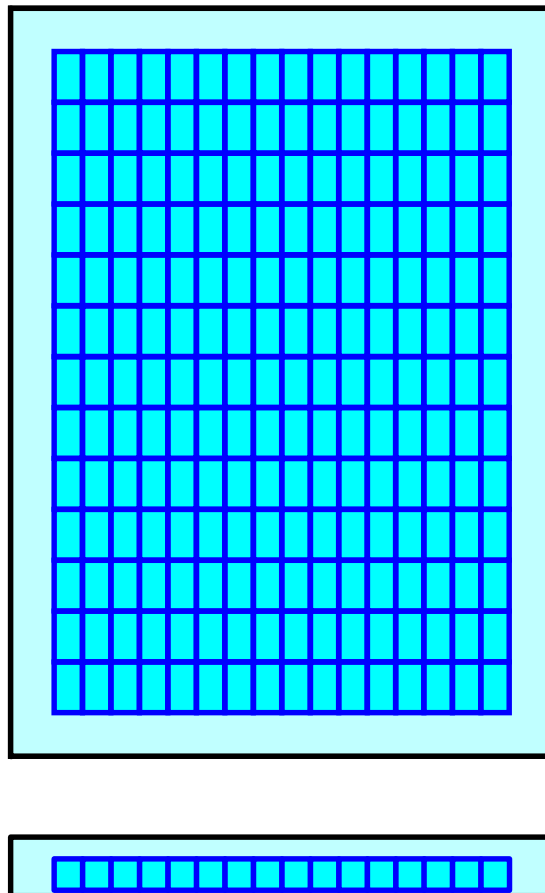
Overall Storage Efficiency = 61.9%

Overall System Size = 34.50' x 25.00' x 2.69'

208 Chambers

86.0 cy Field

51.8 cy Stone



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Cumberland 24-hr S1 25-yr Rainfall=5.80"

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Summary for Pond 6P: SSSF2

Inflow Area = 0.355 ac, 88.46% Impervious, Inflow Depth = 4.76" for 25-yr event
 Inflow = 2.01 cfs @ 12.02 hrs, Volume= 0.141 af
 Outflow = 0.13 cfs @ 11.08 hrs, Volume= 0.141 af, Atten= 94%, Lag= 0.0 min
 Primary = 0.13 cfs @ 11.08 hrs, Volume= 0.141 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 295.08' @ 13.30 hrs Surf.Area= 2,299 sf Storage= 1,829 cf

Plug-Flow detention time= 102.4 min calculated for 0.141 af (100% of inflow)
 Center-of-Mass det. time= 102.3 min (895.3 - 793.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	294.00'	1,268 cf	38.12'W x 60.30'L x 2.04'H Field A 4,683 cf Overall - 1,513 cf Embedded = 3,171 cf x 40.0% Voids
#2A	294.25'	1,437 cf	ACF R-Tank SD 1 x 624 Inside #1 Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf 624 Chambers in 26 Rows
		2,705 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	294.00'	2.410 in/hr Exfiltration over Surface area

Primary OutFlow Max=0.13 cfs @ 11.08 hrs HW=294.02' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.13 cfs)

Pond 6P: SSSF2 - Chamber Wizard Field A**Chamber Model = ACF R-Tank SD 1 (ACF Environmental R-Tank SD)**

Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf

Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf

24 Chambers/Row x 2.35' Long = 56.30' Row Length +24.0" End Stone x 2 = 60.30' Base Length

26 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 38.12' Base Width

3.0" Stone Base + 9.4" Chamber Height + 12.0" Stone Cover = 2.04' Field Height

624 Chambers x 2.3 cf = 1,436.9 cf Chamber Storage

624 Chambers x 2.4 cf = 1,512.6 cf Displacement

4,683.3 cf Field - 1,512.6 cf Chambers = 3,170.7 cf Stone x 40.0% Voids = 1,268.3 cf Stone Storage

Chamber Storage + Stone Storage = 2,705.2 cf = 0.062 af

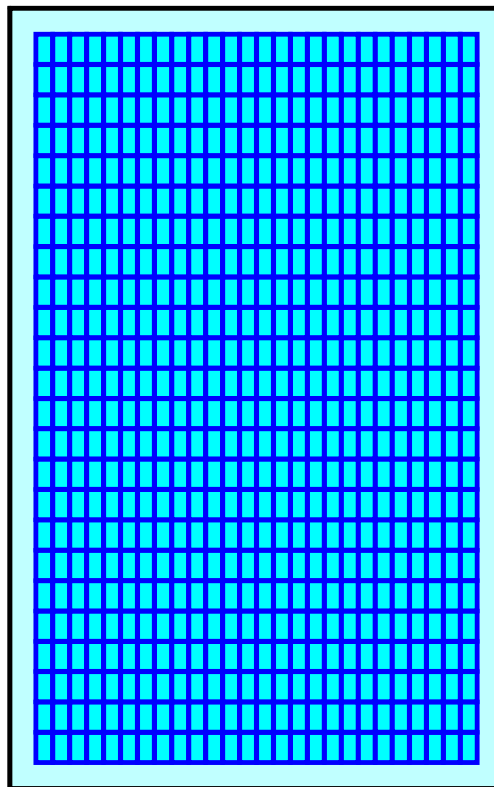
Overall Storage Efficiency = 57.8%

Overall System Size = 60.30' x 38.12' x 2.04'

624 Chambers

173.5 cy Field

117.4 cy Stone



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Summary for Pond 7P: CB

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.325 ac, 93.64% Impervious, Inflow Depth = 5.26" for 25-yr event
Inflow = 0.56 cfs @ 12.98 hrs, Volume= 0.581 af
Primary = 0.56 cfs @ 12.98 hrs, Volume= 0.581 af, Atten= 0%, Lag= 0.0 min
Routed to Reach POI1 : POI#1

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Summary for Subcatchment 1: Store Roof

Runoff = 1.14 cfs @ 12.03 hrs, Volume= 0.077 af, Depth= 3.03"
Routed to Pond 5P : Roof Infiltration

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Area (sf)	CN	Description
5,262	98	Roofs, HSG A
784	39	>75% Grass cover, Good, HSG A
6,698	39	>75% Grass cover, Good, HSG A
559	98	Paved parking, HSG A
13,303	65	Weighted Average
7,482		56.24% Pervious Area
5,821		43.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 2: C-Store Parking

Runoff = 7.01 cfs @ 12.02 hrs, Volume= 0.529 af, Depth= 6.54"
Routed to Pond 3P : SSSF1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Area (sf)	CN	Description
40,368	98	Paved parking, HSG A
136	74	>75% Grass cover, Good, HSG C
1,560	74	>75% Grass cover, Good, HSG C
189	74	>75% Grass cover, Good, HSG C
42,253	97	Weighted Average
1,885		4.46% Pervious Area
40,368		95.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 3:

[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 0.19 cfs @ 11.97 hrs, Volume= 0.016 af, Depth= 1.11"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Area (sf)	CN	Description
281	39	>75% Grass cover, Good, HSG A
635	98	Paved parking, HSG A
6,652	39	>75% Grass cover, Good, HSG A
7,568	44	Weighted Average
6,933		91.61% Pervious Area
635		8.39% Impervious Area

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Summary for Subcatchment 4: (new Subcat)

Runoff = 0.49 cfs @ 12.02 hrs, Volume= 0.037 af, Depth= 6.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Area (sf)	CN	Description
2,935	98	Roofs, HSG A
2,935		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 5: Woods/Lawn

Runoff = 0.00 cfs @ 18.04 hrs, Volume= 0.001 af, Depth= 0.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 6: Woods/Lawn

Runoff = 0.02 cfs @ 12.52 hrs, Volume= 0.011 af, Depth= 0.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Area (sf)	CN	Description
8,326	30	Woods, Good, HSG A
6,046	39	>75% Grass cover, Good, HSG A
14,372	34	Weighted Average
14,372		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

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Summary for Subcatchment 7: Woods/Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.03 cfs @ 12.41 hrs, Volume= 0.018 af, Depth= 0.41"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs*Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"*

Area (sf)	CN	Description
12,831	30	Woods, Good, HSG A
10,847	39	>75% Grass cover, Good, HSG A
23,678	34	Weighted Average
23,678		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B Smooth surfaces $n=0.011$ $P2=3.00"$

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Summary for Subcatchment 8: Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.05 cfs @ 12.02 hrs, Volume= 0.009 af, Depth= 0.73"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs*Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"*

Area (sf)	CN	Description
6,349	39	>75% Grass cover, Good, HSG A
6,349		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces $n=0.011$ $P2=3.00"$
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved $K_v=16.1$ fps
2.5	186	Total			

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Summary for Subcatchment 9:[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.41 cfs @ 12.00 hrs, Volume= 0.027 af, Depth= 2.15"
 Routed to Reach POI1 : POI#1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt= 0.04$ hrs
 Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Area (sf)	CN	Description
4,245	39	>75% Grass cover, Good, HSG A
1,652	98	Paved parking, HSG A
380	39	>75% Grass cover, Good, HSG A
228	98	Paved parking, HSG A
6,505	56	Weighted Average
4,625		71.10% Pervious Area
1,880		28.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B Smooth surfaces $n= 0.011$ $P2= 3.00"$

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Summary for Subcatchment 10:

Runoff = 0.20 cfs @ 12.04 hrs, Volume= 0.017 af, Depth= 1.35"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Area (sf)	CN	Description
3,751	39	>75% Grass cover, Good, HSG A
1,957	39	>75% Grass cover, Good, HSG A
444	98	Paved parking, HSG A
139	98	Paved parking, HSG A
369	98	Paved parking, HSG A
6,660	47	Weighted Average
5,708		85.71% Pervious Area
952		14.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 11: Drive Entrance

Runoff = 0.70 cfs @ 12.03 hrs, Volume= 0.047 af, Depth= 4.06"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Area (sf)	CN	Description
832	39	>75% Grass cover, Good, HSG A
1,321	39	>75% Grass cover, Good, HSG A
221	39	>75% Grass cover, Good, HSG A
3,674	98	Paved parking, HSG A
6,048	75	Weighted Average
2,374		39.25% Pervious Area
3,674		60.75% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 30: Bank Parking

Runoff = 2.44 cfs @ 12.02 hrs, Volume= 0.173 af, Depth= 5.84"
Routed to Pond 6P : SSSF2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Area (sf)	CN	Description
13,681	98	Paved parking, HSG A
969	39	>75% Grass cover, Good, HSG A
240	39	>75% Grass cover, Good, HSG A
380	39	>75% Grass cover, Good, HSG A
196	39	>75% Grass cover, Good, HSG A
15,466	91	Weighted Average
1,785		11.54% Pervious Area
13,681		88.46% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Reach POI1: POI#1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.474 ac, 87.08% Impervious, Inflow Depth = 5.93" for 50-yr event
Inflow = 0.90 cfs @ 12.01 hrs, Volume= 0.728 af
Outflow = 0.90 cfs @ 12.01 hrs, Volume= 0.728 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.292 ac, 36.40% Impervious, Inflow Depth = 2.64" for 50-yr event
Inflow = 0.90 cfs @ 12.03 hrs, Volume= 0.064 af
Outflow = 0.90 cfs @ 12.03 hrs, Volume= 0.064 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Cumberland Post

Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

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Summary for Pond 3P: SSSF1

Inflow Area = 0.970 ac, 95.54% Impervious, Inflow Depth = 6.54" for 50-yr event
 Inflow = 7.01 cfs @ 12.02 hrs, Volume= 0.529 af
 Outflow = 0.54 cfs @ 12.93 hrs, Volume= 0.529 af, Atten= 92%, Lag= 54.7 min
 Primary = 0.54 cfs @ 12.93 hrs, Volume= 0.529 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 12.64' @ 12.93 hrs Surf.Area= 4,163 sf Storage= 7,294 cf

Plug-Flow detention time= 126.0 min calculated for 0.528 af (100% of inflow)
 Center-of-Mass det. time= 125.9 min (876.7 - 750.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	10.00'	2,374 cf	74.87'W x 55.61'L x 2.69'H Field A 11,214 cf Overall - 5,279 cf Embedded = 5,934 cf x 40.0% Voids
#2A	10.25'	5,015 cf	ACF R-Tank HD 1 x 1188 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 1188 Chambers in 54 Rows
7,389 cf			Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	10.00'	2.410 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 8.00'

Primary OutFlow Max=0.54 cfs @ 12.93 hrs HW=12.64' (Free Discharge)
 ↑ **1=Exfiltration** (Controls 0.54 cfs)

Pond 3P: SSSF1 - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

22 Chambers/Row x 2.35' Long = 51.61' Row Length +24.0" End Stone x 2 = 55.61' Base Length

54 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 74.87' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

1,188 Chambers x 4.2 cf = 5,015.5 cf Chamber Storage

1,188 Chambers x 4.4 cf = 5,279.5 cf Displacement

11,213.7 cf Field - 5,279.5 cf Chambers = 5,934.2 cf Stone x 40.0% Voids = 2,373.7 cf Stone Storage

Chamber Storage + Stone Storage = 7,389.2 cf = 0.170 af

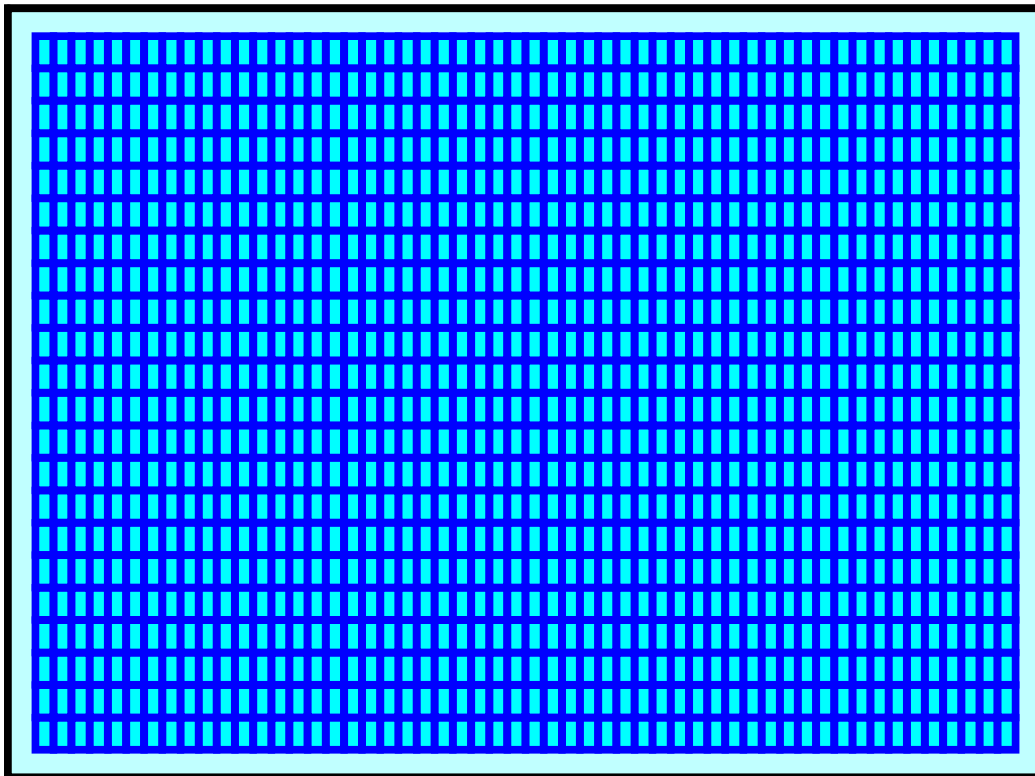
Overall Storage Efficiency = 65.9%

Overall System Size = 55.61' x 74.87' x 2.69'

1,188 Chambers

415.3 cy Field

219.8 cy Stone



Cumberland Post

Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

Prepared by Priority Real Estate Group LLC

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Summary for Pond 5P: Roof Infiltration

Inflow Area = 0.305 ac, 43.76% Impervious, Inflow Depth = 3.03" for 50-yr event
 Inflow = 1.14 cfs @ 12.03 hrs, Volume= 0.077 af
 Outflow = 0.05 cfs @ 11.16 hrs, Volume= 0.077 af, Atten= 96%, Lag= 0.0 min
 Discarded = 0.05 cfs @ 11.16 hrs, Volume= 0.077 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 297.49' @ 15.87 hrs Surf.Area= 862 sf Storage= 1,367 cf

Plug-Flow detention time= 307.2 min calculated for 0.077 af (100% of inflow)
 Center-of-Mass det. time= 307.3 min (1,185.5 - 878.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	295.00'	559 cf	25.00'W x 34.50'L x 2.69'H Field A 2,323 cf Overall - 924 cf Embedded = 1,398 cf x 40.0% Voids
#2A	295.25'	878 cf	ACF R-Tank HD 1 x 208 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 208 Chambers in 16 Rows
		1,437 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	295.00'	2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.05 cfs @ 11.16 hrs HW=295.03' (Free Discharge)↑ **1=Exfiltration** (Exfiltration Controls 0.05 cfs)

Pond 5P: Roof Infiltration - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

13 Chambers/Row x 2.35' Long = 30.50' Row Length +24.0" End Stone x 2 = 34.50' Base Length

16 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 25.00' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

208 Chambers x 4.2 cf = 878.1 cf Chamber Storage

208 Chambers x 4.4 cf = 924.4 cf Displacement

2,322.7 cf Field - 924.4 cf Chambers = 1,398.3 cf Stone x 40.0% Voids = 559.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,437.5 cf = 0.033 af

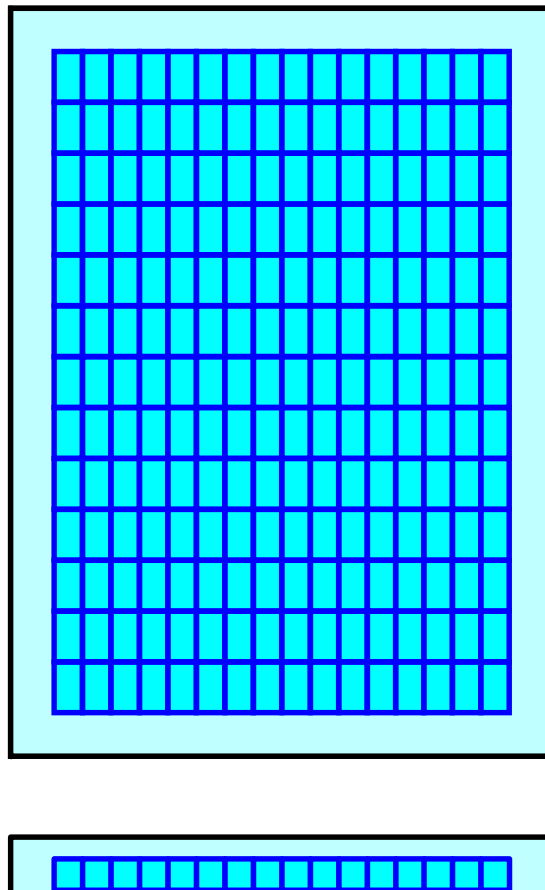
Overall Storage Efficiency = 61.9%

Overall System Size = 34.50' x 25.00' x 2.69'

208 Chambers

86.0 cy Field

51.8 cy Stone



Cumberland Post

Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"

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Summary for Pond 6P: SSSF2

Inflow Area = 0.355 ac, 88.46% Impervious, Inflow Depth = 5.84" for 50-yr event
 Inflow = 2.44 cfs @ 12.02 hrs, Volume= 0.173 af
 Outflow = 0.13 cfs @ 10.72 hrs, Volume= 0.173 af, Atten= 95%, Lag= 0.0 min
 Primary = 0.13 cfs @ 10.72 hrs, Volume= 0.173 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 295.79' @ 13.73 hrs Surf.Area= 2,299 sf Storage= 2,477 cf

Plug-Flow detention time= 151.9 min calculated for 0.173 af (100% of inflow)
 Center-of-Mass det. time= 151.7 min (937.6 - 785.9)

Volume	Invert	Avail.Storage	Storage Description
#1A	294.00'	1,268 cf	38.12'W x 60.30'L x 2.04'H Field A 4,683 cf Overall - 1,513 cf Embedded = 3,171 cf x 40.0% Voids
#2A	294.25'	1,437 cf	ACF R-Tank SD 1 x 624 Inside #1 Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf 624 Chambers in 26 Rows
		2,705 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	294.00'	2.410 in/hr Exfiltration over Surface area

Primary OutFlow Max=0.13 cfs @ 10.72 hrs HW=294.02' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.13 cfs)

Pond 6P: SSSF2 - Chamber Wizard Field A**Chamber Model = ACF R-Tank SD 1 (ACF Environmental R-Tank SD)**

Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf

Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf

24 Chambers/Row x 2.35' Long = 56.30' Row Length +24.0" End Stone x 2 = 60.30' Base Length

26 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 38.12' Base Width

3.0" Stone Base + 9.4" Chamber Height + 12.0" Stone Cover = 2.04' Field Height

624 Chambers x 2.3 cf = 1,436.9 cf Chamber Storage

624 Chambers x 2.4 cf = 1,512.6 cf Displacement

4,683.3 cf Field - 1,512.6 cf Chambers = 3,170.7 cf Stone x 40.0% Voids = 1,268.3 cf Stone Storage

Chamber Storage + Stone Storage = 2,705.2 cf = 0.062 af

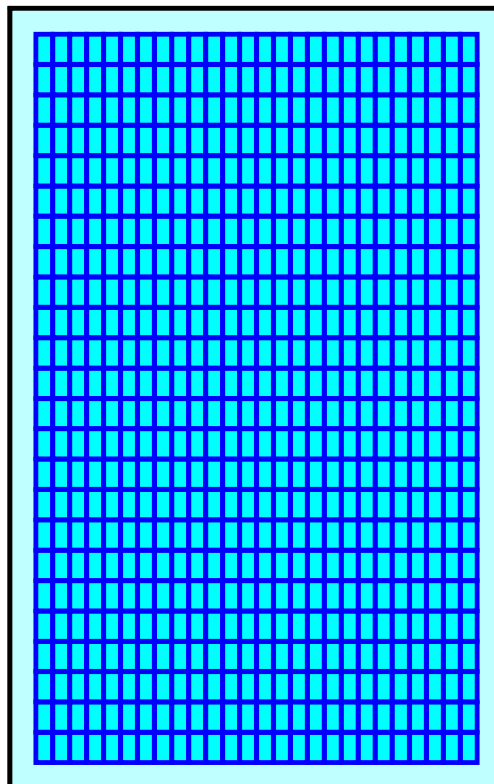
Overall Storage Efficiency = 57.8%

Overall System Size = 60.30' x 38.12' x 2.04'

624 Chambers

173.5 cy Field

117.4 cy Stone



Cumberland Post*Cumberland 24-hr S1 25-yr 50-yr Rainfall=6.90"*

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Summary for Pond 7P: CB

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.325 ac, 93.64% Impervious, Inflow Depth = 6.35" for 50-yr event
Inflow = 0.67 cfs @ 12.93 hrs, Volume= 0.702 af
Primary = 0.67 cfs @ 12.93 hrs, Volume= 0.702 af, Atten= 0%, Lag= 0.0 min
Routed to Reach POI1 : POI#1

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Memorandum

To: Planning Board

Re: Planning Board Agenda Item # 6: Rusty Lantern Site Plan Review

From: Carla Nixon, Town Planner

Date: February 15, 2024

This is the first review for the proposed Rusty Lantern Market and bank to be located at the corner of Rt. 100 and Skillin Road.

This application is not ready for approval at this meeting, so the findings of fact are incomplete. I recommend the Board hear the presentation, ask questions, hold the public hearing, consider and act on the requested waivers, and then table the application.

While I have not had anyone reach out to me to comment on this project, I anticipate there will be residents at the meeting as there is concern about the safety of the gas tanks being located above the aquifer. A full hydrogeologic Report was submitted but has not had a peer review yet as that would require a hydrogeologist review the plan. Gorrill Palmer has done the peer review for the rest of the application.

Date: February 20, 2024
To: Town of Cumberland Planning Board
From: Carla Nixon, Town Planner
Subject: **Site Plan Review: Rusty Lantern Convenience Store with Bank Drive-Through**

REQUEST/PROJECT DESCRIPTION:

The applicant is the Cumberland Real Estate Group, LLC. The development will affect all of Tax Map U19, Lot 12 - owned by Ronald Copp, Sr. and Ronald Copp, Jr., and a portion of Tax Map U 19, Lot 13 owned by Ronald Copp, Sr., Howell Copp and Jerald Copp, Jr. The total developed area will be 1.87 acres. There is a purchase and sale agreement dated March 14, 2023, on file. The request is for site plan review and approval for a 5,038-sf. convenience store with fuel pumps and a 2,935-sf bank with drive through to be located at 181 Gray Rd. in the Village Center Commercial (VCC) zoning district.

The applicant is represented by Curtis Neufeld, P.E., Priority Real Estate Group.

The project is being reviewed for conformance with Chapter 229, Site Plan Ordinance and the Route 100 Design Standards.

DEPARTMENT HEAD REVIEWS:

Dan Small, Fire Chief:

- 1) An ambulance trying to go through one of the drive through lanes when a person is in the process of making a transaction does not work.
 - a. There would be a delay with the vehicle making the transaction and even longer if another vehicle is in line and can't move until the first vehicle moves.
 - b. If the car moves prior to receiving the money/receipt/ATM card there would be a liability to the Town if the money is taken by another person or it blows away in the wind.
- 2) With two people on the ambulance(one driving/one performing patient care) there would be nobody to assist with backing the vehicle up to make sure there are no vehicles/pedestrians to the rear of the ambulance.
- 3) The turning radius you show on the updated drawing will likely be further restricted with snowbanks when they are not immediately cleared during/after a storm.
- 4) Curbing and/or bollard(s) would be a concern with trying to make a tight turn through the non-drive through lane. Can the island be shortened?

Charles Rumsey, Police Chief: No comments.

OUTSIDE AGENCY REVIEWS:

Maine DEP: Stormwater Permit by Rule Required. Outstanding.

Maine DOT: Traffic Movement Permit. Outstanding.

REQUESTED WAIVERS

1. High intensity soils survey.
- ~~2. Hydrogeologic evaluation.~~
- ~~3. Traffic study.~~
4. Market study.

TOWN ENGINEER'S REVIEW:

Doug Reynold, PE, Gorrill Palmer Engineers, February 12, 2024:

As requested by the Town, Gorrill Palmer has conducted an Engineering Peer Review for the above referenced project. Information received for this assignment included:

- Site Plan Application, dated January 29, 2024, prepared by Priority Real Estate Group, LLC on behalf of Cumberland Property Holdings, LLC, consisting of 509 pages
- Drawing Set, dated January, 2024, prepared by Priority Real Estate Group, LLC consisting of 32 drawings.
- Revised Site Plan Application form and Stormwater Management Report received February 12, 2024 prepared by Priority Real Estate Group, LLC.
- Revised Drawing Set, received February 12, 2024, prepared by Priority Real Estate Group, LLC consisting of 21 drawings.

Based on our review of this information, general engineering principles and the Town of Cumberland Zoning Ordinance, we offer the following comments related to the engineering and design aspects of this project. As there are substantial comments to follow, Gorrill Palmer reserves the right to provide additional comments on future submissions.

Site Plan Application:

- I. As stated in the Application, two waivers were requested:
 - a. High Intensity soil survey
 - b. Market StudyGP has no objections to the granting of waivers for items above from an engineering perspective based on the scale and nature of the project.
2. Survey does not show existing internal lot line. Please clarify if the lots are going to be combined, or remain the same.
3. Are there any environmental permitting requirements associated with this project? Specifically, regarding the underground propane tanks.
4. Is this for Cumberland Real Estate Group, LLC or Cumberland Property Holdings, LLC? Please clarify as both are discussed.
5. Attachment A – Application form & Checklists
 - a. Application form states no deed restrictions or easements, however there is a 25' easement for Route 100. Please show this easement along the site's frontage.
 - b. Please provide applicable sign information.
 - c. Has the Fire/EMS Department reviewed for compliance with Town & State requirements for fire and alarm systems?
 - d. Proposed disturbance exceeds 1 acre, has a MDEP general construction (stormwater) permit been applied for?
 - e. Please provide a signed copy of the application form.

Ordinance Compliance:

6. Chapter 229 Section 10.B
 - a. The cover letter states *"the site has been designed to accommodate fuel tankers and emergency vehicles"*
Comment: The tanker movement appears to go through the parking spaces located at the center of the site. Based on review of the Town Ordinances, it appears only 28 and 17 parking spaces are required for the gas station and bank respectively. The proposed site has 37 and 24 parking spaces for

the gas station and bank respectively. It may be advisable to remove these parking spaces to prevent conflicts with parked cars. Has the Fire Department reviewed these plans? A turnaround area for the fire truck does not appear feasible.

- b. The cover letter states *“Entrances have been reviewed by MaineDOT and Gorrill-Palmer”*.

Comment: MaineDOT doesn’t allow slopes exceeding 4% within 6’ of the gutter line. Slopes also exceed the maximum allowed by the ordinances, please revise.

- c. Section (1)(h)[2] states *“No use which generates 100 or more vehicle trips per day shall have more than two points of entry from and two points of egress to a single roadway. The combined width of all accessways must not exceed 60 feet.”*.

Comment: The combined width appears to be 62 feet, please revise or request a waiver of this section.

- d. Section (2)(a) states; *“Private entrances/exits must be located at least 50 feet from the closest unsignalized intersection and 150 feet from the closest signalized intersection, as measured from the point of tangency for the corner to the point of tangency for the accessway. This requirement may be reduced if the shape of the site does not allow conformance with this standard.”*

Comment: It appears that the entrance on Skillin Road may be within 50’ of the point of tangency for the roundabout, a waiver should be requested for this.

- e. Section (4) states *“Parking lots on adjoining lots may be connected by accessways not exceeding 24 feet in width.”*

Comment: The access way appears to be 32 feet, please revise or request a waiver of this section.

7. Chapter 229 Section 10.D

- a. **Comment:** There is a hydrant at the corner of Rt 100 and Skillin Rd that will be used for fire protection, has the fire department reviewed these plans and concurred that the fire hydrant is close enough to the bank?
- b. **Comment:** Please provide ability to serve letters from the water district.

8. Chapter 229 Section 10.E

- a. **Comment:** All nearby wells should be depicted on the site plans.
- b. The hydrogeological report prepared and stamped by Sevee & Maher dated January 2024 states “the Site is suitable for the proposed storage of refined petroleum products”. GP has no objections to the findings in this report.

Supporting Documents:

9. Attachment E – Supporting Documents

- a. HHE200 Applications should be signed by the owner/applicant.

10. Attachment F – Supporting Graphics

- a. **Comment:** What is the intent of the signing plan? Some items depicted on the signing plan do not appear in the plan set. Please note which signs are to be provided by the Town (if any).

11. Attachment G – Financial and Technical Capacity

- a. Letter states that the applicant has the financial capability up to \$6,000,000, please confirm this is adequate for the project.

12. Attachment I – Stormwater Management Report

- a. As there are substantial comments to follow, Gorrill Palmer reserves the right to provide additional comments on future submissions.
- b. **Comment:** Please provide a statement from the MaineDEP that an Individual Stormwater Law Permit is not required for this project.
- c. **Comment:** Roof drip edge treatment measures are mentioned throughout the report, but this is not shown on plans/modeling. Additionally, there appears to be three SSSFs instead of two that are mentioned in the report.
- d. **Comment:** The report states that 1.36 acres or 63,190 s.f. of impervious area is being treated, please check conversions.
- e. **Comment:** Please provide BMP sizing calculations, including isolator rows.
- f. **Comment:** Please provide a letter from the Manufacturer stating the BMPs have been sized and designed in accordance with MaineDEP and the Manufacturer’s requirements.
- g. **Comment:** Please describe the points of analysis in the report.

- h. **Comment:** Provide narrative and details on how outflow is being controlled to ensure a 24-48 hour release time.
- i. **Comment:** Please show test pits on plans and provide a narrative on the results of the test pits in the stormwater report discussing; separation from seasonal high water table, bedrock, and if proposing infiltration, permeability of the underlying soils and if underlying soils need to be amended to meet MaineDEP permeability rates.
- j. **Comment:** Please note if impermeable liners or infiltration are proposed for each system in the report and plans.
- k. **Comment:** Please review to make sure existing and proposed impervious/developed areas noted on the plans are consistent with the stormwater report. Without spot grades showing the breaks in subcatchments, it is difficult to review these areas.
- l. **Comment:** For all ponds, please provide inverts & elevations that match the plans.
- m. **Comment:** Please discuss overflow measures for SSSF#1 that will allow it to drain without flooding the roadway or building should the system becomes clogged.
- n. **Comment:** Please stamp the stormwater report.

Site Plans

13. C2

- a. Please show existing lot lines for the development.

14. C3

- a. Please provide dimensions of proposed buildings.
- b. Please confirm the site is decreasing impervious area by 0.61 acres & update General Note 8 if needed.
- c. Concerns with midblock crossing for Route 100. Doesn't appear to coincide with roundabout and could potentially be dangerous with Driveway.

15. C4

- a. Please show the location and dimensions of the underground petroleum storage tanks to confirm there are no conflicts with other site features.

16. C5

- a. § 229-10.B.(c) states "The grade of any proposed drive or street must be not more than +3% for a minimum of two car lengths, or 40 feet, from the intersection." The proposed grades appear to exceed 5% at entrances, please revise.
- b. Please provide adequate spot grades to match the subcatchment boundaries in the stormwater analysis.
- c. Please review spot grades throughout, localized areas exceeding a 10% slope were noticed.

17. L1

- a. Please review proposed landscaping plan, the layout does not match the layout from the rest of the set.
- b. Confirm plantings will not affect stormwater management facilities.
- c. Please verify if plantings will need to be adjusted for the roundabout.

18. Lighting Plan

- a. Please review proposed lighting plan, the layout does not match the layout from the rest of the set.
- b. Foot candle points do not appear to align with the location of the proposed lighting fixtures, please review.

19. SW

- a. Approx limits of cut/fill extend onto private property. Please provide additional information relative to title-right-interest.

20. IA

- a. Area called out as wooded area as of 1997 should also include what is currently wooded area. Calculations should be updated.

21. C11

- a. Please show underdrain piping and overflow piping and inverts for each system.
- b. Please show isolator/maintenance rows and sizing calculations.
- c. Please indicate in the proposed systems are to be lined with an impermeable membrane, or if these are proposed to be infiltration systems.

MEMORANDUM
C-Store with Gas Fueling / Branch Bank
Traffic Peer Review
Cumberland, Maine
February 9, 2024

INTRODUCTION

Per the Town of Cumberland requests, Gorrill Palmer (GP) has completed a traffic peer review of submitted material for a Convenience Store with Gasoline Fueling and Branch Bank Development located on the easterly side of Route 100 in Cumberland, Maine. The following information was included in this review:

- Traffic Movement Permit Application: “Sections 1-7, Traffic Movement Permit Application”, Submitted to: Maine Department of Transportation and prepared by Sewall (Diane Morabito) and dated November 22, 2023.

For the purposes of this review, GP focused on Section 7 – Traffic Impact Study (TIS), since the TIS should reflect previous comments as provided at the MaineDOT scoping meeting on Monday, October 30, 2023. Based on our review, we offer the following comments.

TRAFFIC IMPACT STUDY – SECTION 7

GP has no comments on the following sections as presented in the TIS:

- A. Study Preparation
- B. Study Horizon
- C. Site and Traffic Information
- D. Trip Assignments

E. TRAFFIC VOLUMES

- Turning movement counts were completed on August 9, 2023. This is an acceptable time-period to collect traffic volumes. Because the volumes were collected in the summer, we concur with the TIS that no seasonal adjustment was needed.
- The traffic volumes were adjusted by a yearly growth of 0.5% to 2024 design hourly volumes. We concur with this methodology and growth factor.
- GP concurs with the other development
- GP concurs with the 2024 Build volumes provided in the TIS

F. CAPACITY ANALYSES

- We concur with the criteria and general methodology used to complete the capacity analysis.

Auxiliary Turn Lane Warrants

- GP concurs with the methodology and results of the lane warrant analysis and neither left nor right turn lanes are required on Route 100.

Unsignalized Intersection Analysis

- GP concurs with the general methodology and results of the unsignalized analysis. All the unsignalized intersections evaluated were forecast to operate at acceptable levels of service.

Queue Analysis

- GP concurs with the general methodology and results of the queue analysis. There are no anticipated issues with the queuing of vehicles.

Pedestrian and Multi-Modal Considerations

- GP concurs with the general location of the proposed sidewalks. We support the suggestion for the development to be assessed an impact fee for the sidewalks such that the MaineDOT or Town can use that money toward sidewalks once the final design of the intersection is determined and is being re-constructed.

G. TRAFFIC SIGNAL WARRANT ANALYSIS

- GP concurs that a traffic signal warrant was not requested for this project.

H. SIGHT DISTANCE ANALYSIS

- GP concurs that no additional sight distance evaluation was requested of the applicant. The applicant should confirm that no signage or landscaping will restrict available sight lines within the sight triangles.

I. TRAFFIC ACCIDENTS

- GP concurs that this project does not require any further action to address traffic crashes.

J. RECOMMENDATIONS

- No comments.

K. CONCLUSIONS

- No comments.
Dunton, PE, PTOE



Prepared By: Randy

SECTION 229 - SITE PLAN REVIEW

NOTE: THE FOLLOWING APPROVAL STANDARDS HAVE NOT BEEN FULLY ADDRESSED PRIOR TO THIS MEETING. THERE ARE DRAFT FINDINGS FOR A FUTURE REVIEW.

SECTION 10: APPROVAL STANDARDS AND CRITERIA

The following criteria shall be used by the Planning Board in reviewing applications for site plan review and shall serve as minimum requirements for approval of the application. The application shall be approved unless the Planning Board determines that the applicant has failed to meet one or more of these standards. In all instances, the burden of proof shall be on the applicant who must produce evidence sufficient to warrant a finding that all applicable criteria have been met.

10.A Utilization of the Site

A. Utilization of the Site: The plan for the development, including buildings, lots, and support facilities, must reflect the natural capabilities of the site to support development. Environmentally sensitive areas, including but not limited to, wetlands, steep slopes, floodplains, significant wildlife habitats, fisheries, scenic areas, habitat for rare and endangered plants and animals, unique natural communities and natural areas, and sand and gravel aquifers must be maintained and preserved to the maximum extent. The development must include appropriate measures for protecting these resources, including but not limited to, modification of the proposed design of the site, timing of construction, and limiting the extent of excavation.

There is a sand and gravel aquifer located beneath the site, but safeguards have been proposed that will protect the aquifer.

The Town Engineer has made comments that must be addressed prior to approval.

Based on the above findings of fact, the Board finds the standards of this section have NOT been met.

B. Traffic, Circulation and Parking

(1) Traffic Access and Parking. Vehicular access to and from the development must be safe and convenient.

(a) Any driveway or proposed street must be designed so as to provide the minimum sight distance according to the Maine Department of Transportation standards, to the maximum extent possible.

(b) Points of access and egress must be located to avoid hazardous conflicts with existing turning movements and traffic flows.

(c) The grade of any proposed drive or street must be not more than + 3% for a minimum of two (2) car lengths, or forty (40) feet, from the intersection.

(d) The intersection of any access/egress drive or proposed street must function: (a) at a Level of Service D, or better, following development if the project will generate one thousand (1,000) or more vehicle trips per twenty-four (24) hour period; or (b) at a level which will allow safe access into and out of the project if less than one thousand (1,000) trips are generated.

(e) Where a lot has frontage on two (2) or more streets, the primary access to and egress from the lot must be provided from the street where there is less potential for traffic congestion and for traffic and pedestrians hazards. Access from other streets may be allowed if it is safe and does not promote short cutting through the site.

(f) Where it is necessary to safeguard against hazards to traffic and pedestrians and/ or to avoid traffic congestion, the applicant shall be responsible for providing turning lanes, traffic directional islands, and traffic controls within public streets.

(g) Access ways must be designed and have sufficient capacity to avoid queuing of entering vehicles on any public street.

(h) The following criteria must be used to limit the number of driveways serving a proposed project:

- (1) No use which generates less than one hundred (100) vehicle trips per day shall have more than one (1) two-way driveway onto a single roadway. Such driveway must be no greater than thirty (30) feet wide.
- (2) No use which generates one hundred (100) or more vehicle trips per day shall have more than two (2) points of entry from and two (2) points of egress to a single roadway. The combined width of all access ways must not exceed sixty (60) feet.

(2) Access way Location and Spacing

Access ways must meet the following standards:

(a) Private entrance / exits must be located at least fifty (50) feet from the closest un-signalized intersection and one hundred fifty (150) feet from the closest signalized intersection, as measured from the point of tangency for the corner to the point of tangency for the access way. This requirement may be reduced if the shape of the site does not allow conformance with this standard.

(b) Private access ways in or out of a development must be separated by a minimum of seventy-five (75) feet where possible.

(3) Internal Vehicular Circulation. The layout of the site must provide for the safe movement of passenger, service, and emergency vehicles through the site.

(a) Projects that will be served by delivery vehicles must provide a clear route for such vehicles with appropriate geometric design to allow turning and backing.

(b) Clear routes of access must be provided and maintained for emergency vehicles to and around buildings and must be posted with appropriate signage (fire lane - no parking).

(c) The layout and design of parking areas must provide for safe and convenient circulation of vehicles throughout the lot.

(d) All roadways must be designed to harmonize with the topographic and natural features of the site insofar as practical by minimizing filling, grading, excavation, or other similar activities which result in unstable soil conditions and soil erosion, by fitting the development to the natural contour of the land and avoiding substantial areas of excessive grade and tree removal, and by retaining existing vegetation during construction. The road network must provide for vehicular, pedestrian, and cyclist safety, all season emergency access, snow storage, and delivery and collection services.

(4) Parking Layout and Design. Off street parking must conform to the following standards:

(a) Parking areas with more than two (2) parking spaces must be arranged so that it is not necessary for vehicles to back into the street.

(b) All parking spaces, access drives, and impervious surfaces must be located at least fifteen (15) feet from any side or rear lot line, except where standards for buffer yards require a greater distance. No parking spaces or asphalt type surface shall be located within fifteen (15) feet of the front property line. Parking lots on adjoining lots may be connected by accessways not exceeding twenty-four (24) feet in width.

(c) Parking stalls and aisle layout must conform to the following standards.

Parking Angle	Stall Width	Skew Width	Stall Depth	Aisle Width
90°	9'-0"		18'-0"	24'-0" 2-way
60°	8'-6"	10'-6"	18'-0"	16'-0" 1-way
45°	8'-6"	12'-9"	17'-6"	12'-0" 1-way
30°	8'-6"	17'-0"	17'-0"	12'-0" 1 way

(d) In lots utilizing diagonal parking, the direction of proper traffic flow must be indicated by signs, pavement markings or other permanent indications and maintained as necessary.

(e) Parking areas must be designed to permit each motor vehicle to proceed to and from the parking space provided for it without requiring the moving of any other motor vehicles.

(f) Provisions must be made to restrict the "overhang" of parked vehicles when it might restrict traffic flow on adjacent through roads, restrict pedestrian or bicycle movement on adjacent walkways, or damage landscape materials.

(5) Building and Parking Placement

(a) The site design should avoid creating a building surrounded by a parking lot. Parking should be to the side and preferably in the back. In rural, uncongested areas buildings should be set well back from the road so as to conform to the rural character of the area. If the parking is in front, a generous, landscaped buffer between road and parking lot is to be provided. Unused areas should be kept natural, as field, forest, wetland, etc.

(b) Where two or more buildings are proposed, the buildings should be grouped and linked with sidewalks; tree planting should be used to provide shade and break up the scale of the site. Parking areas should be separated from the building by a minimum of five (5) to ten (10) feet. Plantings should be provided along the building edge, particularly where building facades consist of long or unbroken walls.

(6) Pedestrian Circulation: The site plan must provide for a system of pedestrian ways within the development appropriate to the type and scale of development. This system must connect the major building entrances/ exits with parking areas and with existing sidewalks, if they exist or are planned in the vicinity of the project. The pedestrian network may be located either in the street right-of-way or outside of the right-of-way in open space or recreation areas. The system must be designed to link the project with residential, recreational, and commercial facilities, schools, bus stops, and existing sidewalks in the neighborhood or, when appropriate, to connect the amenities such as parks or open space on or adjacent to the site

The location of the entrance drive provides adequate sight distance in both directions. Parking spaces are in conformance with the town ordinance. An application for a Maine DEP Traffic Movement Permit has been made. The site has been designed to accommodate fuel tankers and emergency vehicles. A pedestrian crosswalk with pedestrian activated flashing signage is shown for Route 100 and a crosswalk will be added on Skillin Road. Sidewalks will be constructed along Skillin Road to Kathy Lane and northerly along Gray Road to Faraday Lane.

The Town Engineer has made comments that must be addressed prior to approval.

Based on the above findings of fact, the Board finds the standards of this section have not been met.

C. Stormwater Management and Erosion Control

(1) Stormwater Management. Adequate provisions must be made for the collection and disposal of all stormwater that runs off proposed streets, parking areas, roofs, and other surfaces, through a stormwater drainage system and maintenance plan, which must not have adverse impacts on abutting or downstream properties.

(a) To the extent possible, the plan must retain stormwater on the site using the natural features of the site.

(b) Unless the discharge is directly to the ocean or major river segment, stormwater runoff systems must detain or retain water such that the rate of flow from the site after development does not exceed the predevelopment rate.

(c) The applicant must demonstrate that on - and off-site downstream channel or system capacity is sufficient to carry the flow without adverse effects, including but not limited to, flooding and erosion of shoreland areas, or that he / she will be responsible for whatever improvements are needed to provide the required increase in capacity and / or mitigation.

(d) All natural drainage ways must be preserved at their natural gradients and must not be filled or converted to a closed system unless approved as part of the site plan review.

(e) The design of the stormwater drainage system must provide for the disposal of stormwater without damage to streets, adjacent properties, downstream properties, soils, and vegetation.

(f) The design of the storm drainage systems must be fully cognizant of upstream runoff which must pass over or through the site to be developed and provide for this movement.

(g) The biological and chemical properties of the receiving waters must not be degraded by the stormwater runoff from the development site. The use of oil and grease traps in manholes, the use of on-site vegetated waterways, and vegetated buffer strips along waterways and drainage swales, and the reduction in use of deicing salts and fertilizers may be required, especially where the development stormwater discharges into a gravel aquifer area or other water supply source, or a great pond.

(2) Erosion Control

(a) All building, site, and roadway designs and layouts must harmonize with existing topography and conserve desirable natural surroundings to the fullest extent possible, such that filling, excavation and earth moving activity must be kept to a minimum. Parking lots on sloped sites must be terraced to avoid undue cut and fill, and / or the need for retaining walls. Natural vegetation must be preserved and protected wherever possible.

(b) Soil erosion and sedimentation of watercourses and water bodies must be minimized by an active program meeting the requirements of the Maine Erosion and Sediment Control Handbook for Construction: Best Management Practices, dated March 1991, and as amended from time to time.

The Town Engineer has made comments that must be addressed prior to approval.

Based on the above findings of fact, the Board finds the standards of this section have not been met.

(D) Water, Sewer, and Fire Protection

(1) Water Supply Provisions: The development must be provided with a system of water supply that provides each use with an adequate supply of water. If the project is to be served by a public water supply, the applicant must secure and submit a written statement from the supplier that the proposed water supply system conforms with its design and construction standards, will not result in an undue burden on the source of distribution system, and will be installed in a manner adequate to provide needed domestic and fire protection flows.

(2) Sewage Disposal Provisions: The development must be provided with a method of disposing of sewage which is in compliance with the State Plumbing Code. If provisions are proposed for on-site waste disposal, all such systems must conform to the Subsurface Wastewater Disposal Rules.

(3) Utilities: The development must be provided with electrical, telephone, and telecommunication service adequate to meet the anticipated use of the project. New utility lines and facilities must be screened from view to the extent feasible. If the service in the street or on adjoining lots is underground, the new service must be placed underground.

(4) Fire Protection: The site design must comply with the Fire Protection Ordinance. The Fire Chief shall issue the applicant a "Certificate of Compliance" once the applicant has met the design requirement of the Town's Fire Protection Ordinance.

Water service will be extended to the lots from the existing utilities located on Skillin and Gray Roads. Sewerage for each building will be managed by private subsurface disposal systems. The water and septic plans have been reviewed and approved by the Town Engineer. Utility lines will be underground.

The Town Engineer has made comments that must be addressed prior to approval.

Based on the above findings of fact, the Board finds the standards of this section have been met.

E. Water Protection

(1) Groundwater Protection: The proposed site development and use must not adversely impact either the quality or quantity of groundwater available to abutting properties or to the public water supply systems. Applicants whose projects involve on-site water supply or sewage disposal systems with a capacity of two thousand (2,000) gallons per day or greater must demonstrate that the groundwater at the property line will comply, following development, with the standards for safe drinking water as established by the State of Maine. **The project will be served by public water so there will be no extraction of groundwater for operations or irrigation. The sewage disposal system will comply with the standards for safe drinking water as established by the State of Maine.**

(2) Water Quality: All aspects of the project must be designed so that:

(a) No person shall locate, store, discharge, or permit the discharge of any treated, untreated, or inadequately treated liquid, gaseous, or solid materials of such nature, quantity, obnoxious, toxicity, or temperature that may run off, seep, percolate, or wash into surface or groundwaters so as to contaminate, pollute, or harm such waters or cause nuisances, such as objectionable shore deposits, floating or submerged debris, oil or scum, color, odor, taste, or unsightliness or be harmful to human, animal, plant, or aquatic life.

(b) All storage facilities for fuel, chemicals, chemical or industrial wastes, and biodegradable raw materials, must meet the standards of the Maine Department of Environmental Protection and the State Fire Marshall's Office.

Stormwater runoff will be directed to new subsurface soil filters which will be lined with an impermeable liner to prevent any groundwater contamination.

(3) Aquifer Protection: If the site is located within the Town Aquifer Protection Area, a positive finding by the Board that the proposed plan will not adversely affect the aquifer is required.

The site is located within the Town Aquifer Protection Area. A hydrogeologic evaluation was conducted by Sevee and Maher Engineers that included field work to determine soils characteristics and groundwater depth and direction of flow. The report states that the "Site is suitable for proposed storage of refined petroleum products."

The refueling system will include double-walled fiberglass tanks that have advanced monitoring methods to detect any leaks before any product escapes the tank. The pipes to the fuel dispensers will also be double-walled. The leak detection system will have visual and audible alerts in the store. The concrete pad around the dispensers will have grooves, referred to as Positive Limiting Barriers, at the perimeter that will contain spills during refueling vehicles. A spill kit will be maintained at the store and all store operators are trained per State and Federal standards.

The Town Engineer has made comments that must be addressed prior to approval.

Based on the above findings of fact, the Board finds that the standards of this section have NOT been met.

F. Floodplain Management: If any portion of the site is located within a special flood hazard area as identified by the Federal Emergency Management Agency, all use and development of that portion of the site must be consistent with the Town's Floodplain management provisions.

Based on a review of the FEMA floodplain maps, the site is not located within a floodplain. The location is classified as Zone C (areas of minimal flooding risk).

Based on the above finding of fact, the Board finds the standards of this section have been met.

Based on the above finding of fact, the Board finds the standards of this section have been met.

G. Historic and Archaeological Resources: If any portion of the site has been identified as containing historic or archaeological resources, the development must include appropriate measures for protecting these resources, including but not limited to, modification of the proposed design of the site, timing of construction, and limiting the extent of excavation.

There are no known historic or archeological resources located on the site. There is a letter on file from the Maine Historic Preservation Commission. will not have an adverse effect on any historical or archaeological resources.

Based on the above finding of fact, the Board finds the standards of this section have been met.

H. Exterior Lighting:

The proposed development must have adequate exterior lighting to provide for its safe use during nighttime hours, if such use is contemplated. All exterior lighting must be designed and shielded to avoid undue glare, adverse impact on neighboring properties and rights - of way, and the unnecessary lighting of the night sky.

Exterior lighting has been designed to provide adequate lighting for parking areas. Full cutoff fixtures be utilized to avoid glare and adverse impact on neighboring properties and rights of way, and unnecessary lighting of the night sky. A photometric plan has been submitted.

The Town Engineer has made comments that must be addressed prior to approval.

Based on the above finding of fact, the Board finds the standards of this section have NOT been met.

I. Buffering and Landscaping

- (1) Buffering of Adjacent Uses:** The development must provide for the buffering of adjacent uses where there is a transition from one type of use to another use and for the screening of mechanical equipment and service and storage areas. The buffer may be provided by distance, landscaping, fencing, changes in grade, and / or a combination of these or other techniques.

Buffering in the form of fences, grade changes, and landscaping, have been designed to screen the businesses and generally soften the appearance of the development. The existing wooded area between the businesses and the houses on Kathy Lane will be maintained to the extent possible.

- (2) Landscaping:** Landscaping must be provided as part of site design. The landscape plan for the entire site must use landscape materials to integrate the various elements on site, preserve and enhance the particular identity of the site, and create a pleasing site character. The landscaping should define street edges, break up parking areas, soften the appearance of the development, and protect abutting properties.

The Town Engineer has made comments that must be addressed prior to approval.

Based on the above findings of fact, the Board finds the standards of this section have NOT been met.

J. Noise: The development must control noise levels such that it will not create a nuisance for neighboring properties.

It is not anticipated that the development will create a noise level that will be a nuisance for adjacent properties. Ambient sounds will be comparable to those of Gray and Skillin Roads.

Based on the above findings of fact, the Board finds the standards of this section have been met.

K. Storage of Materials

(1) Exposed nonresidential storage areas, exposed machinery, and areas used for the storage or collection of discarded automobiles, auto parts, metals or other articles of salvage or refuse must have sufficient setbacks and screening (such as a stockade fence or a dense evergreen hedge) to provide a visual buffer sufficient to minimize their impact on abutting residential uses and users of public streets.

(2) All dumpsters or similar large collection receptacles for trash or other wastes must be located on level surfaces which are paved or graveled. Where the dumpster or receptacle is located in a yard which abuts a residential or institutional use or a public street, it must be screened by fencing or landscaping.

(3) Where a potential safety hazard to children is likely to arise, physical screening sufficient to deter small children from entering the premises must be provided and maintained in good condition.

The dumpsters are screened by either fencing or landscaping. A shed is proposed to be constructed as an accessory building to store dry goods for the convenience store. Other than some seasonal items displayed on the sidewalk at the building, there will be no storage of items or other materials outdoors.

Based on the above findings of fact, the Board finds the standards of this section have been met.

L. Capacity of the Applicant: The applicant must demonstrate that he / she has the financial and technical capacity to carry out the project in accordance with this ordinance and the approved plan.

Technical Ability: *The applicant has retained professional engineers, surveyors, traffic, lighting and geotechnical consultants.*

Financial Capacity: *There is a letter on file dated 1/26/24 from Maine Community Bank stating that the Cumberland Real Estate Group has the financial capability to borrow up to \$6,000,000 for the construction project located at 187 Gray Road.*

The Town Engineer has asked for an estimate of values to ensure that the amount of \$6 M is an accurate cost for construction.

Based on the above findings of fact, the Board finds the standards of this section have been met.

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M. Design and Performance Standards

(1) Route 100 Design Standards are applicable to this project.

- (2) Route 1 Design Standards
- (3) Town Center District Design and Performance Standards
- (4) Village Mixed Use Performance Standards.

ROUTE 100 DESIGN STANDARDS

1.2 Site Planning and Design

1.1 Master Planning

On properties that are large enough to accommodate more than a single structure, developers will be expected to prepare a conceptual master plan to show the Planning Board the general location of future buildings, parking lots, circulation patterns, open space, utilities, provisions for stormwater management, and other components of site development.

On sites with multiple buildings, the outdoor space defined by the structures should be designed as a focal point for the development, with provisions for seating and other outdoor use. Landscaping, bollards and other site features should maintain a safe separation between vehicles and pedestrians.

FINDING:

1.2 Professional Design

Developers shall have their site plans designed by licensed professionals (civil engineers, architects or landscape architects) as required by State of Maine professional licensing requirements to address the health, safety, welfare and visual pleasure of the general public, during all hours of operation and all seasons of the year.

FINDING:

1.3 Vehicular Access

Development along Cumberland's Route 100 corridor should promote safe, user-friendly and efficient vehicular movement while reducing both the number of trips on the roadway and the number of curb cuts wherever possible.

The vehicular movements discussed in this chapter, both on-site and off-site, shall be designed by a professional engineer and shall be in conformance with all Maine Department of Transportation requirements.

FINDING:

1.3.1 Route 100 Curb Cuts

To promote vehicular, bicycle and pedestrian safety, the number of curb cuts on Route 100 should be kept to a minimum. Adjacent uses are encouraged to use shared driveways wherever possible, thereby reducing the number of turning motions onto and off of Route 100. This practice will increase motorist, bicycle and pedestrian safety, and has the added environmental benefit of helping to reduce impervious (paved) area.

Driveways and their associated turning movements should be carefully designed and spaced to reduce interruptions in Route 100's level of service and to promote safe and easily understandable vehicular movements. Where curb cuts will interrupt sidewalks, ADA requires that the cross slope not exceed 2% in order to maintain accessibility.

New driveways and existing driveways for which the use has changed or expanded require a Maine Department of Transportation "Driveway Entrance Permit." The Planning Board will not grant project approval until the Town has been provided a copy of the permit, or alternately, until the applicant provides the Town a letter from the DOT stating that such a permit is not required. The MDOT may also require a Traffic Movement Permit if the number of vehicle trips exceeds the threshold established by the MDOT.

FINDING:

1.3.2 Site Circulation

Internal vehicular movement on each site should be designed to achieve the following goals: to ensure the safety of motorists, delivery vehicles, pedestrians and cyclists by providing clear cues to the motorist as to where to drive or park, etc., once they enter the site. Landscaping, to reduce impervious areas, is encouraged as much possible.

Every effort should be made to restrict paved surfaces to a maximum of two sides of the building. The site should not feature a building surrounded by drive lanes and parking.

To ensure safe and easily understandable circulation, parking spaces, directional arrows, crosswalks and other markings on the ground should be painted on the pavement paint or shown by other suitable methods.

FINDING:

1.3.3 Driveways between Parcels

Driveways between adjacent parcels should be used where feasible in order to make deliveries easier and reduce unnecessary trips and turning movements on Route 100.

These driveways should provide safe, direct access between adjacent lots, but only where the paved areas of the two adjacent lots are reasonably close together. However, they are inappropriate where they would require excessive impervious (paved) area or impose undue financial burden on the owner.

All such driveways between parcels should have pedestrian walkways when possible.

FINDING:

1.4 Building Placement

Objective: Buildings should be placed on their sites in a way that is sensitive to existing site conditions and respectful of adjacent uses.

1.4.1 Location of Building on the Site

In placing the building on the site, the designer should carefully consider the building's relationship to existing site features such as the size of the site, existing vegetation and topography, drainage, etc., as well as the abutting land uses.

The site design should make every effort to avoid creating a building surrounded by parking lot. In addition, buildings should generally be square to Route 100 and should avoid unusual geometry in building placement unless the site requires it.

FINDING:

1.4.2 Building Entrances

The building's main entrance should be a dominant architectural feature of the building, clearly demarcated by the site design and landscaping. Main entrances should front onto the most convenient parking area.

At building entrance areas and drop-off areas, site furnishings such as benches, sitting walls and, if appropriate, bicycle racks should be encouraged. Additional plantings may be desirable at these points to clearly identify the building entrance and to invite pedestrians into it.

Where building entrances do not face Route 100, the Route 100 façade should still be made interesting and attractive to drivers on Route 100.

FINDING:

1.4.3 Building Setbacks

If adjacent building facades are parallel with Route 100 and buildings have consistent setbacks from Route 100, the visual effect from the road will be orderly and attractive.

Side and rear building setbacks must conform to the requirements of the underlying zone.

FINDING:

1.4.4 Hillside Development

When a proposed development is located on a hillside that is visible from Route 100 or from other public areas, its presence will be much more obvious than development on a level site. Because of this, it is even more important that the structure be designed to fit harmoniously into the visual environment. The use of berms and plantings, where appropriate, will help soften the impact of buildings located in open fields.

Site clearing should also be minimized and vegetation should be retained or provided to minimize the visual impact of the development. Issues of drainage, run-off and erosion should also be closely examined.

FINDING:

1.4.5 Universal Accessibility

Development of all properties, buildings, parking lots, crosswalks, walkways and other site features must comply with the applicable standards of the Americans with Disabilities Act (ADA).

FINDING:

1.5 Parking

Objective: Development should provide safe, convenient and attractive parking. Parking lots should be designed to complement adjacent buildings, the site and the Route 100 corridor without becoming a dominant visual element.

Every effort should be made to break up the scale of parking lots by reducing the amount of pavement visible from the road. Careful attention should be given to circulation, landscaping, lighting and walkways.

FINDING:

1.5.1 Location

Parking lots should be located to the side or rear of buildings. Parking should only be placed between the building and Route 100 if natural site constraints such as wetlands or topography, allow no other option. If parking must be built between the building and Route 100, it should be limited, if at all possible, to only one row of parking spaces and be adequately buffered.

FINDING:

1.5.2 Landscaping

A 25' landscaping easement to the Town of Cumberland will be required of each new development that is on Route 100. This easement will provide an area for the Town to install curbing, if needed, a sidewalk and the planting of trees. Beyond this easement, the developer will provide adequate landscaping to ensure that views from Route 100 are attractive and to buffer the presence of the parking and buildings.

Parking should be separated from the building by a landscaped strip a minimum of five to ten feet wide.

Landscaping around and within parking lots will shade hot surfaces and visually soften the appearance of the hard surfaces. Parking lots should be designed and landscaped to create a pedestrian-friendly environment. A landscaped border around parking lots is encouraged, and landscaping should screen the parking area from adjacent residential uses. Tree plantings between rows of parking are very desirable. Granite curbs, while more expensive, are more attractive and require less maintenance than asphalt ones.

Where there are trees in the 25' landscaping easement between Route 100 and the building, existing healthy trees should be maintained in their natural state. Where there are few or no trees in the 25' buffer, the buffer area should be landscaped either with trees, or with flowering shrubs, fencing, or such architectural elements as stone walls.

Where plantings do not survive or grow to a point where they no longer serve as effective buffers, they shall be replaced or enhanced to meet the intent of the approved plan.

FINDING:

1.5.3 Snow Storage

Provision should be made for snow storage in the design of all parking areas, and these areas should be indicated on the site plan. The area used for snow storage should not conflict with proposed landscaping or circulation patterns. These areas should be sited to avoid problems with visibility, drainage or icing during winter months.

FINDING:

1.5.4 Impervious Surfaces

The amount of paved surface required for parking, driveways and service areas should be limited as much as possible in order to provide green space, reduce run-off and preserve site character. This will have the added benefit of reducing construction and maintenance costs.

FINDING:

1.6 Service Areas

Objective: Service areas include exterior dumpsters, recycling facilities, mechanical units, loading docks and other similar uses. Service areas associated with uses along Route 100 should be designed to meet the needs of the facility with a minimum of visual, odor or noise problems. They should be the smallest size needed to fit the specific requirements of the building and its intended operation and should be fully screened from view by either plantings or architectural elements such as attractive fences.

FINDING:

1.6.1 Location

Service areas should, if possible, be located so that they are not visible from Route 100 or from the building entrance. Locations that face abutting residential properties should also be avoided wherever possible.

Dumpster, recycling facilities and other outdoor service facilities should be consolidated into a single site location, in accordance with appropriate life safety requirements.

FINDING:

1.6.2 Design

Service areas should be designed to accommodate the turning movements of anticipated vehicles, and should be separated from other vehicle movements, parking areas and pedestrian routes.

Wherever possible, service drives should be separated from areas where people will be walking by landscaped islands, grade changes, berms, or other devices to minimize conflicts.

Gates on enclosures should be designed to prevent sagging or binding. Wooden fencing is always preferred, but where chain link is necessary for safety considerations, it should be screened by landscaping and painted a dark color or coated with dark vinyl.

FINDING:

1.6.3 Buffering/Screening

Service areas should be screened to minimize visibility from sensitive viewpoints such as Route 100, nearby residential dwellings, public open space, pedestrian pathways, and building entrances. Landscape screening may consist of evergreen trees, shrubs, and/or planted earth berms. Architectural screening may consist of walls, fences or shed structures, and should complement the design of the main structure through repetition of materials, detailing, scale and color.

Where plantings do not survive, or where they grow to a point where they no longer serve as effective screens, they shall be replaced or supplemented to meet the intent of the plan as approved by the Planning Board.

FINDING:

1.7 Open Space

Objective: In order to provide an attractive, hospitable and usable environment, future development along Route 100 should have generous amounts of open space and attractive site details for such elements as pavement, curbing, sitting and other public areas, landscaping, planters, walls, signage, lighting, bollards, waste receptacles and other elements in the landscape.

FINDING:

1.7.1 Internal Walkways

Internal walkways should invite pedestrians onto the property and make them feel welcome.

Walkways extending the full length of a commercial building are encouraged along any façade that features a customer entrance and an abutting parking area. Such walkways should be located five to ten feet from the face of the building to allow for planting beds. Such walkways should be shown on the project's landscaping plan.

Wherever feasible, interconnections between adjacent properties should be developed to encourage pedestrian movement and reduce vehicle trips.

At a minimum bituminous concrete should be used as the primary material for internal walkways, except that for entrance areas and other special features the use of brick or special paving shall be encouraged. Walkways should be separated from parking areas and travel lanes by raised curbing. Granite is strongly preferred for its durability, appearance and low maintenance requirements.

Driveway crosswalks should be marked by a change in pavement texture, pattern or color to maximize pedestrian safety in parking and other potentially hazardous areas.

FINDING:

1.7.2 Landscaping

Where there are trees in the 75' buffer between Route 100 and the building, existing healthy trees should be maintained in their natural state. Where there are few or no trees in the 75' buffer, the buffer area should be landscaped either with trees, or with flowering shrubs, fencing, or such architectural elements as stone walls.

Where plantings do not survive, or grow to a point where they no longer serve as effective buffers, they shall be replaced or enhanced to meet the intent of the approved plan.

FINDING:

1.7.3 Usable Open Space

Whenever possible, site plans should provide inviting open spaces where people can sit, relax and socialize. Open spaces should be thought of as outdoor rooms, with consideration to ground surfaces, landscaping, lighting and other physical elements. Examples of such spaces include a forecourt outside a building entrance, or a peaceful place outdoors where employees can sit down and eat lunch or have breaks.

FINDING:

1.8 Buffering of Adjacent Uses

Objective: Buffering or screening may be necessary to effectively separate quite different land uses such as housing and office or commercial buildings. Plantings, earth berms, stone walls, grade changes, fences, distance and other means can be used to create the necessary visual and psychological separation.

1.8.1 Appropriateness

The selection of the proper type of buffer should result from considering existing site conditions, distances to property lines, the intensity (size, number of users) of the proposed land use, and the degree of concern expressed by the Planning Department, Planning Board, and abutting landowners. Discussions regarding the need for buffers, and appropriate sizes and types, should begin at the sketch plan stage of review.

FINDING:

1.8.2 Design

Buffers and screens should be considered an integral part of the site and landscaping plans. Stone walls, plantings, fencing, landforms, berms, and other materials used for buffers should be similar in form, texture, scale and appearance to other landscape elements. Structural measures, such as screening walls, should likewise be related to the architecture in terms of scale, materials, forms and surface treatment.

FINDING:

1.8.3 Maintenance

Where plantings do not survive, or where they grow to a point where they no longer serve as effective buffers, they shall be replaced or supplemented to meet the intent of the plan as approved by the Planning Board.

1.9 Erosion, Sedimentation and Stormwater Management

Objective: Protecting the natural environment in Cumberland is as much a priority in these design guidelines as protecting the visual environment. A developer should take every measure possible in the construction and operation of a project to ensure that little or no adverse impact to the natural environment occurs. These measures should be as visually attractive as possible.

1.10.1 Erosion and Sedimentation

Before any site work, construction or the disturbance of any soil occurs on a property, methods, techniques, designs, practices and other means to control erosion and sedimentation, as approved or required by the Maine Department of Environmental Protection, shall be in place. For guidance developers should refer to “Maine Erosion and Sedimentation Control Handbook for Construction – Best Management Practices,” produced by the Cumberland County Soil and Water Conservation District and the Maine DEP.

FINDING:

1.10 Utilities

Objective: It is important to make efficient use of the utility infrastructure that exists along the Route 100 corridor, and to ensure that utility connections to individual development lots are as inconspicuous as possible.

FINDING:

1.10.1 Water and Sewer

All proposed development along the Route 100 Corridor must connect to the municipal water supply and the municipal sewer, wherever such connections are available. Proposed connections are subject to review by the Town and/or its peer reviewers.

FINDING:

1.10.2 Electric, Telephone and Cable

Electric, telephone, cable and other wired connections from existing utilities on Route 100 should be made to individual development lots via underground conduit wherever possible. This prevents the accumulation of unsightly overhead wires, and preserves the natural character of the corridor.

FINDING:

2. Building Types

The purpose of these guidelines is to encourage architectural styles within the Route 100 corridor that draw their inspiration from traditional New England examples. “Vernacular” or commonly used styles that are well represented in Cumberland are center-chimney Federal buildings in brick or clapboard, 100 and a half story Greek Revival “capess” with dormers, in white clapboard with corner pilasters or columns, and Victorians buildings with more steeply pitched roofs, porches and gingerbread trim. Except for mill buildings, the scale and nature of older commercial buildings in towns like Cumberland and Yarmouth, was similar to that of houses of the same period. Modern interpretations and versions of these styles, are entirely appropriate and encouraged. Because of their larger size, traditional barns are also sometimes used as inspiration for modern commercial buildings.

2.1 General Architectural Form

Traditional New England buildings look like they do because of the climate, the materials and technologies available for building and the styles and fads of the 19th century. This is what is meant when people talk about “vernacular architecture”. It is the architecture that develops in a particular geographic area. Typically, while there may be architects who work in a particular “vernacular”, vernacular architecture evolves over time and is not the product of a particular person’s powerful vision.

These guidelines encourage the use of materials and forms that are characteristic of the construction of ordinary houses and commercial buildings of 19th century in northern New England, and particularly in Maine. Modern interpretations and versions of these materials and forms are entirely appropriate and encouraged.

FINDING:

2.1.1 Roofs

Because of the need to shed snow, New England roofs have generally been pitched rather than flat. Federal roofs are sometimes gambrel-shaped. In the Greek Revival style they are often gabled or have dormers, and have decorative “returns” at the bottom edge of the gable or dormers, suggesting the pediment of a Greek temple. Victorian houses typically have more steeply sloped roofs. Flat roofs are to be avoided.

FINDING:

2.1.2 Windows

Windows are typically vertical rectangles, often with two or more panes of glass. They may have shutters. If shutters are used, each should be wide enough to actually cover half of the window. Horizontal and vertical “lights”, rows of small panes of New England buildings such as parapets. Where parapets are used to break up a flat roofline, the height of glass, are common over and next to doors. Window frames often have a decorative wood or stone pediment over them.

FINDING:

2.1.3 Detailing

Each historical period also has its characteristic embellishments. Federal buildings may have a decorative fanlight over the entrance door. Greek Revival buildings have corner-boards in the form of pilasters or even rows of actual columns across 100 façade, below a pediment. Victorian buildings use a wealth of turned columns and decorative scroll-work and shingle-work. Too many embellishments can look “busy”, and mixing the details of several periods or styles can also spoil the desired effect. Modern interpretations of older styles often used simplified forms to suggest the details that were more elaborately defined in earlier periods.

FINDING:

2.1.4 Building Materials

Traditional siding materials common to Northern New England are brick, painted clapboard and either painted or unpainted shingles. Contemporary materials that have the same visual characteristics as traditional materials (e.g., cementitious clapboards or vinyl siding) are acceptable if attention is paid to detailing (e.g., corners, trim at openings, changes in material). Metal cladding is not permitted.

Common traditional roofing materials are shingles – cedar originally or asphalt now, as well as standing seam metal. Where visible, the roofing color should be selected to complement the color and texture of the building's façade. Roofing colors are usually darker than the color of the façade.

Colors commonly found in historic New England houses vary by period. In the Federal and Greek Revival periods, white was the most common color, often with green or black shutters. But houses were not infrequently painted "sober" colors such as dull mustard or gray. In the Victorian period much brighter colors were often used, with trim in complementary colors. The characteristic colors for barns are white, barn red, or weathered shingle.

FINDING:

2.2 Large Scale Buildings

Objective: Due to their visibility and mass, the design of new large structures (10,000 square feet or greater) have the ability to greatly enhance or detract from Route 100's visual character. These structures should be designed as attractive pieces of commercial architecture that are responsive to their site and compatible with adjacent development.

FINDING:

2.2.1 Design and Massing

Large structures should be designed so that their large mass is broken up into smaller visual components through the use of clustered volumes, projections, recesses and varied façade treatment. The design should provide variation to add shadow and depth and a feeling of reduced scale.

FINDING:

2.2.2 Site Design

Wherever possible, large buildings should fit into the existing topography and vegetation, and should not require dramatic grade changes around their perimeter. Landscaping, site walls, pedestrian amenities and existing trees can be effective in reducing the apparent scale of large buildings.

FINDING:

2.2.3 Architectural Details

Large structures should have the same degree of detailing found in well-designed smaller and medium sized buildings along the Route 100 corridor. Architectural details can be used to reduce the scale and uniformity of large buildings. Elements such as colonnades, pilasters, gable ends, awnings, display windows and appropriately positioned light fixtures can be effective means of achieving a human scale.

FINDING:

2.2.4 Facades and Exterior Walls

Unbroken facades in excess of 80 feet are overwhelming whether they are visible from Route 100, other roadways or pedestrian areas, or when they abut residential areas. Breaking up the plane of the wall can reduce this sense of overwhelming scale. Where the plane of the wall is broken, the offset should be proportionate to the building's height and length. A general rule of thumb for such projections or recesses is that their depth shall be at least 3% of the façade's length, and they shall extend for at least 20% of the façade's length.

Other devices to add interest to long walls include strong shadow lines, changes in rooflines, pilasters and similar architectural details, as well as patterns in the surface material and wall openings. All façade elements should be coordinated with the landscape plan.

Facades of commercial buildings that face Route 100 or other roadways should have transparent openings (e.g. display windows or entry areas) along 30% or more of the length of the ground floor. Blank or unadorned walls facing public roads, residential neighborhoods, or abutting properties are boring and unattractive.

FINDING:

2.2.5 Building Entrances

Large structures should have clearly defined and highly visible entrances emphasized through such devices as significant variations in rooflines or cornice lines, changes in materials, porticos, landscape treatments, distinctive lighting or other architectural treatments.

FINDING:

2.3 Linear Commercial Buildings

Objective: Linear commercial structures, such as multi-tenant offices or commercial buildings may be appropriate along Route 100 provided that they are designed with façade and roofline elements that reduce their sense of large scale and add visual interest.

2.3.1 Design

Buildings with multiple storefronts should be visually unified through the use of complementary architectural forms, similar materials and colors, consistent details, and a uniform signage size and mounting system.

FINDING:

2.3.2 Façade Design

The use of covered walkways, arcades, or open colonnades is strongly encouraged along long facades to provide shelter, encourage people to walk from store to store, and to visually unite the structure. Pedestrian entrances to each business or tenant should be clearly defined and easily accessible.

FINDING:

2.3.3 Focal Points

Linear commercial buildings can include a focal point – such as a raised entranceway or clock tower, or other architectural element – to add visual interest and help reduce the scale of the building.

FINDING:

2.3.4 Façade Offsets

Variations in the plane of the front façade add visual interest. They also create opportunities for common entries, and social or landscaped spaces.

FINDING:

2.3.5 Rooflines

Variations in rooflines, detailing, cornice lines and building heights should be incorporated into the design to break up the scale of linear commercial buildings.

FINDING:

2.4 Smaller Freestanding Commercial Buildings

Objective: Smaller freestanding commercial buildings can easily make use of traditional New England building forms and should be designed to be attractive pieces of architecture, expressive of their use and compatible with surrounding buildings.

2.4.1 Single Use Buildings

Buildings that are constructed for use by a single business are generally smaller in scale than multi-tenant buildings. Single use buildings should be designed to be attractive and architecturally cohesive. To the greatest extent possible, the same materials, window types and roof types should be used throughout.

FINDING:

2.4.2 Franchise Design

Franchise architecture with highly contrasting color schemes, non-traditional forms, reflective siding and roof materials are not related to any traditional New England style. They are buildings that are stylized to the point where the structure is a form of advertising. However, franchises have been willing to use existing “vernacular” buildings, and sometimes have designs that somewhat reflect local styles.

FINDING:

2.4.3 Mixed Use Buildings

Buildings containing mixed uses (e.g., health club on the first floor with professional offices on the second floor) are encouraged. The architecture of a mixed-use building can reflect the different uses on the upper floors by a difference in façade treatment, as long as the building has a unified design theme.

FINDING:

2.5 Residential Structures

Objective: Cumberland’s future housing stock in the Route 100 corridor should be well designed and constructed, and is encouraged to have some connection to the traditional styles of New England residential architecture. The large mass of multiplex dwellings, can be broken up by façade articulation and architectural detailing in order to reduce their apparent size.

Building form and massing can conform to traditional New England residences by using gable or gambrel roofs with generous overhangs. Traditional vertically hung windows are encouraged. Garages should not constitute a major element of the front of the house that faces the street, but should be located to the side or rear wherever possible.

Dwellings with ells and additions, and ones with multiple roof planes harken back to traditional New England farm and seaside homes. Box-like, ranch or split-level “contractor modern” type dwellings do not particularly reflect Maine styles.

Similarly, traditional New England building materials such as wooden shingles and clapboards are encouraged. Modern low-maintenance materials such as cementitious shingles and clapboards may be substituted.

FINDING:

2.6 Residential Care Facilities

Objective: Ensure that the future needs of Cumberland’s aging population are met in healthy and well-designed facilities, and that the architecture and site design of such facilities fit into the Cumberland context.

The design of Residential Care Facilities can also draw on the local vernacular architecture of gable roofs, multiple building forms and traditional materials. Landscaping, site design and resident amenities will also be of concern to the Planning Board. The site should offer outdoor amenities such as decks, terraces, gardens, gazebos, lawns or similar features. Residential Care Facilities should be buffered from roadways and adjacent uses as much as possible.

FINDING:

2.7 Hotels

Objective: To ensure that any future hotels in the Town of Cumberland are in keeping with the character of the surrounding area, and that the scale and design respects the architectural context of the region.

Using traditional building materials and colors is encouraged, and the use of large blocks of bright, primary colors is discouraged.

The signage and lighting standards contained in this publication will help as well.

FINDING:

2.7.1 All Building Types: Awnings and Canopies

Awnings and canopies can enhance the appearance and function of a building by providing shade, shelter, shadow patterns, and visual interest. Where awnings are used, they should complement the overall design and color of the building.

Whether fixed or retractable, awnings and canopies should be an integral element of the architecture. They should be located directly over windows and doors to provide protection from the elements. Awnings or canopies should not be used as light sources or advertising features. Graphics and wording located on canopies and awnings will be considered part of the total signage area. Any such graphics shall be designed as an integral part of the signage program for the property, and coordinated with other sign elements in terms of typeface, color and spacing.

FINDING:

3 Signage

Signs play a central role in providing much-needed information and setting the tone for the Route 100 corridor. They inform motorists and pedestrians, and have a direct effect on the overall appearance of the roadway. Signage should not create visual clutter along the roadway, yet must provide basic, legible information about commercial goods and services. Signs should be compatible with the architecture and the context of the development.

3.1 Sign Design

Objective: Commercial uses along Route 100 in Cumberland should be identified by attractive, legible signs that serve the need of the individual business, while complementing the site and the architecture. All signage shall comply with the requirements of the Zoning Ordinance of the Town of Cumberland.

3.1.1 Signage Plan

For development proposals requiring one or more signs, the applicant shall provide a detailed signage plan as part of Site Plan or Subdivision review. The signage plan should show the location of all signs on a site plan drawing and on building elevations, as well as sign construction details, dimensions, elevations, etc., and accurate graphic representations of the proposed wording.

FINDING:

3.1.2 Sign Location

Signs should be placed in locations that do not interfere with the safe and logical usage of the site. They should not block motorists' lines of sight or create hazards for pedestrians or bicyclists. Roof mounted signs are not encouraged.

FINDING:

3.1.3 Sign Design

The shape and materials and finish of all proposed signage should complement the architectural features of the associated building. Simple geometric forms are preferable for all signs. All signage shall comply with the requirements of the Zoning Ordinance of the Town of Cumberland.

FINDING:

3.1.4 Sign Colors

Signs should be limited to two or three contrasting colors that are clearly complimentary to the colors of the associated building.

FINDING:

3.1.5 Sign Content

To ensure a clear and easily readable message, a single sign with a minimum of informational content should be used. As a general rule no more than about 30 letters should be used on any sign.

Lettering on any sign intended to be read by passing motorists needs to be legible at the posted speed limit. In general a minimum letter height of 6 inches is appropriate. Smaller letters can require motorists to slow down thereby creating traffic and safety hazards. Upper and lower case lettering is preferred to all upper case, as it is easier to read.

The use of variable message “reader boards”, sponsor logos, slogans or other messages that promote products or services other than the tenants’ are not permitted.

Signage for any proposed development should prominently feature its assigned street address to facilitate general way-finding and e-911 emergency response.

FINDING:

3.2 Sign Type

Objective: To ensure that any sign type complements the architecture of the associated building, and to ensure that they are attractively designed and functional while clearly delivering the intended information.

3.2.1 Building Mounted Signs

Building or façade mounted signs should be designed as an integral element of the architecture, and should not obscure any of the architectural details of the building. Signage should be mounted on vertical surfaces and should not project past or interfere with any fascia trim. Signs should be located a minimum of 18” from the edge of a vertical wall, however the overall proportions of both the wall and sign should be taken into consideration in the placement of the sign.

Flush mounted (flat) signage should be mounted with concealed hardware. Perpendicularly mounted hanging signs should be mounted with hardware designed to complement the building’s architecture. All metal hardware should be corrosion and rust resistant to prevent staining or discoloration of the building.

FINDING;

□

3.2.2 Freestanding Signs

An alternative to a façade-mounted sign is a freestanding “pylon” sign. These signs are typically located between the building and the roadway right-of-way, adjacent to the site’s vehicular entry point.

As with façade-mounted signage, design and content standards shall apply. Because freestanding signs amount to architecture themselves, it is important that they be carefully designed to complement the associated building. This will entail similar forms, materials, colors and finishes. Landscaping surrounding the base of such signs shall be consistent with the landscaping of the entire site.

Where a freestanding sign lists multiple tenants, there should be an apparent hierarchy: i.e., Address, name of the building or development, primary tenant, other tenants.

FINDING:

3.2.3 Wayfinding Signs

To prevent visual clutter and motorist confusion, additional smaller signs indicating site circulation are generally discouraged. However they are sometimes needed to clarify complex circulation patterns. Wayfinding signage is also sometimes required to indicate different areas of site usage, such as secondary building entries, loading, or service areas. The Planning Board shall exercise its discretion in the requirement or prohibition of such signs.

Where required, wayfinding signage should be unobtrusive, no taller than absolutely necessary, and shall complement the overall architecture and signage plan in terms of materials, color, form and finishes.

FINDING:

3.3 Sign Illumination

Only externally lit signs are permitted in the Route 100 corridor because, compared with internally lit signs, the direction and intensity of the light can be more easily controlled. Externally illuminated signs are made of an opaque material and have a dedicated light fixture or fixtures mounted in close proximity, aimed directly at the sign face. The illumination level on the vertical surface of the sign should create a noticeable contrast with the surrounding building or landscape without causing undue reflection or glare.

Lighting fixtures should be located, aimed and shielded such that light is only directed onto the surface of the sign. Wherever possible, fixtures should be mounted above the sign and be aimed downward to prevent illumination of the sky.

FINDING:

4 Lighting

Outdoor lighting is used to identify businesses and illuminate roadways, parking lots, yards, sidewalks and buildings. When well designed and properly installed it can be very useful in providing us with better visibility, safety, and a sense of security, while at the same time minimizing energy use and operating costs. If outdoor lighting is not well designed or is improperly installed it can be a costly and inefficient nuisance. The main issues are glare (hampering the safety of motorists and pedestrians rather than enhancing it), light trespass (shining onto neighboring properties and into residential windows), energy waste (lighting too brightly or lighting areas other than intended or necessary), and sky glow (lighting shining outward and upward washing out views of the nighttime sky).

4.1 Good Lighting

Objective: Good lighting does only the job it is intended to do, and with minimum adverse impact on the environment. Common sense and respect for neighbors goes a long way toward attaining this goal.

The applicant should provide sufficient lighting for the job without over-illuminating.

Fixtures should be fully shielded, giving off no light above the horizontal plane. They should also direct the light onto the intended areas. Fully shielded produce very little glare, which can dazzle the eyes of motorists and pedestrians.

The height and positioning of fixtures is also important, since even well shielded fixtures placed on tall poles can create light trespass. Fixtures should be positioned to uniformly illuminate the subject area. Hot spots created by too-bright or too-low fixtures make the in between areas seem dark, which can create safety problems.

High efficiency lamps are encouraged. Shielded lights can be lower in wattage, and will actually light an area better than unshielded high-output lights because they don't waste light by casting it outward and upward.

FINDING:

4.2 The Lighting Plan

Objective: As part of Site Plan or Subdivision review the Planning Board may, at its discretion, require that a lighting plan be provided. It should be prepared by a professional with expertise in lighting design. The intent of the lighting plan is to show how the least amount of light possible will be provided to achieve the lighting requirements.

4.2.1 Elements of the Lighting Plan

In addition to meeting the requirements of the Zoning Ordinance, the Lighting Plan should contain a narrative that describes the hierarchy of site lighting, describes how lighting will be used to provide safety and security, and describes how it will achieve aesthetic goals. The Lighting Plan should include specifications and illustrations of all proposed fixtures, including mounting heights, photometric data, and other descriptive information. It should also include a maintenance and replacement schedule for the fixtures and bulbs.

The Planning Board may require a photometric diagram that shows illumination levels from all externally and internally visible light sources, including signage.

The location and design of lighting systems should complement adjacent buildings, pedestrian routes, and site plan features. Pole fixtures should be proportionate to the buildings and spaces they are designed to illuminate.

Buffers, screen walls, fencing and other landscape elements should be coordinated with the lighting plan to avoid dark spots and potential hiding places.

Where proposed lighting abuts residential areas, parking lot lighting and other use-related site lighting should be substantially reduced in intensity within one hour of the business closing.

FINDING:

4.3 Types of Lighting

4.3.1 Façade and Landscaping Lighting

Lighting on the front of a building can highlight architectural features or details of a building and add depth and interest to landscaping. This style of lighting should not be used to wash an entire façade in light or light the entire yard. Rather should be used to emphasize particular aspects of the project. All fixtures should be located, aimed and shielded so that they only illuminate the façade or particular plantings and do not illuminate nearby roadways, sidewalks or adjacent properties. For lighting a façade, the fixtures should be designed to illuminate the portion of the face of the building from above, aimed downward, to eliminate skyglow.

4.3.2 Parking Lot and Driveway Lighting

Parking lot and driveway lighting should be designed to provide the minimum lighting necessary for safety and visibility. Poles and fixtures should be in proportion to the roadways and areas they are intended to illuminate.

All fixtures should be fully shielded or “cut-off” style, such that no light is cast above the horizontal plane. Decorative fixtures are strongly encouraged as long as they meet the cut-off criteria, and their design and color complements the architecture and landscaping of the project.

FINDING:

4.3.3 Pedestrian Lighting

Places where people walk, such as sidewalks, stairs, sitting areas, curbs and landscaping should be adequately but not excessively illuminated.

Mounting heights for pedestrian lighting should be appropriate in design and scale for the project and its setting. Bollard fixtures of 3' to 4' in height and ornamental fixtures of up to 12' in height are encouraged. Fixtures should be a maximum of 100 watts and should not create glare or light trespass onto abutting properties.

FINDING:

LIMITATION OF APPROVAL:

Construction of the improvements covered by any site plan approval must be substantially commenced within twelve (12) months of the date upon which the approval was granted. If construction has not been substantially commenced and substantially completed within the specified period, the approval shall be null and void. The applicant may request an extension of the approval deadline prior to expiration of the period. Such request must be in writing and must be made to the Planning Board. The Planning Board may grant up to two (2), six (6) month extensions to the periods if the approved plan conforms to the ordinances in effect at the time the extension is granted and any and all federal and state approvals and permits are current.

STANDARD CONDITION OF APPROVAL:

This approval is dependent upon and limited to the proposals and plans contained in the application and supporting documents submitted by the applicant. Any variation from the plans, proposals and supporting documents, except de minimus changes as so determined by the Town Planner which do not affect approval standards, is subject to review and approval of the Planning Board prior to implementation.

CONDITIONS OF APPROVAL:

SITE PLAN REVIEW APPLICATION

RUSTY LANTERN MARKET

TAX MAP R01, LOT 11-3
181 GRAY ROAD
CUMBERLAND, MAINE 04021



January 29, 2024

Prepared For

CUMBERLAND PROPERTY HOLDINGS, LLC

2 Main Street
Topsham, Maine 04086

Prepared By



2 Main Street, Topsham, Maine 04086
207-837-6198 ■ www.priorityrealestategroup.com



January 26, 2024

22-RLT-004

Carla Nixon, Town Planner
Town of Cumberland
290 Tuttle Road
Cumberland, Maine 04021

Re: Site Plan Review
PROPOSED CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME
Tax Map U19, Lot 12 & 13

Dear Carla:

Cumberland Real Estate Group, LLC, is pleased to submit the enclosed Site Plan Review Application for the development of a convenience store with fuel pumps and a bank with drive through service located on Gray Road at Skillin Road in Cumberland. This letter is intended to summarize the project to facilitate the review process.

PROPERTY

Cumberland Real Estate Group, LLC, has a purchase and sale agreement for a parcel of land located along Route 26 in Cumberland. The project parcel is identified as Tax Map U19, Lot 12 and a portion of Lot 13 on the Town of Cumberland Tax Maps. The parcel will be 1.87 ac (81,259 s.f.)

Lot 12 was developed as a gas station in 1957 and operated under different owners until 1989, at which time the tanks were removed. The building served as an auto maintenance garage for several years. A used car dealership has operated on that lot for several years. Lot 13 has been partially cleared since the mid to late 1980s. Although no permanent structure has been built, the lot has been used for pre-manufactured cabins and sheds at different times. Between 2003 and 2006, the last of the wooded area between the lots was cleared. The existing curb cuts from Gray Road and Skillin Road have been in use since the 1980s.

SITE DESIGN

The proposed site consists of an approximately 5,038 s.f. convenience store building, a 2,935 s.f. bank, associated parking, infrastructure, and landscaping. A total of 37 parking spaces will be provided for the convenience store, two (2) of which will be ADA compliant. The bank site will have 24 parking spaces, with one (1) ADA compliant. The site will be accessed via a new curb cut on Gray Road. Water, electric, and natural gas utilities are available to the parcels and contact has been made with the respective utility providers.

More

Based on the specifics of the project, the applicant requests waivers for the following application items:

- High intensity soils survey
- Market Study

Review Standards

To facilitate your review of our proposal, the following issues are summarized in accordance with *Chapter 229, Section 10 – Approval Standards and Criteria* of the Ordinance:

A. Utilization of the Site

There are no environmentally sensitive areas, such as wetlands, floodplains, significant wildlife habitats, fisheries, scenic areas, habitats for rare or endangered plants and animals, unique nature communities and natural areas, or sand and gravel aquifers present on site. The site has been previously developed and has been paved or packed gravel for several years.

B. Traffic, Circulation, and Parking

The location of the entrance drive provides adequate sight distance in both directions. Parking spaces have been designed to conform with the Town of Cumberland standards. An application for a Traffic Movement Permit from the Maine Department of Transportation has been made for the site. The site has been designed to accommodate fuel tankers and will accommodate emergency vehicles. The entrances to the site have been designed to accommodate the proposed roundabout under consideration and have been reviewed by MaineDOT and Gorrill-Palmer.

During the scoping meeting with MaineDOT, the existing concerns with traffic at the intersection of Skillin and Gray Roads was discussed. It was noted that a plan for new signage was being prepared by Gorrill-Palmer that will increase the awareness of drivers approaching the intersection. The locations of the proposed signs have been added to the Site Plans. In addition, as part of the MaineDOT comments at the meeting, new pedestrian features have been added to the plan. A crosswalk with pedestrian activated flashing signage has been added for people wanting to cross Gray Road. The location of the crosswalk was chosen to separate pedestrians from the proposed entrance while being set as far from the roundabout under consideration as possible. Additionally, a crosswalk across Skillin Road will be added, including a new ADA ramp across from the site. Finally, sidewalks will be constructed along Skillin Road to Kathy Lane and northerly along Gray Road to Faraday Lane.

C. Stormwater Management and Erosion Control

A stormwater management plan and erosion control plan have been included in Attachment I of this application.

D. Water, Sewer, and Fire Protection

Water service will be extended to the lots from the existing utilities located on Skillin and Gray Roads. Sewerage for each building will be managed by private subsurface disposal systems. The systems have been designed by Frick and Associates and the designs are included in the supporting documentation.



E. Water Protection

It is not anticipated that the proposed site development will adversely the quality of quantity of groundwater available to abutting properties or public water supply systems. The project will not extract groundwater for operations or irrigation. The new building will utilize the existing public sewer system. Stormwater runoff from the developed areas will be directed to a new subsurface soil filters which will be lined with an impermeable liner to prevent any groundwater contamination.

All storage for fuel, chemicals, chemical or industrial waters, and biodegradable raw materials will meet the standards of the Maine Department of Environmental Protection and the State Fire Marshal's office.

The site is located within the aquifer protection area as identified on the Official Aquifer Protection Map. A hydrogeologic evaluation was conducted by Sevee & Maher Engineers that included field work to determine soils characteristics and groundwater depth and direction of flow. The report is included under Supporting Documents and concluded that "the Site is suitable for the proposed storage of refined petroleum products."

The refueling system will include double-walled fiberglass tanks that have advanced monitoring methods to detect any leaks before any product escapes the tank. The pipes to the fuel dispensers will also be double-walled. The leak detection system will have visual and audible alerts in the store. The concrete pad around the dispensers will have grooves, referred to as Positive Limiting Barriers, at the perimeter that will contain spills during refueling vehicles. A spill kit will be maintained at the store and all store operators are trained per State and Federal standards.

F. Floodplain Management

The site is in Zone C (areas of minimal flooding risk) as identified by the Federal Emergency Management Agency Flood Insurance Rate Map included in Attachment F of this application.

G. Historic and Archaeological Resources

There are no known historic or archaeological resources located on site. A letter verifying that there are no historic or archaeological resources on site was provided by the Maine Historic Preservation Commission, and is included under Supporting Documents.

H. Exterior Lighting

Exterior lighting has been designed to provide adequate lighting for parking areas. Full cutoff fixtures will be utilized to avoid glare and adverse impact on neighboring properties and rights-of-way, and any unnecessary lighting of the night sky. Details of the lighting fixtures have been included in Attachment H and a photometric plan showing lighting levels throughout the development has been included on Sheet L2.

I. Buffering and Landscaping

Buffers in the form of fences, grade changes, and landscaping, have been designed to screen the businesses and generally soften the appearance of the development. The existing wooded area

between the businesses and the houses on Kathy Lane will be maintained to the extent possible. A detailed landscape plan has been included on sheet L1.

J. Noise

It is not anticipated that the development will create a noise level that will be a nuisance for adjacent properties. Ambient sounds will be comparable to those of Gray and Skillins Roads.

K. Storage of Materials

The dumpsters are screened by either fencing or landscaping. A shed is proposed to be constructed as an accessory building to store dry goods for the convenience store. Other than some seasonal items displayed on the sidewalk at the building, there will be no storage of items or other materials outdoors.

L. Capacity of the Applicant

Evidence of financial capacity has been included in Attachment G of this application. The design team, led by Priority Real Estate Group, LLC, has extensive experience planning, designing, and gaining approvals for commercial development projects throughout the state.

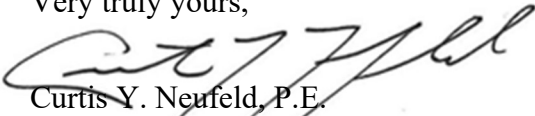
M. Design and Performance Standards

As the site is located along Route 26, the Route 100 Design Guidelines are applicable and have been followed to the greatest extent possible. Renderings of the proposed building and site development are included for reference.

SUMMARY

We look forward to presenting the project to the Planning Board at the meeting on February 20, 2024. Should you have any questions, please call or contact me at cneufeld@priorityrealestategroup.com.

Very truly yours,


Curtis Y. Neufeld, P.E.
Vice-President

Enclosures

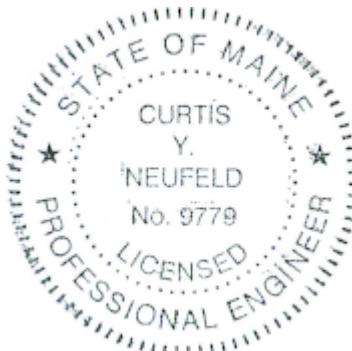


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Attachment A
Application Form & Checklists

A completed copy of the Site Plan Review Application Form and the Checklist are enclosed.

A

Application Form & Checklist

**SITE PLAN REVIEW
Town of Cumberland**

**Appendix C
Planning Board Site Plan Review Application**

Applicant's name _____

Applicant's address _____

Cell phone _____ Home phone _____ Office phone _____

Email Address _____

Project address _____

Project name _____

Describe project _____

Number of employees _____

Days and hours of operation _____

Project review and notice fee _____

Name of representative _____

Contact information: Cell: _____ Office: _____

What is the applicant's interest in the property?

Own _____ Lease _____ Purchase and sale agreement _____ (provide copy of document)

If you are not the owner, list owner's name, address and phone number _____

If you are not the owner, list owner's name, address and phone number _____

Boundary Survey

Submitted? Yes _____ No _____

Are there any deed restrictions or easements? Yes _____ No _____ If yes, provide information and show easement location on site plan.

Building Information

Are there existing buildings on the site? Yes _____ No _____ Number: _____

Will they be removed? Yes _____ No _____ (Note: A demolition permit is required 10 days prior to demolition.)

Will a new structure(s) be built on the site? Yes _____ No _____

Describe: _____

Number of new buildings _____

Square footage _____

Number of floor levels including basement _____

Parking

Number of existing parking spaces _____

Number of new parking spaces _____

Number of handicapped spaces _____

Will parking area be paved? ____ Yes ____ No

Entrance

Location: _____

Width _____ Length _____

Is it paved? ____ Yes ____ No ____ If not, do you plan to pave it?

Where will snow storage for entrance and parking be located? Show on site plan.

Utilities**Water:** Public water ____ Well ____ (Show location on site plan.)**Sewer/septic:** Public sewer ____ Private septic ____ Show location on site plan and submit HHE-200 septic design or location of passing test pit locations if new system is proposed. Also show any wells on abutting properties within 200 feet of the site.**Electric:** On site? Yes ____ No ____

Show location of existing and proposed utilities on the site plan and indicate if they are above or below ground.

Signs

Number: _____

Size: _____

Material: _____

Submit sign design and completed sign application.

Will the sign be lighted? ____ Submit information on type and wattage of lights.

Show location of sign(s) on the site plan.

Natural Features

Show location of any of the following on the site plan:

River ____ Stream ____ Wetland ____ Pond ____ Lake ____ Stone walls ____

Are there any other historic or natural features? _____

Lighting

Will there be any exterior lights? Yes ____ No ____ Show location on site plan (e.g., pole fixtures, wall packs on building) and provide fixture and lumen information.

Trees

Show location of existing trees on the site plan and indicate if any are to be removed.

Landscaping

Is there existing landscaping on the site? Yes ____ No ____ Show type and location on site plan.

Is new landscaping proposed? (Note: if property has frontage on Route 100, a twenty-five-foot landscape easement to the Town is required.)

Buffering

Show any existing or proposed buffering measures for adjacent properties, e.g., plantings, fences.

Erosion Control

Has an erosion and sedimentation control plan been submitted? Yes _____ No _____

Stormwater Management Plan

Provide stormwater information for both pre and post development of the site. Show location of any detention areas and/or culverts on the site plan.

Fire Protection

Location of nearest hydrant _____ Sprinklers? Yes _____ No _____

Do you plan to have an alarm system? Yes _____ No _____ Please contact the Fire/EMS Department at 829-4573 to discuss any Town or state requirements.

Trash

Will trash be stored inside _____ outside _____. If outside, will a dumpster be used?

Yes _____ No _____. Show location on site plan and show type of screening proposed (e.g., fencing, plantings).

Technical Capacity

List and provide contact information for all consultants who worked on the project, for example: licensed land surveyor, licensed soils evaluator, professional engineer, attorney, etc.

Financial Capacity

Please indicate how project will be financed. If obtaining a bank loan, provide a letter from the bank _____

-
- Zoning district: _____
 - Minimum lot size: _____
 - Classification of proposed use: _____
 - Parcel size: _____
 - Frontage: _____
 - Setbacks: Front _____ Side _____ Rear _____
 - Board of Appeals Required? _____
 - Tax Map _____ Lot _____ Deed book _____ Deed page _____
 - Floodplain map number _____ Designation _____
 - Vernal pool identified? _____
 - Is parcel in a subdivision? _____
 - Outside agency permits required:
 - MDEP Tier 1 _____ MDEP Tier 2 _____ Army Corps of Engineers _____
 - MDEP general construction (stormwater) permit (for disturbance of 1 acre or more)
 - MDOT entrance permit _____
 - MDOT traffic movement permit _____
 - Traffic study required _____
 - Hydrogeologic evaluation _____
 - Market study _____
 - Route 1 Design Guidelines? _____
 - Route 100, VMU or TCD Design Standards? _____

Applicant's signature _____

Submission date: _____

PLANNING BOARD SITE PLAN REVIEW SUBMISSION CHECKLIST

FOR ALL PROJECTS:

Submission Requirement	Provide Location in Application Packet (e.g., plan sheet number, binder section, narrative	If requesting a waiver, indicate below:
<i>Example: Erosion Control</i>	<i>Plan Sheet E-1</i>	
General Information:		
Completed Site Plan Application Form		
Names and addresses of all consultants		
Narrative describing existing conditions and the proposed project		
Evidence of right, title or interest (deed, option, etc.)		
Names and Addresses of all property owners within 200 feet		
Boundaries of all contiguous property under control of owner		
Tax map and lot numbers		
Area of the parcel		
FEMA Floodplain designation & map #		
Zoning classification		
Evidence of technical and financial capability to carry out the project		
Boundary survey		
List of waiver requests on separate sheet with reason for request.		
Proposed solid waste disposal plan		
Existing Conditions Plan showing:		
Name, registration number and seal of person who prepared plan		
North arrow, date, scale, legend		
Area of the parcel		
Setbacks and building envelope		
Utilities, including sewer & water, culverts & drains, on-site sewage		
Location of any septic systems		
Location, names, widths of existing public or private streets ROW's		

Location, dimension of ground floor elevation of all existing buildings		
Location, dimension of existing driveways, parking, loading, walkways		
Location of intersecting roads & driveways within 200 feet of the site		
Wetland areas		
Natural and historic features such as water bodies, stands of trees, streams, graveyards, stonewalls, floodplains		
Direction of existing surface water drainage across the site & off site		
Location, front view, dimensions and lighting of existing signs		
Location and dimensions of existing easements & copies of documents		
Location of nearest fire hydrant or water supply for fire protection		
Proposed Development Site Plan showing:		
Name of development		
Date		
North arrow		
Scale		
Legend		
Landscape plan		
Stormwater management		
Wetland delineation		
Current & proposed stands of trees		
Erosion control plan		
Landscape plan		
Lighting/photometric plan		
Location and dimensions of all proposed buildings		
Location and size of utilities, including sewer, water, culverts and drains		
Location and dimension of proposed on-site septic system; test pit locations and nitrate plumes		
Location of wells on subject property and within 200' of the site		
Location, names and widths of existing and proposed streets and ROW's		

Location and dimensions of all accessways and loading and unloading facilities		
Location and dimension of all existing and proposed pedestrian ways		
Location, dimension and # of spaces of proposed parking areas, including handicapped spaces		
Total floor area and ground coverage of each proposed building and structure		
Proposed sign location and sign lighting		
Proposed lighting location and details		
Covenants and deed restrictions proposed		
Snow storage location		
Solid waste storage location and fencing/buffering		
Location of all fire protection		
Location of all temporary & permanent monuments		
Street plans and profiles		

ADDITIONAL REQUIREMENTS FOR MAJOR SITE PLAN PROJECTS:

Submission Requirement	Provide Location in Application Packet (e.g., plan sheet number, binder section, narrative)	If requesting a waiver, indicate below:
High intensity soils survey		
Hydro geologic evaluation		
Traffic Study		
Market Study		
Location of proposed recreation areas (parks, playgrounds, other public areas)		
Location and type of outdoor furniture and features such as benches, fountains.		

Attachment B
Right, Title, & Interest

Copies of the current deed are included with this attachment.

B

Right, Title, & Interest

DEED OF SALE BY PERSONAL REPRESENTATIVE (TESTATE)
Maine Statutory Short Form

WILLIAM B. GERRY, of Pea Ridge, County of Benton, and State of Arkansas, duly appointed and acting personal representative of the **ESTATE OF EILEEN G. RACKLEY, DECEASED** (testate), as shown by the probate records of Cumberland County, Maine, (Docket no. 2003-217), the said **EILEEN G. RACKLEY** being formerly known as **EILEEN M. GERRY**, and having given notice to each person succeeding to an interest in the real property described below at least ten (10) days prior to the sale, by the power conferred by the Probate Code, and every other power, for consideration paid, grants to **RONALD W. COPP, SR.** and **RONALD W. COPP, JR.**, of Cumberland, in the County of Cumberland, and State of Maine, whose mailing address is 187 Gray Road, Cumberland, Maine 04021, the real property in the Town of Cumberland, County of Cumberland, and State of Maine described as follows:

A certain lot or parcel of land, with the buildings and improvements thereon, situated in Cumberland, in the County of Cumberland, and State of Maine, bounded and described as follows:

Beginning at a point on the easterly boundary of the new Gray Road, so called, at the northwesterly corner of the second parcel conveyed by Eva A. Burgess to Jeanette D. Goodoff by deed dated April 7, 1941 and recorded in Cumberland County Registry of Deeds, Book 1631, Page 468; thence northerly two hundred seven (207) feet more or less by said easterly boundary of said Gray Road to the intersection thereof with the southerly boundary of the Skillin Road, so called; thence easterly along said southerly boundary of said Skillin Road two hundred (200) feet to a point; thence southerly to a point on the northerly boundary of said land now or formerly of Goodoff which point is two hundred (200) feet easterly from the point of beginning; thence westerly along said northerly boundary of said land now or formerly of Goodoff two hundred (200) feet to the point of beginning.

Being the same premises described in the deed of Eva A. Burgess to Eileen M. Gerry dated August 30, 1956 and recorded in the Cumberland County Registry of Deeds in Book 2313, Page 493, and all rights in a lease, an assignment of which is attached hereto.

WITNESS my hand and seal this 25th day of September, 2003.

Witness

William B. Gerry P.R.
William B. Gerry, Personal Representative
Estate of Eileen G. Rackley, Deceased

State of Maine
Cumberland, ss

September 25, 2003

Personally appeared before me the above-named **William B. Gerry** in his said capacity and acknowledged the foregoing instrument to be his free act and deed.

Kenneth E. Snitger
Notary Public/Attorney at Law
KENNETH E. SNITGER
MAINE ATTORNEY AT LAW

Printed Name

MAINE REAL ESTATE TAX PAID

ASSIGNMENT

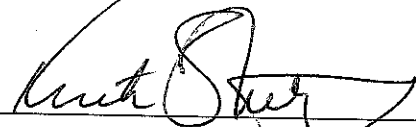
KNOW ALL PERSONS BY THESE PRESENTS that William B. Gerry, of 14996 It'll Do Road, Pea Ridge, Arkansas 72751, duly appointed and acting personal representative of the Estate of Eileen G. Rackley, deceased (testate), as shown by the probate records of the County of Cumberland, Maine, Docket No. 2003-217 (hereinafter referred to as "Assignor"), for consideration paid by Ronald W. Copp, Sr. and Ronald W. Copp, Jr., both of 187 Gray Road, Cumberland, Maine 04021 ("Assignee"), hereby assigns all of Assignor's right, title and interest in and to:

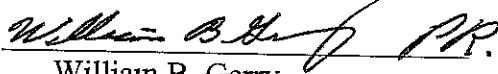
A certain Lease on the premises situated at 181 Gray Road, Cumberland, Maine, being known as the property for "Mr. Bill's Auto Sales", which lease was executed between William Richards dba Mr. Bill's Auto Sales, Inc. and Eileen Rackley.

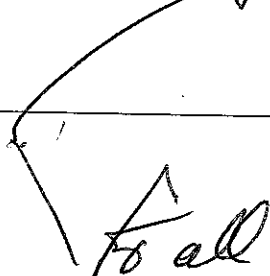
TO HAVE AND TO HOLD the same unto the Assignee and their heirs, successors, personal representatives and assigns, of the Assignee forever.

Witness my hand this 25th day of September, 2003.

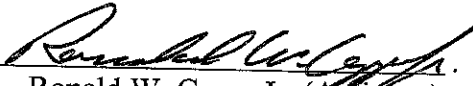
Estate of Eileen G. Rackley (Assignor)


Attny: at law

By:  P.R.
William B. Gerry,
Personal Representative


To all

By: 
Ronald W. Copp, Sr. (Assignee)

By: 
Ronald W. Copp, Jr. (Assignee)

Received
Recorded Register of Deeds
Sep 25, 2003 03:11:10P
Cumberland County
John B. O'Brien

QUIT CLAIM DEED WITH COVENANT

Instr 53407 bk 9758 p 327

I, JERALD E. COPP of West Cumberland, in the County of Cumberland and State of Maine

for consideration paid, hereby grant to

ELEANOR M. COPP, of West Cumberland, in the County of Cumberland and State of Maine, with QUIT CLAIM COVENANTS, the following described real estate:

A certain lot or parcel of land with any buildings or improvements thereon and easements appurtenant thereto as described in Appendix A attached hereto and made a part hereof.

Meaning and intending to convey and hereby conveying my one-third (1/3) undivided interest in that certain parcel of land conveyed to grantor herein et al by deed of Michael M. Wilson et al dated May 4, 1976, recorded in the Cumberland County Registry of Deeds in Book 3841, Page 153.

WITNESS my hand this 2nd day of Aug., 1982.

Jerald E. Copp
Jerald E. Copp

THE STATE OF MAINE

Cumberland ss.

August 2, 1982

Then personally appeared the above-named JERALD E. COPP and acknowledged the foregoing instrument to be his free act and deed.

Before me,

Naomi H. Meadows
Attorney-at-law / Notary Public

SEAL

NAOMI H. MEADOWS
NOTARY PUBLIC, MAINE
MY COMMISSION EXPIRES JUNE 12, 1984

a certain lot or parcel of land situated in the Town of Cumberland, County of Cumberland and State of Maine, being a part of the parcel as described on the Cumberland Town Tax Map U-19, Lot #8, more particularly bounded and described as follows:

Beginning at a point on the Westerly sideline of the New Gray Road (Routes 26 and 100) at the Northeasterly corner of land now or formerly of Elizabeth I. Pendexter (Lot #7 on said Tax Map) and running in a general Westerly direction on a line parallel to the Northerly boundary of said Pendexter land in a straight line to a point on the boundary line of land of Mabel I. Wilson; thence in a general Northwesterly direction along the line of land of said Mabel I. Wilson to a point marking the boundary of land owned by the Town of Cumberland; thence in a general Northeasterly direction SIX HUNDRED SIXTY-SEVEN (667) FEET, more or less, along the line of land of said Town of Cumberland to a point marking the Southeasterly corner of land of Grantees herein; thence in a general Easterly direction a distance of ONE HUNDRED SIXTY-FIVE (165) FEET, more or less, to the Westerly sideline of said New Gray Road; thence Southerly along the Westerly sideline of said New Gray Road a distance of SIX HUNDRED FORTY (640) FEET, more or less, to the point of beginning.

Recorded
Cumberland County
Registry of Deeds
10/22/91 12:55:28PM
Robert P. Titcomb
Register

MAINE SHORT FORM QUITCLAIM DEED WITH COVENANT

ELEANOR M. COPP, of Cumberland, Cumberland County, Maine, and **RONALD W. COPP** of Cumberland, Cumberland County, Maine, for consideration paid, hereby grant to **COPP BROTHERS REAL ESTATE**, a Maine corporation with a mailing address of 187 Gray Road, Cumberland, Maine 04021, with **QUITCLAIM COVENANT**, certain lots or parcels of land situated in Cumberland, Cumberland County, Maine, being more particularly described in the deed of Jerald E. Copp to Eleanor M. Copp, dated August 2, 1988, and recorded in the Cumberland County Registry of Deeds in Book 9758, Page 327, and in the deed of Michael M. Wilson dated May 4, 1976, and recorded in Book 3841, Page 153.

WITNESS my hand and seal this 31st day of December, 2004.

Linda O'Connor
Witness

Robert Curtis
Witness

Eleanor M. Copp
Eleanor M. Copp

Ronald W. Copp
Ronald W. Copp

STATE OF MAINE
COUNTY OF Cumberland, SS.

Personally appeared before me this 4 day of January, 2005 ~~November, 2004~~, the above-named Eleanor Copp, Ronald Copp acknowledged the foregoing instrument to be his/her/their free act and deed.

Amy Maheux
Notary Public/Attorney-at-Law

AMY D. MAHEUX
NOTARY PUBLIC, STATE OF MAINE
Type or Print Name MY COMMISSION EXPIRES OCT. 26, 2007

My commission expires: _____

TITLE NOT SEARCHED.
DESCRIPTION NOT VERIFIED.

H:\DOCS\RATTEY\Copp Brothers 33404\quitclaim deed - Wilson Lot.wpd
"Wilson Lot"

SEAL

Received
Recorded Register of Deeds
Jan 27, 2005 03:21:10P
Cumberland County
John B O'Brien

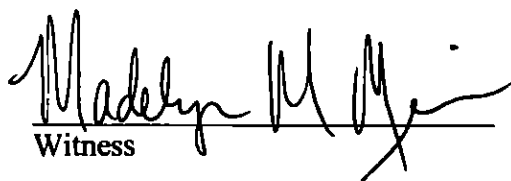
MAINE SHORT FORM QUITCLAIM DEED WITH COVENANT

KNOW ALL MEN BY THESE PRESENTS that **COPP BROTHERS REAL ESTATE**, a Maine corporation with a principal place of business in Cumberland, Cumberland County, Maine for consideration paid, hereby grants to **RONALD COPP, SR., HOWELL COPP**, and **JERALD COPP, JR.**, individuals with a mailing address of 187 Gray Road, Cumberland, Maine 04021, as tenants in common, with QUITCLAIM COVENANT, those certain lots or parcel of land situated in **Cumberland**, Cumberland County, Maine, being more particularly described ion the following deeds:

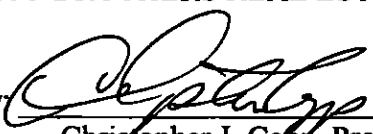
1. Deed from Eleanor M. Copp and Ronald W. Copp to Copp Brothers Real Estate recorded in the Cumberland County Registry of Deeds on January 27, 2005, in Book 22269, Page 349 (Wilson Lot)
2. Deed from Eleanor M. Copp and Ronald W. Copp to Copp Brothers Real Estate recorded in the Cumberland County Registry of Deeds on January 25, 2005, in Book 22270, Page 4 (Log Cabin).

The premises are conveyed subject to any easements and restrictions of record and include all rights, easements, and privileges pertaining thereto.

IN WITNESS whereof, Copp Brothers Real Estate has caused this instrument to be signed and sealed by Christopher J. Copp, its President, there unto duly authorized this 21st day of ~~December, 2017.~~
January 2018


Witness

COPP BROTHERS REAL ESTATE

By 
Christopher J. Copp, President

SEAL

STATE OF MAINE
COUNTY OF CUMBERLAND, SS.

Personally appeared before me this ____ day of December, 2017, the above-named Christopher J. Copp, President of Copp Brothers Real Estate and acknowledged the foregoing instrument to be his free act and deed in said capacity and the free act and deed of Copp Brothers Real Estate.

Notary Public/Maine Attorney-at-Law

Type or Print Name

My commission expires: _____

TITLE NOT SEARCHED.

H:\DOCS\RATTEY\Copp Brothers 33404\MSFQCCDEED-R-H-J.docx

STATE OF MAINE - COUNTY OF Cumberland
Subscribed and sworn (or affirmed) before me this
this 23rd day of January, 20 18
by Christopher Copp
Personally Known _____ OR Produced Identification ☒
Type of Identification Driver's License
Nolan J. Lovell
NOLAN J. LOVELL, Notary Public
My Commission Expires May 8, 2024

Received
Recorded Register of Deeds
Feb 06, 2018 01:37:23P
Cumberland County
Nancy A. Lane

Attachment C
Abutting Property Owners

A copy of the abutters map and a list of abutting property owners are included in this attachment for reference.

TOWN OF CUMBERLAND 290
TUTTLE RD.
CUMBERLAND CTR, ME 04021-9321

WSAH PROPERTY LLC
C/O CHARLES PERKINS, VMD
GRAY, ME 04039

COPP CHRISTOPHER J
17 BROWNING WAY
CUMBERLAND CTR, ME 04021

COPP RONALD W SR
187 GRAY ROAD
CUMBERLAND, ME 04021

COPP, RONALD SR; COPP, HOWELL
187 GRAY RD
CUMBERLAND CTR, ME 04021

COPP HOWELL
PO BOX 501
GRAY, ME 04039

WEED CLAYTON E
PO BOX 324
CUMBERLAND, ME 04021

TAYLOR, JENNIFER B
10 KATHY LN
CUMBERLAND, ME 04021

BUDD IRREVOCABLE TRUST
157 GRAY RD
CUMBERLAND, ME 04021

MARSH TIMOTHY J & AMY E
15 KATHY LANE
CUMBERLAND, ME 04021

GIBBS RICHARD S
7 KATHY LANE
CUMBERLAND, ME 04021

GRANT, KRISTINA L
10 SKILLIN RD
CUMBERLAND, ME 04021

RICHARDSON JAMES M
15 MILL RIDGE ROAD
CUMBERLAND, ME 04021

RICHARDSON JAMES M
15 MILL RIDGE ROAD
CUMBERLAND, ME 04021

GREEN SIP CONSTRUCTION, INC
110 MARGINAL WAY
PORTLAND, ME 04101

COPP RONALD W SR
187 GRAY ROAD
CUMBERLAND, ME 04021

CASCO HOLDINGS, LLC
1 FARADAY DRIVE, SUITE 1
CUMBERLAND, ME 04021

BOCCELLI, ADAM
8 WISTERIA LN
INLET BEACH, FL 32461

WETZEL CURTIN J*
6 SKILLIN ROAD
CUMBERLAND, ME 04021

Attachment D **Photographs**

D

Photographs of the project area are included for reference.

Abutting Property Owners

Photographs of Existing Site



Aerial View of Existing Site

Photographs of Existing Site



Photograph 1: Auto Sales & Service Building



Photograph 2: Looking North from Proposed Entrance on Gray Road

Photographs of Existing Site



Photograph 3: Looking South from Proposed Entrance on Gray Road



Photograph 4: Looking East from Proposed Entrance on Skillin Road

Photographs of Existing Site



Photograph 5: Looking South from Intersection



Photograph 6: View of Site from South End

Attachment E
Supporting Documents

Supporting Documents

Copies of relevant correspondence and documents pertaining to the project are enclosed.

**CONVENIENCE STORE WITH GASOLINE FUELING
and
BRANCH BANK DEVELOPMENT
CUMBERLAND, MAINE**

**SECTIONS 1 – 7
TRAFFIC MOVEMENT PERMIT APPLICATION**

**Submitted to:
MAINE DEPARTMENT OF TRANSPORTATION
REGION 1, SCARBOROUGH, MAINE**

November 22, 2023

**Applicant:
Cumberland Real Estate Group, LLC
2 Main Street
Topsham, ME 04086**



A handwritten signature in black ink that reads "Diane W. Morabito" with a stylized flourish at the end.



INTRODUCTION

The purpose of this application is to summarize the information required by the Maine Department of Transportation (MaineDOT) in a Traffic Movement Permit application for a proposed development to be located on Route 26/100 in Cumberland, Maine. Trip generation, performed using the Institute of Transportation Engineers (ITE) report, indicates that the development will generate more than 100 new peak hour trips. As a result, the project requires a Traffic Movement Permit (TMP). The Scoping Meeting was held on Monday, October 30th at 11:00 AM via Zoom.

SITE DESCRIPTION - SECTION 1A

The site is located in the southeast quadrant of the intersection of Route 26, Skillin Road and Blackstrap Road in Cumberland, as shown on the map in Figure 1.

EXISTING AND PROPOSED USES - SECTION 1B

The proposed convenience store building will be 4,890 square feet (S.F.) in size, and it will provide eight (8) gasoline fueling positions. Additionally, a proposed branch bank will be located on site, 2,820 S.F. in size, which will provide two drive-through lanes. The site was recently occupied by a used car dealership, which was operating in 2022. The existing car dealership building is 1,120 S.F.

There are no sidewalks extending much beyond the intersection along Skillin Road, Blackstrap Road or Gray Road given the rural nature. However, there are some on-site sidewalks extending along the Route 26 and the Blackstrap Road property frontage at the development on the opposite side of Route 26. Similarly, the site plan for the proposed convenience store and bank shows sidewalks along the site frontage on Route 26 and down along Skillin Road to the proposed entrance. There is no public scheduled bus serving this portion of Cumberland.

SITE VICINITY - SECTION 1C

The site location is shown on the map in Figure 1.

OTHER DEVELOPMENT - SECTION 1D

The Town of Cumberland Planner was contacted to determine if there are any other approved (but unbuilt) developments, expected to significantly impact future volumes in the vicinity of the site, which should be considered in the traffic analysis. One other pending development project was identified, a 72-unit condominium complex at 77 Blackstrap Road. It is understood that the condominiums will be single-family detached homes. No traffic study has yet been performed for this proposed development but based upon ITE data these 72 condominiums would be expected to generate:

- 50 AM Peak Hour Trips, 13 entering and 37 exiting
- 68 PM peak Hour Trips, 43 entering and 25 exiting

TRIP GENERATION - SECTION 1E

The number of trips to be generated by the proposed convenience store and bank were estimated utilizing the latest Institute of Transportation Engineers (ITE) "Trip Generation, 11th edition". Land use code (LUC) 945 – Convenience Store/Gas station was utilized on the bases of both square footage and fueling positions. The bank was estimated utilizing LUC 912 – Drive-Bank on the bases of both 2,820 S.F. and 2 drive-in lanes. The results were averaged for both uses, as is customary. The results are summarized in the following table:

<u>Time Period</u>	PROPOSED TRIP GENERATION (One-Way Trip-Ends)						Total <u>Trips</u>
	<u>F.P.</u>	<u>S.F.</u>	<u>Avg.</u>	<u>S.F.</u>	<u>Lanes</u>	<u>Avg.</u>	
Weekday	2058	3052	2556	284	250	268	2824
AM Peak Hour – Adjacent Street	216	198	207	28	17	23	230
Entering	108	99	104	16	10	13	117
Exiting	108	99	103	12	7	10	113
PM Peak Hour – Adjacent Street	182	237	210	59	54	57	267
Entering	91	119	105	30	27	29	134
Exiting	91	118	105	29	27	28	133
AM Peak Hour – Generator	216	203	210	42	34	38	248
Entering	108	101	105	22	19	21	126
Exiting	108	102	105	20	15	17	122

<u>Time Period</u>	C-Store			Bank			Total Trips
	<u>F.P.</u>	<u>S.F.</u>	<u>Avg.</u>	<u>S.F.</u>	<u>Lanes</u>	<u>Avg.</u>	
PM Peak Hour – Generator	191	245	218	59	45	52	270
Entering	96	123	109	29	22	26	135
Exiting	95	122	109	30	23	26	135
Saturday Peak Hour - Generator	164	--	164	74	55	65	229
Entering	83	--	83	38	27	33	116
Exiting	81	--	81	36	28	32	113

As seen above, total one-way trips to the site are estimated to range from 229 to 270 in peak hours. There is credit for grandfathered trips for recent uses. The trips for the former used car dealership were similarly estimated using ITE. Land use code 841 – Automobile Sales (Used) was used based on the 1,120 S.F. The results are summarized below:

FORMER TRIP GENERATION (One-Way Trip-Ends)	
<u>Time Period</u>	<u>Trips</u>
Weekday	30
AM Peak Hour – Adjacent Street	2
Entering	2
Exiting	0
PM Peak Hour – Adjacent Street	4
Entering	2
Exiting	2
AM Peak Hour – Generator	5
Entering	3
Exiting	2
PM Peak Hour – Generator	6
Entering	3
Exiting	3
Saturday Peak Hour - Generator	--
Entering	--
Exiting	--

As seen above, the former used cars sales facility generated few trips, from 2 to 6 one-way trips, in peak hours. This does not alter the TMP level, nor would the credit have any significant impact on any traffic analysis. Hence, to simplify the analysis, since those trips would not be reflected in the current traffic counts, no credit was taken for these grandfathered trips in the trip assignments or forthcoming analysis.

Not all the trips generated by the convenience store or bank will be new trips to the adjacent street system. Many of the trips will be pass-by trips, trips that are already on Route 26 or Skillin Road. ITE data, from the 11th edition, indicates the following pass-by rates for the AM and PM peak hours:

<u>Land Use</u>	<u>AM Pass-by Rate</u>	<u>PM Pass-by Rate</u>
Convenience Store w/ Gasoline Pumps	60 %	56 %
Drive-In bank	29 %	35 %

The above percentages result in the following trip summary for the peak hours of the adjacent street, the expected analysis periods:

<u>Peak Hour</u>	C-Store		Bank		Total Trips	
	<u>Pass-By</u>	<u>Primary</u>	<u>Pass-By</u>	<u>Primary</u>	<u>Pass-By</u>	<u>Primary</u>
AM Peak Hour – Adjacent Street	124	83	7	16	131	99
Entering	62	42	4	9	66	51
Exiting	62	41	3	7	65	48
PM Peak Hour – Adjacent Street	118	92	20	37	138	129
Entering	59	46	10	19	69	65
Exiting	59	46	10	18	69	64

As seen above, the proposed development is expected to generate 99 primary trips in the AM peak hour and 129 in the PM peak hour. The remaining trips are expected to be pass-by trips, trips that are already on Route 26 or Skillin Road that simply divert into the site. The trip generation analysis and pass-by rates were reviewed and approved at the Scoping Meeting.

TRIP DISTRIBUTION AND ASSIGNMENTS - SECTION 1F & G

Turning movement/classification counts were conducted by Sewall during the weekday AM and PM peak hour periods as outlined below:

<u>Intersection</u>	<u>Count Date</u>	<u>Count Period</u>	<u>Peak Hour</u>
Route 26, Skillin & Blackstrap Roads	8/9/2023	7:00 – 9:00 AM	7:45 – 8:45
Route 26, Skillin & Blackstrap Roads	8/9/2023	3:00 – 6:00 PM	4:15 – 5:15

Additionally, a PM peak hour count was conducted at the intersection of Gray Road, Falmouth Road & Mountain Road on August 22, 2023. The peak hour occurred from 4:30 – 5:30.

The count records were included in the Section 1 – 6 submittal. Given that the counts were conducted under peak summer conditions no seasonal adjustments were necessary to obtain 30th highest hour volumes for analysis purposes. The count results are summarized in Figure 2.

The trip assignments were based upon the travel patterns recorded during the counts. The pass-by trips were assigned based upon the volumes passing the site during the peak hours. The resulting trip assignments are shown in Figures 3 & 4 for the AM and PM peak hours. These trip assignments were reviewed and approved at the Scoping Meeting. Based upon the trip assignments the study area for capacity analysis purposes was defined as the intersection of Route 26/100, Skillin Road and Blackstrap Road, as well as the site drive intersections.

ACCIDENT REVIEW - SECTION 2

The Maine Department of Transportation uses two criteria to determine high crash locations (HCLs). The first is the critical rate factor (CRF), which is a measure of the accident rate. A CRF greater than one indicates a location which has a higher than expected crash rate. The expected rate is calculated as a statewide average of similar facilities. The second criterion, which must also be met, is based upon the number of accidents that occur at a particular location. Eight or more accidents must occur over the three-year study period for the location to be considered a high crash location.

Accident data was obtained from MaineDOT for the vicinity of the site for the most recent 3-year period (2020 – 2022) for an extended study area, from Falmouth Road in Falmouth, to Yarmouth Road in Gray, as well as Skillin Road. The number of crashes and CRF are summarized by location in the following tables:

<u>Route 26 Location Description</u>	<u># of Crashes</u>	<u>CRF</u>
Intersection of Falmouth and Mountain Roads in Falmouth	6	0.38
Between Eastern Avenue and 0.95 mile north	9	0.42
Between 0.95 mile north Eastern Avenue and Hadlock Road	2	0.29
Intersection of Hadlock Road in Falmouth	1	0.33
Between Hadlock and Hurricane Roads	7	0.53
Intersection of Hurricane Road in Falmouth	1	0.39
Between Hurricane and Schuster Roads	6	0.56
<i>Between Schuster Road and Falmouth-Cumberland line</i>	7	1.24
Between Falmouth-Cumberland line and Range Road	8	0.88
Intersection of Range Road in Cumberland	5	1.69
Between Range and Lower Methodist Roads	4	0.61
Between Lower Methodist and Castlerock Drive	3	0.44
Between Castlerock and Rooster Ridge	3	1.08
Between Rooster Ridge and Mill Road	1	0.28
Intersection of Mill Road in Cumberland	1	0.43
Between Mill and Skillin/Blackstrap Roads	2	0.24
Intersection of Skillin & Blackstrap Roads	5	1.34
Between Skillin/Blackstrap Roads and Highland Avenue	1	0.23
Intersection of Highland Avenue in Cumberland	1	0.43
<i>Between Forest Ave and Old Gray Road</i>	7	1.00
Intersection of Old Gray Road in Cumberland	2	0.89
Between Old Gray Road and Cumberland-Gray line	2	0.40
Between I-95 Parking and Verrill Road	1	0.11
Between Two Lights and Dutton HL	3	0.56
Intersection of Dutton HL	1	0.41

<u>Route 26 Location Description</u>	<u># of Crashes</u>	<u>CRF</u>
Between Dutton HL and 0.63 Mile North	8	0.75
Between 0.63 mile north Dutton HL and Upper Marginal Way	1	0.21
Between Whitney Road and 0.36 mile north	5	0.66
Between 0.36 mile north Whitney Road and Old Hunts Hill Road	2	0.46
Between Old Hunts Hill and Long Hill Roads	1	0.51
Between Hunts Hill Road and 1.26 mile north	13	0.46
Between 1.26 mile north Hunts Hill and Yarmouth Road	5	0.34
Intersection of Yarmouth Road and Portland Road in Gray	11	0.43

<u>Skillin Road Location Description</u>	<u># of Crashes</u>	<u>CRF</u>
Between Kathy Lane and Pond Shore Drive	1	0.17
Intersection of Blanchard Road	1	0.60

As seen above, there are no high crash locations within the extended study area. Two Route 26 segments are approaching the criteria with a CRF of 1.00 or more and 7 crashes. As a result, collision diagrams were requested from MaineDOT to determine if there are any accident patterns or trends are evident that may indicate a correctable safety deficiency. The diagrams are evaluated as follows:

<u>Between Schuster Road and Falmouth-Cumberland line</u>	7	1.24
---	---	------

There were two crashes in 2020, three in 2021 and two in 2022. Five of the seven crashes were single vehicle deer hits. One single vehicle off the road crash occurred when a driver fell asleep. Lastly, there was a head on type crash that occurred when a driver fell asleep. There is no pattern of correctable type crashes, but “deer” warning signs could be considered. A Google Earth review of the segment did not reveal any deer warning signs but the images are not up to date.

<u>Between Forest Ave and Old Gray Road</u>	7	1.00
---	---	------

There were two crashes in 2020, one in 2021 and four in 2022. Five of the seven crashes were single vehicle deer hits, all in the northbound direction. There was a single head on type crash attributed to a driver going the wrong way. There was a single vehicle fire. There is no pattern of correctable type crashes but “deer” warning signs, again, could be considered.

At the Scoping Meeting the Town Manager expressed concern with the accident data for the intersection of Skillin Road and Blackstrap Road. While the 2020 – 2022 crash data, the most recent full 3-year study period, did not identify the intersection as a high crash location it is understood that there have been several crashes in 2023. As a result, an updated collision diagram was obtained from MaineDOT for the 2021 to 2023 period. This diagram is included in the appendix and is evaluated as follows:

Intersection of Route 100, Skillin Road and Blackstrap Road

There were nine crashes at the intersection over the 3-year period 10/1/20 to 9/30/23. The CRF factor for this period is 2.29 making the intersection a HCL. The diagram shows that there were two rear-end collisions, one on the Blackstrap Road approach attributed to following too close and one on Skillin Road attributed to excessive speed. There was a single vehicle car fire. The remaining six crashes were angle collisions between Route 100 vehicles and side street movements, three involving vehicles exiting Skillin Road and three involving vehicles exiting Blackstrap Road.

The Town has planned a signage improvement project to reduce the angle collisions. Sewall has reviewed the plan prepared by Gorrill Palmer and concurs with the recommended actions. It is important to note that the Town has been opposed to other corrective measures, such as all-way stop control. The Town is seeking MaineDOT funding to have a roundabout constructed to address the crash issues long-term.

ENTRANCES AND EXITS - SECTION 3

The site plan provides for two curb cuts, as is typical for on-site flow for a convenience store with gasoline fueling facilities. A single curb cut is proposed to Gray Road, aligning with the opposite drive and providing 300' of corner clearance. The single curb cut to Skillin Road is as far as possible from Gray Road, providing over 150' of corner clearance. The speed limits and sight distances are shown on the site plan prepared by Priority Real Estate Group, which is included in this application. Given that large delivery vehicles will cross the centerline of the drives, these deliveries are expected to be restricted to off-peak hours in the TMP.

TITLE, RIGHT OR INTEREST - SECTION 4

The deeds and sales agreements for the two parcels were included in Section 1 – 6 application package.

PUBLIC OR PRIVATE RIGHTS-OF-WAY - SECTION 5

No new public rights-of-way are proposed.

SCHEDULE - SECTION 6

Construction is expected to begin in spring of 2024 after permits are issued with completion in fall of 2024. Hence, 2024 was selected as the study year for traffic analysis purposes.

TRAFFIC IMPACT STUDY - SECTION 7

INTRODUCTION

The purpose of Section 7 of this report is to summarize the traffic study components requested by the Maine Department of Transportation (MaineDOT) during the Scoping Meeting for a Traffic Movement Permit for the proposed convenience store and bank development. The Scoping Meeting was held at 11:00 AM on Monday, October 30th, 2023 via Zoom.

A. STUDY PREPARATION

This study was prepared by Diane W. Morabito, Maine P.E. 5077 and PTOE 571.

B. STUDY HORIZON

Given the preceding construction schedule, 2024 was selected as the Build analysis year.

C. SITE AND TRAFFIC INFORMATION

Site and traffic information are provided in Section 1 of this report.

D. TRIP ASSIGNMENTS

The trip assignments are described in Section 1F and are shown in Figures 3 and 4, which were reviewed and approved at the Scoping Meeting. Based upon the trip assignments, the study area was defined as extending from the site through the unsignalized intersection of Gray Road, Skillin Road and Blackstrap Road.

E. TRAFFIC VOLUMES

As previously noted, Sewall conducted turning movement/classification counts at the intersection of Route 26/100, Skillin Road and Blackstrap Road under peak summer conditions in 2023, as outlined below:

<u>Intersection</u>	<u>Count Date</u>	<u>Count Period</u>	<u>Peak Hour</u>
Route 26, Skillin & Blackstrap Roads	8/9/2023	7:00 – 9:00 AM	7:45 – 8:45
Route 26, Skillin & Blackstrap Roads	8/9/2023	3:00 – 6:00 PM	4:15 – 5:15

The count records were included in the Section 1 – 6 application package. Given that the counts were conducted under peak summer conditions, no seasonal adjustments were necessary to obtain 30th highest hour volumes for analysis purposes. The count results are summarized in Figure 2.

Average annual daily traffic (AADT) data for the area was obtained from MaineDOT's Interactive Traffic Map. This data is summarized below:

<u>Location Description</u>	Average Annual Daily Traffic				
	<u>2013</u>	<u>2015</u>	<u>2016</u>	<u>2018</u>	<u>2022</u>
Route 26/100, south of Skillin/Blackstrap Rds	6100	6540	6260	6210	5560
Route 26/100, north of Skillin/Blackstrap Rds	6710	6120	6110	5720	5610
Route 26/100, north of Mountain/Falmouth Rds	8500	--	7550	--	6690
Route 26, north of Hunt Hill Road in Gray	6760	--	6340	--	6610

As seen above, traffic volumes on Route 26/100 have declined at the site, as well as north and south of the site, during the period 2013 to 2022. Based upon this historical data, a 0.50 % percent growth rate was utilized to project the 2023 volumes to base 2024 conditions.

As previously noted, one other development was identified, a proposed 72-unit condominium complex at 77 Blackstrap Road. It is understood that the condominiums will be single-family detached homes. No traffic study has yet been performed for the proposed development but based upon ITE data these 72 condominiums would be expected to generate:

- 50 AM Peak Hour Trips, 13 entering and 37 exiting
- 68 PM peak Hour Trips, 43 entering and 25 exiting

These trips were assigned to Blackstrap Road as shown in Figure 5. The projected 2024 No Build volumes, allowing for annual traffic growth and the condominiums to be fully occupied, are shown in Figure 6. Lastly, the projected 2024 Build volumes are shown in Figure 7.

F. CAPACITY ANALYSES

Traffic operations are evaluated in terms of level of service (LOS). Level of service is a qualitative measure that describes operations by letter designation. The levels range from A - very little delay to F - extreme delays. Level of service "D" is generally considered acceptable in urban locations while LOS "E" is generally considered the capacity of a facility and the minimum tolerable level. The level of service for unsignalized intersections is based upon average control delay per vehicle for each minor, opposed movement, as defined in the following table excerpted from the 2010 "Highway Capacity Manual":

Unsignalized Intersection Level of Service

<u>LOS</u>	<u>Delay Range</u>
A	< = 10.0 seconds
B	> 10.0 and <= 15.0
C	> 15.0 and <= 25.0
D	> 25.0 and <= 35.0
E	> 35.0 and <= 50.0
F	> 50.0

AUXILIARY TURN LANE WARRANTS

Auxiliary right-turn and left-turn lane warrant analyses were requested at the Scoping Meeting for the proposed Gray Road site drive intersection. The analyses were performed utilizing the warrant charts in NCHRP 457, which are included in the appendix. The projected Build volumes were adjusted to an average day utilizing MaineDOT group mean factors. Sewall utilized 40-mph for the analyses as opposed to the posted 35-mph speed limit. The results show that neither a right-turn lane nor a left-turn lane are warranted on Route 100 to store traffic entering the site.

UNSIGNALIZED INTERSECTION ANALYSIS

The level of service (LOS) was calculated for the unsignalized study area intersection and the site drives for projected 2024 No Build and Build conditions using Synchro 11/SimTraffic to assure acceptable levels of service, the average of ten (10) runs. The results are summarized in the following tables:

Route 26/100, Skillin Road and Blackstrap Road		
AM Peak Hour Level of Service		
<u>Approach/Lane</u>	No Build <u>2024</u>	Build <u>2024</u>
Blackstrap Rd Eastbound Approach	A (8.8)	A (9.6)
Skillin Rd Westbound Approach	A (7.7)	A (8.9)
Route 26/100 Northbound Approach	A (0.9)	A (1.1)
Route 26/100 Southbound approach	A (2.0)	A (2.1)
Intersection Overall	A (4.2)	A (4.7)

PM Peak Hour Level of Service		
<u>Approach/Lane</u>	No Build <u>2024</u>	Build <u>2024</u>
Blackstrap Rd Eastbound Approach	B (11.9)	B (12.2)
Skillin Rd Westbound Approach	B (10.6)	B (11.5)
Route 26/100 Northbound Approach	A (1.5)	A (1.6)
Route 26/100 Southbound approach	A (1.9)	A (2.1)
Intersection Overall	A (4.6)	A (4.8)

As seen above, the SimTraffic analysis shows the side street approaches operate at LOS “A” during the AM peak hour and at LOS “B” during the PM peak hour, demonstrating no capacity concerns. The results also demonstrate the minimal impact the convenience store will have off-site with no significant change in delays (less than 1 second) between No Build and Build conditions.

Route 26/100 & Site Drive	
AM Peak Hour Level of Service	
<u>Approach/Lane</u>	Build <u>2024</u>
Site Drive Westbound Lefts/Rights	A (5.9)
Route 26/100 Northbound Thrus/Rights	A (1.0)
Route 26/100 Southbound Thrus/Lefts	A (1.0)
Intersection Overall	A (1.6)

PM Peak Hour Level of Service	
<u>Approach/Lane</u>	<u>Build 2024</u>
Site Drive Westbound Lefts/Rights	A (8.4)
Route 26/100 Northbound Thrus/Rights	A (1.9)
Route 26/100 Southbound Thrus/Lefts	A (1.3)
Intersection Overall	A (2.5)

As seen above, the Gray Road site drive will operate at LOS “A” during both the AM and PM peak hours. Hence, no capacity concerns are anticipated at the site drive.

Skillin Road & Site Drive AM Peak Hour Level of Service	
<u>Approach/Lane</u>	<u>Build 2024</u>
Skillin Rd Eastbound Thrus/Rights	A (1.2)
Skillin Rd Westbound Lefts/Thrus	A (1.5)
Site Drive Northbound Approach Lefts/Rights	A (3.6)
Intersection Overall	A (1.6)

PM Peak Hour Level of Service	
<u>Approach/Lane</u>	<u>Build 2024</u>
Skillin Rd Eastbound Thrus/Rights	A (1.1)
Skillin Rd Westbound Lefts/Thrus	A (1.9)
Site Drive Northbound Approach Lefts/Rights	A (4.1)
Intersection Overall	A (1.7)

As seen above, the Skillin Road site drive will also operate at LOS “A” during both peak hours demonstrating no capacity concerns.

QUEUE ANALYSIS

In addition to level of service, queues were also evaluated using SimTraffic, as requested at the Scoping Meeting. The results, averaging ten (10) runs, are summarized in the following tables:

Route 26/100, Blackstrap & Skillin Roads AM Peak Hour 95th Percentile Queues

<u>Approach/Movement</u>	No Build <u>2024</u>	Build <u>2024</u>
Blackstrap Rd Eastbound Approach	86'	92'
Skillin Rd Westbound Approach	70'	76'
Route 26/100 Northbound Approach	40'	45'
Route 26/100 Southbound Approach	43'	44'

PM Peak Hour 95th Percentile Queues

<u>Approach/Movement</u>	No Build <u>2024</u>	Build <u>2024</u>
Blackstrap Rd Eastbound Approach	87'	91'
Skillin Rd Westbound Approach	89'	93'
Route 26/100 Northbound Approach	56'	60'
Route 26/100 Southbound Approach	45'	50'

As seen above, the SimTraffic results do not project any unreasonable 95th percentile queues on any of the intersection approaches, during either peak hour. There is no significant change in any queue length due to the added convenience store and bank trips.

Route 26/100 and Site Drive AM Peak Hour 95th Percentile Queues

<u>Approach/Movement</u>	Build <u>2024</u>
Site Drive Westbound Lefts/Rights	73'
Route 26/100 Northbound Thrus/Rights	--
Route 26/100 Southbound Lefts/Thrus	48'

PM Peak Hour 95th Percentile Queues

<u>Approach/Movement</u>	<u>Build 2024</u>
Site Drive Westbound Lefts/Rights	71'
Route 26/100 Northbound Thrus/Rights	5'
Route 26/100 Southbound Lefts/Thrus	51'

As seen above, no unreasonable 95th percentile queues are projected on Gray Road due to vehicles entering the site.

PEDESTRIAN AND MULTI-MODAL CONSIDERATIONS

Multimodal analysis was requested at the Scoping Meeting for pedestrians and bicyclists. ITE does have some pedestrian and bicycle trip data. Data for the proposed land uses, convenience store with gasoline fueling facilities and drive-in bank, is quite limited since these uses are not high pedestrian or bicycle generators. There is no multimodal data for a drive-in bank. There is data for a convenience store with gasoline fueling facilities for the AM and PM peak hours of the adjacent street. However, this data is from just one study and ITE cautions use of the data given the very small sample size.

In terms of existing pedestrian and bicycle trips, Sewall counts pedestrians and bicycles during turning movement counts. The following activity was recorded at the intersection of Gray Road, Blackstrap Road and Skillin Road under peak summer conditions in August:

- During the AM peak hour, there was one pedestrian crossing Skillin Road and two crossing Blackstrap Road.
- During the PM peak hour, there were two pedestrians crossing Blackstrap Road.
- There were no bicycles recorded at the intersection during either period and no pedestrians crossed Gray Road.

Sewall recommends, based upon a review of the vicinity of the site (1/4 mile radius), that sidewalk be provided to connect the site to serve the following residences where pedestrians may originate:

- Along the east side of Gray Road, to the north to Farraday Drive, providing for the Mill House Townhouse Condominiums
- Along the south side of Skillin Road, to the east to Kathy Lane

Concept plans for the recommended new sidewalk locations are included in the appendix. It is noted that the Town of Cumberland has asked MaineDOT to fund construction of a roundabout at the Gray/Skillin/Blackstrap intersection. The concept plan for the roundabout shows new sidewalks in these locations as well as a center-left turn lane on Gary Road. As such, the convenience store concept plan locates the Gray Road sidewalk at the right-of-way line (with esplanade) to allow for this future construction, but this may not be sufficient to allow for the proposed center-turn lane. Hence, if the roundabout project is likely to proceed, MaineDOT may wish to assess the convenience store development a traffic impact fee towards sidewalks versus having to remove recently installed sidewalk.

Additionally, MaineDOT requested at the Scoping Meeting that a crosswalk be provided on Gray Road to connect the proposed sidewalks along the site frontage to the existing sidewalks on the opposite side of Gray Road. Sewall ran AutoTurn analysis for a single unit truck exiting the site drive, and Skillin and Blackstrap Roads, to locate this crosswalk outside of the vehicle turning paths. The proposed location is shown on the site plan. Note there is an existing light pole on the opposite parcel at this location. Additionally, the applicant will locate a light pole on the easterly side of Gray Road to light the easterly side of the crosswalk. Given the midblock location, this crosswalk will be equipped with RRFBs.

G. TRAFFIC SIGNAL WARRANT ANALYSIS

No traffic signal warrant analysis was requested at the Scoping Meeting. A recent Traffic Signal Warrant Analysis was conducted by VHB. This analysis showed that a traffic signal is not warranted at the intersection.

H. SIGHT DISTANCE ANALYSIS

No additional sight distance analysis was requested at the Scoping Meeting.

I. TRAFFIC ACCIDENTS

Traffic accidents were previously discussed under Section 2 and at the Scoping Meeting. The Town has developed a short-term improvement plan, focused on advanced and improved warning signage, to reduce the angle collisions that are occurring. Sewall has reviewed this plan and concurs with the proposed signage improvements. The Town is seeking MaineDOT funding to replace the two-way stop controlled intersection with a roundabout to improve safety long-term. Other short-term measures to improve safety, such as the implementation of all-way stop, have been rejected by the Town.

J. RECOMMENDATIONS

No capacity concerns were identified by the analysis and turn lanes are not warranted on Gray Road given the Gray Road volumes. Since sidewalk is proposed along the site frontage, and since there is existing sidewalk on the opposite side of Gray Road, a crosswalk to connect the two facilities was requested at the Scoping Meeting. Sewall has located this crosswalk outside of the turning path for vehicles exiting the site and Skillin/Blackstrap Road so that drivers will be focused straight ahead. This crosswalk should be marked with bold markings and equipped with RRFBs given the midblock location. Additionally, new sidewalk is recommended along Gray Road to the north to Farraday Drive and to the east along Skillin Road to Kathy Lane since pedestrians may originate from residences in these locations.

K. CONCLUSION

Safe and convenient site access is expected to be provided, based upon the capacity analysis results, and with the planned town intersection signage improvements. Area pedestrian facilities will be enhanced with the addition of sidewalks on Gray Road and Skillin Road, and with the proposed Gray Road crosswalk, to be equipped with RRFBs.



Figure 1

Site Location Map

Convenience Store & Bank Development

Cumberland, Maine





-- = AM Peak Hour
 (--) = PM Peak Hour

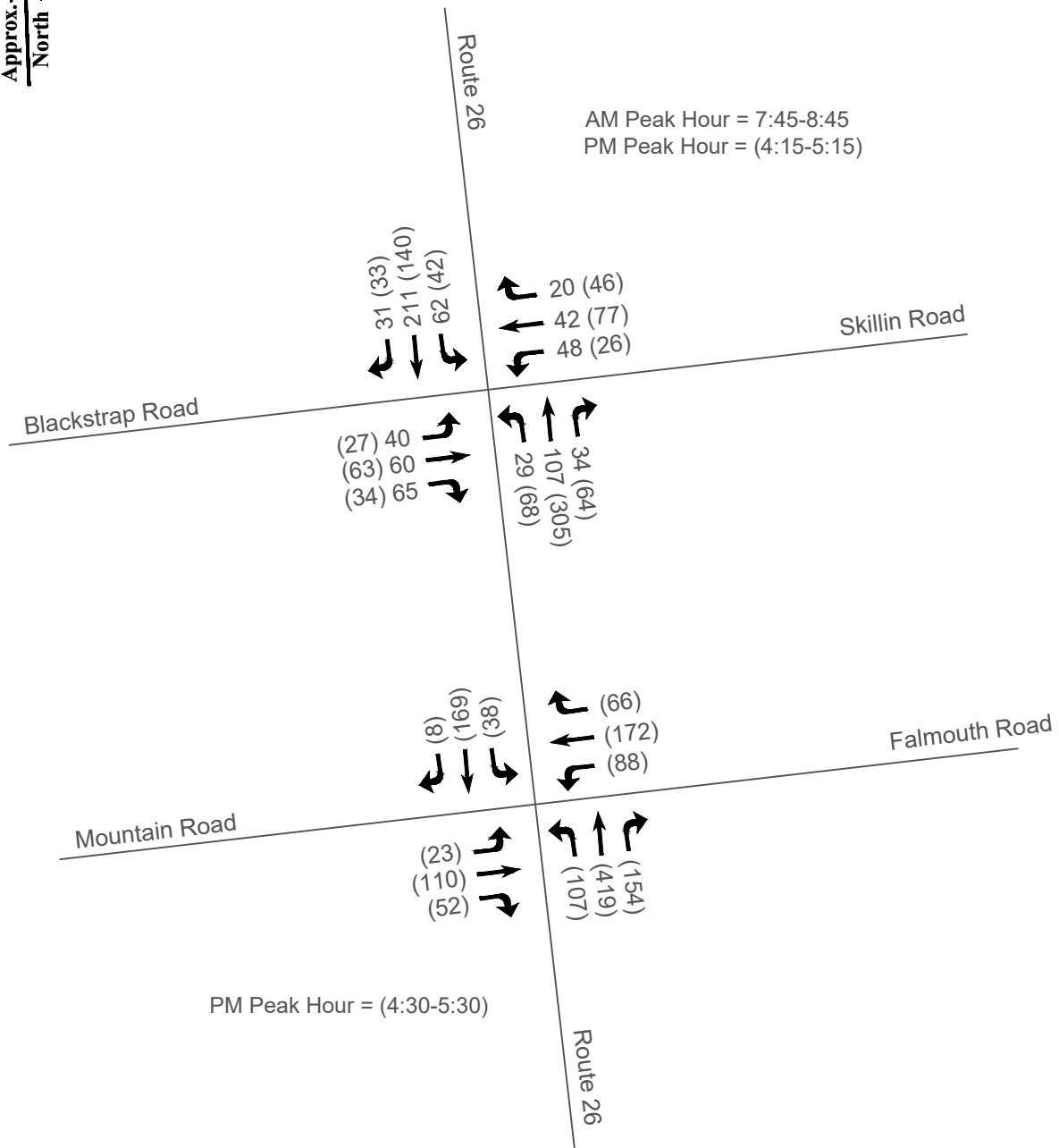


Figure 2

2023 Existing Peak Hour Volumes
Convenience Store & Bank Development
Cumberland, Maine





-- = Primary
(--) = Pass-By

99 Primary Trips

51 In
48 Out

(131 Pass-By Trips)

66 In
65 Out

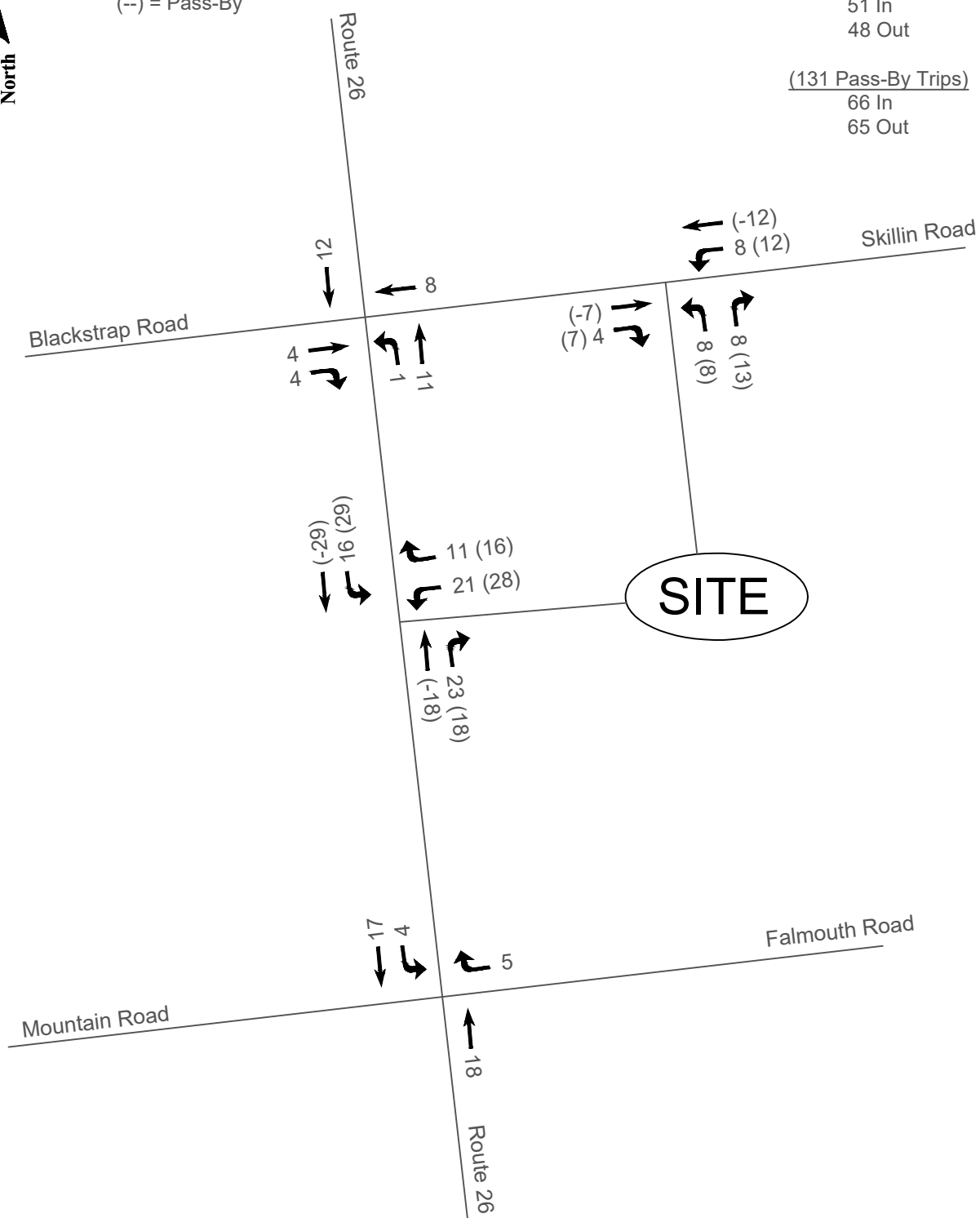


Figure 3

AM Peak Hour Trip Assignments
Convenience Store & Bank Development
Cumberland, Maine



-- = Primary
 (--) = Pass-By

129 Primary Trips

65 In
 64 Out

(138 Pass-By Trips)

69 In
 69 Out

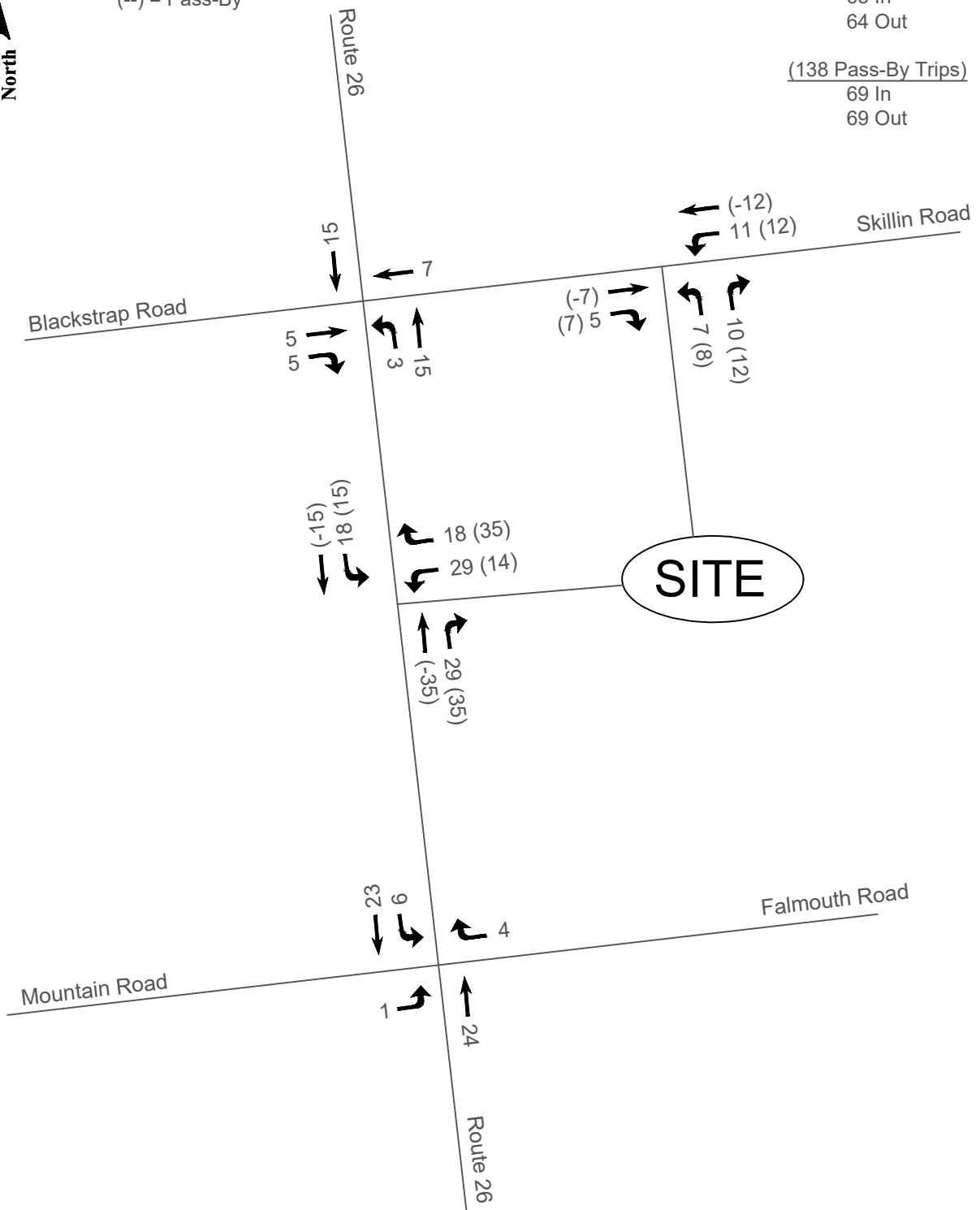


Figure 4

PM Peak Hour Trip Assignments
Convenience Store & Bank Development
Cumberland, Maine





-- = Primary
(--) = Pass-By

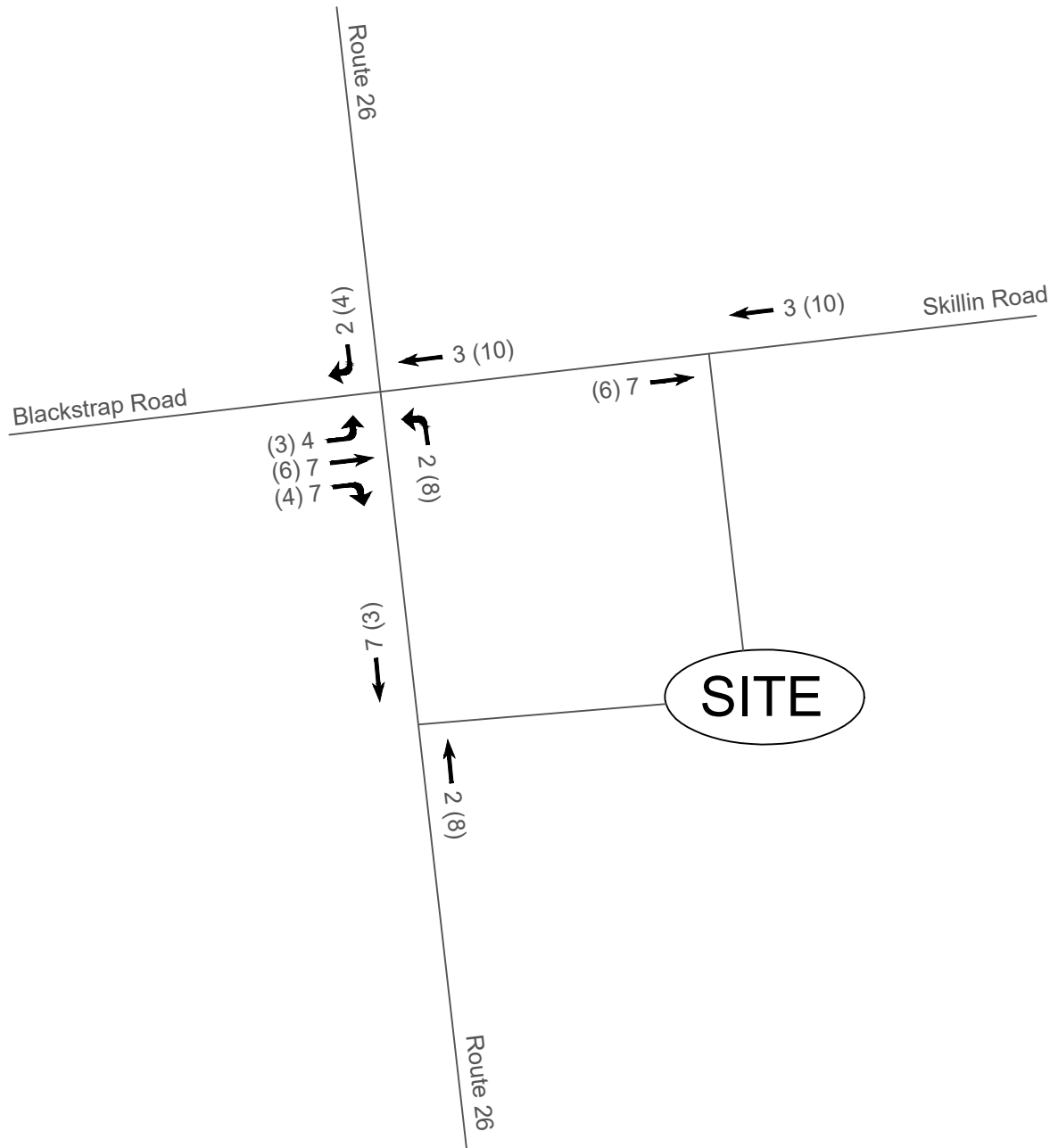


Figure 5

Other Development Trips
Convenience Store & Bank Development
Cumberland, Maine



-- = Primary
(--) = Pass-By

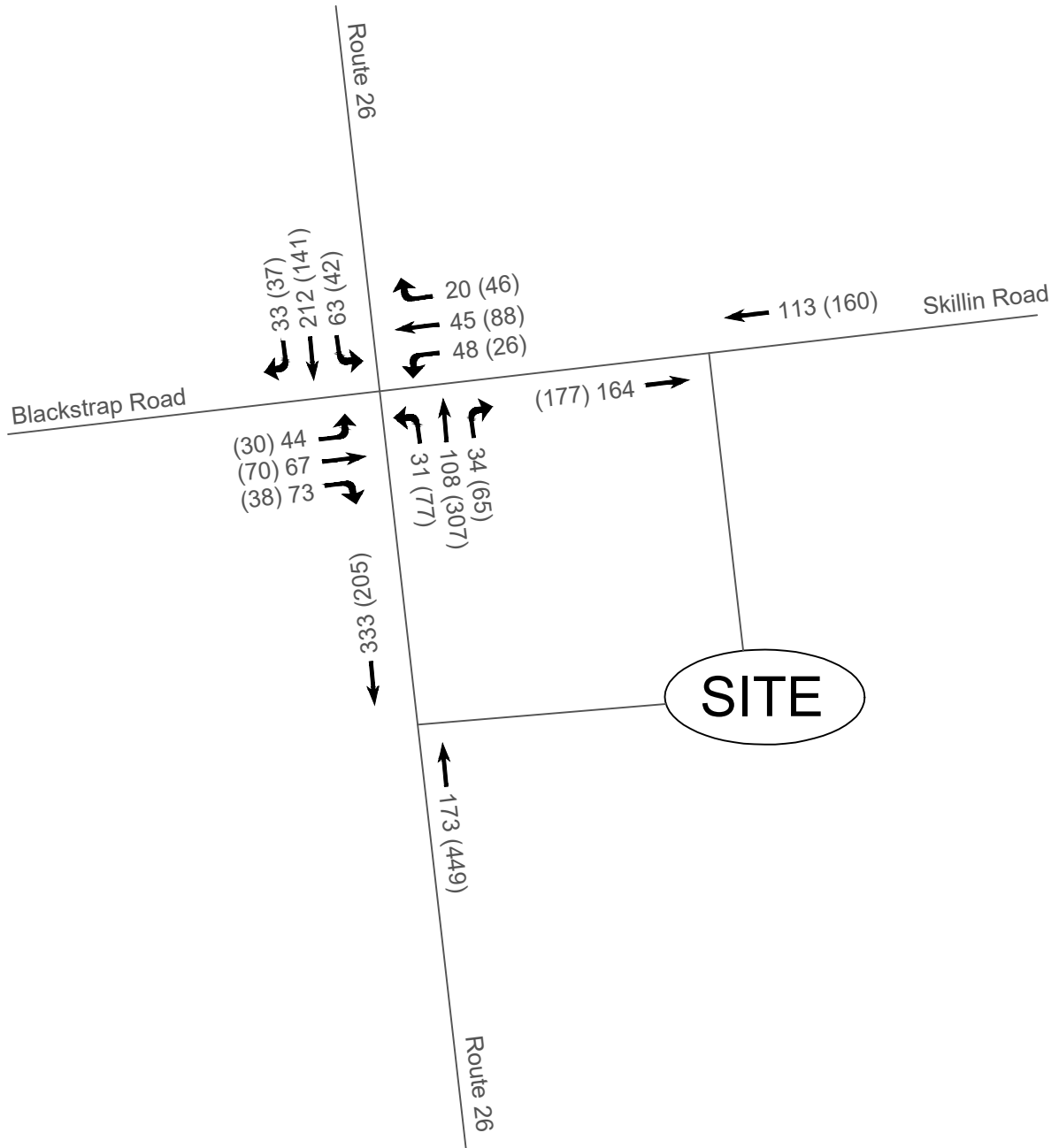


Figure 6

2024 No Build Peak Hour Volumes
Convenience Store & Bank Development
Cumberland, Maine





-- = Primary
(--) = Pass-By

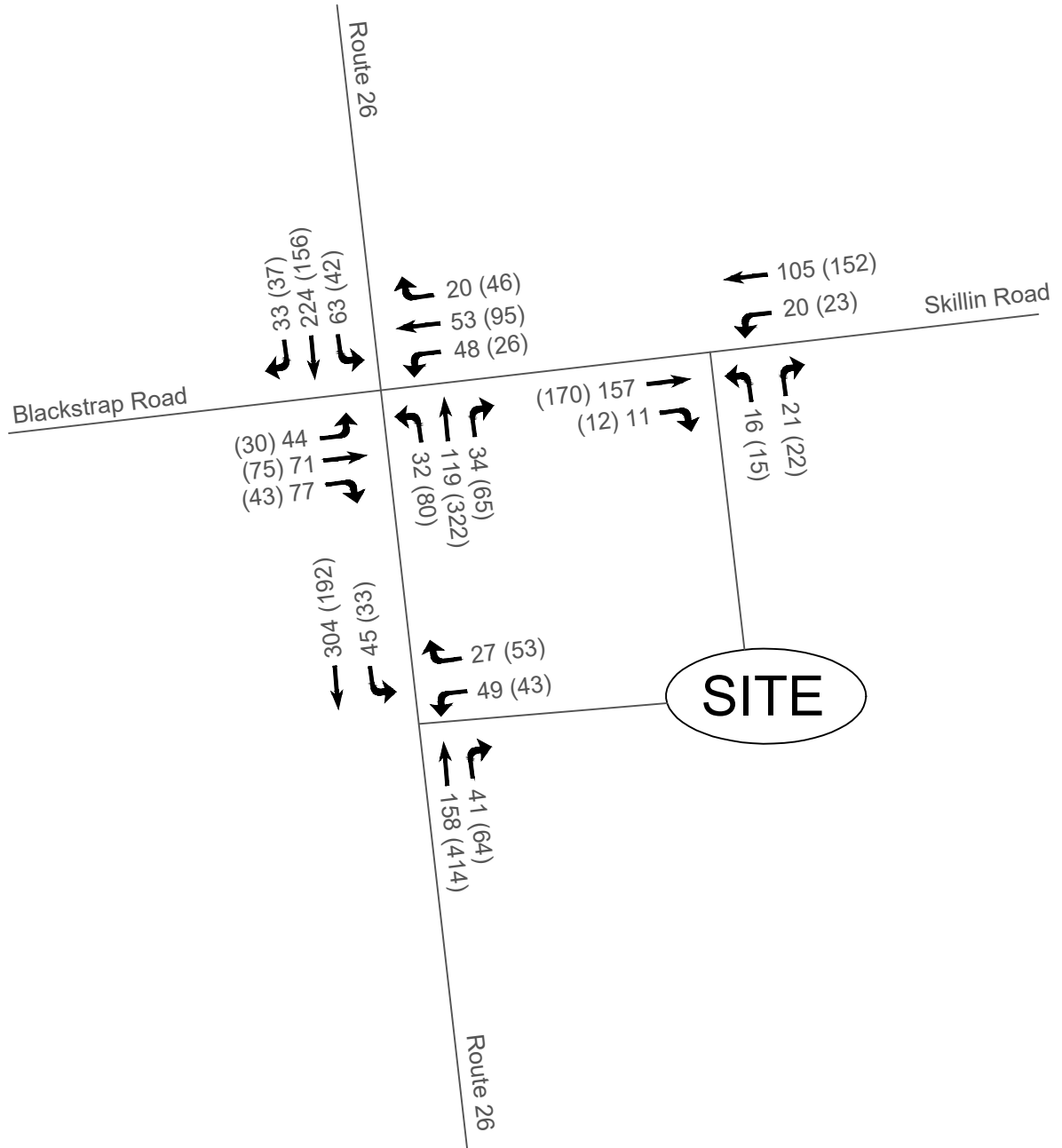


Figure 7

2024 Build Peak Hour Volumes
Convenience Store & Bank Development
Cumberland, Maine

APPENDIX

Collision Diagram

Auxiliary Turn Lane Warrants

Capacity Analysis

Concept Plan for Sidewalks

Site Plan

H. C. L. CRASH COLLISION DIAGRAM DATA PACKAGE

COUNTY: CUMBERLAND

TOWN: CUMBERLAND

LOW NODE: 17087 HIGH NODE: 0000

REGION: 1

U/R: URBAN

DESCRIPTION: Int Gray Rd & Skillin Rd/Blackstrap Rd

RTE # / RD #: 0026X

DATE DRAWN: 10/31/2023 DRAWN BY: Michelle

STUDY FROM: 10/1/2020

STUDY TO: 9/30/2023

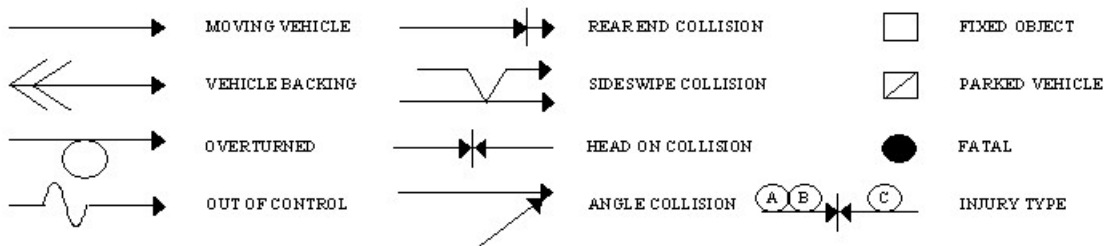
CRASH RATE: 0.97

CRF: 2.29

% INJURY: 44.4

TOTAL CRASHES: 9

LEGEND

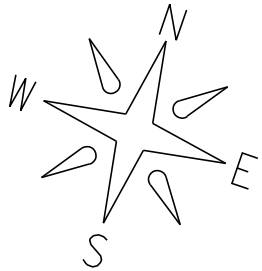


--- PATH OF: [P] PEDESTRIAN [B] BICYCLE [A] ANIMAL [S] SLED

PAVEMENT: D - DRY, I - ICY, W - WET, S - SNOW

WEATHER: C - CLEAR, F - FOG, R - RAIN, SL - SLEET, S - SNOW, CL - CLOUDY

TIME: A - AM, P - PM



Rt 26 & 100/Gray Rd

Cumberland

Node: 17087

Study Period: 10-1-20 to 9-30-23

of Crashes: 9 / CRF: 2.29

Prepared by Office of Safety & Mobility (MP 10/31/23)



Stop

Blackstrap Rd

9304 4-9-21 3:46P D/C Fail to Yield

9887 4-19-21 7:45A D/C Fail to Yield

12608 4-28-23 10:13A D/C Speed

21309 7-25-23 4:41P D/C Fail to Yield

12625 5-2-22 7:08A D/C Follow Too Close

Stop



= Flashing Light

Rt 26 & 100/Gray Rd

Skillins Rd

38487 12-18-22 4:14P D/C L Ran Red Light

9244 3-15-23 10:06A D/C Fail to Yield

20604 7-20-23 12:59P D/C Fail to Yield

1366 1-8-22 10:05P D/C Fire



Crash Summary Report

Report Selections and Input Parameters

REPORT SELECTIONS

☒ Crash Summary I - Single Node ☐ Section Detail ☒ Crash Summary II ☐ 1320 Public ☐ 1320 Private ☐ 1320 Summary

REPORT DESCRIPTION

Cumberland
Intersection of Rte. 26/100/Gray Rd. & Blackstrap/Skillin Rd.

REPORT PARAMETERS

Year 2020, Start Month 10 through Year 2023 End Month: 9

Route: 0026X

Start Node: 17087

Start Offset: 0

☐ Exclude First Node

End Node: 17087

End Offset: 0

☐ Exclude Last Node

Crash Summary I

Nodes

Node	Route - MP	Node Description			U/R	Total Crashes	K	Injury Crashes			PD	Percent Injury	Annual M Ent-Veh	Crash Rate	Critical Rate	CRF
17087	0026X - 11.49	Int of BLACKSTRAP RD	GRAY RD	SKILLIN RD	2	9	0	1	1	2	5	44.4	3.097	0.97	0.42	2.29
														Statewide Crash Rate: 0.15		
Study Years:	3.00	NODE TOTALS:				9	0	1	1	2	5	44.4	3.097	0.97	0.42	2.29

Figure 2 - 5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

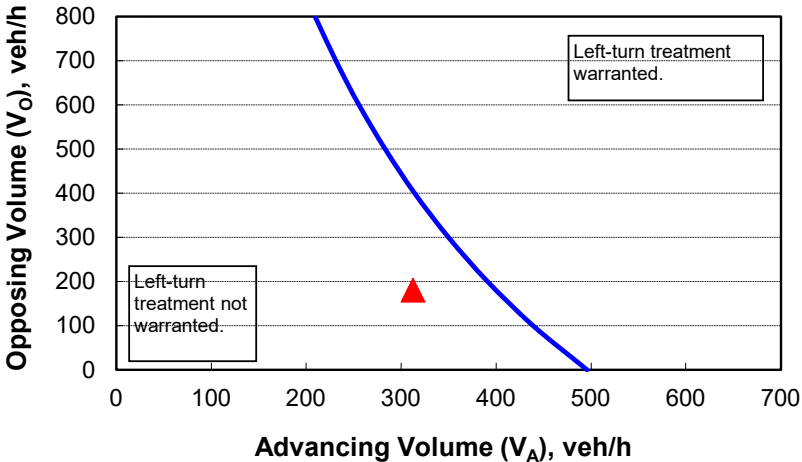
2-lane roadway (English)

INPUT

Variable	Value
85 th percentile speed, mph:	40
Percent of left-turns in advancing volume (V_A), %:	14%
Advancing volume (V_A), veh/h:	313
Opposing volume (V_O), veh/h:	180

OUTPUT

Variable	Value
Limiting advancing volume (V_A), veh/h:	400
Guidance for determining the need for a major-road left-turn bay:	
Left-turn treatment NOT warranted.	



CALIBRATION CONSTANTS

Variable	Value
Average time for making left-turn, s:	3.0
Critical headway, s:	5.0
Average time for left-turn vehicle to clear the advancing lane, s:	1.9

2024 AM BUILD - GRAY ROAD AND SITE DRIVE - LEFT TURN LANE WARRANT NOT MET

Figure 2 - 5. Guideline for determining the need for a major-road left-turn bay at a two-way stop-controlled intersection.

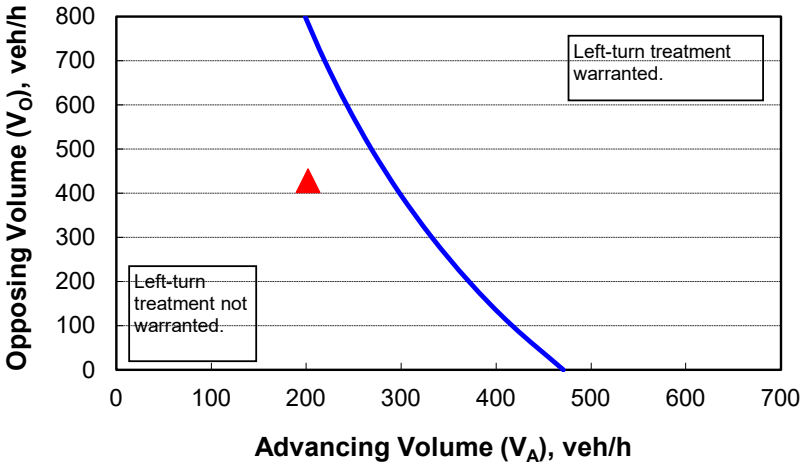
2-lane roadway (English)

INPUT

Variable	Value
85 th percentile speed, mph:	40
Percent of left-turns in advancing volume (V_A), %:	16%
Advancing volume (V_A), veh/h:	202
Opposing volume (V_O), veh/h:	428

OUTPUT

Variable	Value
Limiting advancing volume (V_A), veh/h:	290
Guidance for determining the need for a major-road left-turn bay:	
Left-turn treatment NOT warranted.	



CALIBRATION CONSTANTS

Variable	Value
Average time for making left-turn, s:	3.0
Critical headway, s:	5.0
Average time for left-turn vehicle to clear the advancing lane, s:	1.9

2024 PM BUILD - GRAY ROAD AND SITE DRIVE - LEFT TURN LANE WARRANT NOT MET

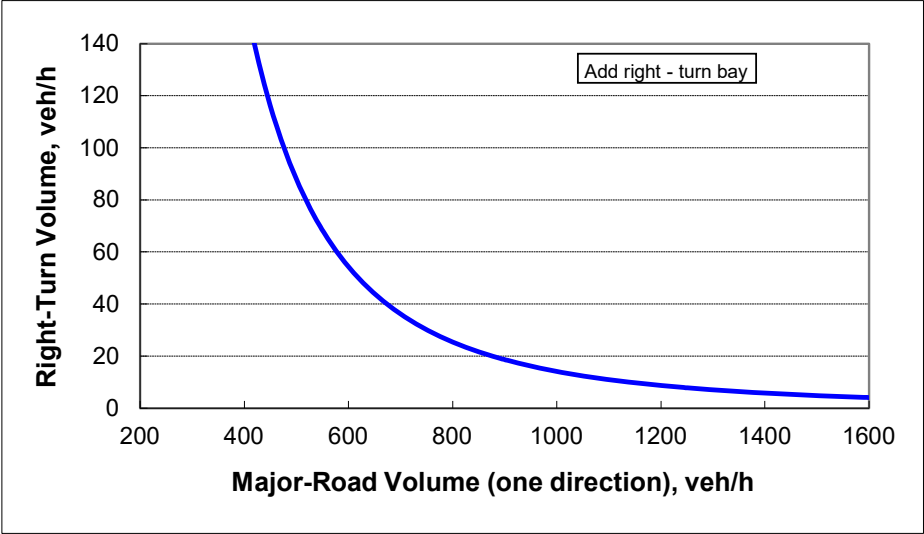
Figure 2 - 6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

INPUT

Roadway geometry:	2-lane roadway
Variable	Value
Major-road speed, mph:	40
Major-road volume (one direction), veh/h:	180
Right-turn volume, veh/h:	41

OUTPUT

Variable	Value
Limiting right-turn volume, veh/h:	1305
Guidance for determining the need for a major-road right-turn bay for a 2-lane roadway:	
Do NOT add right-turn bay.	



2024 AM BUILD - GRAY ROAD AND SITE DRIVE - RIGHT TURN LANE WARRANT NOT MET

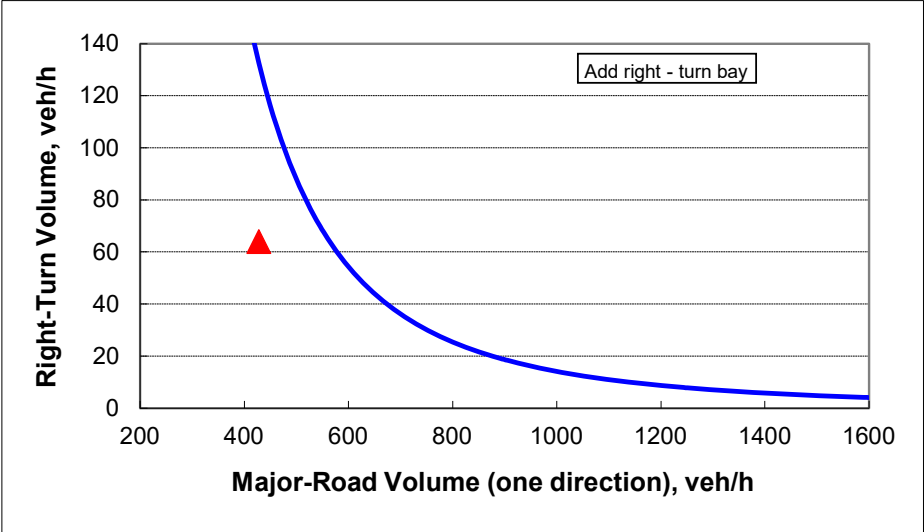
Figure 2 - 6. Guideline for determining the need for a major-road right-turn bay at a two-way stop-controlled intersection.

INPUT

Roadway geometry:	2-lane roadway
Variable	Value
Major-road speed, mph:	40
Major-road volume (one direction), veh/h:	428
Right-turn volume, veh/h:	64

OUTPUT

Variable	Value
Limiting right-turn volume, veh/h:	132
Guidance for determining the need for a major-road right-turn bay for a 2-lane roadway:	
Do NOT add right-turn bay.	



2024 PM BUILD - GRAY ROAD AND SITE DRIVE - RIGHT TURN LANE WARRANT NOT MET

Summary of All Intervals

Run Number	1	2	3	4	5	6	7
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70	70	70	70
Time Recorded (min)	60	60	60	60	60	60	60
# of Intervals	2	2	2	2	2	2	2
# of Recorded Intervals	1	1	1	1	1	1	1
Vehs Entered	777	757	770	742	748	789	793
Vehs Exited	769	755	775	753	746	797	789
Starting Vehs	12	11	14	22	13	20	12
Ending Vehs	20	13	9	11	15	12	16
Travel Distance (mi)	454	444	457	438	440	469	466
Travel Time (hr)	15.3	14.8	15.3	14.8	14.7	15.8	15.7
Total Delay (hr)	1.3	1.2	1.2	1.2	1.1	1.3	1.4
Total Stops	325	312	336	279	309	315	330
Fuel Used (gal)	14.1	13.6	14.1	13.8	13.5	14.5	14.5

Summary of All Intervals

Run Number	8	9	10	Avg
Start Time	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70
Time Recorded (min)	60	60	60	60
# of Intervals	2	2	2	2
# of Recorded Intervals	1	1	1	1
Vehs Entered	743	773	749	764
Vehs Exited	742	776	765	767
Starting Vehs	13	17	29	15
Ending Vehs	14	14	13	11
Travel Distance (mi)	440	459	445	451
Travel Time (hr)	14.8	15.4	14.9	15.1
Total Delay (hr)	1.2	1.3	1.3	1.2
Total Stops	315	329	307	314
Fuel Used (gal)	13.4	14.2	13.6	13.9

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Growth Factors.	
No data recorded this interval.	

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	6	7
Vehs Entered	777	757	770	742	748	789	793
Vehs Exited	769	755	775	753	746	797	789
Starting Vehs	12	11	14	22	13	20	12
Ending Vehs	20	13	9	11	15	12	16
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Total Delay (hr)	1.3	1.2	1.2	1.2	1.1	1.3	1.4
Total Stops	325	312	336	279	309	315	330
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Interval #1 Information Off-Peak

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Total Time (min)	60

Volumes adjusted by Growth Factors.

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Total Delay (hr)	1.2	1.3	1.3	1.2
Total Stops	315	329	307	314
Fuel Used (gal)	13.4	14.2	13.6	13.9

3: Route 26 & Blackstrap Rd/Skillin Rd Performance by lane

Lane	EB	WB	NB	SB	All
Movements Served	LTR	LTR	LTR	LTR	
Denied Del/Veh (s)					0.1
Total Del/Veh (s)	8.8	7.7	0.9	2.0	4.2

6: Route 26 & Site Drive Performance by lane

Lane	NB	SB	All
Movements Served	TR	LT	
Denied Del/Veh (s)			0.1
Total Del/Veh (s)	0.6	0.5	0.5

7: Site Drive & Skillin Rd Performance by lane

Lane	EB	WB	All
Movements Served	TR	LT	
Denied Del/Veh (s)			0.1
Total Del/Veh (s)	1.2	1.1	1.1

Total Network Performance

Denied Del/Veh (s)	0.2
Total Del/Veh (s)	5.6

Queuing and Blocking Report

2024 No Build AM

10/31/2023

Intersection: 3: Route 26 & Blackstrap Rd/Skillin Rd

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (ft)	106	90	62	67
Average Queue (ft)	50	42	10	12
95th Queue (ft)	86	70	40	43
Link Distance (ft)	1767	110	127	1360
Upstream Blk Time (%)	0			
Queuing Penalty (veh)	0			
Storage Bay Dist (ft)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 6: Route 26 & Site Drive

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)

Intersection: 7: Site Drive & Skillin Rd

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)

Network Summary

Network wide Queuing Penalty: 0

Summary of All Intervals

Run Number	1	2	3	4	5	6	7
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70	70	70	70
Time Recorded (min)	60	60	60	60	60	60	60
# of Intervals	2	2	2	2	2	2	2
# of Recorded Intervals	1	1	1	1	1	1	1
Vehs Entered	777	757	770	742	748	789	793
Vehs Exited	769	755	775	753	746	797	789
Starting Vehs	12	11	14	22	13	20	12
Ending Vehs	20	13	9	11	15	12	16
Travel Distance (mi)	454	444	457	438	440	469	466
Travel Time (hr)	15.3	14.8	15.3	14.8	14.7	15.8	15.7
Total Delay (hr)	1.3	1.2	1.2	1.2	1.1	1.3	1.4
Total Stops	325	312	336	279	309	315	330
Fuel Used (gal)	14.1	13.6	14.1	13.8	13.5	14.5	14.5

Summary of All Intervals

Run Number	8	9	10	Avg
Start Time	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70
Time Recorded (min)	60	60	60	60
# of Intervals	2	2	2	2
# of Recorded Intervals	1	1	1	1
Vehs Entered	743	773	749	764
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Starting Vehs	13	17	29	15
Ending Vehs	14	14	13	11
Travel Distance (mi)	440	459	445	451
Travel Time (hr)	14.8	15.4	14.9	15.1
Total Delay (hr)	1.2	1.3	1.3	1.2
Total Stops	315	329	307	314
Fuel Used (gal)	13.4	14.2	13.6	13.9

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Growth Factors.	
No data recorded this interval.	

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	6	7
Vehs Entered	777	757	770	742	748	789	793
Vehs Exited	769	755	775	753	746	797	789
Starting Vehs	12	11	14	22	13	20	12
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Travel Time (hr)	15.3	14.8	15.3	14.8	14.7	15.8	15.7
Total Delay (hr)	1.3	1.2	1.2	1.2	1.1	1.3	1.4
Total Stops	325	312	336	279	309	315	330
Fuel Used (gal)	14.1	13.6	14.1	13.8	13.5	14.5	14.5

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	8	9	10	Avg
Vehs Entered	743	773	749	764
Vehs Exited	742	776	765	767
Starting Vehs	13	17	29	15
Ending Vehs	14	14	13	11
Travel Distance (mi)	440	459	445	451
Travel Time (hr)	14.8	15.4	14.9	15.1
Total Delay (hr)	1.2	1.3	1.3	1.2
Total Stops	315	329	307	314
Fuel Used (gal)	13.4	14.2	13.6	13.9

3: Route 26 & Blackstrap Rd/Skillin Rd Performance by approach

Approach	EB	WB	NB	SB	All
Denied Del/Veh (s)	0.2	0.0	0.0	0.3	0.1
Total Del/Veh (s)	8.9	7.8	0.9	2.0	4.2

6: Route 26 & Site Drive Performance by approach

Approach	NB	SB	All
Denied Del/Veh (s)	0.2	0.0	0.1
Total Del/Veh (s)	0.6	0.5	0.5

7: Site Drive & Skillin Rd Performance by approach

Approach	EB	WB	All
Denied Del/Veh (s)	0.0	0.1	0.1
Total Del/Veh (s)	1.2	1.1	1.1

Total Network Performance

Denied Del/Veh (s)	0.2
Total Del/Veh (s)	5.6

Queuing and Blocking Report

2024 No Build AM

10/31/2023

Intersection: 3: Route 26 & Blackstrap Rd/Skillin Rd

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (ft)	106	90	62	67
Average Queue (ft)	50	42	10	12
95th Queue (ft)	86	70	40	43
Link Distance (ft)	1767	110	127	1360
Upstream Blk Time (%)	0			
Queuing Penalty (veh)	0			
Storage Bay Dist (ft)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 6: Route 26 & Site Drive

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)

Intersection: 7: Site Drive & Skillin Rd

Movement
Directions Served
Maximum Queue (ft)
Average Queue (ft)
95th Queue (ft)
Link Distance (ft)
Upstream Blk Time (%)
Queuing Penalty (veh)
Storage Bay Dist (ft)
Storage Blk Time (%)
Queuing Penalty (veh)

Network Summary

Network wide Queuing Penalty: 0

Summary of All Intervals

Run Number	1	2	3	4	5	6	7
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70	70	70	70
Time Recorded (min)	60	60	60	60	60	60	60
# of Intervals	2	2	2	2	2	2	2
# of Recorded Intervals	1	1	1	1	1	1	1
Vehs Entered	959	959	956	1004	933	992	993
Vehs Exited	965	960	968	1006	931	993	996
Starting Vehs	24	21	27	24	22	21	21
Ending Vehs	18	20	15	22	24	20	18
Travel Distance (mi)	565	564	561	592	544	583	576
Travel Time (hr)	19.3	19.1	19.2	20.6	18.5	19.9	19.5
Total Delay (hr)	1.9	1.7	1.9	2.3	1.7	1.9	1.8
Total Stops	348	353	338	383	316	362	323
Fuel Used (gal)	17.5	17.4	17.2	18.5	16.7	18.0	17.6

Summary of All Intervals

Run Number	8	9	10	Avg
Start Time	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70
Time Recorded (min)	60	60	60	60
# of Intervals	2	2	2	2
# of Recorded Intervals	1	1	1	1
Vehs Entered	989	939	960	968
Vehs Exited	989	942	976	972
Starting Vehs	20	19	31	22
Ending Vehs	20	16	15	15
Travel Distance (mi)	582	555	569	569
Travel Time (hr)	19.8	19.2	19.3	19.4
Total Delay (hr)	1.9	2.0	1.9	1.9
Total Stops	340	355	339	345
Fuel Used (gal)	17.8	17.2	17.7	17.6

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Growth Factors.	
No data recorded this interval.	

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	6	7
Vehs Entered	959	959	956	1004	933	992	993
Vehs Exited	965	960	968	1006	931	993	996
Starting Vehs	24	21	27	24	22	21	21
Ending Vehs	18	20	15	22	24	20	18
Travel Distance (mi)	565	564	561	592	544	583	576
Travel Time (hr)	19.3	19.1	19.2	20.6	18.5	19.9	19.5
Total Delay (hr)	1.9	1.7	1.9	2.3	1.7	1.9	1.8
Total Stops	348	353	338	383	316	362	323
Fuel Used (gal)	17.5	17.4	17.2	18.5	16.7	18.0	17.6

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	8	9	10	Avg
Vehs Entered	989	939	960	968
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Total Delay (hr)	1.9	2.0	1.9	1.9
Total Stops	340	355	339	345
Fuel Used (gal)	17.8	17.2	17.7	17.6

3: Route 26 & Blackstrap Rd/Skillin Rd Performance by lane

Lane	EB	WB	NB	SB	All
Movements Served	LTR	LTR	LTR	LTR	
Denied Del/Veh (s)					0.1
Total Del/Veh (s)	11.9	10.6	1.5	1.9	4.6

6: Route 26 & Site Drive Performance by lane

Lane	NB	SB	All
Movements Served	TR	LT	
Denied Del/Veh (s)			0.2
Total Del/Veh (s)	1.3	0.4	1.0

7: Site Drive & Skillin Rd Performance by lane

Lane	EB	WB	All
Movements Served	TR	LT	
Denied Del/Veh (s)			0.1
Total Del/Veh (s)	1.2	1.6	1.4

Total Network Performance

Denied Del/Veh (s)	0.3
Total Del/Veh (s)	6.7

Queuing and Blocking Report
2024 No Build PM

10/31/2023

Intersection: 3: Route 26 & Blackstrap Rd/Skillin Rd

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (ft)	113	109	76	60
Average Queue (ft)	49	54	19	14
95th Queue (ft)	87	89	56	45
Link Distance (ft)	1767	110	127	1360
Upstream Blk Time (%)		0	0	
Queuing Penalty (veh)		1	0	
Storage Bay Dist (ft)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 6: Route 26 & Site Drive

Movement	NB
Directions Served	TR
Maximum Queue (ft)	12
Average Queue (ft)	0
95th Queue (ft)	12
Link Distance (ft)	1095
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 7: Site Drive & Skillin Rd

Movement	WB
Directions Served	LT
Maximum Queue (ft)	35
Average Queue (ft)	2
95th Queue (ft)	17
Link Distance (ft)	1892
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Network Summary

Network wide Queuing Penalty: 1

Summary of All Intervals

Run Number	1	2	3	4	5	6	7
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70	70	70	70
Time Recorded (min)	60	60	60	60	60	60	60
# of Intervals	2	2	2	2	2	2	2
# of Recorded Intervals	1	1	1	1	1	1	1
Vehs Entered	959	959	956	1004	933	992	993
Vehs Exited	965	960	968	1006	931	993	996
Starting Vehs	24	21	27	24	22	21	21
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Total Delay (hr)	1.9	1.7	1.9	2.3	1.7	1.9	1.8
Total Stops	348	353	338	383	316	362	323
Fuel Used (gal)	17.5	17.4	17.2	18.5	16.7	18.0	17.6

Summary of All Intervals

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Start Time	6:50	6:50	6:50	6:50
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Total Delay (hr)	1.9	2.0	1.9	1.9
Total Stops	340	355	339	345
Fuel Used (gal)	17.8	17.2	17.7	17.6

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Growth Factors.	
No data recorded this interval.	

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	6	7
Vehs Entered	959	959	956	1004	933	992	993
Vehs Exited	965	960	968	1006	931	993	996
Starting Vehs	24	21	27	24	22	21	21
Ending Vehs	18	20	15	22	24	20	18
Travel Distance (mi)	565	564	561	592	544	583	576
Travel Time (hr)	19.3	19.1	19.2	20.6	18.5	19.9	19.5
Total Delay (hr)	1.9	1.7	1.9	2.3	1.7	1.9	1.8
Total Stops	348	353	338	383	316	362	323
Fuel Used (gal)	17.5	17.4	17.2	18.5	16.7	18.0	17.6

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	8	9	10	Avg
Vehs Entered	989	939	960	968
Vehs Exited	989	942	976	972
Starting Vehs	20	19	31	22
Ending Vehs	20	16	15	15
Travel Distance (mi)	582	555	569	569
Travel Time (hr)	19.8	19.2	19.3	19.4
Total Delay (hr)	1.9	2.0	1.9	1.9
Total Stops	340	355	339	345
Fuel Used (gal)	17.8	17.2	17.7	17.6

3: Route 26 & Blackstrap Rd/Skillin Rd Performance by approach

Approach	EB	WB	NB	SB	All
Denied Del/Veh (s)	0.2	0.0	0.0	0.2	0.1
Total Del/Veh (s)	11.9	10.5	1.5	1.9	4.6

6: Route 26 & Site Drive Performance by approach

Approach	NB	SB	All
Denied Del/Veh (s)	0.3	0.0	0.2
Total Del/Veh (s)	1.3	0.4	1.0

7: Site Drive & Skillin Rd Performance by approach

Approach	EB	WB	All
Denied Del/Veh (s)	0.0	0.2	0.1
Total Del/Veh (s)	1.2	1.6	1.4

Total Network Performance

Denied Del/Veh (s)	0.3
Total Del/Veh (s)	6.7

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Intersection: 3: Route 26 & Blackstrap Rd/Skillin Rd

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (ft)	113	109	76	60
Average Queue (ft)	49	54	19	14
95th Queue (ft)	87	89	56	45
Link Distance (ft)	1767	110	127	1360
Upstream Blk Time (%)		0	0	
Queuing Penalty (veh)		1	0	
Storage Bay Dist (ft)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 6: Route 26 & Site Drive

Movement	NB
Directions Served	TR
Maximum Queue (ft)	12
Average Queue (ft)	0
95th Queue (ft)	12
Link Distance (ft)	1095
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Intersection: 7: Site Drive & Skillin Rd

Movement	WB
Directions Served	LT
Maximum Queue (ft)	35
Average Queue (ft)	2
95th Queue (ft)	17
Link Distance (ft)	1892
Upstream Blk Time (%)	
Queuing Penalty (veh)	
Storage Bay Dist (ft)	
Storage Blk Time (%)	
Queuing Penalty (veh)	

Network Summary

Network wide Queuing Penalty: 1

Summary of All Intervals

Run Number	1	2	3	4	5	6	7
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70	70	70	70
Time Recorded (min)	60	60	60	60	60	60	60
# of Intervals	2	2	2	2	2	2	2
# of Recorded Intervals	1	1	1	1	1	1	1
Vehs Entered	938	919	985	984	957	927	1009
Vehs Exited	944	915	992	992	966	929	1003
Starting Vehs	21	15	28	21	28	17	12
Ending Vehs	15	19	21	13	19	15	18
Travel Distance (mi)	503	485	522	521	506	480	521
Travel Time (hr)	17.4	16.8	18.3	18.2	17.5	16.5	18.5
Total Delay (hr)	1.6	1.7	1.9	1.9	1.7	1.5	2.0
Total Stops	456	442	476	485	477	455	488
Fuel Used (gal)	16.0	15.5	16.8	17.0	16.1	15.1	16.9

Summary of All Intervals

Run Number	8	9	10	Avg
Start Time	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70
Time Recorded (min)	60	60	60	60
# of Intervals	2	2	2	2
# of Recorded Intervals	1	1	1	1
Vehs Entered	972	901	950	953
Vehs Exited	965	912	955	958
Starting Vehs	9	23	15	15
Ending Vehs	16	12	10	14
Travel Distance (mi)	506	478	496	502
Travel Time (hr)	17.7	16.5	17.3	17.5
Total Delay (hr)	1.8	1.5	1.8	1.7
Total Stops	482	438	447	465
Fuel Used (gal)	16.2	15.3	15.9	16.1

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Growth Factors.	
No data recorded this interval.	

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	6	7
Vehs Entered	938	919	985	984	957	927	1009
Vehs Exited	944	915	992	992	966	929	1003
Starting Vehs	21	15	28	21	28	17	12
Ending Vehs	15	19	21	13	19	15	18
Travel Distance (mi)	503	485	522	521	506	480	521
Travel Time (hr)	17.4	16.8	18.3	18.2	17.5	16.5	18.5
Total Delay (hr)	1.6	1.7	1.9	1.9	1.7	1.5	2.0
Total Stops	456	442	476	485	477	455	488
Fuel Used (gal)	16.0	15.5	16.8	17.0	16.1	15.1	16.9

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	8	9	10	Avg
Vehs Entered	972	901	950	953
Vehs Exited	965	912	955	958
Starting Vehs	9	23	15	15
Ending Vehs	16	12	10	14
Travel Distance (mi)	506	478	496	502
Travel Time (hr)	17.7	16.5	17.3	17.5
Total Delay (hr)	1.8	1.5	1.8	1.7
Total Stops	482	438	447	465
Fuel Used (gal)	16.2	15.3	15.9	16.1

3: Route 26 & Blackstrap Rd/Skillin Rd Performance by lane

Lane	EB	WB	NB	SB	All
Movements Served	LTR	LTR	LTR	LTR	
Denied Del/Veh (s)					0.1
Total Del/Veh (s)	9.6	8.9	1.1	2.1	4.7

6: Route 26 & Site Drive Performance by lane

Lane	WB	NB	SB	All
Movements Served	LR	TR	LT	
Denied Del/Veh (s)				0.1
Total Del/Veh (s)	5.9	1.0	1.0	1.6

7: Site Drive & Skillin Rd Performance by lane

Lane	EB	WB	NB	All
Movements Served	TR	LT	LR	
Denied Del/Veh (s)				0.1
Total Del/Veh (s)	1.2	1.5	3.6	1.6

Total Network Performance

Denied Del/Veh (s)	0.2
Total Del/Veh (s)	6.3

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Intersection: 3: Route 26 & Blackstrap Rd/Skillin Rd

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (ft)	117	97	76	71
Average Queue (ft)	56	45	11	11
95th Queue (ft)	92	76	45	44
Link Distance (ft)	1767	110	127	1360
Upstream Blk Time (%)	0			
Queuing Penalty (veh)	0			
Storage Bay Dist (ft)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 6: Route 26 & Site Drive

Movement	WB	SB
Directions Served	LR	LT
Maximum Queue (ft)	89	77
Average Queue (ft)	39	12
95th Queue (ft)	73	48
Link Distance (ft)	223	127
Upstream Blk Time (%)	0	
Queuing Penalty (veh)	0	
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 7: Site Drive & Skillin Rd

Movement	EB	WB	NB
Directions Served	TR	LT	LR
Maximum Queue (ft)	5	40	65
Average Queue (ft)	0	5	23
95th Queue (ft)	4	25	52
Link Distance (ft)	110	1892	120
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Network Summary

Network wide Queuing Penalty: 0

Summary of All Intervals

Run Number	1	2	3	4	5	6	7
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70	70	70	70
Time Recorded (min)	60	60	60	60	60	60	60
# of Intervals	2	2	2	2	2	2	2
# of Recorded Intervals	1	1	1	1	1	1	1
Vehs Entered	938	919	985	984	957	927	1009
Vehs Exited	944	915	992	992	966	929	1003
Starting Vehs	21	15	28	21	28	17	12
Ending Vehs	15	19	21	13	19	15	18
Travel Distance (mi)	503	485	522	521	506	480	521
Travel Time (hr)	17.4	16.8	18.3	18.2	17.5	16.5	18.5
Total Delay (hr)	1.6	1.7	1.9	1.9	1.7	1.5	2.0
Total Stops	456	442	476	485	477	455	488
Fuel Used (gal)	16.0	15.5	16.8	17.0	16.1	15.1	16.9

Summary of All Intervals

Run Number	8	9	10	Avg
Start Time	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70
Time Recorded (min)	60	60	60	60
# of Intervals	2	2	2	2
# of Recorded Intervals	1	1	1	1
Vehs Entered	972	901	950	953
Vehs Exited	965	912	955	958
Starting Vehs	9	23	15	15
Ending Vehs	16	12	10	14
Travel Distance (mi)	506	478	496	502
Travel Time (hr)	17.7	16.5	17.3	17.5
Total Delay (hr)	1.8	1.5	1.8	1.7
Total Stops	482	438	447	465
Fuel Used (gal)	16.2	15.3	15.9	16.1

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Growth Factors.	
No data recorded this interval.	

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	6	7
Vehs Entered	938	919	985	984	957	927	1009
Vehs Exited	944	915	992	992	966	929	1003
Starting Vehs	21	15	28	21	28	17	12
Ending Vehs	15	19	21	13	19	15	18
Travel Distance (mi)	503	485	522	521	506	480	521
Travel Time (hr)	17.4	16.8	18.3	18.2	17.5	16.5	18.5
Total Delay (hr)	1.6	1.7	1.9	1.9	1.7	1.5	2.0
Total Stops	456	442	476	485	477	455	488
Fuel Used (gal)	16.0	15.5	16.8	17.0	16.1	15.1	16.9

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	8	9	10	Avg
Vehs Entered	972	901	950	953
Vehs Exited	965	912	955	958
Starting Vehs	9	23	15	15
Ending Vehs	16	12	10	14
Travel Distance (mi)	506	478	496	502
Travel Time (hr)	17.7	16.5	17.3	17.5
Total Delay (hr)	1.8	1.5	1.8	1.7
Total Stops	482	438	447	465
Fuel Used (gal)	16.2	15.3	15.9	16.1

3: Route 26 & Blackstrap Rd/Skillin Rd Performance by approach

Approach	EB	WB	NB	SB	All
Denied Del/Veh (s)	0.2	0.0	0.0	0.3	0.1
Total Del/Veh (s)	9.6	9.0	1.1	2.1	4.7

6: Route 26 & Site Drive Performance by approach

Approach	WB	NB	SB	All
Denied Del/Veh (s)	0.2	0.2	0.0	0.1
Total Del/Veh (s)	6.0	1.0	1.0	1.6

7: Site Drive & Skillin Rd Performance by approach

Approach	EB	WB	NB	All
Denied Del/Veh (s)	0.0	0.2	0.1	0.1
Total Del/Veh (s)	1.2	1.5	3.6	1.6

Total Network Performance

Denied Del/Veh (s)	0.2
Total Del/Veh (s)	6.3

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Intersection: 3: Route 26 & Blackstrap Rd/Skillin Rd

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (ft)	117	97	76	71
Average Queue (ft)	56	45	11	11
95th Queue (ft)	92	76	45	44
Link Distance (ft)	1767	110	127	1360
Upstream Blk Time (%)	0			
Queuing Penalty (veh)	0			
Storage Bay Dist (ft)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 6: Route 26 & Site Drive

Movement	WB	SB
Directions Served	LR	LT
Maximum Queue (ft)	89	77
Average Queue (ft)	39	12
95th Queue (ft)	73	48
Link Distance (ft)	223	127
Upstream Blk Time (%)	0	
Queuing Penalty (veh)	0	
Storage Bay Dist (ft)		
Storage Blk Time (%)		
Queuing Penalty (veh)		

Intersection: 7: Site Drive & Skillin Rd

Movement	EB	WB	NB
Directions Served	TR	LT	LR
Maximum Queue (ft)	5	40	65
Average Queue (ft)	0	5	23
95th Queue (ft)	4	25	52
Link Distance (ft)	110	1892	120
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Network Summary

Network wide Queuing Penalty: 0

Summary of All Intervals

Run Number	1	2	3	4	5	6	7
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70	70	70	70
Time Recorded (min)	60	60	60	60	60	60	60
# of Intervals	2	2	2	2	2	2	2
# of Recorded Intervals	1	1	1	1	1	1	1
Vehs Entered	1165	1203	1122	1200	1149	1188	1232
Vehs Exited	1165	1191	1124	1190	1151	1185	1233
Starting Vehs	21	14	25	16	26	22	25
Ending Vehs	21	26	23	26	24	25	24
Travel Distance (mi)	610	627	593	626	604	629	641
Travel Time (hr)	21.7	22.5	21.0	22.2	21.4	22.5	22.9
Total Delay (hr)	2.5	2.7	2.3	2.5	2.4	2.8	2.7
Total Stops	517	521	498	535	490	547	554
Fuel Used (gal)	19.8	20.2	19.0	20.1	19.3	20.3	20.5

Summary of All Intervals

Run Number	8	9	10	Avg
Start Time	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70
Time Recorded (min)	60	60	60	60
# of Intervals	2	2	2	2
# of Recorded Intervals	1	1	1	1
Vehs Entered	1163	1154	1150	1174
Vehs Exited	1160	1164	1149	1171
Starting Vehs	16	26	24	19
Ending Vehs	19	16	25	18
Travel Distance (mi)	611	605	607	615
Travel Time (hr)	21.7	21.6	21.4	21.9
Total Delay (hr)	2.5	2.6	2.4	2.5
Total Stops	517	530	501	523
Fuel Used (gal)	19.4	19.3	19.4	19.7

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Growth Factors.	
No data recorded this interval.	

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	6	7
Vehs Entered	1165	1203	1122	1200	1149	1188	1232
Vehs Exited	1165	1191	1124	1190	1151	1185	1233
Starting Vehs	21	14	25	16	26	22	25
Ending Vehs	21	26	23	26	24	25	24
Travel Distance (mi)	610	627	593	626	604	629	641
Travel Time (hr)	21.7	22.5	21.0	22.2	21.4	22.5	22.9
Total Delay (hr)	2.5	2.7	2.3	2.5	2.4	2.8	2.7
Total Stops	517	521	498	535	490	547	554
Fuel Used (gal)	19.8	20.2	19.0	20.1	19.3	20.3	20.5

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	8	9	10	Avg
Vehs Entered	1163	1154	1150	1174
Vehs Exited	1160	1164	1149	1171
Starting Vehs	16	26	24	19
Ending Vehs	19	16	25	18
Travel Distance (mi)	611	605	607	615
Travel Time (hr)	21.7	21.6	21.4	21.9
Total Delay (hr)	2.5	2.6	2.4	2.5
Total Stops	517	530	501	523
Fuel Used (gal)	19.4	19.3	19.4	19.7

3: Route 26 & Blackstrap Rd/Skillin Rd Performance by lane

Lane	EB	WB	NB	SB	All
Movements Served	LTR	LTR	LTR	LTR	
Denied Del/Veh (s)					0.1
Total Del/Veh (s)	12.2	11.5	1.6	2.1	4.8

6: Route 26 & Site Drive Performance by lane

Lane	WB	NB	SB	All
Movements Served	LR	TR	LT	
Denied Del/Veh (s)				0.2
Total Del/Veh (s)	8.4	1.9	1.3	2.5

7: Site Drive & Skillin Rd Performance by lane

Lane	EB	WB	NB	All
Movements Served	TR	LT	LR	
Denied Del/Veh (s)				0.1
Total Del/Veh (s)	1.1	1.9	4.1	1.7

Total Network Performance

Denied Del/Veh (s)	0.3
Total Del/Veh (s)	7.4

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Intersection: 3: Route 26 & Blackstrap Rd/Skillin Rd

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (ft)	111	114	82	67
Average Queue (ft)	53	56	22	17
95th Queue (ft)	91	93	60	50
Link Distance (ft)	1767	110	127	1360
Upstream Blk Time (%)		1	0	
Queuing Penalty (veh)		1	0	
Storage Bay Dist (ft)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 6: Route 26 & Site Drive

Movement	WB	NB	SB
Directions Served	LR	TR	LT
Maximum Queue (ft)	96	12	73
Average Queue (ft)	40	0	16
95th Queue (ft)	71	5	51
Link Distance (ft)	223	1095	127
Upstream Blk Time (%)			0
Queuing Penalty (veh)			0
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 7: Site Drive & Skillin Rd

Movement	EB	WB	NB
Directions Served	TR	LT	LR
Maximum Queue (ft)	5	49	54
Average Queue (ft)	0	5	24
95th Queue (ft)	5	28	49
Link Distance (ft)	110	1892	120
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Network Summary

Network wide Queuing Penalty: 1

Summary of All Intervals

Run Number	1	2	3	4	5	6	7
Start Time	6:50	6:50	6:50	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70	70	70	70
Time Recorded (min)	60	60	60	60	60	60	60
# of Intervals	2	2	2	2	2	2	2
# of Recorded Intervals	1	1	1	1	1	1	1
Vehs Entered	1165	1203	1122	1200	1149	1188	1232
Vehs Exited	1165	1191	1124	1190	1151	1185	1233
Starting Vehs	21	14	25	16	26	22	25
Ending Vehs	21	26	23	26	24	25	24
Travel Distance (mi)	610	627	593	626	604	629	641
Travel Time (hr)	21.7	22.5	21.0	22.2	21.4	22.5	22.9
Total Delay (hr)	2.5	2.7	2.3	2.5	2.4	2.8	2.7
Total Stops	517	521	498	535	490	547	554
Fuel Used (gal)	19.8	20.2	19.0	20.1	19.3	20.3	20.5

Summary of All Intervals

Run Number	8	9	10	Avg
Start Time	6:50	6:50	6:50	6:50
End Time	8:00	8:00	8:00	8:00
Total Time (min)	70	70	70	70
Time Recorded (min)	60	60	60	60
# of Intervals	2	2	2	2
# of Recorded Intervals	1	1	1	1
Vehs Entered	1163	1154	1150	1174
Vehs Exited	1160	1164	1149	1171
Starting Vehs	16	26	24	19
Ending Vehs	19	16	25	18
Travel Distance (mi)	611	605	607	615
Travel Time (hr)	21.7	21.6	21.4	21.9
Total Delay (hr)	2.5	2.6	2.4	2.5
Total Stops	517	530	501	523
Fuel Used (gal)	19.4	19.3	19.4	19.7

Interval #0 Information Seeding

Start Time	6:50
End Time	7:00
Total Time (min)	10
Volumes adjusted by Growth Factors.	
No data recorded this interval.	

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	1	2	3	4	5	6	7
Vehs Entered	1165	1203	1122	1200	1149	1188	1232
Vehs Exited	1165	1191	1124	1190	1151	1185	1233
Starting Vehs	21	14	25	16	26	22	25
Ending Vehs	21	26	23	26	24	25	24
Travel Distance (mi)	610	627	593	626	604	629	641
Travel Time (hr)	21.7	22.5	21.0	22.2	21.4	22.5	22.9
Total Delay (hr)	2.5	2.7	2.3	2.5	2.4	2.8	2.7
Total Stops	517	521	498	535	490	547	554
Fuel Used (gal)	19.8	20.2	19.0	20.1	19.3	20.3	20.5

Interval #1 Information Off-Peak

Start Time	7:00
End Time	8:00
Total Time (min)	60

Volumes adjusted by Growth Factors.

Run Number	8	9	10	Avg
Vehs Entered	1163	1154	1150	1174
Vehs Exited	1160	1164	1149	1171
Starting Vehs	16	26	24	19
Ending Vehs	19	16	25	18
Travel Distance (mi)	611	605	607	615
Travel Time (hr)	21.7	21.6	21.4	21.9
Total Delay (hr)	2.5	2.6	2.4	2.5
Total Stops	517	530	501	523
Fuel Used (gal)	19.4	19.3	19.4	19.7

3: Route 26 & Blackstrap Rd/Skillin Rd Performance by approach

Approach	EB	WB	NB	SB	All
Denied Del/Veh (s)	0.2	0.0	0.0	0.2	0.1
Total Del/Veh (s)	12.2	11.5	1.6	2.1	4.8

6: Route 26 & Site Drive Performance by approach

Approach	WB	NB	SB	All
Denied Del/Veh (s)	0.1	0.4	0.0	0.2
Total Del/Veh (s)	8.3	1.9	1.3	2.5

7: Site Drive & Skillin Rd Performance by approach

Approach	EB	WB	NB	All
Denied Del/Veh (s)	0.0	0.2	0.1	0.1
Total Del/Veh (s)	1.1	1.9	4.0	1.7

Total Network Performance

Denied Del/Veh (s)	0.3
Total Del/Veh (s)	7.4

Queuing and Blocking Report

2024 Build PM

10/31/2023

Intersection: 3: Route 26 & Blackstrap Rd/Skillin Rd

Movement	EB	WB	NB	SB
Directions Served	LTR	LTR	LTR	LTR
Maximum Queue (ft)	111	114	82	67
Average Queue (ft)	53	56	22	17
95th Queue (ft)	91	93	60	50
Link Distance (ft)	1767	110	127	1360
Upstream Blk Time (%)		1	0	
Queuing Penalty (veh)		1	0	
Storage Bay Dist (ft)				
Storage Blk Time (%)				
Queuing Penalty (veh)				

Intersection: 6: Route 26 & Site Drive

Movement	WB	NB	SB
Directions Served	LR	TR	LT
Maximum Queue (ft)	96	12	73
Average Queue (ft)	40	0	16
95th Queue (ft)	71	5	51
Link Distance (ft)	223	1095	127
Upstream Blk Time (%)			0
Queuing Penalty (veh)			0
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

Intersection: 7: Site Drive & Skillin Rd

Movement	EB	WB	NB
Directions Served	TR	LT	LR
Maximum Queue (ft)	5	49	54
Average Queue (ft)	0	5	24
95th Queue (ft)	5	28	49
Link Distance (ft)	110	1892	120
Upstream Blk Time (%)			
Queuing Penalty (veh)			
Storage Bay Dist (ft)			
Storage Blk Time (%)			
Queuing Penalty (veh)			

















Network Summary

Network wide Queuing Penalty: 1

Lanes, Volumes, Timings










3: Route 26 & Blackstrap Rd/Skillin Rd

11/15/2023

												
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	44	67	73	48	45	20	31	108	34	63	212	33
Future Volume (vph)	44	67	73	48	45	20	31	108	34	63	212	33
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.946			0.976			0.973			0.985	
Flt Protected		0.988			0.979			0.991			0.990	
Satd. Flow (prot)	0	1691	0	0	1713	0	0	1621	0	0	1732	0
Flt Permitted		0.988			0.979			0.991			0.990	
Satd. Flow (perm)	0	1691	0	0	1713	0	0	1621	0	0	1732	0
Link Speed (mph)		40			35			35			35	
Link Distance (ft)		1795			174			178			1389	
Travel Time (s)		30.6			3.4			3.5			27.1	
Peak Hour Factor	0.83	0.83	0.83	0.69	0.69	0.69	0.92	0.92	0.92	0.77	0.77	0.77
Heavy Vehicles (%)	5%	5%	5%	6%	6%	6%	13%	13%	13%	7%	7%	7%
Adj. Flow (vph)	53	81	88	70	65	29	34	117	37	82	275	43
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	222	0	0	164	0	0	188	0	0	400	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)		0			0			0			0	
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane												
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		9	15		9	15		9	15		9
Sign Control		Stop			Stop			Free			Free	
Intersection Summary												
Area Type:	Other											
Control Type:	Unsignalized											
Intersection Capacity Utilization	41.5%						ICU Level of Service A					
Analysis Period (min)	15											










Lanes, Volumes, Timings
6: Route 26 & Site Drive

11/15/2023

						
Lane Group	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Volume (vph)	0	0	173	0	0	333
Future Volume (vph)	0	0	173	0	0	333
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt						
Flt Protected						
Satd. Flow (prot)	1681	0	1681	0	0	1776
Flt Permitted						
Satd. Flow (perm)	1681	0	1681	0	0	1776
Link Speed (mph)	25		35			35
Link Distance (ft)	252		1129			178
Travel Time (s)	6.9		22.0			3.5
Peak Hour Factor	0.92	0.92	0.92	0.92	0.77	0.77
Heavy Vehicles (%)	13%	13%	13%	13%	7%	7%
Adj. Flow (vph)	0	0	188	0	0	432
Shared Lane Traffic (%)						
Lane Group Flow (vph)	0	0	188	0	0	432
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Right	Left	Left
Median Width(ft)	12		0			0
Link Offset(ft)	0		0			0
Crosswalk Width(ft)	16		16			16
Two way Left Turn Lane						
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15	9		9	15	
Sign Control	Stop		Free			Free
Intersection Summary						
Area Type:	Other					
Control Type:	Unsignalized					
Intersection Capacity Utilization	20.9%			ICU Level of Service A		
Analysis Period (min)	15					

Lanes, Volumes, Timings
7: Site Drive & Skillin Rd

















11/15/2023

						
Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Volume (vph)	164	0	0	113	0	0
Future Volume (vph)	164	0	0	113	0	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt						
Flt Protected						
Satd. Flow (prot)	1810	0	0	1792	1792	0
Flt Permitted						
Satd. Flow (perm)	1810	0	0	1792	1792	0
Link Speed (mph)	30			35	30	
Link Distance (ft)	174			1915	149	
Travel Time (s)	4.0			37.3	3.4	
Peak Hour Factor	0.83	0.83	0.69	0.69	0.60	0.60
Heavy Vehicles (%)	5%	5%	6%	6%	6%	6%
Adj. Flow (vph)	198	0	0	164	0	0
Shared Lane Traffic (%)						
Lane Group Flow (vph)	198	0	0	164	0	0
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Left	Left	Right
Median Width(ft)	0			0	12	
Link Offset(ft)	0			0	0	
Crosswalk Width(ft)	16			16	16	
Two way Left Turn Lane						
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)		9	15		15	9
Sign Control	Free			Free	Stop	
Intersection Summary						
Area Type:	Other					
Control Type: Unsignalized						
Intersection Capacity Utilization 12.0%				ICU Level of Service A		
Analysis Period (min) 15						

Lanes, Volumes, Timings










3: Route 26 & Blackstrap Rd/Skillin Rd

11/15/2023

												
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	30	70	38	26	88	46	77	307	65	42	141	37
Future Volume (vph)	30	70	38	26	88	46	77	307	65	42	141	37
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.963			0.962			0.981			0.977	
Flt Protected		0.989			0.992			0.991			0.991	
Satd. Flow (prot)	0	1723	0	0	1760	0	0	1793	0	0	1821	0
Flt Permitted		0.989			0.992			0.991			0.991	
Satd. Flow (perm)	0	1723	0	0	1760	0	0	1793	0	0	1821	0
Link Speed (mph)		40			35			35			35	
Link Distance (ft)		1795			174			178			1389	
Travel Time (s)		30.6			3.4			3.5			27.1	
Peak Hour Factor	0.76	0.76	0.76	0.93	0.93	0.93	0.95	0.95	0.95	0.84	0.84	0.84
Heavy Vehicles (%)	5%	5%	5%	3%	3%	3%	3%	3%	3%	1%	1%	1%
Adj. Flow (vph)	39	92	50	28	95	49	81	323	68	50	168	44
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	181	0	0	172	0	0	472	0	0	262	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)		0			0			0			0	
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane												
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		9	15		9	15		9	15		9
Sign Control		Stop			Stop			Free			Free	
Intersection Summary												
Area Type:	Other											
Control Type:	Unsignalized											
Intersection Capacity Utilization	49.7%						ICU Level of Service A					
Analysis Period (min)	15											

Lanes, Volumes, Timings
6: Route 26 & Site Drive

11/15/2023

						
Lane Group	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Volume (vph)	0	0	449	0	0	205
Future Volume (vph)	0	0	449	0	0	205
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt						
Flt Protected						
Satd. Flow (prot)	1845	0	1845	0	0	1881
Flt Permitted						
Satd. Flow (perm)	1845	0	1845	0	0	1881
Link Speed (mph)	25		35			35
Link Distance (ft)	252		1129			178
Travel Time (s)	6.9		22.0			3.5
Peak Hour Factor	0.92	0.92	0.92	0.92	0.77	0.77
Heavy Vehicles (%)	3%	3%	3%	3%	1%	1%
Adj. Flow (vph)	0	0	488	0	0	266
Shared Lane Traffic (%)						
Lane Group Flow (vph)	0	0	488	0	0	266
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Right	Left	Left
Median Width(ft)	12		0			0
Link Offset(ft)	0		0			0
Crosswalk Width(ft)	16		16			16
Two way Left Turn Lane						
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15	9		9	15	
Sign Control	Stop		Free			Free
Intersection Summary						
Area Type:	Other					
Control Type:	Unsignalized					
Intersection Capacity Utilization	27.0%			ICU Level of Service A		
Analysis Period (min)	15					

Lanes, Volumes, Timings
7: Site Drive & Skillin Rd

















11/15/2023

	→	↘	↙	←	↖	↗
Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	↰			↱	↘↙	
Traffic Volume (vph)	177	0	0	160	0	0
Future Volume (vph)	177	0	0	160	0	0
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt						
Flt Protected						
Satd. Flow (prot)	1810	0	0	1845	1845	0
Flt Permitted						
Satd. Flow (perm)	1810	0	0	1845	1845	0
Link Speed (mph)	30			35	30	
Link Distance (ft)	174			1915	149	
Travel Time (s)	4.0			37.3	3.4	
Peak Hour Factor	0.76	0.76	0.93	0.93	0.60	0.60
Heavy Vehicles (%)	5%	5%	3%	3%	3%	3%
Adj. Flow (vph)	233	0	0	172	0	0
Shared Lane Traffic (%)						
Lane Group Flow (vph)	233	0	0	172	0	0
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Left	Left	Right
Median Width(ft)	0			0	12	
Link Offset(ft)	0			0	0	
Crosswalk Width(ft)	16			16	16	
Two way Left Turn Lane						
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)		9	15		15	9
Sign Control	Free			Free	Stop	
Intersection Summary						
Area Type:	Other					
Control Type: Unsignalized						
Intersection Capacity Utilization 12.6%				ICU Level of Service A		
Analysis Period (min) 15						

Lanes, Volumes, Timings

3: Route 26 & Blackstrap Rd/Skillin Rd










11/15/2023

												
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	44	71	77	48	53	20	32	119	34	63	224	33
Future Volume (vph)	44	71	77	48	53	20	32	119	34	63	224	33
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.946			0.978			0.975			0.986	
Flt Protected		0.989			0.981			0.991			0.990	
Satd. Flow (prot)	0	1693	0	0	1720	0	0	1625	0	0	1733	0
Flt Permitted		0.989			0.981			0.991			0.990	
Satd. Flow (perm)	0	1693	0	0	1720	0	0	1625	0	0	1733	0
Link Speed (mph)		40			35			35			35	
Link Distance (ft)		1795			174			178			1389	
Travel Time (s)		30.6			3.4			3.5			27.1	
Peak Hour Factor	0.83	0.83	0.83	0.69	0.69	0.69	0.92	0.92	0.92	0.77	0.77	0.77
Heavy Vehicles (%)	5%	5%	5%	6%	6%	6%	13%	13%	13%	7%	7%	7%
Adj. Flow (vph)	53	86	93	70	77	29	35	129	37	82	291	43
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	232	0	0	176	0	0	201	0	0	416	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)		0			0			0			0	
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane												
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		9	15		9	15		9	15		9
Sign Control		Stop			Stop			Free			Free	
Intersection Summary												
Area Type:	Other											
Control Type:	Unsignalized											
Intersection Capacity Utilization	43.0%						ICU Level of Service A					
Analysis Period (min)	15											

Lanes, Volumes, Timings

6: Route 26 & Site Drive










11/15/2023

						
Lane Group	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Volume (vph)	49	27	158	41	45	304
Future Volume (vph)	49	27	158	41	45	304
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.952		0.972			
Flt Protected	0.969					0.994
Satd. Flow (prot)	1551	0	1634	0	0	1765
Flt Permitted	0.969					0.994
Satd. Flow (perm)	1551	0	1634	0	0	1765
Link Speed (mph)	25		35			35
Link Distance (ft)	252		1129			178
Travel Time (s)	6.9		22.0			3.5
Peak Hour Factor	0.92	0.92	0.92	0.92	0.77	0.77
Heavy Vehicles (%)	13%	13%	13%	13%	7%	7%
Adj. Flow (vph)	53	29	172	45	58	395
Shared Lane Traffic (%)						
Lane Group Flow (vph)	82	0	217	0	0	453
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Right	Left	Left
Median Width(ft)	12		0			0
Link Offset(ft)	0		0			0
Crosswalk Width(ft)	16		16			16
Two way Left Turn Lane						
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15	9		9	15	
Sign Control	Stop		Free			Free
Intersection Summary						
Area Type:	Other					
Control Type:	Unsignalized					
Intersection Capacity Utilization	43.7%			ICU Level of Service A		
Analysis Period (min)	15					

Lanes, Volumes, Timings

7: Site Drive & Skillin Rd

















11/15/2023

						
Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations						
Traffic Volume (vph)	157	11	20	105	16	21
Future Volume (vph)	157	11	20	105	16	21
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.991				0.924	
Flt Protected				0.992	0.979	
Satd. Flow (prot)	1793	0	0	1778	1621	0
Flt Permitted				0.992	0.979	
Satd. Flow (perm)	1793	0	0	1778	1621	0
Link Speed (mph)	30			35	30	
Link Distance (ft)	174			1915	149	
Travel Time (s)	4.0			37.3	3.4	
Peak Hour Factor	0.83	0.83	0.69	0.69	0.60	0.60
Heavy Vehicles (%)	5%	5%	6%	6%	6%	6%
Adj. Flow (vph)	189	13	29	152	27	35
Shared Lane Traffic (%)						
Lane Group Flow (vph)	202	0	0	181	62	0
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Left	Left	Right
Median Width(ft)	0			0	12	
Link Offset(ft)	0			0	0	
Crosswalk Width(ft)	16			16	16	
Two way Left Turn Lane						
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)		9	15		15	9
Sign Control	Free			Free	Stop	
Intersection Summary						
Area Type:	Other					
Control Type:	Unsignalized					
Intersection Capacity Utilization	28.9%			ICU Level of Service A		
Analysis Period (min)	15					

Lanes, Volumes, Timings

3: Route 26 & Blackstrap Rd/Skillin Rd










11/15/2023

												
Lane Group	EBL	EBT	EBR	WBL	WBT	WBR	NBL	NBT	NBR	SBL	SBT	SBR
Lane Configurations												
Traffic Volume (vph)	30	75	43	26	95	46	80	322	65	42	156	37
Future Volume (vph)	30	75	43	26	95	46	80	322	65	42	156	37
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Frt		0.961			0.963			0.981			0.979	
Flt Protected		0.990			0.992			0.992			0.991	
Satd. Flow (prot)	0	1722	0	0	1762	0	0	1795	0	0	1825	0
Flt Permitted		0.990			0.992			0.992			0.991	
Satd. Flow (perm)	0	1722	0	0	1762	0	0	1795	0	0	1825	0
Link Speed (mph)		40			35			35			35	
Link Distance (ft)		1795			174			178			1389	
Travel Time (s)		30.6			3.4			3.5			27.1	
Peak Hour Factor	0.76	0.76	0.76	0.93	0.93	0.93	0.95	0.95	0.95	0.84	0.84	0.84
Heavy Vehicles (%)	5%	5%	5%	3%	3%	3%	3%	3%	3%	1%	1%	1%
Adj. Flow (vph)	39	99	57	28	102	49	84	339	68	50	186	44
Shared Lane Traffic (%)												
Lane Group Flow (vph)	0	195	0	0	179	0	0	491	0	0	280	0
Enter Blocked Intersection	No	No	No	No	No	No	No	No	No	No	No	No
Lane Alignment	Left	Left	Right	Left	Left	Right	Left	Left	Right	Left	Left	Right
Median Width(ft)		0			0			0			0	
Link Offset(ft)		0			0			0			0	
Crosswalk Width(ft)		16			16			16			16	
Two way Left Turn Lane												
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15		9	15		9	15		9	15		9
Sign Control		Stop			Stop			Free			Free	
Intersection Summary												
Area Type:	Other											
Control Type:	Unsignalized											
Intersection Capacity Utilization	52.3%						ICU Level of Service A					
Analysis Period (min)	15											

Lanes, Volumes, Timings

6: Route 26 & Site Drive

11/15/2023

						
Lane Group	WBL	WBR	NBT	NBR	SBL	SBT
Lane Configurations						
Traffic Volume (vph)	43	53	414	64	33	192
Future Volume (vph)	43	53	414	64	33	192
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.925		0.982			
Flt Protected	0.978					0.993
Satd. Flow (prot)	1669	0	1811	0	0	1868
Flt Permitted	0.978					0.993
Satd. Flow (perm)	1669	0	1811	0	0	1868
Link Speed (mph)	25		35			35
Link Distance (ft)	252		1129			178
Travel Time (s)	6.9		22.0			3.5
Peak Hour Factor	0.92	0.92	0.92	0.92	0.77	0.77
Heavy Vehicles (%)	3%	3%	3%	3%	1%	1%
Adj. Flow (vph)	47	58	450	70	43	249
Shared Lane Traffic (%)						
Lane Group Flow (vph)	105	0	520	0	0	292
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Right	Left	Left
Median Width(ft)	12		0			0
Link Offset(ft)	0		0			0
Crosswalk Width(ft)	16		16			16
Two way Left Turn Lane						
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)	15	9		9	15	
Sign Control	Stop		Free			Free
Intersection Summary						
Area Type:	Other					
Control Type:	Unsignalized					
Intersection Capacity Utilization	50.4%			ICU Level of Service A		
Analysis Period (min)	15					

Lanes, Volumes, Timings

7: Site Drive & Skillin Rd

11/15/2023

	→	↘	↙	←	↖	↗
Lane Group	EBT	EBR	WBL	WBT	NBL	NBR
Lane Configurations	↰			↱	↘↙	
Traffic Volume (vph)	170	12	23	152	15	22
Future Volume (vph)	170	12	23	152	15	22
Ideal Flow (vphpl)	1900	1900	1900	1900	1900	1900
Lane Util. Factor	1.00	1.00	1.00	1.00	1.00	1.00
Frt	0.991				0.919	
Flt Protected				0.993	0.980	
Satd. Flow (prot)	1793	0	0	1832	1661	0
Flt Permitted				0.993	0.980	
Satd. Flow (perm)	1793	0	0	1832	1661	0
Link Speed (mph)	30			35	30	
Link Distance (ft)	174			1915	149	
Travel Time (s)	4.0			37.3	3.4	
Peak Hour Factor	0.76	0.76	0.93	0.93	0.60	0.60
Heavy Vehicles (%)	5%	5%	3%	3%	3%	3%
Adj. Flow (vph)	224	16	25	163	25	37
Shared Lane Traffic (%)						
Lane Group Flow (vph)	240	0	0	188	62	0
Enter Blocked Intersection	No	No	No	No	No	No
Lane Alignment	Left	Right	Left	Left	Left	Right
Median Width(ft)	0			0	12	
Link Offset(ft)	0			0	0	
Crosswalk Width(ft)	16			16	16	
Two way Left Turn Lane						
Headway Factor	1.00	1.00	1.00	1.00	1.00	1.00
Turning Speed (mph)		9	15		15	9
Sign Control	Free			Free	Stop	
Intersection Summary						
Area Type:	Other					
Control Type:	Unsignalized					
Intersection Capacity Utilization	32.3%			ICU Level of Service A		
Analysis Period (min)	15					



NOT FOR CONSTRUCTION

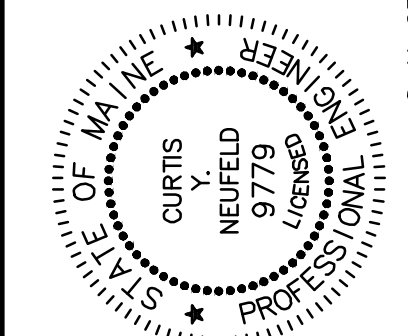
THIS PLAN IS ISSUED FOR REVIEW AND INFORMATION PURPOSES ONLY. THIS PLAN WILL CHANGE AND IS NOT INTENDED FOR PRICING OR CONSTRUCTION.

PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.

SIDEWALK CONCEPT PLAN

PROJECT: RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME 04021

PREPARED FOR: CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086



8-11-23

1.	08-11-23	SUBMITTED FOR MAINEDOT REVIEW
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CYN

PRIORITY
2 MAIN STREET
TOPSHAM, MAINE 04086
(207) 837-6198

SCALE: 1"=30'

FIELD WK:	SCALE: 1"=30'
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DRN BY: CYN	JOB #: 22-RLM-004
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DRN BY: CYN

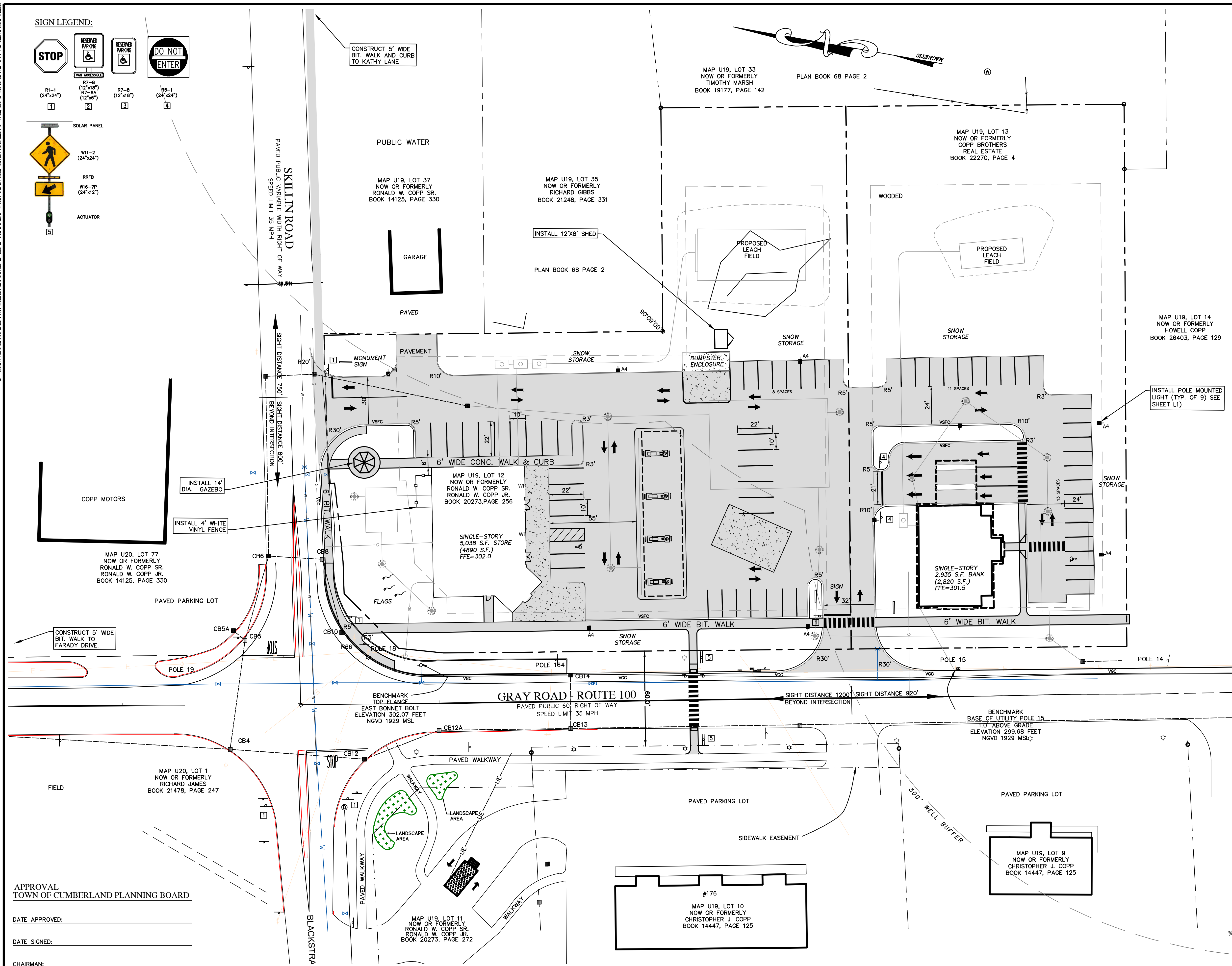
DRN BY: CYN	JOB #
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1"=30'	SHEET:
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1"=30'	SHEET:
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1"=30'	SHEET:
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1"=30'	SHEET:
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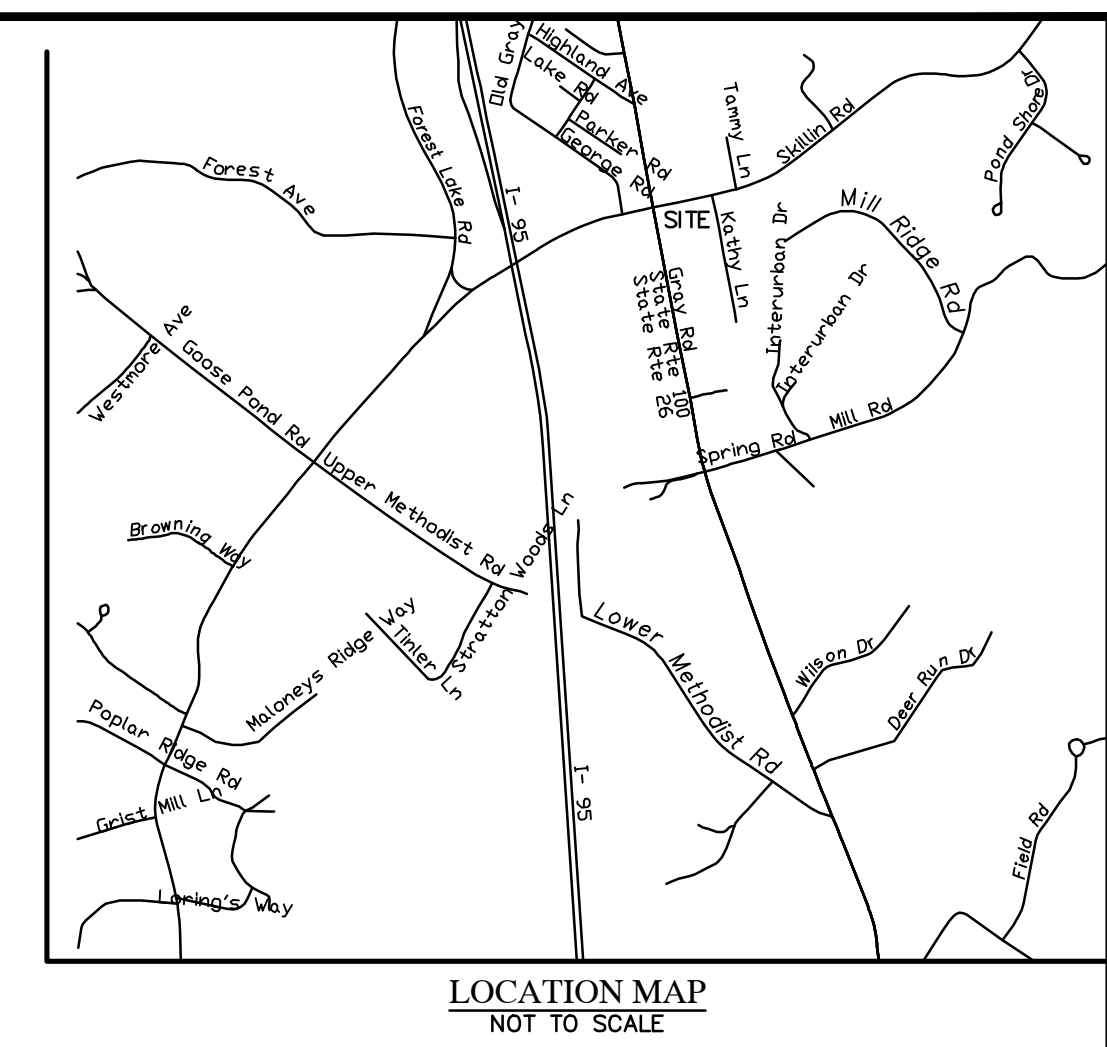


APPROVAL
TOWN OF CUMBERLAND PLANNING BOARD

DATE APPROVED: _____

DATE SIGNED: _____

CHAIRMAN: _____



GENERAL NOTES:

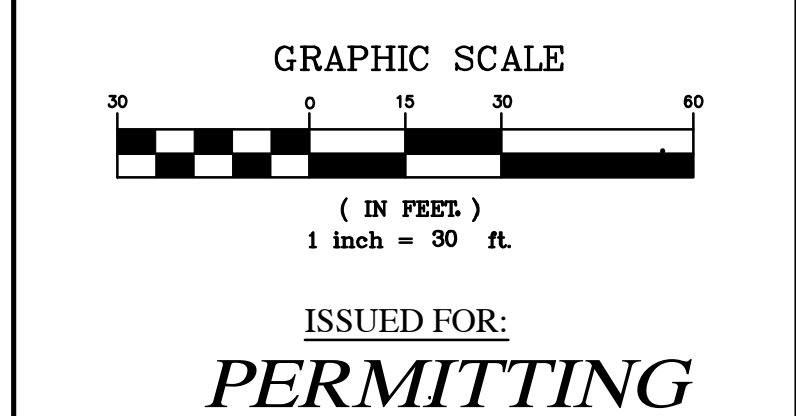
- TITLE REFERENCE FOR SURVEYED PARCEL:**
BK 20273, PG 256 (U19-12)
BK 34640, PG 209 (U19-13)
- PLAN REFERENCE(S):**
(1) EXISTING CONDITIONS SURVEY FOR PRIORITY REAL ESTATE GROUP OF 181 GRAY ROAD, CUMBERLAND, MAINE 04021, PREPARED BY BOUNDARY POINTS, NOT RECORDED.
- AREA INFORMATION:**
LOT AREA: 141,116 S.F. (3.24 ACRES)
- TAX MAP REFERENCE:**
TAX MAP U19, LOT 12 & 13.
- BASIS OF BEARINGS:**
BEARINGS ARE MAINE STATE PLANE, WEST ZONE, NAD 83.
- ELEVATION DATUM:**
NGVD 1929 MSL
- FLOOD ZONE INFORMATION:**
PARCEL IS LOCATED WITHIN ZONE C (AREAS OF MINIMAL FLOODING) OF THE FLOOD INSURANCE RATE MAPS FOR CUMBERLAND COUNTY, MAINE. THE PROJECT IS LOCATED ON PARCEL 15 OF 25 (COMMUNITY PANEL 230162 0015 B, EFF. DATE MAY 19, 1981)
- IMPERVIOUS AREA:**
EXISTING IMPERVIOUS AREA: 94,773 S.F. (2.18 AC)
PROPOSED IMPERVIOUS AREA: 68,232 S.F. (1.57 AC)
NET CHANGE IN IMPERVIOUS AREA: -26,541 S.F. (0.61 AC)

UTILITY NOTES:

- INFORMATION REGARDING THE LOCATION OF EXISTING UNDERGROUND UTILITIES IS A COMPILATION OF THAT FOUND IN THE FIELD AND THAT SHOWN ON A PREVIOUS PLANS, AND SHALL NOT BE CONSIDERED AN AS-BUILT PLAN. CONTRACTOR SHALL BE RESPONSIBLE FOR FIELD VERIFYING UTILITY LOCATIONS PRIOR TO COMMENCING WORK. NOTWITHSTANDING ANY DISCREPANCY BETWEEN UTILITIES AS SHOWN AND AS FOUND, CONTRACTOR SHALL NOTIFY DIG-SAFE PRIOR TO EXCAVATION.
1-888-344-7233

LAYOUT NOTES:

1. ALL DIMENSIONING, UNLESS NOTED OTHERWISE, IS TO THE FACE OF CURB OR FOUNDATION.
2. BOUNDARY INFORMATION ON LAYOUT PLAN IS FOR REFERENCE ONLY, REFER TO CERTIFIED BOUNDARY PLANS FOR BOUNDARY INFORMATION.
3. ALL HANDICAP ACCESSIBLE PARKING SPACES, RAMPS AND SIDEWALKS SHALL BE CONSTRUCTED IN CONFORMANCE WITH THE AMERICANS WITH DISABILITIES ACT (ADA).
4. ALL SITE SIGNAGE AND PAVEMENT MARKINGS SHALL CONFORM TO THE MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES. (MUTCD)
5. BUILDING FOUNDATION SHOWN IS NOT FOR FOUNDATION LAYOUT. COORDINATE SITE WORK WITH ARCHITECTURAL DRAWINGS INCLUDING BUILDING FEATURES AND FOUNDATION PLAN.
6. REFER TO SHEET C4 FOR GRADING AND DRAINAGE INFORMATION.
7. REFER TO SHEET L1 FOR LANDSCAPE INFORMATION.
8. REFER TO SHEET L2 FOR LIGHTING INFORMATION.

[illegible]

PURCHASE AND SALE AGREEMENT
(Commercial Real Estate)

This Agreement is made on this 14th day of March, 2023 (the "Effective Date") by and between **Cumberland Real Estate Group, LLC**, a Maine Limited Liability Company with a mailing address at 2 Main Street, Topsham, Maine 04086 (hereinafter referred to as the "Purchaser"), and **Ronald W. Copp, Sr.** with a mailing address at 187 Gray Rd Cumberland Me 04001 and **Ronald W. Copp, Jr.** with a mailing address at 25 Interurban Dr. Cumberland Me 04001 (hereinafter collectively referred to as the "Seller").

1. **Purchase and Sale.** Subject to the terms and conditions of this Agreement, Seller agrees to sell and convey to Purchaser and Purchaser agrees to purchase from Seller, fee simple absolute title to real estate and buildings located at or near 181 Gray Road, Cumberland, Maine, as more fully described in a Deed of Sale by Personal Representative, Testate, dated September 25, 2003, from William B. Gerry, Personal Representative, to Ronald W. Copp, Sr. and Ronald W. Copp, Jr., recorded in the Cumberland County Registry of Deeds at Book 20273, Page 256, said real estate being more fully described in Exhibit "A" attached hereto and made a part hereof (being the current Town of Cumberland Tax Map U19, Lot 12), together with all rights, privileges, easements, and appurtenances benefitting said real estate (hereinafter collectively referred to as the "Real Property" or the "Real Estate"). For all purposes of this Agreement, the term "Real Estate" and "Real Property" shall be deemed to include the land, structures, and improvements affixed to the Real Estate.

2. **Purchase Price.**

(a) The purchase price for the Real Estate shall be [REDACTED] (the "Purchase Price").

(b) The Purchase Price shall be paid by the Purchaser to the Seller as follows:

(i) Within Three (3) business days subsequent to the Effective Date, the Purchaser shall deliver to the Escrow Agent, hereinafter defined, a deposit of [REDACTED] (the "Deposit"). The Deposit shall be payable to The Bell Firm, P.A., 810 Lisbon Street, P.O. Box 1776, Lewiston, Maine 04241-1776 ("Escrow Agent"). The Deposit shall be held and/or disposed of by the Escrow Agent in accordance with provisions of this Agreement. The Deposit shall be held by the Escrow Agent in a non-interest-bearing account.

(ii) The balance of the Purchase Price ([REDACTED]) shall be paid by the Purchaser to the Seller in lawful currency of the United States in immediately available funds by wire transfer or other means acceptable to Seller.

AS

(iii) The parties hereto acknowledge and agree with the Escrow Agent that the Escrow Agent shall act hereunder as a depository only and shall not be a party to or be bound by any agreement or undertaking which may be evidenced by or arise out of the escrow deposited with it hereunder. The Escrow Agent shall not be responsible or liable in any manner for the identity or rights of any person depositing the Deposit in escrow. The Escrow Agent shall not be liable for any error of judgment or for any act omitted by it in good faith, or for anything which it may in good faith do or refrain from doing in connection herewith. The Escrow Agent is authorized to act on any document believed by it to be genuine and to be signed by the proper party or parties, and will incur no liability in so acting.

In the event of any disagreements or presentation of adverse claims or demands in connection with the Deposit deposited with the Escrow Agent, the Escrow Agent shall at its option be entitled to refuse to comply with any such claims or demands during the continuance of such disagreement and may refrain from delivering any item effected hereby, and in so doing the Escrow Agent shall not become liable to the undersigned, or to any person, due to its failure to comply with any such adverse claim or demand. The Escrow Agent shall be entitled (but not obligated) to continue, without liability, to refrain and refuse to act: (a) until all the rights of the adverse claimants have been finally adjudicated by a court of competent jurisdiction, after which time the Escrow Agent shall be entitled to act in conformity with such adjudication; or (b) until all differences shall have been adjudicated by agreement and the Escrow Agent shall have been notified thereof and shall have been directed in writing signed by the undersigned and by all persons making adverse claims or demands, at which time the Escrow Agent shall be protected in acting in compliance therewith.

Notwithstanding anything elsewhere set forth herein, the Escrow Agent shall not be required to make delivery of the Deposit unless it has been indemnified against any liability for doing so in a manner which it deems satisfactory.

3. **Adjustments.** The following items shall be prorated, adjusted and paid as follows:

(a) All applicable real estate taxes, assessments, and rents affecting the Real Estate shall be apportioned between Seller and Purchaser as of the Closing Date (as hereinafter defined). Utilities shall be prorated up to the date of closing unless otherwise paid for by tenants.

(b) Seller and Purchaser shall each pay their equal share of the real estate transfer taxes.

(c) Each party shall pay all costs and expenses incurred by such party in connection with the transactions contemplated by this Agreement not otherwise adjusted as set forth in this Section or otherwise provided for in this Agreement.

(d) The Purchaser shall be responsible for all costs and expenses associated with its due diligence review. The Seller and the Purchaser shall each be responsible for the payment of costs of their respective legal counsel, tax advisors, and other professionals.

4. **Title.** Seller shall convey the Real Estate to Purchaser by good and sufficient Warranty Deed (the "Deed"), prepared at the Seller's sole expense, conveying good and marketable title to the Real Estate as defined by the standards adopted by the Maine State Bar Association, free and clear of all encumbrances, except for conventional utility easements and such restrictions as would not make the title unmarketable. The title shall also be insurable by any reputable title insurance company licensed to do business in the State of Maine. All costs of title insurance shall be borne by Purchaser. Seller will execute such affidavits as may be required by the applicable title insurance company to cause the deletion of the standard mechanics' lien exception from the to-be issued title insurance policy.

Purchaser may examine, at Purchaser's sole expense, the title to the Real Estate and will report in writing on or before that date which is One Hundred Twenty (120) days from the Effective Date ("Due Diligence Period") any valid objections (hereafter "Exceptions") based on the standards adopted by the Maine State Bar Association. Any Exceptions to the title which would be disclosed by examination of the records shall be deemed to have been accepted by Purchaser if title is transferred to Purchaser without removal of said Exceptions, unless otherwise agreed to in writing and signed by Seller. If Purchaser objects to any Exceptions to the title, Seller shall (i) use all due diligence to remove such exceptions at Seller's own expense within Thirty (30) days thereafter, or (ii) notify the Purchaser that the Seller does not intend to remove said Exceptions. Notwithstanding Seller's due diligence, if such Exceptions objected to by Purchaser cannot be removed within the said Thirty (30) day period, or such additional period as Purchaser in Purchaser's sole discretion may allow, or if the Seller indicates that it does not intend to remove said Exceptions, Purchaser may elect to terminate this Agreement. Purchaser shall notify Seller of such election, in which case the obligations of all parties under this Agreement shall thereupon terminate and the Deposit shall be promptly returned to the Purchaser. Alternatively, Purchaser may elect to purchase the Real Estate under the provisions of this Agreement subject to any title Exceptions which cannot be removed without any adjustment in the Purchase Price.

5. **Due Diligence. Inspections.** The Seller shall, within Five (5) business days from the Effective Date, provide to the Purchaser such information as the Purchaser reasonably requests relating to the Real Estate, provided that said information is within the Seller's possession or control (the "Due Diligence Information"). The Due Diligence period shall be extended by One (1) day for each day that the Seller takes to deliver the Due Diligence Information to the Seller beyond the Five (5) business day period set forth above. All proprietary and confidential information that the Seller provides to the Purchaser relating to the Real Estate shall be used by the Purchaser solely for purposes of the transactions contemplated herein. All such information will be held by the Purchaser in strict confidence and not disclosed to anyone, other than legal counsel, employees and agents on a need-to-know basis, lenders, and third-party due diligence contractors and professionals;

Provided, However, that it shall not be a breach of this covenant in the event of disclosure of any such information if it is or becomes available from other sources which are not subject to an obligation of confidentiality. Notwithstanding anything else set forth herein, nothing shall prohibit the Purchaser from filing or disclosing such information in connection with, and as may be required by, a judicial or regulatory body or law enforcement agency.

During the Due Diligence Period, the Purchaser shall be entitled to conduct such inspections on the Real Estate as the Purchaser, in its sole discretion, shall determine, including, without limitation, general building inspection, sewer disposal, water quality, radon air quality, radon water quality, asbestos air quality, lead-based paint inspections, asbestos inspections, ADA inspections, wetland surveys, environmental inspections, state and local codes, surveys, leases and tenancies, and any and all other inspections which the Purchaser deems just and appropriate. The Purchaser shall indemnify and hold the Seller harmless from any and all injury which the Seller may incur in connection with the Purchaser's inspections on the Real Estate. If the Purchaser is dissatisfied with any of its inspections, in the Purchaser's sole and absolute discretion, the Purchaser shall be entitled to terminate this Agreement on or before the expiration of the Due Diligence Period by notice in writing to the Seller, and the Deposit shall be promptly returned to the Purchaser. If the Purchaser fails to notify the Seller in writing of its election to terminate on or before the expiration of the Due Diligence Period as a result of its due diligence review, then the Purchaser shall be deemed to be satisfied with its due diligence review, and the Purchaser shall have no further right to terminate under this Item 5.

6. **Items to be Delivered to Purchaser from Seller.** Seller shall deliver to Purchaser such information and/or documentation pertaining to the Real Estate as is reasonably requested by Purchaser from time-to-time to the extent the same is in the possession or control of Seller.

7. **Sole Representations and Warranties.** The Seller represents and warrants to the Purchaser that the following are true and correct as of the Effective Date and will be true and correct as of the Closing:

(a) This Agreement is valid, binding, and enforceable against the Seller. Seller has not received any notice from any source claiming or inquiring into the existence of any violations of laws, ordinances, or regulations affecting the Real Estate; and

(b) there is no action, suit, or other proceeding (including condemnation actions) pending or, to the best of Seller's knowledge, threatened against Seller or affecting any portion of the Real Estate in any court or before any arbitrator of any kind or before any governmental body that may materially or adversely affect the Real Estate or the transactions contemplated by this Agreement.

8. **Purchaser Representations and Warranties.** The Purchaser represents and warrants to the Seller that the following are true and correct as of the Effective Date and will be true and correct as of the Closing:



(a) The Purchaser has the requisite power and authority to execute, deliver, and perform its obligations under this Agreement. This Agreement is valid, binding, and enforceable against the Purchaser.

(b) The Purchaser is a Limited Liability Company, duly formed, valid and existing, and in good standing of the laws of the State of Maine.

(c) There are no actions, suits, claims, investigations, or other legal proceedings pending, or to the Purchaser's knowledge, threatened against or by the Purchaser that challenge or seek to prevent, or otherwise delay the consummation of the transactions contemplated herein.

9. **General Covenants and Agreements of Seller.** Seller agrees with Purchaser as follows:

(a) Between the Effective Date and the Closing, Seller shall not, without Purchaser's consent (i) convey or otherwise dispose of any interest in the Real Estate; (ii) mortgage, pledge, lease, or subject to any lien or other encumbrances any interest in the Real Estate which exceed the Purchase Price; (iii) enter into any agreement relating to the Real Estate that would affect the transaction contemplated hereby or survive the Closing; or (iv) alter the physical condition of the Real Estate; and

(b) Between the Effective Date and the Closing, Seller shall not take any action or knowingly fail to take any action that would cause the Real Estate not to conform with the provisions of this Agreement, cause any statements set forth in this Agreement to be untrue or incorrect, or otherwise cause Seller to be unable to perform the Seller's obligations under this Agreement.

(c) The Seller has all requisite power and authority to execute, deliver, and perform Seller's obligations under this Agreement. This Agreement is valid, binding, and enforceable against the Seller.

(d) The Seller is not a "foreign person" as such term is defined in Section 1445 of the Internal Revenue Code of 1986, as amended, or any related regulations.

(e) There are no mechanic's liens or other claims against the Real Estate, and all invoices for work done and materials supplied to the Real Estate have been or will, as of the date of Closing, be paid.

(f) The Seller has received no notices from regulatory agencies regarding any environmental conditions at the Real Estate that have not been remedied or disclosed in writing to the Purchaser prior to the expiration of the Due Diligence Period. The Seller has no knowledge of any environmental issue with respect to the Real Estate.

(g) The Seller has no knowledge of any asbestos or lead-based paint located on structures on the Real Estate.



10. **Closing; Conditions.**

(a) Unless otherwise provided in this Agreement or otherwise agreed by the parties, the consummation of the transaction contemplated hereby (the "Closing") shall take place not later than that date which is Forty-Five (45) days subsequent to the date that all Preconditions to Closing have been satisfied (the "Closing Date"); **Provided, However,** that if the Preconditions to Closing, as hereinafter defined, have not been met by that date which is Twelve (12) months from the Effective Date, the Purchaser shall have the right to extend the Closing Date for a period of up to Ninety (90) additional days by depositing an additional [REDACTED] to become part of the Deposit (all of which shall be applicable to the Purchase Price), or, in the alternative, the Purchaser shall have the right to terminate this Agreement, in which event the Deposit shall be promptly refunded to the Purchaser. The Closing shall take place at the offices of The Bell Firm, P.A., 810 Lisbon Street, Lewiston, Maine, or such other place, and at such time, as the parties shall mutually agree upon. Alternatively, the parties may agree to close this transaction remotely via overnight mail or other appropriate delivery service.

(b) Notwithstanding anything elsewhere set forth herein, the Purchaser's obligation to close hereunder shall be contingent upon the following ("Preconditions to Closing"):

(i) The Purchaser shall enter into a Purchase and Sale Agreement with Ronald W. Copp, Sr., Jerald E. Copp, Jr., and Howell R. Copp relating to certain real estate located at 173 Gray Road, Cumberland, Maine (the "173 Gray Road Agreement");

(ii) The parties to the 173 Gray Road Agreement shall be prepared to, and shall, close the transactions contemplated in the 173 Gray Road Agreement simultaneous with the Closing on the transactions contemplated herein;

(iii) The Purchaser shall have obtained financing for the purchase of the Real Estate upon terms and conditions reasonably satisfactory to the Purchaser;

(iv) The Purchaser shall have obtained all licenses, permits, and approvals necessary and appropriate for the operation of a convenience store and fueling station at the Real Estate; and

(v) The Purchaser shall have entered into a lease with Rusty Lantern relating to the Real Estate upon terms and conditions reasonably acceptable to the Purchaser.



In the event that any of the foregoing Preconditions to Closing have not been met by the Closing Date, as the same may be extended as provided above, the Purchaser shall have the right to terminate this Agreement in which event the Deposit shall be promptly refunded to the Purchaser.

(c) At the Closing, the Seller shall deliver to the Purchaser the following documents:

(i) Duly Executed Warranty Deed in format for recording in the Cumberland County Registry of Deeds, and otherwise reasonably satisfactory to the Purchaser;

(ii) A Real Estate Transfer Tax Declaration for the Real Estate;

(iii) Seller shall deliver certification that Seller is not a "foreign person" as such term is defined in Section 1445 of the Internal Revenue Code of 1986, as amended, and the Seller shall deliver a certification that the Seller is a Maine resident, or otherwise disclose that it is not a Maine resident and deliver such other documentation as the Purchaser shall reasonably request with respect to said certification;

(iv) The Seller shall deliver such title insurance affidavits relating to mechanic's liens and persons in possession; and

(v) The Seller shall convey such other documents as are customary in the State of Maine for commercial real estate transactions, or as otherwise reasonably requested by the Purchaser.

(d) The Purchaser shall deliver to the Seller the following:

(i) The Purchase Price; and

(ii) Such other documents as are customary in the State of Maine for commercial real estate transactions, or as are otherwise reasonably requested by the Seller.

11. Risk of Loss; Possession and Condition.

(a) Risk of loss to the Real Estate prior to the Closing shall be borne by Seller. If between the Effective Date and the Closing any or all of the Real Estate shall be partially or totally destroyed (such that the cost of repairing damage to the Real Estate exceeds Ten Percent (10%) of the Purchase Price), and the Real Estate is, in the reasonable opinion of the Purchaser, rendered unsuitable for its permitted use, Purchaser shall have the option, in its sole and absolute discretion, to (i) terminate this Agreement and receive a refund of the Deposit, or (ii) proceed to Closing, in which event the Seller shall assign all insurance proceeds pertaining to the damage to the Purchaser and credit the Purchaser with any insurance



deductibles (less the amounts Seller expends on repairing such damage prior to the Closing).

(b) The Seller agrees to deliver to the Purchaser at Closing full possession of the Real Estate, free of all tenants and occupants in substantially the same condition as they are in on the Effective Date, reasonable use and wear thereof excepted, and not in violation of any laws, ordinances, or regulations.

12. **Brokers.** Seller and Purchaser warrant and represent to each other that they have not employed or engaged any real estate broker or agent in connection with the transaction contemplated by this Agreement. Each party hereto agrees to hold the other party harmless from and against any and all costs, expenses, claims, losses, or damages, including reasonable attorneys' and paralegal fees and costs, resulting from a breach of such party's representation or covenant contained in this Section. The provisions of this Section shall survive the Closing.

13. **Default.** In the event of a default hereunder by the Seller, the Purchaser shall be entitled to any and all remedies available at law or in equity, including the right to specific performance. In the event of a default by the Purchaser hereunder, the Seller's absolute recourse shall be retaining the Deposit as full and complete liquidated damages.

14. **Notices.** All notices and other communications required or permitted under this Agreement shall be in writing and shall be hand delivered, or given by certified mail, return receipt requested, or by Federal Express or another nationally recognized overnight courier service, addressed to the party to receive such notice at the address set forth on Page 1 to this Agreement. Any notice delivered personally shall be deemed delivered on the date received or first rejected. Any notice sent via certified mail, return receipt requested, shall be deemed delivered on the date received or first rejected. Any notice sent via overnight mail by Federal Express or another nationally recognized overnight courier service shall be deemed delivered Twenty-Four (24) hours after being deposited with the overnight delivery courier. Any party may change the address to which its future notices shall be sent by notice given in the manner set forth above.

15. **Miscellaneous.**

(a) Any time period provided for herein which ends on a Saturday, Sunday or statutory holiday in the State of Maine shall extend to midnight at the end of the next day that is not a Saturday, Sunday, or statutory holiday.

(b) This Agreement shall be binding upon and shall inure to the benefit of Seller and Purchaser and their respective heirs, personal representatives, successors and assigns. The Purchaser shall have the right to assign the Purchaser's rights and obligations hereunder to an entity controlled by James G. Howard, without the prior written consent of the Seller, but upon notification to the Seller of the name and address of the assignee. All other assignments by the Purchaser shall require the prior written consent of the Seller. The Seller shall have the right to assign this Agreement.

(c) All understandings, agreements, warranties, and representations, either oral or in writing, heretofore between the parties hereto with respect to the purchase and sale of the Real Estate are merged into this Agreement, which alone fully and completely expresses the parties' agreement with respect to the transactions described herein. This Agreement may not be modified in any manner except by an instrument in writing signed by Seller and Purchaser. All representations and warranties set forth in this Agreement shall survive the Closing.

(d) This Agreement shall be governed by and interpreted in accordance with the laws of the State of Maine without regard to or application of its conflicts of law principles. Whenever the word "include," "includes," or "including" is used in this Agreement, it is deemed to be followed by the words "without limitation." The terms "this Agreement," "hereof," "herein," "hereby," "hereunder" and similar expressions refer to this Agreement as a whole and not to any particular section of this Agreement. In the event of a breach of this Agreement by any party, the other party shall be entitled to recover reasonable attorneys' and paralegal fees and costs incurred in connection with the enforcement of its rights hereunder. This Agreement may be executed in multiple counterparts, each of which shall constitute an original, and all of which, taken together, shall constitute a single instrument.

(e) The Seller and the Purchaser each (i) has agreed to permit the use from time to time, where appropriate, of pdf, DocuSign, or other electronic signatures in order to expedite the transactions contemplated, (ii) intends to be bound by its respective pdf, DocuSign, or other electronic signature, (iii) is aware that the other will rely on the pdf, DocuSign, or other electronically transmitted signature, and (iv) acknowledges such reliance and waives any defenses to the enforcement of this Agreement and the documents effecting the transactions contemplated herein based on the fact that the signature was sent by electronic



transmission only and in any number of counterparts, each of which shall be deemed to be an original and all of which together shall constitute one and the same instrument.

In Witness Whereof, the parties hereto have duly executed this Agreement as of the date first above written.

Witness:

Martin Wright

Madelyn M. Mein

Madelyn M. Mein

Cumberland Real Estate Group, LLC

By:

James G. Howard

James G. Howard, Manager

Ronald W. Copp, Sr.

Ronald W. Copp, Sr.

Ronald W. Copp, Jr.

Ronald W. Copp, Jr.

EXHIBIT A - Deed

BM

PURCHASE AND SALE AGREEMENT
(Commercial Real Estate)

This Agreement is made on this 14th day of March, 2023 (the "Effective Date") by and between **Cumberland Real Estate Group, LLC**, a Maine Limited Liability Company with a mailing address at 2 Main Street, Topsham, Maine 04086 (hereinafter referred to as the "Purchaser"), and **Ronald W. Copp, Sr.** with a mailing address at 187 Gray Rd Cumberland Me 04001, **Howell R. Copp** with a mailing address at 30 Browning Way Cumberland Me 04001, and **Jerald E. Copp, Jr.** with a mailing address at 40 Blackship Rd Cumberland Me 04001 (hereinafter collectively referred to as the "Seller").

1. **Purchase and Sale.** Subject to the terms and conditions of this Agreement, Seller agrees to sell and convey to Purchaser and Purchaser agrees to purchase from Seller, fee simple absolute title to real estate and buildings located at or near 173 Gray Road, Cumberland, Maine, as more fully described in a Quitclaim Deed with Covenant dated January 23, 2018 from Copp Brothers Real Estate to Ronald Copp, Sr., Howell Copp, and Jerald Copp, Jr. recorded in the Cumberland County Registry of Deeds at Book 34640, Page 209, said real estate being more fully described in Exhibit "A" attached hereto and made a part hereof (being the current Town of Cumberland Tax Map U19, Lot 13), together with all rights, privileges, easements, and appurtenances benefitting said real estate (hereinafter collectively referred to as the "Real Property" or the "Real Estate"). For all purposes of this Agreement, the term "Real Estate" and "Real Property" shall be deemed to include the land, structures, and improvements affixed to the Real Estate.

2. **Purchase Price.**

(a) The purchase price for the Real Estate shall be [REDACTED] (the "Purchase Price").

(b) The Purchase Price shall be paid by the Purchaser to the Seller as follows:

(i) Within Three (3) business days subsequent to the Effective Date, the Purchaser shall deliver to the Escrow Agent, hereinafter defined, a deposit of [REDACTED] (the "Deposit"). The Deposit shall be payable to The Bell Firm, P.A., 810 Lisbon Street, P.O. Box 1776, Lewiston, Maine 04241-1776 ("Escrow Agent"). The Deposit shall be held and/or disposed of by the Escrow Agent in accordance with provisions of this Agreement. The Deposit shall be held by the Escrow Agent in a non-interest-bearing account.

(ii) The balance of the Purchase Price ([REDACTED]) shall be paid by the Purchaser to the Seller in lawful currency of the United States in immediately available funds by wire transfer or other means acceptable to Seller.

(iii) The parties hereto acknowledge and agree with the Escrow Agent that the Escrow Agent shall act hereunder as a depository only and shall not be a party to or be bound by any agreement or undertaking which may be evidenced by or arise out of the escrow deposited with it hereunder. The Escrow Agent shall not be responsible or liable in any manner for the identity or rights of any person depositing the Deposit in escrow. The Escrow Agent shall not be liable for any error of judgment or for any act omitted by it in good faith, or for anything which it may in good faith do or refrain from doing in connection herewith. The Escrow Agent is authorized to act on any document believed by it to be genuine and to be signed by the proper party or parties, and will incur no liability in so acting.

In the event of any disagreements or presentation of adverse claims or demands in connection with the Deposit deposited with the Escrow Agent, the Escrow Agent shall at its option be entitled to refuse to comply with any such claims or demands during the continuance of such disagreement and may refrain from delivering any item effected hereby, and in so doing the Escrow Agent shall not become liable to the undersigned, or to any person, due to its failure to comply with any such adverse claim or demand. The Escrow Agent shall be entitled (but not obligated) to continue, without liability, to refrain and refuse to act: (a) until all the rights of the adverse claimants have been finally adjudicated by a court of competent jurisdiction, after which time the Escrow Agent shall be entitled to act in conformity with such adjudication; or (b) until all differences shall have been adjudicated by agreement and the Escrow Agent shall have been notified thereof and shall have been directed in writing signed by the undersigned and by all persons making adverse claims or demands, at which time the Escrow Agent shall be protected in acting in compliance therewith.

Notwithstanding anything elsewhere set forth herein, the Escrow Agent shall not be required to make delivery of the Deposit unless it has been indemnified against any liability for doing so in a manner which it deems satisfactory.

3. **Adjustments.** The following items shall be prorated, adjusted and paid as follows:

(a) All applicable real estate taxes, assessments, and rents affecting the Real Estate shall be apportioned between Seller and Purchaser as of the Closing Date (as hereinafter defined). Utilities shall be prorated up to the date of closing unless otherwise paid for by tenants.

(b) Seller and Purchaser shall each pay their equal share of the real estate transfer taxes.

(c) Each party shall pay all costs and expenses incurred by such party in connection with the transactions contemplated by this Agreement not otherwise adjusted as set forth in this Section or otherwise provided for in this Agreement.

(d) The Purchaser shall be responsible for all costs and expenses associated with its due diligence review. The Seller and the Purchaser shall each be responsible for the payment of costs of their respective legal counsel, tax advisors, and other professionals.

4. **Title.** Seller shall convey the Real Estate to Purchaser by good and sufficient Warranty Deed (the "Deed"), prepared at the Seller's sole expense, conveying good and marketable title to the Real Estate as defined by the standards adopted by the Maine State Bar Association, free and clear of all encumbrances, except for conventional utility easements and such restrictions as would not make the title unmarketable. The title shall also be insurable by any reputable title insurance company licensed to do business in the State of Maine. All costs of title insurance shall be borne by Purchaser. Seller will execute such affidavits as may be required by the applicable title insurance company to cause the deletion of the standard mechanics' lien exception from the to-be issued title insurance policy.

Purchaser may examine, at Purchaser's sole expense, the title to the Real Estate and will report in writing on or before that date which is One Hundred Twenty (120) days from the Effective Date ("Due Diligence Period") any valid objections (hereafter "Exceptions") based on the standards adopted by the Maine State Bar Association. Any Exceptions to the title which would be disclosed by examination of the records shall be deemed to have been accepted by Purchaser if title is transferred to Purchaser without removal of said Exceptions, unless otherwise agreed to in writing and signed by Seller. If Purchaser objects to any Exceptions to the title, Seller shall (i) use all due diligence to remove such exceptions at Seller's own expense within Thirty (30) days thereafter, or (ii) notify the Purchaser that the Seller does not intend to remove said Exceptions. Notwithstanding Seller's due diligence, if such Exceptions objected to by Purchaser cannot be removed within the said Thirty (30) day period, or such additional period as Purchaser in Purchaser's sole discretion may allow, or if the Seller indicates that it does not intend to remove said Exceptions, Purchaser may elect to terminate this Agreement. Purchaser shall notify Seller of such election, in which case the obligations of all parties under this Agreement shall thereupon terminate and the Deposit shall be promptly returned to the Purchaser. Alternatively, Purchaser may elect to purchase the Real Estate under the provisions of this Agreement subject to any title Exceptions which cannot be removed without any adjustment in the Purchase Price.

5. **Due Diligence. Inspections.** The Seller shall, within Five (5) business days from the Effective Date, provide to the Purchaser such information as the Purchaser reasonably requests relating to the Real Estate, provided that said information is within the Seller's possession or control (the "Due Diligence Information"). The Due Diligence period shall be extended by One (1) day for each day that the Seller takes to deliver the Due Diligence Information to the Seller beyond the Five (5) business day period set forth above. All proprietary and confidential information that the Seller provides to the Purchaser relating to the Real Estate shall be used by the Purchaser solely for purposes of the transactions contemplated herein. All such information will be held by the Purchaser in strict confidence and not disclosed to anyone, other than legal counsel, employees and agents on a need-to-know basis, lenders, and third-party due diligence contractors and professionals;

Provided, However, that it shall not be a breach of this covenant in the event of disclosure of any such information if it is or becomes available from other sources which are not subject to an obligation of confidentiality. Notwithstanding anything else set forth herein, nothing shall prohibit the Purchaser from filing or disclosing such information in connection with, and as may be required by, a judicial or regulatory body or law enforcement agency.

During the Due Diligence Period, the Purchaser shall be entitled to conduct such inspections on the Real Estate as the Purchaser, in its sole discretion, shall determine, including, without limitation, general building inspection, sewer disposal, water quality, radon air quality, radon water quality, asbestos air quality, lead-based paint inspections, asbestos inspections, ADA inspections, wetland surveys, environmental inspections, state and local codes, surveys, leases and tenancies, and any and all other inspections which the Purchaser deems just and appropriate. The Purchaser shall indemnify and hold the Seller harmless from any and all injury which the Seller may incur in connection with the Purchaser's inspections on the Real Estate. If the Purchaser is dissatisfied with any of its inspections, in the Purchaser's sole and absolute discretion, the Purchaser shall be entitled to terminate this Agreement on or before the expiration of the Due Diligence Period by notice in writing to the Seller, and the Deposit shall be promptly returned to the Purchaser. If the Purchaser fails to notify the Seller in writing of its election to terminate on or before the expiration of the Due Diligence Period as a result of its due diligence review, then the Purchaser shall be deemed to be satisfied with its due diligence review, and the Purchaser shall have no further right to terminate under this Item 5.

6. **Items to be Delivered to Purchaser from Seller.** Seller shall deliver to Purchaser such information and/or documentation pertaining to the Real Estate as is reasonably requested by Purchaser from time-to-time to the extent the same is in the possession or control of Seller.

7. **Sole Representations and Warranties.** The Seller represents and warrants to the Purchaser that the following are true and correct as of the Effective Date and will be true and correct as of the Closing:

(a) This Agreement is valid, binding, and enforceable against the Seller. Seller has not received any notice from any source claiming or inquiring into the existence of any violations of laws, ordinances, or regulations affecting the Real Estate; and

(b) there is no action, suit, or other proceeding (including condemnation actions) pending or, to the best of Seller's knowledge, threatened against Seller or affecting any portion of the Real Estate in any court or before any arbitrator of any kind or before any governmental body that may materially or adversely affect the Real Estate or the transactions contemplated by this Agreement.

8. **Purchaser Representations and Warranties.** The Purchaser represents and warrants to the Seller that the following are true and correct as of the Effective Date and will be true and correct as of the Closing:



(a) The Purchaser has the requisite power and authority to execute, deliver, and perform its obligations under this Agreement. This Agreement is valid, binding, and enforceable against the Purchaser.

(b) The Purchaser is a Limited Liability Company, duly formed, valid and existing, and in good standing of the laws of the State of Maine.

(c) There are no actions, suits, claims, investigations, or other legal proceedings pending, or to the Purchaser's knowledge, threatened against or by the Purchaser that challenge or seek to prevent, or otherwise delay the consummation of the transactions contemplated herein.

9. **General Covenants and Agreements of Seller.** Seller agrees with Purchaser as follows:

(a) Between the Effective Date and the Closing, Seller shall not, without Purchaser's consent (i) convey or otherwise dispose of any interest in the Real Estate; (ii) mortgage, pledge, lease, or subject to any lien or other encumbrances any interest in the Real Estate which exceed the Purchase Price; (iii) enter into any agreement relating to the Real Estate that would affect the transaction contemplated hereby or survive the Closing; or (iv) alter the physical condition of the Real Estate; and

(b) Between the Effective Date and the Closing, Seller shall not take any action or knowingly fail to take any action that would cause the Real Estate not to conform with the provisions of this Agreement, cause any statements set forth in this Agreement to be untrue or incorrect, or otherwise cause Seller to be unable to perform the Seller's obligations under this Agreement.

(c) The Seller has all requisite power and authority to execute, deliver, and perform Seller's obligations under this Agreement. This Agreement is valid, binding, and enforceable against the Seller.

(d) The Seller is not a "foreign person" as such term is defined in Section 1445 of the Internal Revenue Code of 1986, as amended, or any related regulations.

(e) There are no mechanic's liens or other claims against the Real Estate, and all invoices for work done and materials supplied to the Real Estate have been or will, as of the date of Closing, be paid.

(f) The Seller has received no notices from regulatory agencies regarding any environmental conditions at the Real Estate that have not been remedied or disclosed in writing to the Purchaser prior to the expiration of the Due Diligence Period. The Seller has no knowledge of any environmental issue with respect to the Real Estate.

(g) The Seller has no knowledge of any asbestos or lead-based paint located on structures on the Real Estate.



10. **Closing; Conditions.**

(a) Unless otherwise provided in this Agreement or otherwise agreed by the parties, the consummation of the transaction contemplated hereby (the "Closing") shall take place not later than that date which is Forty-Five (45) days subsequent to the date that all Preconditions to Closing have been satisfied (the "Closing Date"); **Provided, However,** that if the Preconditions to Closing, as hereinafter defined, have not been met by that date which is Twelve (12) months from the Effective Date, the Purchaser shall have the right to extend the Closing Date for a period of up to Ninety (90) additional days by depositing an additional [REDACTED] to become part of the Deposit (all of which shall be applicable to the Purchase Price), or, in the alternative, the Purchaser shall have the right to terminate this Agreement, in which event the Deposit shall be promptly refunded to the Purchaser. The Closing shall take place at the offices of The Bell Firm, P.A., 810 Lisbon Street, Lewiston, Maine, or such other place, and at such time, as the parties shall mutually agree upon. Alternatively, the parties may agree to close this transaction remotely via overnight mail or other appropriate delivery service.

(b) Notwithstanding anything elsewhere set forth herein, the Purchaser's obligation to close hereunder shall be contingent upon the following ("Preconditions to Closing"):

(i) The Purchaser shall enter into a Purchase and Sale Agreement with Ronald W. Copp, Sr. and Ronald W. Copp, Jr. relating to certain real estate located at 181 Gray Road, Cumberland, Maine (the "181 Gray Road Agreement");

(ii) The parties to the 181 Gray Road Agreement shall be prepared to, and shall, close the transactions contemplated in the 181 Gray Road Agreement simultaneous with the Closing on the transactions contemplated herein;

(iii) The Purchaser shall have obtained financing for the purchase of the Real Estate upon terms and conditions reasonably satisfactory to the Purchaser;

(iv) The Purchaser shall have obtained all licenses, permits, and approvals necessary and appropriate for the operation of a convenience store and fueling station at the Real Estate; and

(v) The Purchaser shall have entered into a lease with Rusty Lantern relating to the Real Estate upon terms and conditions reasonably acceptable to the Purchaser.



In the event that any of the foregoing Preconditions to Closing have not been met by the Closing Date, as the same may be extended as provided above, the Purchaser shall have the right to terminate this Agreement in which event the Deposit shall be promptly refunded to the Purchaser.

(c) At the Closing, the Seller shall deliver to the Purchaser the following documents:

(i) Duly Executed Warranty Deed in format for recording in the Cumberland County Registry of Deeds, and otherwise reasonably satisfactory to the Purchaser;

(ii) A Real Estate Transfer Tax Declaration for the Real Estate;

(iii) Seller shall deliver certification that Seller is not a "foreign person" as such term is defined in Section 1445 of the Internal Revenue Code of 1986, as amended, and the Seller shall deliver a certification that the Seller is a Maine resident, or otherwise disclose that it is not a Maine resident and deliver such other documentation as the Purchaser shall reasonably request with respect to said certification;

(iv) The Seller shall deliver such title insurance affidavits relating to mechanic's liens and persons in possession; and

(v) The Seller shall convey such other documents as are customary in the State of Maine for commercial real estate transactions, or as otherwise reasonably requested by the Purchaser.

(d) The Purchaser shall deliver to the Seller the following:

(i) The Purchase Price; and

(ii) Such other documents as are customary in the State of Maine for commercial real estate transactions, or as are otherwise reasonably requested by the Seller.

11. Risk of Loss; Possession and Condition.

(a) Risk of loss to the Real Estate prior to the Closing shall be borne by Seller. If between the Effective Date and the Closing any or all of the Real Estate shall be partially or totally destroyed (such that the cost of repairing damage to the Real Estate exceeds Ten Percent (10%) of the Purchase Price), and the Real Estate is, in the reasonable opinion of the Purchaser, rendered unsuitable for its permitted use, Purchaser shall have the option, in its sole and absolute discretion, to (i) terminate this Agreement and receive a refund of the Deposit, or (ii) proceed to Closing, in which event the Seller shall assign all insurance proceeds pertaining to the damage to the Purchaser and credit the Purchaser with any insurance



deductibles (less the amounts Seller expends on repairing such damage prior to the Closing).

(b) The Seller agrees to deliver to the Purchaser at Closing full possession of the Real Estate, free of all tenants and occupants in substantially the same condition as they are in on the Effective Date, reasonable use and wear thereof excepted, and not in violation of any laws, ordinances, or regulations.

12. **Brokers.** Seller and Purchaser warrant and represent to each other that they have not employed or engaged any real estate broker or agent in connection with the transaction contemplated by this Agreement. Each party hereto agrees to hold the other party harmless from and against any and all costs, expenses, claims, losses, or damages, including reasonable attorneys' and paralegal fees and costs, resulting from a breach of such party's representation or covenant contained in this Section. The provisions of this Section shall survive the Closing.

13. **Default.** In the event of a default hereunder by the Seller, the Purchaser shall be entitled to any and all remedies available at law or in equity, including the right to specific performance. In the event of a default by the Purchaser hereunder, the Seller's absolute recourse shall be retaining the Deposit as full and complete liquidated damages.

14. **Notices.** All notices and other communications required or permitted under this Agreement shall be in writing and shall be hand delivered, or given by certified mail, return receipt requested, or by Federal Express or another nationally recognized overnight courier service, addressed to the party to receive such notice at the address set forth on Page 1 to this Agreement. Any notice delivered personally shall be deemed delivered on the date received or first rejected. Any notice sent via certified mail, return receipt requested, shall be deemed delivered on the date received or first rejected. Any notice sent via overnight mail by Federal Express or another nationally recognized overnight courier service shall be deemed delivered Twenty-Four (24) hours after being deposited with the overnight delivery courier. Any party may change the address to which its future notices shall be sent by notice given in the manner set forth above.

15. **Miscellaneous.**

(a) Any time period provided for herein which ends on a Saturday, Sunday or statutory holiday in the State of Maine shall extend to midnight at the end of the next day that is not a Saturday, Sunday, or statutory holiday.

(b) This Agreement shall be binding upon and shall inure to the benefit of Seller and Purchaser and their respective heirs, personal representatives, successors and assigns. The Purchaser shall have the right to assign the Purchaser's rights and obligations hereunder to an entity controlled by James G. Howard, without the prior written consent of the Seller, but upon notification to the Seller of the name and address of the assignee. All other assignments by the Purchaser shall require the prior written consent of the Seller. The Seller shall have the right to assign this Agreement.



(c) All understandings, agreements, warranties, and representations, either oral or in writing, heretofore between the parties hereto with respect to the purchase and sale of the Real Estate are merged into this Agreement, which alone fully and completely expresses the parties' agreement with respect to the transactions described herein. This Agreement may not be modified in any manner except by an instrument in writing signed by Seller and Purchaser. All representations and warranties set forth in this Agreement shall survive the Closing.

(d) This Agreement shall be governed by and interpreted in accordance with the laws of the State of Maine without regard to or application of its conflicts of law principles. Whenever the word "include," "includes," or "including" is used in this Agreement, it is deemed to be followed by the words "without limitation." The terms "this Agreement," "hereof," "herein," "hereby," "hereunder" and similar expressions refer to this Agreement as a whole and not to any particular section of this Agreement. In the event of a breach of this Agreement by any party, the other party shall be entitled to recover reasonable attorneys' and paralegal fees and costs incurred in connection with the enforcement of its rights hereunder. This Agreement may be executed in multiple counterparts, each of which shall constitute an original, and all of which, taken together, shall constitute a single instrument.

(e) The Seller and the Purchaser each (i) has agreed to permit the use from time to time, where appropriate, of pdf, DocuSign, or other electronic signatures in order to expedite the transactions contemplated, (ii) intends to be bound by its respective pdf, DocuSign, or other electronic signature, (iii) is aware that the other will rely on the pdf, DocuSign, or other electronically transmitted signature, and (iv) acknowledges such reliance and waives any defenses to the enforcement of this Agreement and the documents effecting the transactions contemplated herein based on the fact that the signature was sent by electronic

transmission only and in any number of counterparts, each of which shall be deemed to be an original and all of which together shall constitute one and the same instrument.

In Witness Whereof, the parties hereto have duly executed this Agreement as of the date first above written.

Witness:

Matt Moplit

Madelyn M. Mein

Madelyn M. Mein

Madelyn M. Mein

Cumberland Real Estate Group, LLC

By:

James G. Howard
James G. Howard, Manager

Ronald W. Copp, Sr.
Ronald W. Copp, Sr.

Jerald E. Copp, Jr.
Jerald E. Copp, Jr.

Howell R. Copp
Howell R. Copp



EXHIBIT A – Deed

A handwritten signature or set of initials, possibly "SP", enclosed within a circular or oval shape.

Curt Nuefeld

From: Sirois, Alison <Alison.Sirois@maine.gov>
Sent: Thursday, August 3, 2023 10:58 AM
To: cneufeld@priorityrealestategroup.com
Subject: RE: Stormwater Law Question

Sorry about that, SW laws became effective July 1, 1997, so it looks like the impervious area on the lots is grandfathered for the most part. Therefore, any disturbance over 1 acre will require SW PBR, and disturbed area does include redevelopment. If the project meets the >1 acre of disturbance and < 1 acre of impervious are proposed a SW PBR is required: <https://www.maine.gov/dep/land/stormwater/SW-PBR-AppBooklet-Fillable.pdf>

Additional Info: Based on the Maine Construction General Permit, July 21, 2006 and Chapter 500, Section 3, August 12, 2015 the definition of disturbed area includes redevelopment:

D. Disturbed area. All land areas that are stripped, graded, grubbed, filled, or excavated at any time during the site preparation or removing vegetation for, or construction of, a project. "Disturbed area" does not include routine maintenance, **but does include re-development** and new impervious areas. "Routine maintenance" is maintenance performed to maintain the original line and grade, hydraulic capacity, and original purpose of the facility. Paving impervious gravel surfaces while maintaining the original line and grade, hydraulic capacity and original purpose of the facility is considered routine maintenance. Cutting of trees, without grubbing, stump removal, disturbance or exposure of soil is not considered "disturbed area." A disturbed area continues to be considered as disturbed area if it meets the definition of "developed area" or "impervious area" following final stabilization.

From: cneufeld@priorityrealestategroup.com <cneufeld@priorityrealestategroup.com>
Sent: Thursday, August 03, 2023 10:12 AM
To: Sirois, Alison <Alison.Sirois@maine.gov>
Subject: RE: Stormwater Law Question

EXTERNAL: This email originated from outside of the State of Maine Mail System. Do not click links or open attachments unless you recognize the sender and know the content is safe.

Hi Alison,

Why doesn't the redevelopment standard apply?

Curt

Curtis Y. Neufeld, PE
Priority Real Estate Group
2 Main Street
Topsham, ME 04086

O: 207-837-6196
M: 207-798-0576

From: Sirois, Alison <Alison.Sirois@maine.gov>
Sent: Thursday, August 3, 2023 8:06 AM
To: cneufeld@priorityrealestategroup.com
Subject: RE: Stormwater Law Question

Hi Curt,

Looks like in 1985 Lot 13 was undeveloped. By 1997 Lot 13 had been cleared and impervious area covers ¾ of the parcel. All impervious area that currently exists on site will count toward permitting thresholds and after the fact permitting will be required for new development

Looks like Lot 12 may have had some impervious area prior 1985, the 1997 impervious area represented would be the only area that may not count toward permitting thresholds. Otherwise, any new impervious area since 1997 counts toward permitting thresholds.

And since ownership is the same, both lots will be considered and permitted together. Any new development will require a partial after-the-fact individual Stormwater permit application. The entire parcel would need to meet current Chapter 500 rules, redevelopment standard would not apply here.



Alison Sirois (she/her)
Regional Manager, Bureau of Land Resources
Maine Department of Environmental Protection
Phone (207)699-7028 Office (207)822-6300
www.maine.gov/dep

From: cneufeld@priorityrealestategroup.com <cneufeld@priorityrealestategroup.com>
Sent: Thursday, July 27, 2023 1:15 PM
To: Sirois, Alison <Alison.Sirois@maine.gov>
Subject: FW: Stormwater Law Question

EXTERNAL: This email originated from outside of the State of Maine Mail System. Do not click links or open attachments unless you recognize the sender and know the content is safe.

Hi Alison,

I would like to follow up with you about this site/project. Can you give me a call at your earliest convenience?

Thanks,
Curt

Curtis Y. Neufeld, PE
Priority Real Estate Group
2 Main Street
Topsham, ME 04086

O: 207-837-6196
M: 207-798-0576

From: cneufeld@priorityrealestategroup.com <cneufeld@priorityrealestategroup.com>
Sent: Monday, July 10, 2023 10:49 AM
To: 'alison.sirois@maine.gov' <alison.sirois@maine.gov>
Subject: Stormwater Law Question

Hi Alison,

I hope all is well with you. Good news – I am not writing about anything at Brunswick Landing.

We are looking at two parcels in Cumberland for the development of a convenience store/gas station and bank/credit union. The parcels are owned by members of the Copp family but by different legal entities. They have been occupied in some form since the mid-'90s. Attached are KML files that would take you to them in Google Earth Pro, if you are used to using that. A few screenshots are from Google Earth and shown below with the month/year. My question is, given the long history of development/impervious area, what are the permitting requirements per Chapter 500? Both parcels have been developed area for long before Priority Real Estate Group has thought about buying them. Our project would result in less than 1-acre of new impervious area.

6/1997



12/2003



4/2006



5/2010



9/2014



6/2020



4/2023



Curtis Y. Neufeld, PE
Priority Real Estate Group
2 Main Street
Topsham, ME 04086

O: 207-837-6196
M: 207-798-0576

PROPOSED FUEL SYSTEM COMPONENTS & SAFETY FEATURES

The following is a technical summary of the proposed fuel system safety features and operational procedures that will be implemented for the Rusty Lanter Market project. The intent of these design enhancements is to maximize safety and minimize any potential petroleum releases to the environment as a result of the proposed redevelopment.

1. Fuel Dispensing Area

- a. Positive Limiting Barriers – The fuel dispensing area will consist of a 6” reinforced concrete mat with spill containment grooves (Positive Limiting Barriers or PLB) around each dispenser island. These concrete grooves will contain any minor spillage that might occur at the fuel dispensing islands and will be designed to contain 5 gallons (minimum) of fuel product. This allows any minor spillage to be trapped at the fuel dispensing area for immediate clean-up by the store attendant using the on-site spill kit.
- b. Dispenser Hoses – The fuel dispensing hoses on each dispenser contain a breakaway coupling (dry-break connection). In the event that a driver inadvertently leaves the dispensing area with the hose nozzle still connected to the vehicle fill pipe, the dry break will disconnect the hose from the dispenser. Mechanisms inside the dry-break coupling will prevent a release of fuel product to the environment at the disconnect.
- c. Dispenser Shear Valves – Within each dispenser, there is an emergency shear valve on the fuel piping supply line below the dispenser. Should the dispenser become dislodged by a vehicle, the emergency shear valve will close and prevent an uncontrolled release of fuel products into the environment.
- d. Dispenser Sumps – A sump constructed of a fiber-reinforced plastic (FRP) is located under each dispenser, along with an electronic liquid sensor located at the bottom of the sump. Should a fuel product leak from within the dispenser unit, it would be captured by the sump, and the electronic sump sensor would activate the central leak detection console located inside of the convenience store.
- e. Fire Suppression System – The fuel dispensing canopy will be equipped with an overhead dry chemical fire suppression system that will be automatically and/or manually activated in the event of a fire.
- f. Emergency Shutoff – The facility will be equipped with an emergency shutoff switch located inside the store at the cashier. This switch allows the attendant to immediately cut all power to the dispensers.

2. Fuel Storage System

- a. Leak Detection Console Unit - The fuel storage system will be monitored 24 hours a day, 365 days a year by a state-of-the-art central monitoring system located inside the convenience store. This electronic monitoring system continuously monitors the level of gasoline in each tank and can detect a 0.1-gallon per hour loss of fuel product. In addition, the system monitors all sensors connected to the fuel piping sumps, dispenser sumps, and the double wall (annular) space of each tank.
- b. Double Wall Fiberglass Tanks - The facility will be supplied with double wall fiberglass underground fuel storage tanks. Fiberglass is inherently corrosion-proof, and the annular space between the two walls is filled with brine (a freeze-resistant liquid solution). The level

of the brine is monitored continuously with an electronic sensor. Any change in the level of the brine will cause the sensor to activate the central console alarm unit in the convenience store.

- c. Double Wall Fuel Piping - The fuel product piping will consist of double-wall construction. The primary pipe contains the gasoline or diesel fuel. In the unlikely event of a failure in the primary pipeline, the interstice between the two pipes will allow the fuel product to flow toward a containment sump on the tank. This tank containment sump will have an electronic sensor located at the bottom of the sump. All underground piping is sloped towards a containment sump, so any potential release of fuel product will flow to the containment sump for detection. Activation of a sump sensor creates an audible/visual alarm at the central console unit located in the convenience store.
- d. Overfill Prevention - When the underground storage tanks are filled by the fuel tanker, numerous precautions are taken to prevent surface spillage. Prior to filling the tanks, the tanker truck driver will check the contents of the tank with a measuring stick. The driver then checks this measurement against a tank gauge chart to verify that the tank will hold the amount of fuel product that was ordered. The central console unit is also checked electronically to confirm the volume of fuel product in the tank. As an additional factor of safety, there is an overfill shut-off valve located inside of each underground tank. This device is designed to prevent the delivery truck from continuing the transfer of fuel product into the tanks once the product level reaches 95% tank capacity.
- e. Fill and Vapor Spill Prevention - In order to prevent minor surface spillage when the fuel tanker delivery hose is removed from the tank connection point on the ground, there is a spill containment manhole proposed on each fill tube and vapor tube which holds a minimum capacity of 5 gallons. In the unlikely event of a spill, the fill containment manhole will contain any fuel product remaining in the delivery hose. Therefore, should the delivery truck driver inadvertently spill any fuel product while disconnecting the delivery hose from the tank fill, it would be contained and removed from the containment manhole.
- f. Pressurized Line Leak Detection - The pressure within the product piping will be continually monitored by an in-line leak detector attached directly to the submerged turbine pump (STP) located in each tank. This detector is activated when the dispenser is turned on by the customer. This detector monitors the pressure in each line electronically. If a pressure loss is detected, the system will shut down the dispensers. These product piping detectors are also connected to the console alarm unit located inside of the store.
- g. Observation Wells - Two observation wells will be installed at the tank field when the facility is constructed. These wells allow access to the groundwater for future testing of the groundwater quality, if necessary. The groundwater in these two wells can be tested prior to the facility opening in order to set up a "baseline" of groundwater data for future reference purposes.
- h. An Oil Stop Valve and a 1,500-gallon sediment & oil separator will be installed. The purpose of this structure is to provide a 'belt and suspenders' approach to capturing any spills that exceed the capacity of the spill bucket and PLB and make it to the catch basin but escape before the Oil Stop Valve is seated.

3. Emergency Preparedness

- a. An emergency response procedure will be developed for this facility to supplement local authorities' preparedness in reacting to an emergency situation. This emergency response plan outlines the procedures to be taken by the employees of the facility in the event of an emergency. This response plan will include an Emergency Contact List, which provides contact names and phone numbers of response personnel and remediation companies that will be contacted if an emergency occurs. This response plan will be conspicuously posted at the convenience store, and employees will be trained in emergency preparedness.

- b. An emergency spill kit will be provided and located in the convenience store for use by the store employees. This kit will include absorbent material (speedy dry/granular cellulose), absorbent pads, absorbent pillows/booms, gloves, safety goggles, and disposal bags.
- 4. **Training** - Federal EPA regulations require that all owners and operators have certified employees operating the fuel facility. There are three categories of operators for each underground tank, known as A, B, or C operators. The A operator is responsible for meeting all regulations at the company level. The B operator must know the equipment and operations of the tank fuel system, including the inspection of these systems on a monthly basis. These inspections include monthly inventory control in accordance with current regulations. The A & B operators are both required to pass a test to become certified. The A and/or B operator is also responsible for training the C operators. The C operator must be present whenever a tank system is in operation. The C operator must also be trained to respond to an emergency.

SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION

Maine Dept. Health & Human Services
Div of Environmental Health, 11 SHS
(207) 287-2070 FAX (207) 287-4172

PROPERTY LOCATION

City, Town, or Plantation	CUMBERLAND
Street or Road	GRAY ROAD
Subdivision, Lot #	

>>CAUTION: LPI APPROVAL REQUIRED<<

Town/City	Permit #
Date Permit Issued	Fee \$
Double Fee Charged []	
L.P.I.#	
Local Plumbing Inspector Signature	
Fee \$	State Fee
Fee \$	Locally Adopted Fee
Copy: [] Owner [] Town [] State	

OWNER/APPLICANT INFORMATION

Name (last, first, MI)	<input type="checkbox"/> Owner <input checked="" type="checkbox"/> Applicant
PRIORITY REAL ESTATE GROUP, LLC	
Mailing Address of Owner/Applicant	C/O BRANDON CUMMINGS PRIORITY REAL ESTATE GROUP, LLC 2 MAIN STREET TOPSHAM, ME 04086
Daytime Tel. #	248-7983

The Subsurface Wastewater Disposal System shall not be installed until a Permit is issued by the Local Plumbing Inspector. The Permit shall authorize the owner or installer to install the disposal system in accordance with this application and the Maine Subsurface Wastewater Disposal Rules.

Municipal Tax Map # 0-19 Lot # 13

OWNER OR APPLICANT STATEMENT

I state and acknowledge that the information submitted is correct to the best of my knowledge and understand that any falsification is reason for the Department and/or Local Plumbing Inspector to deny a permit.

CAUTION: INSPECTION REQUIRED

I have inspected the installation authorized above and found it to be in compliance with the Subsurface Wastewater Disposal Rules Application.

Signature of Owner/Applicant

Date

Local Plumbing Inspector Signature

(1st) Date Approved

(2nd) Date Approved

PERMIT INFORMATION

TYPE OF APPLICATION <input checked="" type="checkbox"/> 1. First Time System <input type="checkbox"/> 2. Replacement System Type Replaced: Year Installed: <input type="checkbox"/> 3. Expanded System <input type="checkbox"/> a. <25% Expansion <input type="checkbox"/> b. >25% Expansion <input type="checkbox"/> 4. Experimental System <input type="checkbox"/> 5. Seasonal Conversion	THIS APPLICATION REQUIRES <input checked="" type="checkbox"/> 1. No Rule Variance <input type="checkbox"/> 2. First Time System Variance <input type="checkbox"/> a. Local Plumbing Inspector Approval <input type="checkbox"/> b. State & Local Plumbing Inspector Approval <input type="checkbox"/> 3. Replacement System Variance <input type="checkbox"/> a. Local Plumbing Inspector Approval <input type="checkbox"/> b. State & Local Plumbing Inspector Approval <input type="checkbox"/> 4. Minimum Lot Size Variance <input type="checkbox"/> 5. Seasonal Conversion Permit	DISPOSAL SYSTEM COMPONENTS <input checked="" type="checkbox"/> 1. Complete Non-Engineered System <input type="checkbox"/> 2. Primitive System (graywater & alt toilet) <input type="checkbox"/> 3. Alternative Toilet, specify: <input type="checkbox"/> 4. Non-Engineered Treatment Tank (only) <input type="checkbox"/> 5. Holding Tank, _____ gallons <input type="checkbox"/> 6. Non-Engineered Disposal Field (only) <input type="checkbox"/> 7. Separated Laundry System <input type="checkbox"/> 8. Complete Engineered System (2000gpd+) <input type="checkbox"/> 9. Engineered Treatment Tank (only) <input type="checkbox"/> 10. Engineered Disposal Field (only) <input type="checkbox"/> 11. Pre-treatment, specify: <input type="checkbox"/> 12. Miscellaneous components
SIZE OF PROPERTY 1. 4 +/- <input type="checkbox"/> SQ. FT. <input checked="" type="checkbox"/> ACRES	DISPOSAL SYSTEM TO SERVE <input type="checkbox"/> 1. Single Family Dwelling Unit, No. of Bedrooms: _____ <input type="checkbox"/> 2. Multiple Family Dwelling, No of Units: _____ <input checked="" type="checkbox"/> 3. Other: <u>BANK</u> (specify) Current Use <input type="checkbox"/> Seasonal <input type="checkbox"/> Year Round <input checked="" type="checkbox"/> Undeveloped	TYPE OF WATER SUPPLY <input type="checkbox"/> 1. Drilled Well <input type="checkbox"/> 2. Dug Well <input type="checkbox"/> 3. Private <input checked="" type="checkbox"/> 4. Public <input type="checkbox"/> 5. Other:
SHORELAND ZONING <input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		

DESIGN DETAILS (SYSTEM LAYOUT SHOWN ON PAGE 3)

TREATMENT TANK <input checked="" type="checkbox"/> 1. Concrete <input checked="" type="checkbox"/> a. Regular <input type="checkbox"/> b. Low Profile <input type="checkbox"/> 2. Plastic <input type="checkbox"/> 3. Other: CAPACITY: <u>1500</u> GAL. SEE NOTE ON PAGE 3	DISPOSAL FIELD TYPE & SIZE <input type="checkbox"/> 1. Stone Bed <input type="checkbox"/> 2. Stone Trench <input checked="" type="checkbox"/> 3. Proprietary Device <input checked="" type="checkbox"/> a. Cluster array <input type="checkbox"/> c. Linear <input type="checkbox"/> b. Regular <input checked="" type="checkbox"/> d. H-20 loaded <input type="checkbox"/> 4. Other: SIZE: <u>1280</u> sq. ft. <input type="checkbox"/> lin. ft. 20 H-20 RATED CONCRETE CHAMBER UNITS	GARBAGE DISPOSAL UNIT <input checked="" type="checkbox"/> 1. No <input type="checkbox"/> 2. Yes <input type="checkbox"/> 3. Maybe If Yes or Maybe, specify one below: <input type="checkbox"/> a. Multi-compartment tank <input type="checkbox"/> b. _____ tanks in series <input type="checkbox"/> c. Increase in tank capacity <input type="checkbox"/> d. Filter on tank outlet	DESIGN FLOW <u>397</u> gallons per day BASED ON: <input type="checkbox"/> 1. Table 4A (dwelling unit(s)) <input checked="" type="checkbox"/> 2. Table 4C (other facilities) SHOW CALCULATIONS for other facilities BANK WITH 6 EMPLOYEES @ 12 GALLONS PER DAY EACH + PUBLIC RESTROOM @ 325 GALLONS PER DAY= <input type="checkbox"/> 3. Section 4G (meter readings) ATTACH WATER-METER DATA
SOIL DATA & DESIGN CLASS PROFILE CONDITION <u>5 / C</u> at Observation Hole # <u>TP 1</u> Depth <u>30</u> " of Most Limiting Soil Factor	DISPOSAL FIELD SIZING <input checked="" type="checkbox"/> 1. Medium - 2.6 sq.ft./gpd <input type="checkbox"/> 2. Medium-Large - 3.3 sq.ft./gpd <input type="checkbox"/> 3. Large - 4.1 sq.ft./gpd <input type="checkbox"/> 4. Extra-Large - 5.0 sq.ft./gpd	EFFLUENT/EJECTOR PUMP <input type="checkbox"/> 1. Not required <input checked="" type="checkbox"/> 2. May be required <input type="checkbox"/> 3. Required Specify only for engineered systems: SEE NOTE ON PAGE 3 DOSE: _____ gallons	LATITUDE AND LONGITUDE at center of disposal area Lat. <u>N 43</u> d <u>48</u> m <u>52.93</u> s Lon. <u>W 70</u> d <u>18</u> m <u>44.28</u> s if g.p.s., state margin of error

SITE EVALUATOR STATEMENT

I certify that on 9/6/23 (date) I completed a site evaluation on this property and state that the data reported are accurate and that the proposed system is in compliance with the Subsurface Wastewater Disposal Rules (10-144A CMR 241).

Site Evaluator Signature

352
SE #

Date

BRADY A. FRICK

Site Evaluator Name Printed

(207) 839-5563
Telephone Number

INFO@ALBERTFRICK.COM
E-mail Address

ALBERT FRICK ASSOCIATES - 731 FOSS ROAD, LIMERICK, MAINE 04048 - (207) 839-5563
Note: Changes to or deviations from the design should be confirmed with the Site Evaluator

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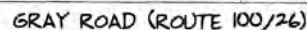
Department of Health and Human Services
Division of Environmental Health
(207) 287-2070 FAX (207) 287-4172

Owner's Name

PRIORITY REAL ESTATE GROUP, LLC

Scale 1" = 100 Ft.
or as shown

SITE LOCATION PLAN
(Attach Map from Maine
Atlas Recommended)



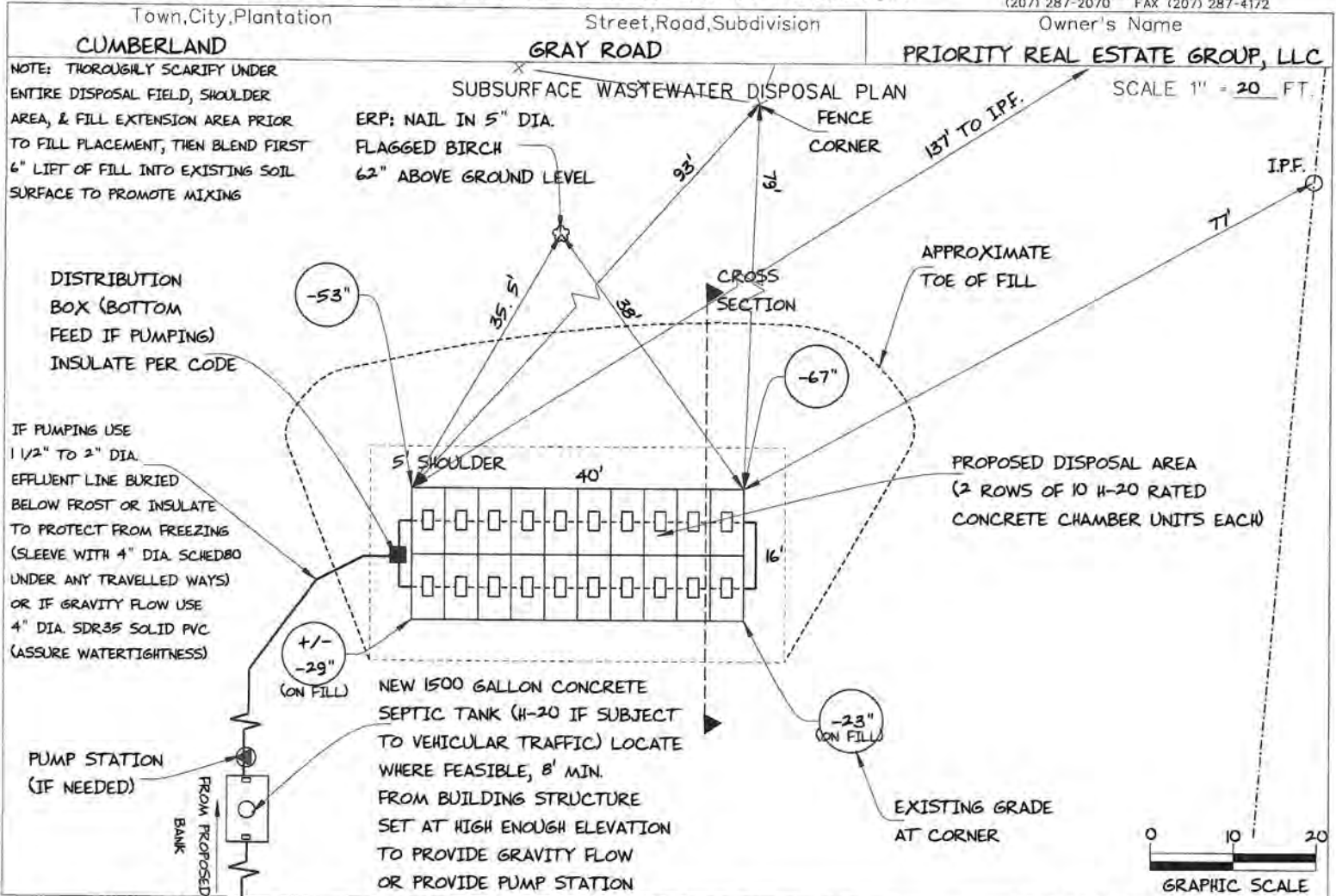
Observation Hole _____ ☐ Test Pit ☐ Boring
 _____ " Depth of Organic Horizon Above Mineral Soil

Date _____

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SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION

Department of Health and Human Services
Division of Environmental Health
(207) 287-2070 FAX (207) 287-4172



FILL REQUIREMENTS

Depth of Fill (Upslope)

0"

Depth of Fill (Downslope)

23" - 37"

DEPTHS AT CROSS-SECTION (shown below)

CONSTRUCTION ELEVATIONS

Finished Grade Elevation

Top of Distribution Pipe or Proprietary Device

Bottom of Disposal Area

SEE
DETAIL
BELOW

ELEVATION REFERENCE POINT

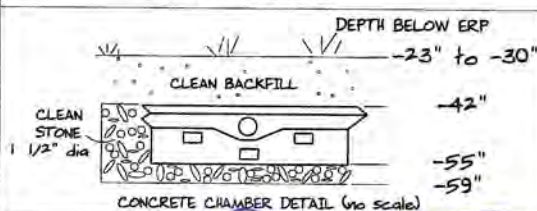
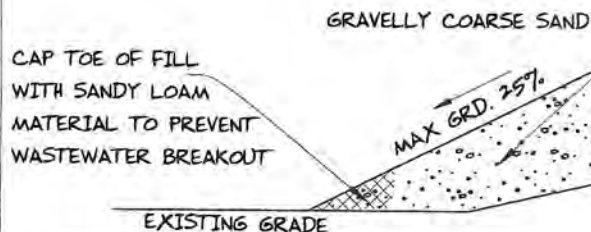
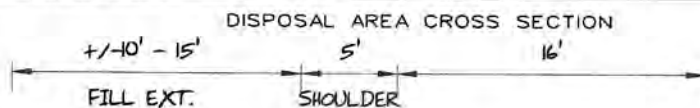
Location & Description 5" DIA. FLAGGED BIRCH, NAIL 62" ABOVE BASE

Reference Elevation is: 0.0" or -----

SCALE:

VERTICAL: 1" = 5 FT

HORIZONTAL: 1" = 10 FT



SCARIFY (SEE NOTE ABOVE)

1 1/2 INCH CLEAN CRUSHED STONE PLACE 12" THICKNESS OF CRUSHED STONE AROUND ENTIRE PERIMETER AND 4" BENEATH DISPOSAL AREA

EXISTING GRADE

REMOVE ALL PORTIONS OF UNCONTROLLED FILL MATERIAL ENCOUNTERED TO A MINIMUM DEPTH OF 2' UNDERNEATH AND 5' ALONGSIDE DISPOSAL AREA AND REPLACE WITH CLEAN GRAVELLY COARSE SAND FILL

Site Evaluator Signature

352

SE

Date

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HHE-200 Rev. 02/11



Albert Frick Associates, Inc.
Soil Scientists & Site Evaluators
731 Foss Road Limerick, Maine 04048
(207) 839-5563

CUMBERLAND

GRAY ROAD

PRIORITY REAL ESTATE GROUP, LLC

TOWN

LOCATION

APPLICANT'S NAME

1) The Plumbing and Subsurface Wastewater Disposal Rules adopted by the State of Maine, Division of Health and Human Services pursuant to 22 M.R.S.A. § 42 (the "Rules") are incorporated herein by reference and made a part of this application and shall be consulted by the owner/applicant, the system installer and/or building contractor for further construction details and material specifications. The system Installer should contact Albert Frick Associates, Inc. 839-5563, if there are any questions concerning materials, procedures or designs. The system installer and/or building contractor installing the system shall be solely responsible for compliance with the Rules and with all state and municipal laws and ordinances pertaining to the permitting, inspection and construction of subsurface wastewater disposal systems.

2) This application is intended to represent facts pertinent to the Rules only. It shall be the responsibility of the owner/applicant, system Installer and/or building contractor to determine compliance with and to obtain permits under all applicable local, state and/or federal laws and regulations (including, without limitation, Natural Resources Protection Act, wetland regulations, zoning ordinances, subdivision regulations, Site Location of Development Act and Minimum Lot Size law) before installing this system or considering the property on which the system is to be installed a "buildable" lot. It is recommended that a wetland scientist be consulted regarding wetland regulations. Prior to the commencement of construction/installation, the local plumbing inspector or Code Enforcement Officer shall inform the owner/applicant and Albert Frick Associates, Inc of any local ordinances which are more restrictive than the Rules in order that the design may be amended. All designs are subject to review by local, state and/or federal authorities. Albert Frick Associates, Inc.'s liability shall be limited to revisions required by regulatory agencies pursuant to laws or regulations in effect at the time of preparation of this application.

3) All information shown on this application relating to property lines, well locations, subsurface structures and underground facilities (such as utility lines, drains, septic systems, water lines, etc.) are based upon information provided by the owner/applicant and has been relied upon by Albert Frick Associates, Inc. in preparing this application. The owner/applicant shall review this application prior to the start of construction and confirm this information. Well locations on abutting properties but not readily visible above grade should be confirmed by the owner/applicant prior to system installation to assure minimum setbacks.

4) Installation of a garbage (grinder) disposal is not recommended. If one is installed, an additional 1000 gallon septic tank or a septic tank filter shall be connected in series to the proposed septic tank. Risers and covers should be installed over the septic tank outlet per the "Rules" to allow for easy maintenance of filter.

5) The septic tank should be pumped within two years of installation and subsequently as recommended by the pump service, but in no event should the septic tank be pumped less often than every three years.

The system user shall avoid introducing kitchen grease or fats into this system. Chemicals such as septic tank cleaners and/or chlorine or water treatment backwash and controlled or hazardous substances shall not be disposed of in this system. Additives such as yeast or enzymes are discouraged, since they have not been proven to extend system life.

6) All septic tanks, pump stations and additional treatment tanks shall be installed to prevent ground water and surface water infiltration. Risers and covers should be properly installed to provide access while preventing surface water intrusion to finished ground surface. One 18" dia. (min) riser and cover is required over septic tank

Vehicular traffic over disposal system is prohibited unless specifically designed with H-20 rated components.

CUMBERLAND

GRAY ROAD

PRIORITY REAL ESTATE GROUP, LLC

TOWN

LOCATION

APPLICANT'S NAME

- 7) The actual waste water flow or number of bedrooms shall not exceed the design criteria indicated on this application without a re-evaluation of the system as proposed
- 8) The general minimum setbacks between a well (public or private) and septic system serving a single family residence is 100-300 feet, unless the local municipality has a more stringent requirement. A well installed by an abutter within the minimum setback distances prior to the issuance of a permit for the proposed disposal system may void this design.
- 9) When a gravity system is proposed: BEFORE CONSTRUCTION/INSTALLATION BEGINS, the system installer or building contractor shall review the elevations of all points given in this application and the elevation of the existing and/or proposed building drain and septic tank inverts for compatibility to minimum pitch requirements. In gravity systems, the invert of the septic tank(s) outlet(s) should be at least 4 inches above the invert of the distribution box outlet at the disposal area.
- 10) When an effluent pump is required: Pump stations should be sized per manufacturer's specifications to meet lift requirements and friction loss. Provisions shall be made to make certain that surface and ground water does not enter the septic tank or pump station, by sealing/grouting all seams and connections, and by placement of a riser and 18" dia. (min.) cover at or above grade.
An alarm device warning of a pump failure shall be installed. Also, when pumping is required of a chamber system, install a 'T' connection in the distribution box and place 3 inches of stone or a splash plate in the first chamber. Insulate gravity pipes, pump lines and the distribution box as necessary to prevent freezing.
- 11) On all systems, remove the vegetation, organic duff and old fill material from under the disposal area and any fill extension. Additional fill beyond indicated on plan may be necessary to replace organic matter. On sites where the proposed system is to be installed in natural soil, scarify the bottom and sides of the excavated disposal area with a rake. Do not use wheeled equipment on the scarified soil surface. For systems installed in fill, scarify the native soil by roto-tilling or scarifying with teeth of backhoe to a depth of at least 8 inches over the entire disposal and fill extension area to prevent glazing and to promote fill bonding. Place fill in loose layers no deeper than 8 inches and compact before placing more fill (this ensures that voids and loose pockets are eliminated to minimize the chance of leakage or differential settling). Do not use wheeled equipment on the scarified soil area until after 12 inches of fill is in place. Keep equipment off proprietary devices. Divert the surface water away from the disposal area by ditching or shallow landscape swales.
- 12) Unless noted otherwise, fill shall be gravelly coarse sand, which contains no more than 5% fines (silt and clay). Crushed stone shall be clean and free of any rock dust from the crushing process.
- 13) Do not install systems on loamy, silty, or clayey soils during wet periods since soil smearing/glazing may seal off the soil interface.
- 14) Seed all filled and disturbed surfaces with perennial grass seed, with 4" min. soil or soil amendment mix suitable for growing, then mulch with hay or equivalent material to prevent erosion. Alternatively, bark or permanent landscape mulch may be used to cover system. Woody trees or shrubs are not permitted on the disposal area or fill extensions.
- 15) If an advanced wastewater treatment unit is part of the design, the system shall be operated and maintained per manufacturer's specifications.



Albert Frick Associates, Inc.

Soil Scientists & Site Evaluators

731 Fox Road Limerick, Maine 04048

(207) 839-5563

SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION

Maine Dept. Health & Human Services
Div of Environmental Health, 11 SHS
(207) 287-2070 FAX (207) 287-4172

PROPERTY LOCATION		>>CAUTION: LPI APPROVAL REQUIRED<<	
City, Town, or Plantation	CUMBERLAND	Town/City	Permit #
Street or Road	GRAY ROAD	Date Permit Issued	Fee \$ Double Fee Charged []
Subdivision, Lot #			L.P.I.#
OWNER/APPLICANT INFORMATION		Local Plumbing Inspector Signature	
Name (last, first, MI)	<input type="checkbox"/> Owner PRIORITY REAL ESTATE GROUP, LLC <input checked="" type="checkbox"/> Applicant	Fee \$	State Fee Fee \$ Locally Adopted Fee
Mailing Address of Owner/Applicant	20 BRANDON CUMMINGS PRIORITY REAL ESTATE GROUP, LLC 2 MAIN STREET TOPSHAM, ME 04086	The Subsurface Wastewater Disposal System shall not be installed until a Permit is issued by the Local Plumbing Inspector. The Permit shall authorize the owner or installer to install the disposal system in accordance with this application and the Maine Subsurface Wastewater Disposal Rules.	
Daytime Tel. #	248-7983	Municipal Tax Map # 1-19 Lot # 13	
OWNER OR APPLICANT STATEMENT		CAUTION: INSPECTION REQUIRED	
I state and acknowledge that the information submitted is correct to the best of my knowledge and understand that any falsification is reason for the Department and/or Local Plumbing Inspector to deny a permit.		I have inspected the installation authorized above and found it to be in compliance with the Subsurface Wastewater Disposal Rules Application.	
Signature of Owner/Applicant		Local Plumbing Inspector Signature	
Date		(1st) Date Approved	
		(2nd) Date Approved	

PERMIT INFORMATION

TYPE OF APPLICATION	THIS APPLICATION REQUIRES	DISPOSAL SYSTEM COMPONENTS
<input checked="" type="checkbox"/> 1. First Time System <input type="checkbox"/> 2. Replacement System Type Replaced: Year Installed: <input type="checkbox"/> 3. Expanded System <input type="checkbox"/> a. <25% Expansion <input type="checkbox"/> b. >25% Expansion <input type="checkbox"/> 4. Experimental System <input type="checkbox"/> 5. Seasonal Conversion	<input checked="" type="checkbox"/> 1.No Rule Variance <input type="checkbox"/> 2.First Time System Variance <input type="checkbox"/> a. Local Plumbing Inspector Approval <input type="checkbox"/> b. State & Local Plumbing Inspector Approval <input type="checkbox"/> 3.Replacement System Variance <input type="checkbox"/> a. Local Plumbing Inspector Approval <input type="checkbox"/> b. State & Local Plumbing Inspector Approval <input type="checkbox"/> 4.Minimum Lot Size Variance <input type="checkbox"/> 5.Seasonal Conversion Permit	<input checked="" type="checkbox"/> 1. Complete Non-Engineered System <input type="checkbox"/> 2. Primitive System(graywater & alt toilet) <input type="checkbox"/> 3. Alternative Toilet, specify: <input type="checkbox"/> 4. Non-Engineered Treatment Tank (only) <input type="checkbox"/> 5. Holding Tank, _____ gallons <input type="checkbox"/> 6. Non-Engineered Disposal Field (only) <input type="checkbox"/> 7. Separated Laundry System <input type="checkbox"/> 8. Complete Engineered System(2000gpd+) <input type="checkbox"/> 9. Engineered Treatment Tank (only) <input type="checkbox"/> 10. Engineered Disposal Field (only) <input checked="" type="checkbox"/> 11. Pre-treatment, specify: 1000 GALLON <input type="checkbox"/> 12. Miscellaneous components GREASE TRAP
SIZE OF PROPERTY	DISPOSAL SYSTEM TO SERVE	TYPE OF WATER SUPPLY
1.9 +/- <input type="checkbox"/> SQ. FT. <input checked="" type="checkbox"/> ACRES	<input type="checkbox"/> 1. Single Family Dwelling Unit, No. of Bedrooms: _____ <input type="checkbox"/> 2. Multiple Family Dwelling, No of Units: _____ <input checked="" type="checkbox"/> 3. Other: GAS STATION & CONVENIENCE STORE (specify) Current Use <input type="checkbox"/> Seasonal <input type="checkbox"/> Year Round <input checked="" type="checkbox"/> Undeveloped	<input type="checkbox"/> 1. Drilled Well <input type="checkbox"/> 2. Dug Well <input type="checkbox"/> 3. Private <input checked="" type="checkbox"/> 4. Public <input type="checkbox"/> 5. Other:
SHORELAND ZONING		
<input type="checkbox"/> Yes <input checked="" type="checkbox"/> No		

DESIGN DETAILS (SYSTEM LAYOUT SHOWN ON PAGE 3)

2 TREATMENT TANKS	DISPOSAL FIELD TYPE & SIZE	GARBAGE DISPOSAL UNIT	DESIGN FLOW
IN SERIES <input checked="" type="checkbox"/> 1. Concrete <input checked="" type="checkbox"/> a. Regular <input type="checkbox"/> b. Low Profile PROVIDE RISERS AND COVERS <input type="checkbox"/> 2. Plastic <input type="checkbox"/> 3. Other: CAPACITY: 2-1500's GAL. SEE NOTE ON PAGE 3	<input type="checkbox"/> 1. Stone Bed <input type="checkbox"/> 2. Stone Trench <input checked="" type="checkbox"/> 3. Proprietary Device <input type="checkbox"/> a. Cluster array <input checked="" type="checkbox"/> c.Linear <input checked="" type="checkbox"/> b. Regular <input type="checkbox"/> d. H-20 loaded <input type="checkbox"/> 4. Other: SIZE: 3300 <input checked="" type="checkbox"/> sq. ft. <input type="checkbox"/> lin. ft. 66 HIGH CAPACITY PLASTIC CHAMBER UNITS	<input checked="" type="checkbox"/> 1. No <input type="checkbox"/> 2. Yes <input type="checkbox"/> 3. Maybe If Yes or Maybe, specify one below: <input type="checkbox"/> a. Multi-compartment tank <input type="checkbox"/> b. _____ tanks in series <input type="checkbox"/> c. Increase in tank capacity <input type="checkbox"/> d. Filter on tank outlet	964 gallons per day BASED ON: <input type="checkbox"/> 1. Table 4A (dwelling unit(s)) <input checked="" type="checkbox"/> 2. Table 4C (other facilities) SHOW CALCULATIONS for other facilities SEE WATER USE RECORDS FROM SIMILAR STORES (USING PEAK FLOW FOR DESIGN PURPOSES) <input type="checkbox"/> 3. Section 4G (meter readings) ATTACH WATER-METER DATA
SOIL DATA & DESIGN CLASS	DISPOSAL FIELD SIZING	EFFLUENT/EJECTOR PUMP	LATITUDE AND LONGITUDE
PROFILE CONDITION S / C at Observation Hole # TP 2 Depth 30 " of Most Limiting Soil Factor	<input checked="" type="checkbox"/> 1. Medium - 2.6 sq.ft./gpd <input type="checkbox"/> 2. Medium-Large - 3.3 sq.ft./gpd <input type="checkbox"/> 3. Large - 4.1 sq.ft./gpd <input type="checkbox"/> 4. Extra-Large - 5.0 sq.ft./gpd	PROVIDE RISERS AND COVERS <input type="checkbox"/> 1. Not required <input checked="" type="checkbox"/> 2. May be required <input type="checkbox"/> 3. Required Specify only for engineered systems: SEE NOTE ON PAGE 3 DOSE: _____ gallons	at center of disposal area Lat. N 43 d 48 m 53.62 s Lon. W 70 d 18 m 44.54 s If g.p.s., state margin of error

SITE EVALUATOR STATEMENT

I certify that on 9/6/23 (date) I completed a site evaluation on this property and state that the data reported are accurate and that the proposed system is in compliance with the Subsurface Wastewater Disposal Rules (10-144A CMR 241).

Site Evaluator Signature BRADY A. FRICK Site Evaluator Name Printed	352 SE # (207) 839-5563 Telephone Number	9/27/23 Date INFO@ALBERTFRICK.COM E-mail Address
---	---	---

ALBERT FRICK ASSOCIATES - 731 FOSS ROAD, LIMERICK, MAINE 04048 - (207) 839-5563

Note: Changes to or deviations from the design should be confirmed with the Site Evaluator

Page 1 of 3
HHE-200 Rev. 11/2013

SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION

Department of Health and Human Services
Division of Environmental Health
(207) 287-2070 FAX (207) 287-4172

Town, City, Plantation CUMBERLAND	Street, Road Subdivision GRAY ROAD	Owner's Name PRIORITY REAL ESTATE GROUP, LLC
ALBERT FRICK ASSOCIATES ARE NOT SURVEYORS PROPERTY INFORMATION APPROXIMATED PER PLAN BY PRIORITY REAL ESTATE GROUP, DATED 8-7-23, TOWN TAX MAP AND AERIAL PHOTOGRAPH. VERIFY PROPERTY LINES TO ASSURE ACCURATE LOCATION PRIOR TO SYSTEM INSTALLATION		SITE LOCATION PLAN (Attach Map from Maine Atlas Recommended)
Scale 1" = 100 Ft. or as shown		
SITE PLAN		
<p>100'± TO WELL (ERP) 16" DIA FLAGGED OAK END OF FENCE WELL IPF FLAGS (4) AS STAKED IN THE FIELD PROPOSED DISPOSAL AREA TP 2 PROPOSED GAS PUMPS PROPOSED PARKING PROPOSED GAS STATION/STORE SKILLIN ROAD GRAY ROAD (ROUTE 100/26) BLACKSTRAP ROAD</p>		

SOIL DESCRIPTION AND CLASSIFICATION (Location of Observation Holes Shown Above)												
Observation Hole <u>TP 2</u> <input checked="" type="checkbox"/> Test Pit <input type="checkbox"/> Boring " Depth of Organic Horizon Above Mineral Soil					Observation Hole _____ <input type="checkbox"/> Test Pit <input type="checkbox"/> Boring " Depth of Organic Horizon Above Mineral Soil							
DEPTH BELOW MINERAL SOIL SURFACE (inches)	0	Texture	Consistency	Color	Mottling	DEPTH BELOW MINERAL SOIL SURFACE (inches)	0	Texture	Consistency	Color	Mottling	
	10	LOAMY SAND		BROWN			10					
	20		FRIABLE	DARK YELLOW BROWN			20					
	30	SAND		YELLOW BROWN			30					
	40		SOMEWHAT FIRM	LIGHT YELLOW BROWN			40					
	50						50					
	Soil Classification <u>S</u> <u>C</u> Slope <u>0-3</u> % Limiting Factor <u>30</u> "						Soil Classification _____ Slope _____ % Limiting Factor _____ "					
	Profile _____ Condition _____						Profile _____ Condition _____					
	<input type="checkbox"/> Ground Water <input type="checkbox"/> Restrictive Layer <input type="checkbox"/> Bedrock <input type="checkbox"/> Pit Depth						<input type="checkbox"/> Ground Water <input type="checkbox"/> Restrictive Layer <input type="checkbox"/> Bedrock <input type="checkbox"/> Pit Depth					

Site Evaluator Signature

352
SE #

Date

9/27/23
Page 2 of 3
HHE-200 Rev. 02/11

SUBSURFACE WASTEWATER DISPOSAL SYSTEM APPLICATION

Department of Health and Human Services
Division of Environmental Health
(207) 287-2070 FAX (207) 287-4172

Town, City, Plantation

Street, Road, Subdivision

Owner's Name

CUMBERLAND

GRAY ROAD

PRIORITY REAL ESTATE GROUP, LLC

NOTE: THOROUGHLY SCARIFY UNDER ENTIRE DISPOSAL FIELD, SHOULDER AREA, & FILL EXTENSION AREA PRIOR TO FILL PLACEMENT, THEN BLEND FIRST 6" LIFT OF FILL INTO EXISTING SOIL SURFACE TO PROMOTE MIXING

IF PUMPING USE 1 1/2" TO 2" DIA. EFFLUENT LINE BURIED BELOW FROST OR INSULATE TO PROTECT FROM FREEZING (SLEEVE WITH 4" DIA. SCHED 80 UNDER ALL TRAVELLED WAYS) OR IF GRAVITY FLOW USE 4" DIA. SDR 35 SOLID PVC (ASSURE WATERTIGHTNESS)

NEW 2-1500 GALLON CONCRETE SEPTIC TANKS IN SERIES LOCATE WHERE FEASIBLE, 8' MIN. FROM BUILDING STRUCTURE SET AT HIGH ENOUGH ELEVATION TO PROVIDE GRAVITY FLOW OR PROVIDE PUMP STATION

FROM STORE
KITCHEN WASTE ONLY

DISTRIBUTION BOX (BOTTOM FEED IF PUMPING) INSULATE PER CODE

PUMP STATION (IF NEEDED)

NEW 1000 GALLON CONCRETE GREASE TRAP (FOR KITCHEN WASTE ONLY) PLACE WHERE FEASIBLE, 8' MIN. FROM BUILDING STRUCTURE SET AT HIGH ENOUGH ELEVATION TO PROVIDE GRAVITY FLOW TO SEPTIC TANK

SUBSURFACE WASTEWATER DISPOSAL PLAN

ERP: NAIL IN 16" DIA. FLAGGED OAK 53" ABOVE GROUND LEVEL

FLAGS (4) AS STAKED IN THE FIELD

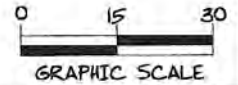
CROSS SECTION

SCALE 1" = 30 FT.
END OF FENCE

EXISTING GRADE AT CORNER

PROPOSED DISPOSAL AREA (6 ROWS 11 HIGH CAPACITY PLASTIC CHAMBER UNITS EACH)

APPROXIMATE TOE OF FILL



FILL REQUIREMENTS

Depth of Fill (Upslope) : 22" - 27"
Depth of Fill (Downslope) : 22" - 27"
DEPTHS AT CROSS-SECTION (shown below)

CONSTRUCTION ELEVATIONS

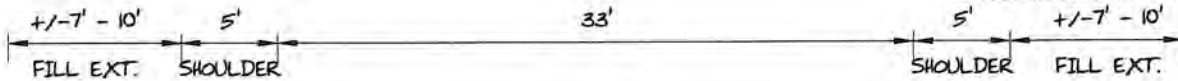
Finished Grade Elevation
Top of Distribution Pipe or Proprietary Device
Bottom of Disposal Area

SEE
DETAIL
BELOW

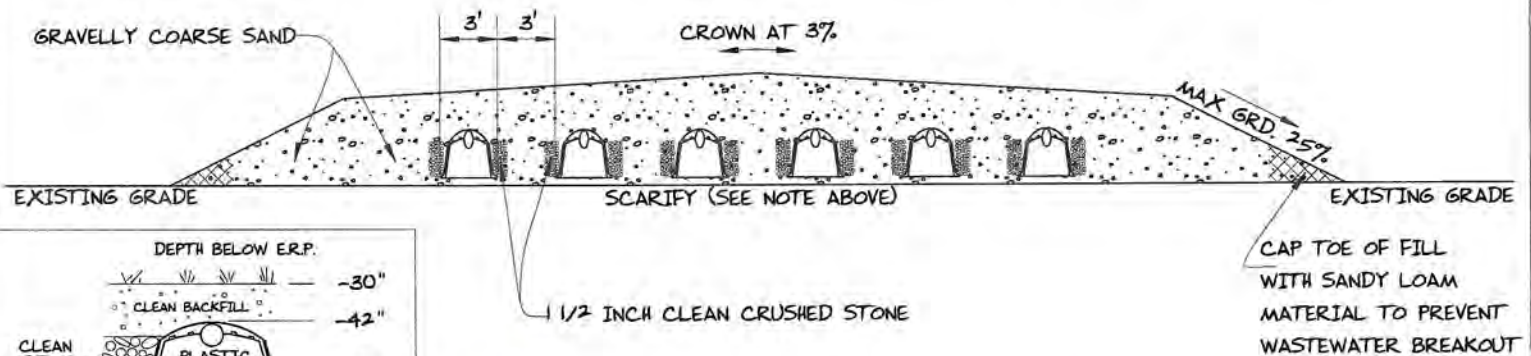
ELEVATION REFERENCE POINT

Location & Description 16" DIA. FLAGGED OAK, NAIL 53" ABOVE BASE
Reference Elevation is: 0.0" or -----

DISPOSAL AREA CROSS SECTION



SCALE:
VERTICAL: 1" = 5 FT
HORIZONTAL: 1" = 10 FT



DEPTH BELOW ERP:

-30"
-42"
-58"

CLEAN STONE 1 1/2" dia 6" envelope

By *Albert Frick*

Site Evaluator Signature

352

SE

7/27/23

Date

Page 3 of 3
HHE-200 Rev. 02/11

CUMBERLAND	GRAY ROAD	PRIORITY REAL ESTATE GROUP, LLC
TOWN	LOCATION	APPLICANT'S NAME

- 7) The actual waste water flow or number of bedrooms shall not exceed the design criteria indicated on this application without a re-evaluation of the system as proposed
- 8) The general minimum setbacks between a well (public or private) and septic system serving a single family residence is 100-300 feet, unless the local municipality has a more stringent requirement. A well installed by an abutter within the minimum setback distances prior to the issuance of a permit for the proposed disposal system may void this design.
- 9) When a gravity system is proposed: BEFORE CONSTRUCTION/INSTALLATION BEGINS, the system installer or building contractor shall review the elevations of all points given in this application and the elevation of the existing and/or proposed building drain and septic tank inverts for compatibility to minimum pitch requirements. In gravity systems, the invert of the septic tank(s) outlet(s) should be at least 4 inches above the invert of the distribution box outlet at the disposal area.
- 10) When an effluent pump is required: Pump stations should be sized per manufacturer's specifications to meet lift requirements and friction loss. Provisions shall be made to make certain that surface and ground water does not enter the septic tank or pump station, by sealing/grouting all seams and connections, and by placement of a riser and 18" dia. (min.) cover at or above grade.
An alarm device warning of a pump failure shall be installed. Also, when pumping is required of a chamber system, install a 'T' connection in the distribution box and place 3 inches of stone or a splash plate in the first chamber. Insulate gravity pipes, pump lines and the distribution box as necessary to prevent freezing.
- 11) On all systems, remove the vegetation, organic duff and old fill material from under the disposal area and any fill extension. Additional fill beyond indicated on plan may be necessary to replace organic matter. On sites where the proposed system is to be installed in natural soil, scarify the bottom and sides of the excavated disposal area with a rake. Do not use wheeled equipment on the scarified soil surface. For systems installed in fill, scarify the native soil by roto-tilling or scarifying with teeth of backhoe to a depth of at least 8 inches over the entire disposal and fill extension area to prevent glazing and to promote fill bonding. Place fill in loose layers no deeper than 8 inches and compact before placing more fill (this ensures that voids and loose pockets are eliminated to minimize the chance of leakage or differential settling). Do not use wheeled equipment on the scarified soil area until after 12 inches of fill is in place. Keep equipment off proprietary devices. Divert the surface water away from the disposal area by ditching or shallow landscape swales.
- 12) Unless noted otherwise, fill shall be gravelly coarse sand, which contains no more than 5% fines (silt and clay). Crushed stone shall be clean and free of any rock dust from the crushing process.
- 13) Do not install systems on loamy, silty, or clayey soils during wet periods since soil smearing/glazing may seal off the soil interface.
- 14) Seed all filled and disturbed surfaces with perennial grass seed, with 4" min. soil or soil amendment mix suitable for growing, then mulch with hay or equivalent material to prevent erosion. Alternatively, bark or permanent landscape mulch may be used to cover system. Woody trees or shrubs are not permitted on the disposal area or fill extensions.
- 15) If an advanced wastewater treatment unit is part of the design, the system shall be operated and maintained per manufacturer's specifications.



Albert Frick Associates, Inc.
Soil Scientists & Site Evaluators
731 Fox Road Limerick, Maine 04048
(207) 839-5563



Albert Frick Associates, Inc.
Soil Scientists & Site Evaluators
731 Foss Road Limerick, Maine 04048
(207) 839-5563

CUMBERLAND

GRAY ROAD

PRIORITY REAL ESTATE GROUP, LLC

TOWN

LOCATION

APPLICANT'S NAME

1) The Plumbing and Subsurface Wastewater Disposal Rules adopted by the State of Maine, Division of Health and Human Services pursuant to 22 M.R.S.A. § 42 (the "Rules") are incorporated herein by reference and made a part of this application and shall be consulted by the owner/applicant, the system installer and/or building contractor for further construction details and material specifications. The system Installer should contact Albert Frick Associates, Inc. 839-5563, if there are any questions concerning materials, procedures or designs. The system installer and/or building contractor installing the system shall be solely responsible for compliance with the Rules and with all state and municipal laws and ordinances pertaining to the permitting, inspection and construction of subsurface wastewater disposal systems.

2) This application is intended to represent facts pertinent to the Rules only. It shall be the responsibility of the owner/applicant, system Installer and/or building contractor to determine compliance with and to obtain permits under all applicable local, state and/or federal laws and regulations (including, without limitation, Natural Resources Protection Act, wetland regulations, zoning ordinances, subdivision regulations, Site Location of Development Act and Minimum Lot Size law) before installing this system or considering the property on which the system is to be installed a "buildable" lot. It is recommended that a wetland scientist be consulted regarding wetland regulations. Prior to the commencement of construction/installation, the local plumbing inspector or Code Enforcement Officer shall inform the owner/applicant and Albert Frick Associates, Inc of any local ordinances which are more restrictive than the Rules in order that the design may be amended. All designs are subject to review by local, state and/or federal authorities. Albert Frick Associates, Inc.'s liability shall be limited to revisions required by regulatory agencies pursuant to laws or regulations in effect at the time of preparation of this application.

3) All information shown on this application relating to property lines, well locations, subsurface structures and underground facilities (such as utility lines, drains, septic systems, water lines, etc.) are based upon information provided by the owner/applicant and has been relied upon by Albert Frick Associates, Inc. in preparing this application. The owner/applicant shall review this application prior to the start of construction and confirm this information. Well locations on abutting properties but not readily visible above grade should be confirmed by the owner/applicant prior to system installation to assure minimum setbacks.

4) Installation of a garbage (grinder) disposal is not recommended. If one is installed, an additional 1000 gallon septic tank or a septic tank filter shall be connected in series to the proposed septic tank. Risers and covers should be installed over the septic tank outlet per the "Rules" to allow for easy maintenance of filter.

5) The septic tank should be pumped within two years of installation and subsequently as recommended by the pump service, but in no event should the septic tank be pumped less often than every three years.

The system user shall avoid introducing kitchen grease or fats into this system. Chemicals such as septic tank cleaners and/or chlorine or water treatment backwash and controlled or hazardous substances shall not be disposed of in this system. Additives such as yeast or enzymes are discouraged, since they have not been proven to extend system life.

6) All septic tanks, pump stations and additional treatment tanks shall be installed to prevent ground water and surface water infiltration. Risers and covers should be properly installed to provide access while preventing surface water intrusion to finished ground surface. One 18" dia. (min) riser and cover is required over septic tank

Vehicular traffic over disposal system is prohibited unless specifically designed with H-20 rated components.

Water Use Records and Percentile Calculations

rev. 02/2004

Date	cubic feet	gallons	# days	avg. gpd	Daily 80th percentile	Weekly 85th percentile	Monthly 90th percentile	Quarterly 95th percentile
29-Nov-2022	12381	92622.26	96	964.82	185	325	376	621
4-Jan-2023	14270	14129.00	36	392.47				
28-Sep-2023	400	29297.00	95	308.39				

total	cubic feet	gallons
average	27051.00	136048.26
	9017.00	11337.36

To use: Enter the date, number of days, and cubic feet. The gallons and percentiles will be calculated automatically by the spreadsheet. To add more readings, simply insert additional rows into the spreadsheet. Choose the percentile which corresponds to the reading frequency: daily, weekly, monthly, or quarterly.



CITY OF BROCKTON
OFFICE OF THE COLLECTOR OF TAXES
45 SCHOOL STREET
BROCKTON, MA 02301-4059
000084 0021935

The Commonwealth of Massachusetts

MARTIN S. BROPHY - TREASURER / COLLECTOR

ACCOUNT NO.
3-00334

Department of Public Works
WATER, SEWER, REFUSE UTILITY BILL

Hours: Monday - Friday, 8:30 AM - 4:30 PM

Phone: Collector's Office (508) 580-7130 Press 6
for payment questions

DPW (508) 580-7143 option 7 for Water and
Sewer billing questions and address changes.
(ACCOUNT NO. and BILL NUMBER required).

For Refuse/Recycling questions
(508) 580-7827

Interest at a rate of 14% per annum will accrue
on overdue payments from the due date
until the payment is made.

PAY ONLINE AT: www.brockton.ma.us

***NEW WATER USAGE MONITORING PROGRAM

my-broc.sensus-analytics.com/login.html#/signin

DO NOT USE THE DASH IN YOUR ACCOUNT NUMBER TO REGISTER

ALL FOR AADC 023 000084 0021935
BROCKTON 683 PLEASANT LLC
858 WASHINGTON ST STE 309
DEDHAM, MA 02026-6021



CUSTOMER PORTION

WATER & SEWER USER FEES - These fees are for the purpose of
repairing and maintaining the water and sewer infrastructure.

LOCATION		PARCEL ID		ACCOUNT NO.		BILL DATE	BILL NUMBER
683 PLEASANT ST		032017		3-00334		11/17/2022	1383267
CODE	READ CODE	PREVIOUS READ DATE	CURRENT READ DATE	PREVIOUS READING	CURRENT READING	USAGE	CHARGE
1WTRIR	A	06/25/2022	09/28/2022	3059	32356	29297	\$2,395.23

***If you do not have an "A" under the READ CODE column,
please call 508-580-7143 Ext. 7 for assistance. Thank you.***

NOTE: For the yard waste pickup schedule please refer to the insert. Winter parking ban in
effect on 12/01/22, please see insert. Per ordinance: **DO NOT** rake/blow leaves or snow into
the street. Sewer Preventative Maintenance: **DO NOT** use your sink, toilet or any other
drains to dispose of grease, oil, or fat.

REMINDER - Tampering with a City water meter results in a \$1,000.00 fine.

Water User Fee	
Sewer User Fee	
Total Current Charges	\$2,395.23
Past Due	\$0.00
Interest to Bill Date	\$0.00
Amount Due	\$2,395.23
Due & Payable	12/16/2022

PLEASE SEE REVERSE SIDE FOR IMPORTANT INFORMATION

YOUR CANCELLED CHECK IS YOUR RECEIPT

PLEASE USE ENCLOSED ENVELOPE FOR PAYMENT

Detach Here

Please return this portion of the bill with your payment

Detach Here

THE COMMONWEALTH OF MASSACHUSETTS
CITY OF BROCKTON - OFFICE OF THE COLLECTOR OF TAXES
45 SCHOOL STREET, BROCKTON, MA 02301-4059

LOCATION	PARCEL ID	ACCOUNT NO.	BILL DATE	BILL NUMBER
683 PLEASANT ST	032017	3-00334	11/17/2022	1383267
DEPARTMENT OF PUBLIC WORKS WATER, SEWER, REFUSE UTILITY BILL		Total Current Charges		\$2,395.23
		Past Due		\$0.00
		Interest to Bill Date		\$0.00
		Amount Due		\$2,395.23
		Due & Payable		12/16/2022

To pay your bill on-line go to
www.brockton.ma.us and click below Make a Payment.

To pay your bill on-line go to
www.brockton.ma.us and click below Make a Payment.

BROCKTON 683 PLEASANT LLC
858 WASHINGTON ST STE 309
DEDHAM, MA 02026-6021

"Please write ACCOUNT NO. on your check"

AMOUNT ENCLOSED

MAKE CHECKS PAYABLE TO: CITY OF BROCKTON
or PAY ONLINE AT: www.brockton.ma.us

04486042023001383267000002395234

PAYMENT COUPON



PROVIDENCE WATER

PO BOX 1456
PROVIDENCE, RI 02901-1456

This page has Billing and History Detail ONLY.

For TOTAL DUE, please see Total Amount Due
on **FIRST PAGE** of Billing Statement.

Account Number	820344
Bill To	C/O RUSTY LANTERN #4038, LLC 38 PLEASANT VALLEY PKWY 9 INDUSTRIAL PKWY SUITE 4 BRUNSWICK ME 04011
Service Location	36 PLEASANT VALLEY PKWY

Current Consumption

#Days	Read Date	Read Type	Meter Read	HCF
	11/29/2022	Actual	12381	
36	01/04/2023	Actual	14270	18.89
Total HCF				18.89

PROVIDENCE WATER OFFERS 0% INTEREST LOAN TO HELP HOMEOWNERS REPLACE PRIVATE LEAD SERVICE LINES

Providence Water is offering 10-year 0% interest loans for homeowners to replace their private lead service lines. To learn more, please call (401) 521-6303 or visit us online at: www.provwater.com/loan.

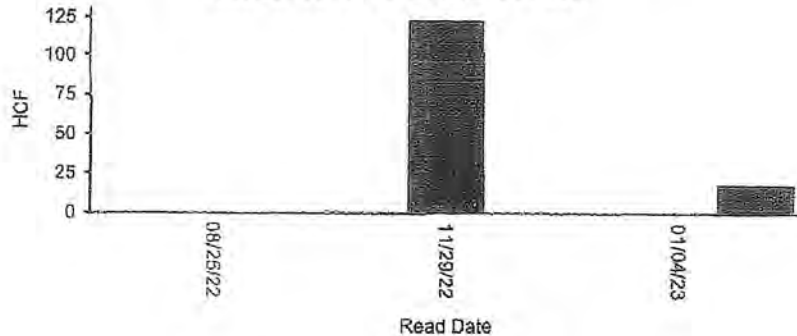
WATER QUALITY REPORT

The 2021 Water Quality Report is now available online at: www.provwater.com/waterqualityreport. To receive a printed copy, please call (401) 521-6303.

IMPORTANT INFORMATION: LEAD IN DRINKING WATER

Providence Water found high lead levels in drinking water in some homes with lead plumbing or service connections. Lead can cause serious health problems. Always flush from the cold faucet for at least 30 seconds when using water for drinking or cooking. If water has not been used for several hours, flush cold water for at least 3-5 minutes. For more information, please call Providence Water at (401) 521-6303 or visit our website at: www.provwater.com/lead.

Historical Usage Trend



# Days	Read Date	Actual Usage			
		Read	HCF	GAL	Gals/Day
0	08/25/22	0	0.00	0	
96	11/29/22	12381	123.81	92609	965
36	01/04/23	14270	18.89	14129	392

1 HCF = 100 CF = 748 gallons

The recommended usage is 65 gallons per person per day. Divide the gallons per day by the number of people in your household to determine your daily, per person usage.

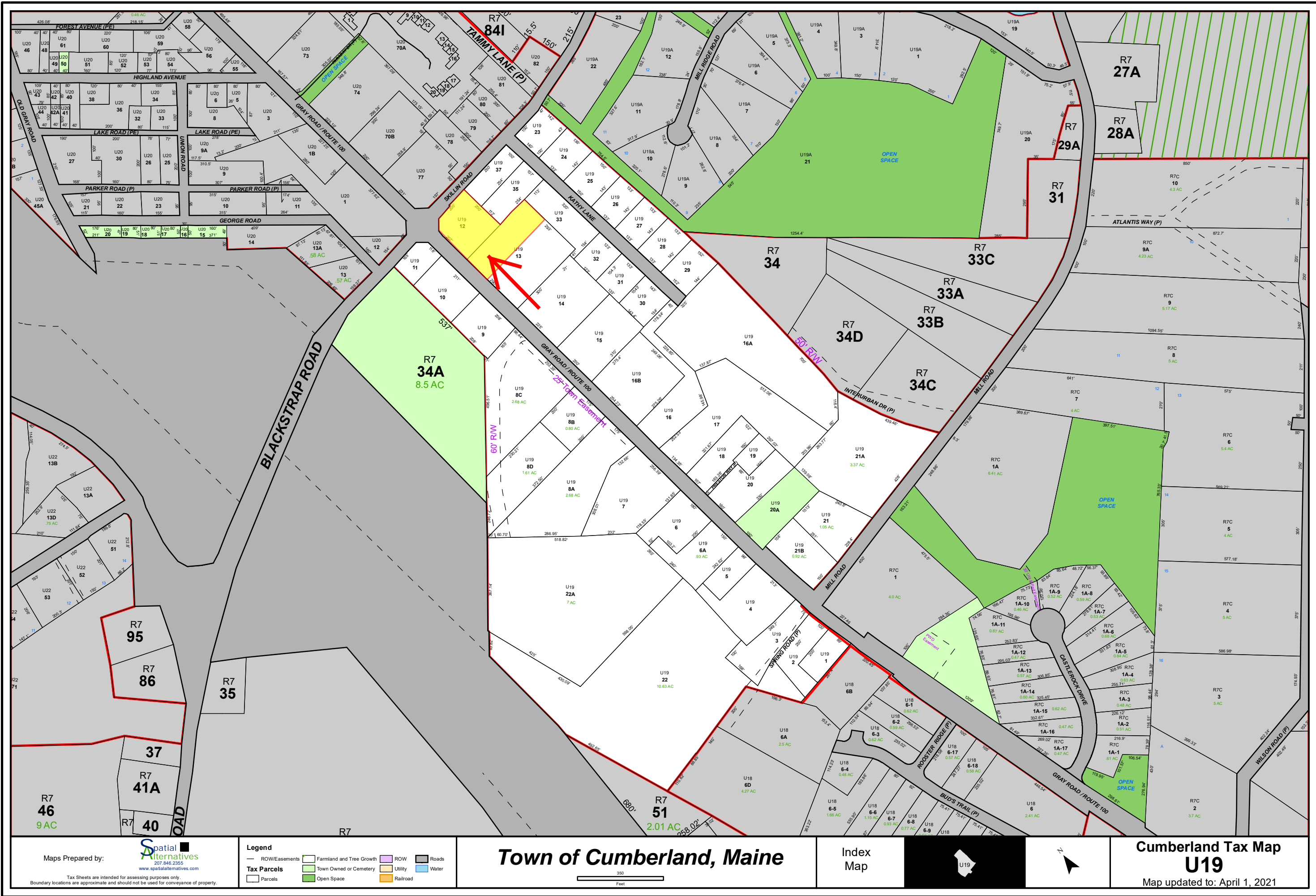
Attachment F **Supporting Graphics**

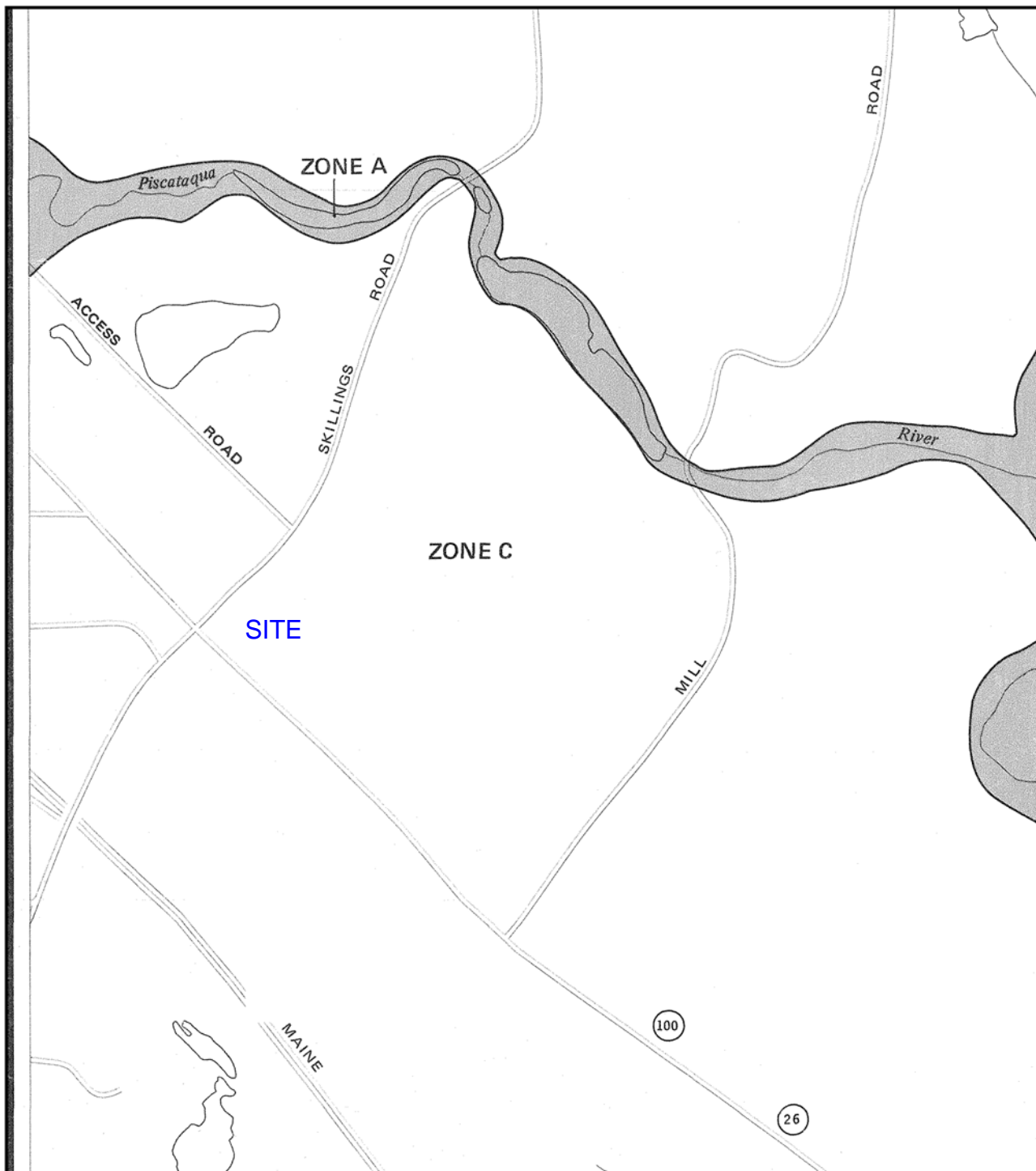
F

This attachment includes supporting materials and graphics for this application. This includes an excerpt of the applicable USGS 7.5-minute quadrangle map, an excerpt of the FEMA flood rate insurance map (FIRM), a reduced size copy of the tax map, and a NRCS soils map.

Supporting Graphics







Program at (800) 638-6620, or (800) 424-8872.



APPROXIMATE SCALE

800 0 800 FEET

NATIONAL FLOOD INSURANCE PROGRAM

FIRM
FLOOD INSURANCE RATE MAP

TOWN OF
CUMBERLAND, MAINE
CUMBERLAND COUNTY

PANEL 15 OF 25
(SEE MAP INDEX FOR PANELS NOT PRINTED)

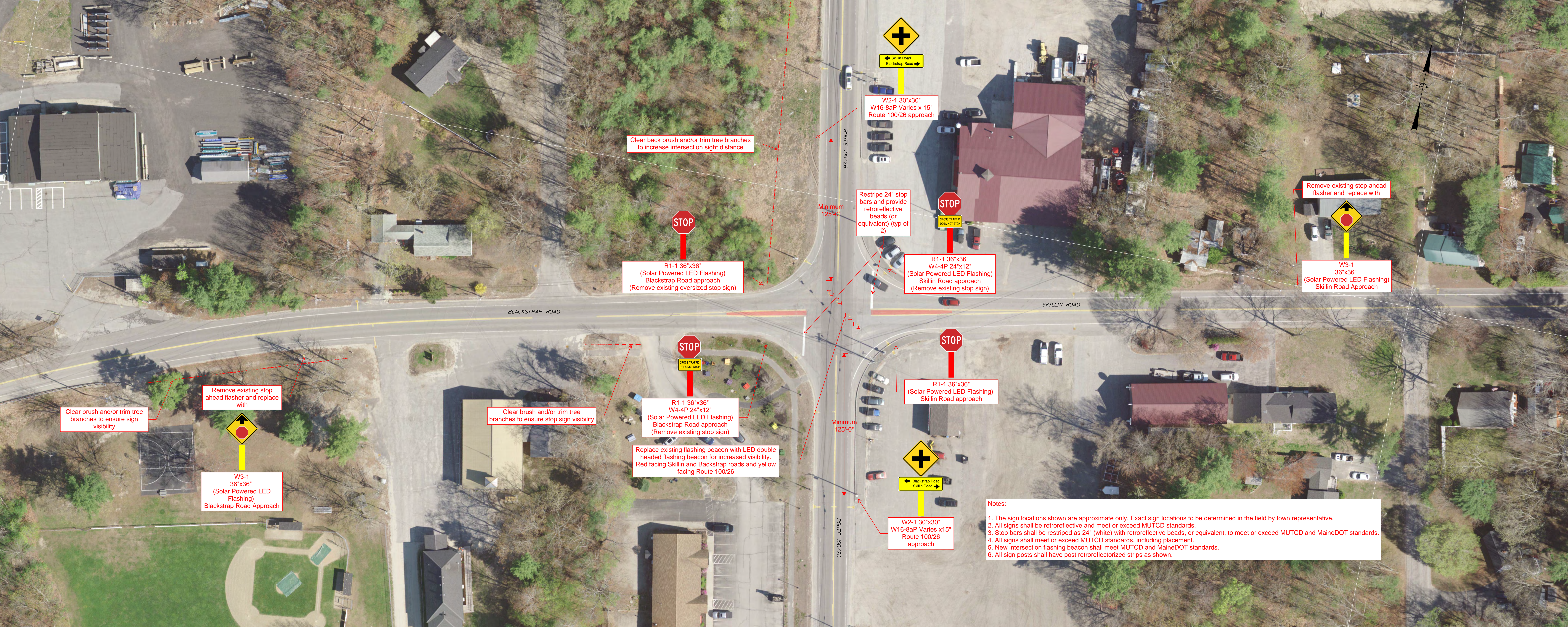
COMMUNITY-PANEL NUMBER
230162 0015 B

EFFECTIVE DATE:
MAY 19, 1981



federal emergency management agency
federal insurance administration

This is an official FIRMette showing a portion of the above-referenced flood map created from the MSC FIRMette Web tool. This map does not reflect changes or amendments which may have been made subsequent to the date on the title block. For additional information about how to make sure the map is current, please see the Flood Hazard Mapping Updates Overview Fact Sheet available on the FEMA Flood Map Service Center home page at <https://msc.fema.gov>.



Clear brush and/or trim tree branches to ensure sign visibility

Remove existing stop ahead flasher and replace with



W3-1 36"x36"
(Solar Powered LED Flashing)
Blackstrap Road Approach

Clear brush and/or trim tree branches to ensure stop sign visibility



R1-1 36"x36"
W4-4P 24"x12"
(Solar Powered LED Flashing)
Blackstrap Road approach
(Remove existing stop sign)

Replace existing flashing beacon with LED double headed flashing beacon for increased visibility. Red facing Skillin and Blackstrap roads and yellow facing Route 100/26

Clear back brush and/or trim tree branches to increase intersection sight distance



R1-1 36"x36"
(Solar Powered LED Flashing)
Blackstrap Road approach
(Remove existing oversized stop sign)

Minimum 125'-0"

ROUTE 100/26



W2-1 30"x30"
W16-8aP Varies x 15"
Route 100/26 approach

Restripe 24" stop bars and provide retroreflective beads (or equivalent) (typ of 2)



R1-1 36"x36"
W4-4P 24"x12"
(Solar Powered LED Flashing)
Skillin Road approach
(Remove existing stop sign)



R1-1 36"x36"
(Solar Powered LED Flashing)
Skillin Road approach



W2-1 30"x30"
W16-8aP Varies x15"
Route 100/26 approach

Remove existing stop ahead flasher and replace with



W3-1 36"x36"
(Solar Powered LED Flashing)
Skillin Road Approach

Notes:

1. The sign locations shown are approximate only. Exact sign locations to be determined in the field by town representative.
2. All signs shall be retroreflective and meet or exceed MUTCD standards.
3. Stop bars shall be restriped as 24" (white) with retroreflective beads, or equivalent, to meet or exceed MUTCD and MaineDOT standards.
4. All signs shall meet or exceed MUTCD standards, including placement.
5. New intersection flashing beacon shall meet MUTCD and MaineDOT standards.
6. All sign posts shall have post retroreflectorized strips as shown.

Attachment G **Financial and Technical Capability**

G

Priority Real Estate Group, LLC, has developed dozens of convenience stores over the last decade. The most recent Rusty Lantern Market locations are in Turner, West Paris, and Bethel, and have all opened in the last 6 months. Additional locations include Lisbon and Sabattus, Maine, and Loudon, NH. By focusing on Rusty Lantern Market projects, Priority Real Estate Group, LLC, has developed a proven system for designing and constructing facilities, which are operated by Rusty Lantern Market. Priority Real Estate Group, LLC, has assembled a team of contractors that construct the facilities and have a solid understanding of means and methods to execute the plans.

The project budget, including land acquisition and soft costs, is \$6,000,000. Financial support will be provided by Maine Community Bank. This attachment includes a Certificate of Good Standing from the Department of the Secretary of the State and a letter of financial capacity from Maine Community Bank.

**MAINE**Department of the Secretary of State
Bureau of Corporations, Elections and Commissions**Corporate Name Search**

Information Summary

[Subscriber activity report](#)

This record contains information from the CEC database and is accurate as of: Fri Jan 26 2024 16:22:35. Please print or save for your records.

Legal Name	Charter Number	Filing Type	Status
CUMBERLAND REAL ESTATE GROUP, LLC	20241327DC	LIMITED LIABILITY COMPANY	GOOD STANDING

Filing Date	Expiration Date	Jurisdiction
01/19/2023	N/A	MAINE

Other Names (A=Assumed ; F=Former)

NONE

Principal Home Office Address

Physical

Mailing

Clerk/Registered Agent

Physical

Mailing

SHAWN K BELL
C/O THE BELL FIRM, P.A.
810 LISBON STREET
LEWISTON, ME 04240

SHAWN K BELL
C/O THE BELL FIRM, P.A.
P.O. BOX 1776
LEWISTON, ME 04241-1776

[New Search](#)

Click on a link to obtain additional information.

List of Filings

[View list of filings](#)



January 26, 2024

Cumberland Real Estate Group
James Howard
2 Main Street, Suite 200
Topsham, ME 04086

To Whom it May Concern,

This letter is to confirm that Cumberland Real Estate Group has the financial capability to borrow up to \$6,000,000 in regards to the construction project located at 187 Gray Road, Cumberland, ME.

This is not a formal commitment letter.

Sincerely,



Justin Laverriere
Vice-President
Commercial Loan Officer III

Attachment H
Lighting Details

H

Information on the proposed lighting is enclosed for reference.

Lighting Details

Compact by design – **Packed with Performance!** The compact LED LNC2 family offers five different lumens packages for maximum light level and mounting height flexibility. LNC2 is designed for perimeter illumination for safety, security and identity. Typical mounting height is up to 15 feet with 50-60ft fixture spacing (without acrylic diffuser) and 40ft spacing (with acrylic diffuser installed). LNC2 is available with battery back-up in LNC2-12L units for egress applications.

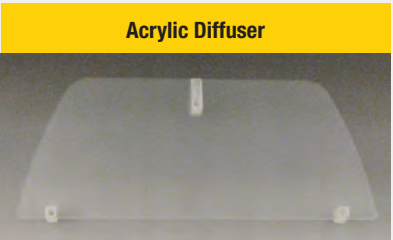


Shown with acrylic diffuser for reduced brightness applications



Quick Mounting

Quick mount – easy mounting without opening fixture. Attach adapter plate to wall, connect wires, hang fixture and tighten set screws.



Acrylic Diffuser

Frosted acrylic diffuser accessory – included with fixture! Softens output improves uniformity and protects LED lenses. Use near pedestrian entry applications or where low brightness is preferred.



Battery Backup

Battery back-up option provides 1fc average over 16'L x 48"W at 11' mounting in battery mode – Cold pack for operation down to -20°C



Motion Sensor

Sensor offers greater control and energy savings with SCP - programmable sensor with adjustable delay and dimming levels (factory default is 10%) – Accessory option

PERFORMANCE



LNC2-18L	3311 Lumens
Equivalency	250w MH



LNC2-12L	2420 Lumens
Equivalency	150w-175w MH

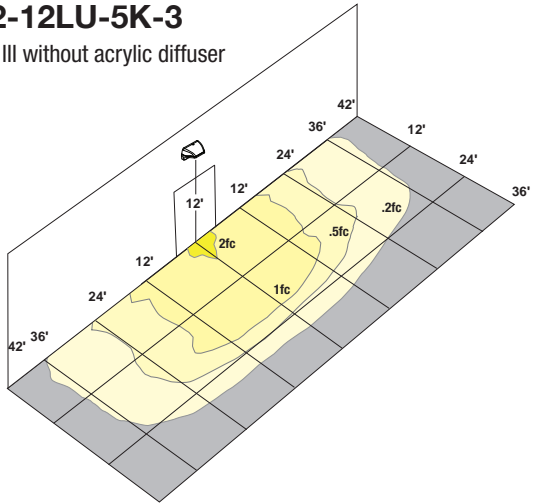


LNC-9L	1745 Lumens
Equivalency	70w MH

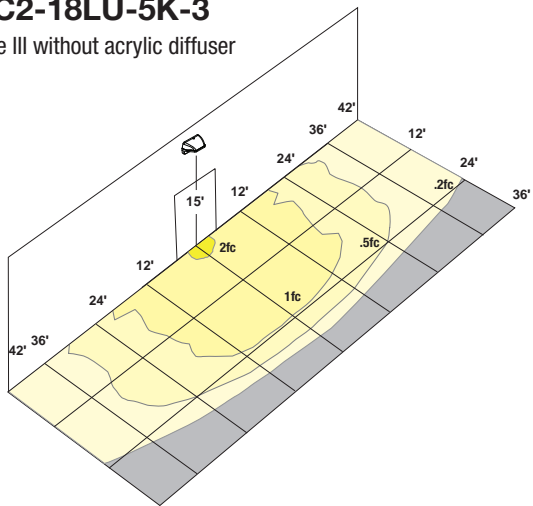


LNC-7L	1389 Lumens
Equivalency	50w MH

LNC2-12LU-5K-3
Type III without acrylic diffuser

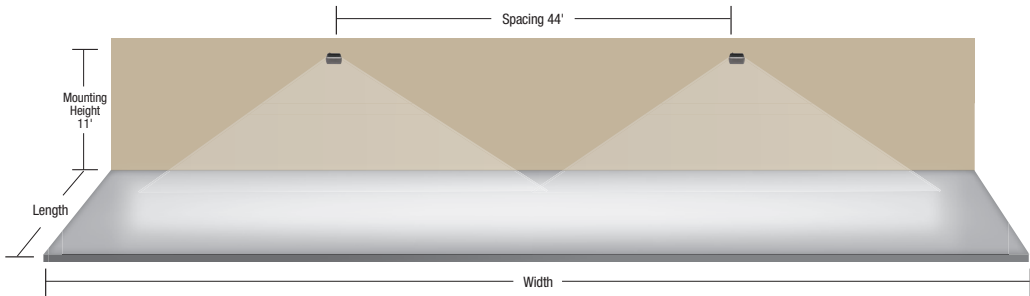


LNC2-18LU-5K-3
Type III without acrylic diffuser

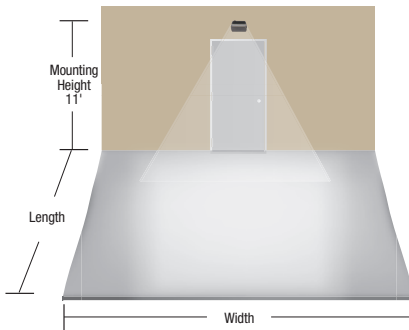


LNC2-12 BATTERY BACK-UP MODE PERFORMANCE

Provides Life Safety Code average illuminance of 1.0 fc. Assumes open space with no obstructions and mounting height of 11'. Diagrams for illustration purposes only, please consult factory for application layout.



Targeted Light Level Coverage		
Twin Unit installation	1 fc Average	1 fc Minimum
Length	16'	15'
Width	112'	68'



Targeted Light Level Coverage		
Single Unit installation	1 fc Average	1 fc Minimum
Length	16'	15'
Width	48'	24'

1 Over traditional sources
† Conduit wiring option not available in BBU unit

Due to our continued efforts to improve our products, product specifications are subject to change without notice.

LNC2 SERIES

Cat.#

Job

Type



HUBBELL
Outdoor Lighting

Approvals

SPECIFICATIONS

The small sized LNC2 is designed for perimeter illumination for safety, security and identification. No uplight and prismatic lenses offer neighbor friendly lighting at typical mounting heights of 8-15'. Units have protective polyester finish for long lasting appearance. Ideal for schools, factories, hospitals, warehouses and retail applications. Energy efficient LEDs provide up to 85% energy savings when compared to traditional light sources with little to no maintenance.

Construction:

Rugged die-cast aluminum housing protects components and provides an architectural appearance. Casting thermally conducts LED heat to optimize performance and long life. Powder paint finish provides durability in outdoor environments.

Electrical:

- 120V-277V universal voltage 50/60Hz 0-10V dimming drivers
- 347V and 480V dimmable driver option in 12L-070 configuration
- Minimum operating temperature is -40°C/-40°F (excludes 12L-035 and P15 configurations)
- Drivers have greater than .90 power factor and less than 20% Total Harmonic Distortion
- Driver RoHS and IP66
- 10kA surge protector

LED(s) CCT:

- 3000K CCT nominal, 4000K CCT nominal, 5000K CCT nominal (70 CRI)
- 9, 12 and 18 LED configurations available see pages 2 and 3 for electrical and photometric details

Optical:

Zero uplight distributions using individual acrylic LED optics provide IES type II, III and IV distributions. Optional (CS) acrylic diffuser available for reduced glare. Prismatic refractor lens provides ~10% uplight for increased vertical FC and forward light projection ideal for security lighting.

Lumen Maintenance:

L96 at 60,000hrs (Projected per IESNA TM-21-11), see table on page 2 for all values

Installation:

Quick-mount adapter provides easy installation to wall or to recessed junction boxes (4" square junction box). Designed for direct j-box mount. Optional 1/2" conduit hubs available (standard for sensor, SiteSync and battery versions).

Options/Controls:

- Universal button photocontrol
- Occupancy sensor options available for complete on/off and dimming control
- SiteSync pre-commissioned wireless controls (with or without sensor)
- Integral Battery Backup provides emergency lighting for the required 90 minute path of egress
- Dual Driver and Dual Power Feed option for 18L-070 versions

Listings:

- Listed to UL1598 and CSAC22.2#250.0-24 for wet locations
- DesignLights Consortium® (DLC) qualified. Please refer to the DLC website for specific product qualifications at www.designlights.org
- Made-to-order versions are IP-65 rated

Warranty:

Five year limited warranty (for more information visit: <https://www.hubbell.com/hubbelllighting/en/warranty>)

PRODUCT IMAGE(S)



Standard 9, 12, and 18L Version*



Prismatic Version



Surface Conduit Hubs, Sensor & SiteSync Version

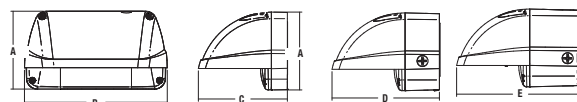


Battery Backup Version

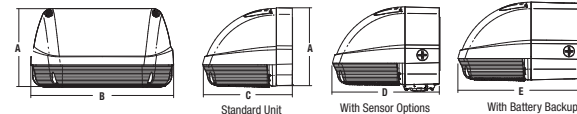
*Shown with CS acrylic diffuser

DIMENSIONS

9, 12, 18L units



Prismatic Refractor Units



A	B	C	D	E
5.54"	10.16"	6.33"	7.64"	9.10"
40.7 mm	258 mm	160.7 mm	194 mm	231 mm

BASE MODEL 7.0 lbs / 3.2 kg

PC SENSOR 7.5 lbs / 3.4 kg • BBU MODELS 9.5 lbs / 4.3 kg

SHIPPING INFORMATION (Stock)

Catalog Number	G.W(kg)/CTN	Carton Dimensions			Carton Qty. per Master Pack
		Length Inch (cm)	Width Inch (cm)	Height Inch (cm)	
LNC2-12LU	14.3 (6.5)	14.5 (37)	11.4 (29)	8.4 (21.5)	2
LNC2-18LU	14.8 (6.7)	14.9 (38)	11.4 (29)	8.4 (21.5)	2

CERTIFICATIONS/LISTINGS



C US



Turtle Friendly



*3000K and warmer CCTs only



LISTED

ORDERING INFORMATION – ORDERING EXAMPLE: LNC2-12L-4K-070-3-1-DB-PCU-EH-CS

LNC2

SERIES

LED SELECTION

CCT/CRI

DRIVE CURRENT

VOLTAGE

MOUNTING

CONTROL OPTIONS

OPTIONS

LNC2 Small
LitePak
LNC2

9L 9 LEDs
12L 12 LEDs
18L 18 LEDs
P15 15w Prismatic Refractor
P25 25w Prismatic Refractor
P35 35w Prismatic Refractor

3K 3000K, 70 CRI
4K 4000K, 70 CRI
5K 5000K, 70 CRI
AM Amber (350mA only)

070 700mA
035 350mA (12L & 18L only)

IES DISTRIBUTION

2' IES Type II
3' IES Type III
4' IES Type IV

FT Forward Throw (Prismatic Refractor only)

U 120V-277V
1 120V
2 208V
3 240V
4 277V
5⁸ 480V
F⁸ 347V

Leave Blank for down position
NV² Inverted

FINISH

DB Dark Bronze Textured
BL Black Textured
GYS Gray Smooth
PS Platinum Silver Smooth
WH White Textured
CC Custom Color

SCP^{4,5} Occupancy Sensor Programmable (Dim)
PCU Universal Button Photocontrol
SWP⁶ SiteSync Pre-Commission
SWPM SiteSync Pre-^{6,7} Commission w/ OCC Sensor

SPECIFY SCP HEIGHT

8F Up to 8ft mount height
20F Up to 20ft mount height

EH³ Battery Backup Unit with Heater (-30°C)
E³ Battery Backup Unit (0°C)
F³ Fuse & Fuse-holder (not available with Battery Backup)
CS Comfort Shield (N/A with Prismatic Refractor)
2DR Dual Driver (18L - 700mA only)
2PF Dual Power Feed (18L - 700mA only)
CH Surface Conduit Hubs

1 IES distributions only available with 9L, 12L, and 18L versions

2 Not available with occupancy sensor, battery backup or prismatic refractor options

3 Must specify voltage (120 or 277 only for E & EH)

4 Must order minimum of one remote control to program dimming settings, 0-10V fully adjustable dimming with automatic daylight calibration and different time delay settings, 120-277V only

5 PCU option not applicable, included in sensor

6 18L - 700mA versions only. Not available with 2DR or 2PF options. Must specify group and zone information at time of order

7 Specify time delay; dimming level and mounting height

8 12L - 700mA version only



HUBBELL
Outdoor Lighting

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Due to our continued efforts to improve our products, product specifications are subject to change without notice.

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VIPER Area/Site

VIPER LUMINAIRE

MICROSTRIKE | STRIKE OPTICS

FEATURES

- Low profile LED area/site luminaire with a variety of IES distributions for lighting applications such as auto dealership, retail, commercial, and campus parking lots
- Featuring two different optical technologies, Strike and Micro Strike Optics, which provide the best distribution patterns for retrofit or new construction
- Rated for high vibration applications including bridges and overpasses. All sizes are rated for 1.5G
- Control options including photo control, occupancy sensing, NX Lighting Controls™, wiSCAPE and 7-Pin with networked controls
- New customizable lumen output feature allows for the wattage and lumen output to be customized in the factory to meet whatever specification requirements may entail
- Field interchangeable mounting provides additional flexibility after the fixture has shipped



CONTROL TECHNOLOGY



SPECIFICATIONS

CONSTRUCTION

- Die-cast housing with hidden vertical heat fins are optimal for heat dissipation while keeping a clean smooth outer surface
- Corrosion resistant, die-cast aluminum housing with 1000 hour powder coat paint finish
- External hardware is corrosion resistant

OPTICS

- Micro Strike Optics (160, 320, 480, or 720 LED counts) maximize uniformity in applications and come standard with mid-power LEDs which evenly illuminate the entire luminous surface area to provide a low glare appearance. Catalog logic found on page 2
- Strike Optics (36, 72, 108, or 162 LED counts) provide best in class distributions and maximum pole spacing in new applications with high powered LEDs. Strike optics are held in place with a polycarbonate bezel to mimic the appearance of the Micro Strike Optics so both solutions can be combined on the same application. Catalog logic found on page 3
- Both optics maximize target zone illumination with minimal losses at the house-side, reducing light trespass issues. Additional backlight control shields and house side shields can be added for further reduction of illumination behind the pole
- One-piece silicone gasket ensures a weatherproof seal
- Zero up-light at 0 degrees of tilt
- Field rotatable optics

INSTALLATION

- Mounting patterns for each arm can be found on page 11
- Optional universal mounting block for ease of installation during retrofit applications. Available as an option (ASQU) or accessory for square and round poles
- All mounting hardware included

INSTALLATION (CONTINUED)

- Knuckle arm fitter option available for 2-3/8" OD tenon
- For products with EPA less than 1 mounted to a pole greater than 20ft, a vibration damper is recommended

ELECTRICAL

- Universal 120-277 VAC or 347-480 VAC input voltage, 50/60 Hz
- Ambient operating temperature -40°C to 40°C
- Drivers have greater than 90% power factor and less than 20% THD
- LED drivers have output power over-voltage, over-current protection and short circuit protection with auto recovery
- Field replaceable surge protection device provides 20kA protection meeting ANSI/IEEE C62.41.2 Category C High and Surge Location Category C3; Automatically takes fixture off-line for protection when device is compromised
- Dual Driver option provides 2 drivers within luminaire but only one set of leads exiting the luminaire, where Dual Power Feed provides two drivers which can be wired independently as two sets of leads are extended from the luminaire. Both options cannot be combined

CONTROLS

- Photo control, occupancy sensor programmable controls, and Zigbee wireless controls available for complete on/off and dimming control
- Please consult brand or sales representative when combining control and electrical options as some combinations may not operate as anticipated depending on your application
- 7-pin ANSI C136.41-2013 photocontrol receptacle option available for twist lock photocontrols or wireless control modules (control accessories sold separately)



10-DAY QUICK SHIP PROGRAM



CONTROLS (CONTINUED)

- 0-10V Dimming Drivers are standard and dimming leads are extended out of the luminaire unless control options require connection to the dimming leads. Must specify if wiring leads are to be greater than the 6" standard
- NX Lighting Controls™ available with in fixture wireless control module, features dimming and occupancy sensor
- wiSCAPE® available with in fixture wireless control module, features dimming and occupancy sensor. Also available in 7-pin configuration

CERTIFICATIONS

- DLC® (DesignLights Consortium Qualified), with some Premium Qualified configurations. Not all product variations listed in this document are DLC® qualified. Refer to <http://www.designlights.org> for the most up-to-date list.
- Listed to UL1598 and CSA C22.2#250.0-24 for wet locations and 40°C ambient temperatures
- 1.5 G rated for ANSI C136.31 high vibration applications
- Fixture is IP65 rated
- Meets IDA recommendations using 3K CCT configuration at 0 degrees of tilt
- This product qualifies as a "designated country construction material" per FAR 52.225-11 Buy American-Construction Materials under Trade Agreements effective 04/23/2020.

WARRANTY

- 5 year warranty

KEY DATA	
Lumen Range	5,000–80,000
Wattage Range	36–600
Efficacy Range (LPW)	92–155
Weight lbs. (kg)	13.7-30.9 (6.2-13.9)

VIPER Area/Site

VIPER LUMINAIRE

MICROSTRIKE OPTICS – ORDERING GUIDE

Example: VP-2-320L-145-3K7-2-R-UNV-A3-BLT

 = Service Program
 Limit of 15 luminaires


CATALOG #

VP	Optic Platform	Size	Light Engine	CCT/CRI	Distribution	Optic Rotation	Voltage
VP Viper	Micro Strike	1 Size 1	160L-35 ⁶ 5500 lumens 160L-50 ⁶ 7500 lumens 160L-75 10000 lumens 160L-100 12500 lumens 160L-115 15000 lumens 160L-135 18000 lumens 160L-160 21000 lumens 320L-145 21000 lumens 320L-170 24000 lumens 320L-185 27000 lumens 320L-210 30000 lumens 320L-235 33000 lumens 320L-255 36000 lumens 320L-315 ⁶ 40000 lumens 480L-285 40000 lumens 480L-320 44000 lumens 480L-340 48000 lumens 480L-390 52000 lumens 480L-425 55000 lumens 480L-470 60000 lumens 720L-435 60000 lumens 720L-475 65000 lumens 720L-515 70000 lumens 720L-565 ⁶ 75000 lumens 720L-600 ⁶ 80000 lumens CLO Custom Lumen Output ¹	AP AP-Amber Phosphor Converted 27K8 2700K, 80 CRI 3K7 3000K, 70 CRI 3K8 3000K, 80 CRI 35K8 3500K, 80 CRI 3K9 3000K, 90 CRI 4K7 4000K, 70 CRI 4K8 4000K, 80 CRI 4K9 4000K, 90 CRI 5K7 5000K, 70 CRI 5K8 5000K, 80 CRI	2 Type 2 3 Type 3 4F Type 4 Forward 4W Type 4 Wide 5QW Type 5 Square Wide	BLANK No Rotation L Optic rotation left R Optic rotation right	UNV 120-277V 120 120V 208 208V 240 240V 277 277V 347 347V 480 480V
		2 Size 2					
		3 Size 3					
		4 Size 4					

Mounting	Color	Options	Network Control Options
A Arm mount for square pole/flat surface (B3 Drill Pattern) (Does not include round pole adapter) A_ Arm mount for round pole ² ASQU Universal arm mount for square pole. Can be used with B3 or S2 Drill Pattern A_U Universal arm mount for round pole ² AAU Adjustable arm for pole mounting (universal drill pattern) AA_U Adjustable arm mount for round pole ² ADU Decorative upswept Arm (universal drill pattern) AD_U Decorative upswept arm mount for round pole ² MAF Mast arm fitter for 2-3/8" OD horizontal arm K Knuckle T Trunnion WB Wall Bracket, horizontal tenon with MAF WM Wall mount bracket with decorative upswept arm WA Wall mount bracket with adjustable arm	BLT Black Matte Textured BLS Black Gloss Smooth DBT Dark Bronze Matte Textured DBS Dark Bronze Gloss Smooth GTT Graphite Matte Textured LGS Light Grey Gloss Smooth LGT Light Grey Gloss Textured PSS Platinum Silver Smooth WHT White Matte Textured WHS White Gloss Smooth VGT Verde Green Textured Color Option CC Custom Color	F Fusing 2PF Dual Power Feed 2DR Dual Driver TE Toolless Entry BC Backlight Control ⁸ TB Terminal Block	NXWS16F NX Networked Wireless Enabled Integral NXSMP2-LMO PIR Occupancy Sensor with Automatic Dimming Photocell and Bluetooth Programming ^{1,3,4} NXWS40F NX Networked Wireless Enabled Integral NXSMP2-HMO PIR Occupancy Sensor with Automatic Dimming Photocell and Bluetooth Programming ^{1,3,4} NXW NX Networked Wireless Radio Module NXRM2 and Bluetooth Programming, without Sensor ^{3,4} WIR wiSCAPE® In-Fixture Module ^{3,4} WIRSC wiSCAPE® Module and Occupancy Sensor ^{3,4} Stand Alone Sensors BTS-14F Bluetooth® Programmable, BTSMP-LMO PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ⁹ BTS-40F Bluetooth® Programmable, BTSMP-HMO PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ⁹ BTSO-12F Bluetooth® Programmable, BTSMP-OMNI-O PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ⁹ 7PR 7-Pin Receptacle ⁴ 7PR-SC 7-Pin Receptacle with shorting cap ⁴ 3PR 3-Pin twist lock ⁴ 3PR-SC 3-Pin receptacle with shorting cap ⁴ 3PR-TL 3-Pin PCR with photocontrol ⁴ Programmed Controls SCP_F Sensor Control Programmable, 8F or 40F ¹⁰ ADD AutoDim Timer Based Dimming ⁴ ADT AutoDim Time of Day Dimming ⁴ Photocontrols PC Button Photocontrol ^{4,7}

1 – Items with a grey background can be done as a custom order. Contact brand representative for more information

2 – Replace “_” with “2” for 2.5”-3.4” OD pole, “3” for 3.5”-4.13” OD pole, “4” for 4.18”-5.25” OD pole, “5” for 5.5”-6.5” OD pole

3 – Networked Controls cannot be combined with other control options

4 – Not available with 2PF option

5 – Not available with Dual Driver option

6 – Some voltage restrictions may apply when combined with controls

7 – Not available with 480V

8 – BC not available on 4F and type 5 distributions

9 – BTS and BTSO are only available on Size 3 and Size 4

10 – At least one SCPREMOTE required to program SCP motion sensor. Must select 8ft or 40ft.



VIPER Area/Site

VIPER LUMINAIRE

DATE:	LOCATION:
TYPE:	PROJECT:
CATALOG #:	

STRIKE OPTIC – ORDERING GUIDE

Example: VP-ST-1-36L-39-3K7-2-UNV-A-BLT

CATALOG #								
VP								
Series	Optic Platform	Size	Light Engine		CCT/CRI		Distribution	Optic Rotation
VP Viper	ST Strike	1 Size 1	36L-39 ⁸	5500 lumens	AM	monochromatic amber, 595nm	FR Auto Front Row	BLANK No Rotation
			36L-55 ⁸	7500 lumens			2 Type 2	L Optic rotation left
			36L-85	10000 lumens	27K8	2700K, 80 CRI	3 Type 3	R Optic rotation right
			36L-105	12500 lumens	3K7	3000K, 70 CRI	4F Type 4 Forward	
			36L-120	14000 lumens	3K8	3000K, 80 CRI	4W Type 4 Wide	
		2 Size 2	72L-115	15000 lumens	3K9	3000K, 90 CRI	5QN Type 5 Square Narrow	
			72L-145	18000 lumens	35K8	3500K, 80 CRI	5QW Type 5 Square Wide	
			72L-180	21000 lumens	4K7	4000K, 70 CRI	5QM Type 5 Square Medium	
			72L-210	24000 lumens	4K8	4000K, 80 CRI	5W Type 5 Wide (Round)	
			72L-240	27000 lumens	4K9	4000K, 90 CRI	5RW Type 5 Rectangular	
		3 Size 3	108L-215 ⁸	27000 lumens	5K7	5000K, 70 CRI	C Corner Optic	
			108L-250	30000 lumens	5K8	5000K, 80 CRI	TC Tennis Court Optic	
			108L-280	33000 lumens				
			108L-325	36000 lumens				
			108L-365	40000 lumens				
		4 Size 4	162L-320	40000 lumens				
			162L-365 ¹⁰	44000 lumens				
			162L-405	48000 lumens				
			162L-445	52000 lumens				
			162L-485	55000 lumens				
			162L-545 ⁸	60000 lumens				
			CLO	Custom Lumen Output ¹				

Mounting	Color	Options	Network Control Options
A Arm mount for square pole/flat surface	BLT Black Matte Textured	F Fusing	NXWS16F NX Networked Wireless Enabled Integral NXSMP2-LMO PIR Occupancy Sensor with Automatic Dimming Photocell and Bluetooth Programming ^{1,3,4}
A_ Arm mount for round pole ³	BLS Black Gloss Smooth	E Battery Backup ^{1,2,7,8,9}	NXWS40F NX Networked Wireless Enabled Integral NXSMP2-HMO PIR Occupancy Sensor with Automatic Dimming Photocell and Bluetooth Programming ^{1,3,4}
ASQU Universal arm mount for square pole	DBT Dark Bronze Matte Textured	2PF Dual Power Feed	NXW NX Networked Wireless Radio Module NXRM2 and Bluetooth Programming, without Sensor ^{3,4}
A_U Universal arm mount for round pole ³	DBS Dark Bronze Gloss Smooth	2DR Dual Driver	WIR wiSCAPE® In-Fixture Module ^{3,4}
AAU Adjustable arm for pole mounting (universal drill pattern)	GTT Graphite Matte Textured	TE Tooless Entry	WIRSC wiSCAPE® Module and Occupancy Sensor ^{3,4}
AA_U Adjustable arm mount for round pole ³	LGS Light Grey Gloss Smooth	BC Backlight Control	Stand Alone Sensors
ADU Decorative upswept Arm (universal drill pattern)	LGT Light Grey Gloss Textured	TB Terminal Block	BTS-14F Bluetooth® Programmable, BTSMP-LMO PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ¹¹
AD_U Decorative upswept arm mount for round pole ³	PSS Platinum Silver Smooth		BTS-40F Bluetooth® Programmable, BTSMP-HMO PIR Occupancy Sensor with Automatic Dimming® Photocell and 360° Lens ¹¹
MAF Mast arm fitter for 2-3/8" OD horizontal arm	WHT White Matte Textured		BTSO-12F Bluetooth® Programmable, BTSMP-OMNI-O PIR Occupancy Sensor with Automatic Dimming Photocell and 360° Lens ¹¹
K Knuckle	WHS White Gloss Smooth		7PR 7-Pin Receptacle ⁴
T Trunnion	VGt Verde Green Textured		7PR-SC 7-Pin Receptacle with shorting cap ⁴
WB Wall Bracket, horizontal tenon with MAF	Color Option		3PR 3-Pin twist lock ⁴
WM Wall mount bracket with decorative upswept arm	CC Custom Color		3PR-SC 3-Pin receptacle with shorting cap ⁴
WA Wall mount bracket with adjustable arm			3PR-TL 3-Pin PCR with photocontrol ⁴
			Programmed Controls
			SCP_F Sensor Control Programmable, 8F or 40F ¹²
			ADD AutoDim Timer Based Dimming ⁴
			ADT AutoDim Time of Day Dimming ⁴
			Photocontrols
			PC Button Photocontrol ^{4,7}

¹ – Items with a grey background can be done as a custom order. Contact brand representative for more information

² – Battery temperature rating -20C to 55C

³ – Replace “_” with “3” for 3.5”-4.13” OD pole, “4” for 4.18”-5.25” OD pole, “5” for 5.5”-6.5” OD pole

⁴ – Networked Controls cannot be combined with other control options

⁵ – Not available with 2PF option

⁶ – Not available with 480V

⁷ – Not available with 347 or 480V

⁸ – Not available with Dual Driver option

⁹ – Only available in Size 1 housing, up to 105 Watts

¹⁰ – Some voltage restrictions may apply when combined with controls

¹¹ – BTS and BTSO are only available on Size 3 and Size 4

¹² – At least one SCPREMOTE required to program SCP motion sensor. Must select 8ft or 40ft.



currentlighting.com/beacon

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VIPER Area/Site

VIPER LUMINAIRE

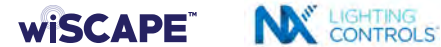
ORDERING GUIDE (CONTINUED)

CATALOG #

Accessory Type		Size	Option	Color			
SHD	Shield	1	Size 1	HSS-90-B	House Side Shield 90° Back	BLS	Black Gloss Smooth
		2	Size 2	HSS-90-F	House Side Shield 90° Front	BLT	Black Matte Textured
		3	Size 3	HSS-90-S	House Side Shield 90° Side	DBS	Dark Bronze Gloss Smooth
		4	Size 4	HSS-270-BSS	House Side Shield 270° Back/Side/Side	DBT	Dark Bronze Matte Textured
			HSS-270-FSS	House Side Shield 270° Front/Side/Side	GTT	Graphite Matte Textured	
			HSS-270-FSB	House Side Shield 270° Front/Side/Back	LGS	Light Gray Gloss Smooth	
			HSS-360	House Side Shield 360°	PSS	Platinum Silver Smooth	
			BC	Back Light Control	WHS	White Gloss Smooth	
MTG	Mounting		A	Arm Mount for square pole/flat surface	WHT	White Matte Textured	
			ASQU	Universal Arm Mount for square pole	VGT	Green Landscape Decorative	
			AAU	Adjustable Arm for pole mounting	LEG	Legacy Colors	
			ADU	Decorative upswept Arm	Color Option		
			RPA	Round Pole Adapter	CC	Custom Color	
			MAF	Mast Arm Fitter for 2-3/8" OD horizontal arm			
			K	Knuckle			
			T	Trunnion			
			WB	Wall Bracket (compatible with universal arm mounts)			
Accessory Type			Option				
MSC	Miscellaneous		BIRD SPK	Bird Spike			

Current Control Solutions — Accessories (Sold Separately)		
NX Lighting Controls		
<input type="checkbox"/>	NXOFM-1R1D-UNV	On-fixture Module (7-pin), On / Off / Dim, Daylight Sensor with NX Radio and Bluetooth® Radio, 120–480VAC
wiSCAPE® Lighting Control		
<input type="checkbox"/>	WIR-RME-L	On-fixture Module (7-pin or 5-pin), On / Off / Dim, Daylight Sensor with wiSCAPE Radio, 110–480VAC
<input type="checkbox"/>	SCP-REMOTE	Remote Control for SCP/_F option. Order at least one per project to program and control the occupancy sensor
For additional information related to these accessories please visit currentlighting.com/beacon . Options provided for use with integrated sensor, please view specification sheet ordering information table for details.		

CONTROLS



Control Option	Sensor	Networkable	Scheduling	Occupancy	Daylight Harvesting	On/Off Control	Programming	Pair with Sensor	Sensor Mounting Height
NXW	—	✓	✓	—	—	✓	✓	—	—
NXWS_F	NXSMP2	✓	✓	✓	✓	✓	✓	—	16ft, 40ft
BTSO12F	BTSMP-OMNI-O	—	—	✓	✓	✓	Bluetooth	—	12ft
BTS_F	BTSMP	—	—	✓	✓	✓	Bluetooth	—	14ft, 40ft
SCP_F	—	—	—	✓	—	✓	✓	—	—
ADD	—	—	✓	—	—	✓	—	✓	—
ADT	—	—	✓	—	—	✓	—	✓	—
7PR	—	Paired with external control	Paired with external control	—	Paired with external control	Paired with external control	—	✓	—
7PR-SC	—	—	—	—	—	—	—	✓	—
3PR	—	—	—	—	—	Paired with external control	—	✓	—
3PR-SC	—	—	—	—	—	—	—	✓	—
3PR-TL	—	—	—	—	✓	✓	—	✓	—
WIR	—	✓	✓	—	✓	✓	Gateway	—	—
WIRSC	BTSMP	✓	✓	✓	✓	✓	Gateway	—	14ft, 40ft

Vanish

PETROLEUM GAS CANOPY

FEATURES

- Edge-Lit technology for even illumination
- Low profile 2.1" depth design virtually disappears into the canopy
- Illuminates without distraction and glare
- Pendant or surface mounted with 3/4" conduit
- Universal retrofit solution for HID replacements for various sizes
- IP65 rating to keep water and insects out
- Cast Aluminum with integral heat sink to maintain optimal thermal performance for long LED life Cast aluminum



SPECIFICATIONS

CONSTRUCTION

- Die-cast aluminum, low profile housing
- New construction or retrofit solution
- Canopy and soffit applications
- Easy installation
- Driver and optical chamber serviceable from below canopy
- Powder coat finish
- Heat sink design to disperse heat away from fixture
- Suitable for wet locations

OPTICS

- Acrylic Lens
- Type V distribution
- Comfort lens for low glare
- Light Guide Edge-Lit technology

INSTALLATION

- Surface or pendant mounted
- Easy installation and serviceable below the canopy deck
- Hinge for hanging during service

ELECTRICAL

- Universal 120-277, 347, 480 Input Voltage
- Power Factor > 0.9 at full load
- Total Harmonic Distortion < 20% at full load
- 10 kV Surge Protection
- 0-10 Volt Dimmable Driver
- Operating temperature: -40°C to +40°C



CERTIFICATIONS

- UL Certified
- DesignLights Consortium™ 5.1 qualified
- Wet Location Listed
- IP66
- DLC® (DesignLights Consortium Qualified), with some Premium Qualified configurations. Please refer to the DLC website for specific product qualifications at www.designlights.org

WARRANTY

- 5 year warranty
- See [HLI Standard Warranty](#) for additional information

ORDERING GUIDE

Example: VSH-85-5K7-UNV-WHG

CATALOG #

VSH					
Series	Size	Color Temp	Voltage	Finish	
VSH Vanish	30'	4K7	UNV Universal	WHG	Petroleum White
	55	5K7	347 347V	DBS	Petroleum Dark Bronze
	85		480 480V	BLS	Petroleum Black
	140				

Notes:

- 1 Only available in Universal Voltage

KEY DATA	
Lumen Range	4,500 – 20,200
Wattage Range	30 – 140 Watts
Efficacy Range (LPW)	138 – 157
Reported Life (Hours)	>60,000

STOCK ORDERING INFORMATION

Catalog Number	Stock Number	Wattage	Voltage	CCT/CRI	Finish
VSH-85-4K7	93133024	85W	UNV	5000K/70 CRI	Petroleum White
VSH-140-5K7	93139554	140W	UNV	5000K/70 CRI	Petroleum White

PERFORMANCE DATA

Product	Lumens	B	U	G	LPW	CRI	CCT
VSH-30-4K7	4564	2	0	1	150	70	4000K
VSH-30-5K7	4793	2	0	1	157	70	5000K
VSH-55-4K7	8846	3	0	2	153	70	4000K
VSH-55-5K7	9069	3	0	2	157	70	5000K
VSH-85-4K7	13296	3	0	2	152	70	4000K
VSH-85-5K7	13666	3	0	2	157	70	5000K
VSH-140-4K7	19649	4	0	3	138	70	4000K
VSH-140-5K7	20196	4	0	3	142	70	5000K

Data is considered to be representative of the configurations shown. Actual performance may differ as a result of end-user environment application and inherent performance balances of the electrical components.

PROJECTED LUMEN MAINTENANCE

Ambient Temperature	OPERATING HOURS					
	0	25,000	50,000	TM-21-11' L96 60,000	100,000	L70 (Hours)
25°C / 77°F	1.00	0.94	0.92	0.90	0.81	>170,000
40°C / 104°F	0.99	0.94	0.92	0.89	0.80	>160,000

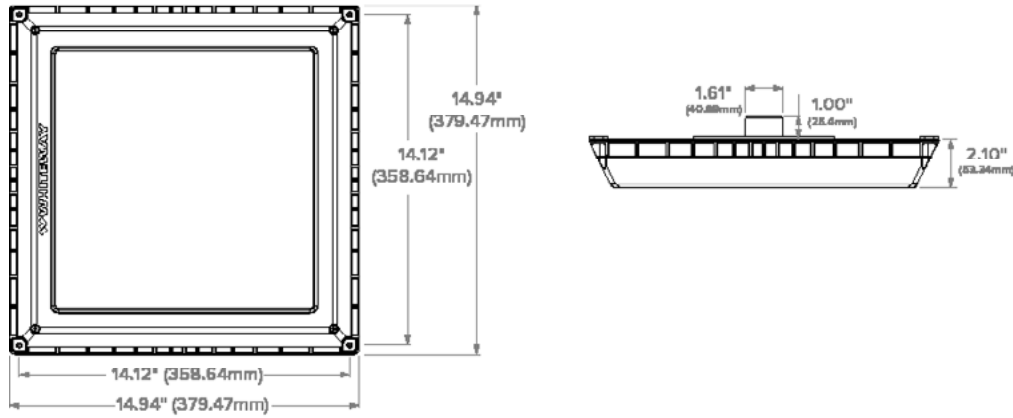
LUMINAIRE AMBIENT TEMPERATURE FACTOR (LATF)

Ambient Temperature		Lumen Multiplier
0°C	32°F	1.03
10°C	50°F	1.01
20°C	68°F	1.00
25°C	77°F	1.00
30°C	86°F	0.99
40°C	104°F	0.98
50°C	122°F	0.97

Vanish

PETROLEUM GAS CANOPY

DIMENSIONS

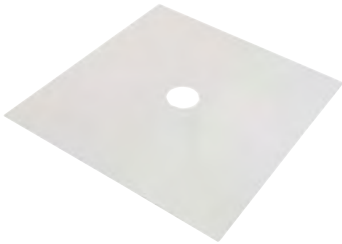


MOUNTING ACCESSORIES

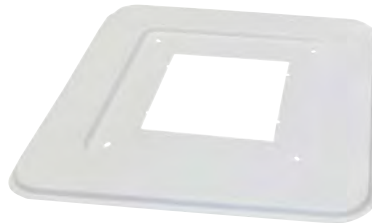
Accessories (order separately)

- | | | |
|-----------------------------------|-------------------------------------|--|
| <input type="checkbox"/> 93133148 | WHITEWAY 15 IN CVR PLT WHT VSH/GSY | Retrofit cover plate for LSI Encore 15" square-replacement for 10" opening |
| <input type="checkbox"/> 93133149 | WHITEWAY DECORATIVE CVR PLT VSH/GSY | 26" Decorative Beauty Plate for Canopy Retrofits |
| <input type="checkbox"/> 93133151 | WHITEWAY HID RETRFT KIT WHT VSH/GSY | Universal HID retrofit kit (fits any square HID housing between 21" & 23" square.) |
| <input type="checkbox"/> 93133177 | WHITEWAY STEM AND JUNCTION BOX | |

93133148

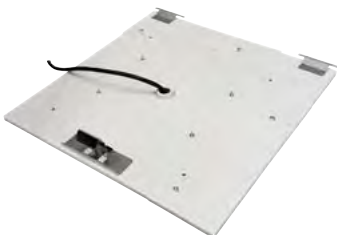


93133149



93133151

- Measure outside dimension of existing housing



93133177



Attachment I
Stormwater Management Report



The Stormwater Management Report has been enclosed for your reference. The backup information is not included in the copies provided to the Planning Board but were included in the submission to the Town Engineer.

Stormwater Management Report

STORMWATER MANAGEMENT PLAN

Rusty Lantern Market 181 Gray Road, Cumberland, Maine

Introduction

Cumberland Real Estate Group, LLC (herein referred to as Applicant) is proposing the construction of a single-story, 5,038 s.f. convenience store building, gasoline pumps, canopy, associated parking, infrastructure, and landscaping situated on a site with frontage on Gray Road (U.S. Route 26) and Skillin Road in Cumberland, Maine. The proposed development will result in approximately 67,548 s.f. (1.55 acres) of impervious area. The increased runoff from the paved areas of site will be directed to one of two Subsurface Soil Filters for water quality treatment and water quantity mitigation. Currently the site has approximately 94,592 s.f. (2.17 acres) of impervious area, comprised of the existing building and pavement, and extensive gravel surfaced area compacted from years of use. The proposed project will result in a reduction of 27,044 s.f. (0.62 acres) of impervious area.

Available historical photographs were reviewed to determine when the existing parcels were previously developed. Most of the development had occurred by 1997, which is before the implementation of the Stormwater Law. The amount of undeveloped area was estimated from the aerial photograph to be approximately 34656 s.f. (0.80 acres). Per Maine Department of Environmental Protection (DEP) rules, only the area developed since 1997 would be required to meet the requirements of Chapter 500; however, since it is less than 1-acre, it does not meet the criteria for a Stormwater Law application. As the project results in less than an acre of new impervious area, it does not require a Stormwater Law permit from the DEP; however, a Stormwater Law Permit-by-Rule will be filed.

In accordance with the Town's ordinances, it is required to conform to Basic, General, and Flooding Standards in accordance with Chapter 500 of the DEP rules.

Study Methodology

Topographical data was obtained from an on-the-ground survey completed by Boundary Points, a division Main-Land. Hydrologic boundaries were generated using the topographic mapping, and the drainage patterns were verified by a site reconnaissance visit.

Surficial soils located in the vicinity of the site were obtained from the United States Department of Agriculture Natural Resources Conservation Service Soil Survey Geographic (SSURGO) Database. The Applicant's parcel includes the soil classifications listed below. Soil units found in the development area are primarily Hinkley Loamy Sand. Flycatcher, LLC, observed test pits to evaluate the seasonal high groundwater table at locations where stormwater best management practices (BMPs) are proposed. The Flycatcher report confirmed the soils were similar to Hinkley; with the observation that some imported fill was evident.

SOIL TYPES IN LOCAL STUDY AREA

Soils Series	Symbol(s)	Hydrologic Group (HSG) **
Hinckley Loamy Sand	H1B	A

**Hydrologic Soils Group taken from SCS TR-55 Manual

Test pits were completed at the site by Summit Geoengineering. A copy of the geotechnical investigation has been enclosed with this submission.

Basic Standards

Erosion control BMPs are shown on the project drawings, and notes and details on implementing them are included on separate drawings in the set. The Contractor will be responsible for maintaining the BMPs throughout construction. After the site is stabilized and accepted by the owner, the owner will be responsible for maintaining the permanent BMPs.

Disturbed area will be minimized by clearing only the amount of land required for the construction of each building, which will not be constructed concurrently.

Major site work activities and their sequence follow:

1. Install a stabilized construction entrance.
2. Cut and remove trees around area of work, as necessary, leaving the duff layer in place.
3. Set sediment barrier and erosion control measures around the perimeter of the limits of work. Stumps shall be ground onsite and used for sediment barrier and/or mulch.
4. Clear and grub the work site as needed to execute plans using caution not to overexpose the site. Topsoil salvaged shall be stockpiled and protected against erosion.
5. Install storm drainage and infrastructure, including access.
6. Construct buildings.
7. Construct pavement.
8. Loam, seed, and mulch disturbed areas.
9. Monitor the site for signs of erosion monthly and after major storm events.
10. Removal of temporary erosion control measures. Ninety (90) days post-construction or upon satisfactory establishment of vegetation has been obtained.
11. Inspect the site semi-annually for any sign of erosion or area requiring additional seeding.

The contractor shall monitor the disturbed area for signs of erosion or sediment transport off-site and take corrective action immediately. Inspections shall be logged using the form supplied in the stormwater facilities maintenance plan and kept on file. Completed logs shall be maintained by the Applicant after construction.

Flooding Standard

The project area is located in Zone C (Areas of Minimal Flooding) of the Flood Insurance Rate Maps (FIRMs) for Cumberland County, Maine. The project area is located on Panel 18 of 25 (Community Panel 230162-0015-B, Effective May 19, 1981). An excerpt of the applicable FIRM is enclosed with the supporting graphics. There is no impact from flooding anticipated for this project.

Off-Site Watersheds

There are no off-site watersheds that were reviewed as part of the stormwater analysis. The project area has little variation in elevation and adjacent roads and developed areas serve as hydrologic boundaries.

On-Site Subcatchments

Pre-Development Conditions

The pre-development hydrologic analysis is based on the existing site condition, which is mostly undeveloped and comprised of paved and unpaved areas. The development area is relatively flat and drains from a high point near the middle to the perimeter of the graveled area. Runoff from the front portion of the site is conveyed into the existing storm drain system in Gray Road.

- | | |
|----------------|--|
| Subcatchment 1 | represents the area immediately adjacent to the intersection of Gray and Skillin Roads. The area drains to existing catch basins connected to the storm drains in the ROW. |
| Subcatchment 2 | represents 0.32 acres that drains internally to a catch basin connected to the storm drain in the Skillin Road ROW. |
| Subcatchment 3 | represents approximately 0.31 acres that drains to the abutting land to the east. |
| Subcatchment 4 | represents approximately 0.74 acres that drains toward Gray Road, where it is collected at a catch basin. |
| Subcatchment 5 | represents a small area that drains to the abutting property. |
| Subcatchment 6 | represents an approximately 0.27 acre area of gravel and woods that drains to the east. |
| Subcatchment 7 | represents an approximately 0.39 acre area of gravel and woods that drains to the southeast. |
| Subcatchment 8 | represents an approximately 0.48 acre area of gravel surface that drains to the parcel to the south of the site. |
| Subcatchment 9 | represents an approximately 0.33 acre area of gravel surface that drains to the Gray Road ROW. |

Post-Development Conditions

Under post-development conditions, the commercial buildings will be constructed with associated paved access, landscaping, and infrastructure. Stormwater runoff from the new impervious area will be directed to one of two Subsurface Soil Filters, with the exception of the roofs, which will drain an infiltration basin or stone drip edge. A summary of the subcatchments is provided below:

- | | |
|----------------|---|
| Subcatchment 1 | represents the convenience store and lawn areas between it and the intersection of the roads. These areas drain to an infiltration gallery. |
|----------------|---|

- Subcatchment 2 represents the parking area, fueling pumps, and entrance from Gray Road. This area is collected by catch basins and conveyed to Subsurface Soil Filter #1 (SSSF#1).
- Subcatchment 3 represents the parking area and drive-thru lanes for the bank. This area is collected by catch basins and conveyed to SSSF#2.
- Subcatchment 4 represents the bank building, which will drain to a drip edge filter BMP.
- Subcatchment 6 represents an approximately 0.27 acre area of gravel and woods that drains to the east.
- Subcatchment 7 represents an approximately 0.39 acre area of gravel and woods that drains to the southeast.
- Subcatchment 8 represents an approximately 0.48 acre area of gravel surface that drains to the parcel to the south of the site.
- Subcatchment 9 represents an approximately 0.33 acre area of gravel surface that drains to the Gray Road ROW.
- Subcatchment 10 represents an approximately 0.33 acre area of gravel surface that drains to the Gray Road ROW.
- Subcatchment 11 represents an approximately 0.33 acre area of gravel surface that drains to the Gray Road ROW.

Results

A comparison of pre-development and post-development peak rates of stormwater runoff at the Analysis Points is presented in the following tables. Peak runoff rates were estimated for the 2-, 10-, 25, and 50-year 24-hour storm events.

Analysis Point 1 (POI#1)	Peak Runoff Rate (cfs)		
Design Storm	Pre-Development	Post-Development	Difference
2-Year	1.05	0.45	-0.60
10-Year	1.50	0.60	-0.90
25-Year	2.00	0.73	-1.27

Analysis Point 1 (POI#2)	Peak Runoff Rate (cfs)		
Design Storm	Pre-Development	Post-Development	Difference
2-Year	3.70	0.17	-3.53
10-Year	5.34	0.37	-4.97
25-Year	7.06	0.63	-6.43

As shown in the tables above, the total net peak rate of flow leaving the site is reduced for all storm events.

General Standard

An analysis of the pre-development and post-development areas shows that the runoff from 96% of the proposed impervious area and 81% of the proposed developed area on the parcel will be directed to the Subsurface Soil Filters for treatment and detention. The results are presented in the following table.

The proposed project will create approximately 67,548 (1.55 acres) of new impervious area. Runoff from approximately 53,323 s.f. (1.22 acres), or 95.1%, of the impervious area will be conveyed to the Subsurface Soil Filters for treatment and detention. In the post-development condition, the site will include approximately 30,829 s.f. (0.71 acres) of landscaped area, for a total of 85,825 s.f. (1.97 acres) of developed area. Runoff from approximately 18,355 s.f. (0.42 acres) of landscaped area will be conveyed to the Filter, resulting in 70,678 s.f. (1.62 acres), or 82.4%, of the developed areas directed to the SSF for treatment and detention.

Water Quality

The project is required to provide stormwater treatment for 95% of the impervious area and 80% of the developed area. This goal for water quality treatment is achieved using two (2) Subsurface Soil Filters for the paved areas, and infiltration system for the convenience store building, and drip-edge treatment BMPs for the bank building.

Subsurface Soil Filters

Two Subsurface Soil Filters with underdrains and liners are proposed for the treatment and detention of the runoff from the proposed paved areas, including the developed landscaped area, paved parking and access aisles. The filter has been sized so that the surface area of the filter is greater than 5% of the impervious tributary area plus 2% of the landscaped tributary area. The media is 18" thick and designed to store a treatment volume greater than 1.0 inch over the impervious area and 0.4 inches over the landscaped area, and filter at a rate of 2.41 inches per hour. Separation is provided between the bottom of the filter media and the high seasonal water table and liners are proposed for the bottoms of the systems. The maximum depth of stored runoff is less than 18 inches. Overflows have been included in the design to allow for detention within the subsurface soil filter footprint.

Conclusion

Through the implementation of erosion and sedimentation control measures and best management practices, the project complies with the requirements of the Basic Standard.

By collecting and treating runoff from new impervious area, 96% of the new impervious area will be treated in accordance with Chapter 500. Similarly, 81% of the developed area will be treated prior to discharge from the site. The runoff from the development will not adversely impact the existing storm drains in Route 26 or the adjacent parcels. By capturing and treating runoff from the impervious surfaces and developed areas the project likewise meets the applicable portions of the General Standard. The General Standard is met and exceeded. By providing detention in the proposed stormwater management BMPs, the peak runoff rates of the post-development condition are reduced to below the pre-development peak runoff rates; the project is not subject to the requirements of the Flooding Standard, but the development has been designed so that the project complies with the requirements of the Flooding Standard.

Attachment 1 – Pre-Development HydroCAD Report
Attachment 2 – Pre-Development Watershed Map
Attachment 3 – Post-Development HydroCAD Report
Attachment 4 – Post-Development Watershed Map

STORMWATER MANAGEMENT INSPECTION AND MAINTENANCE PLAN

1.0 GENERAL

This stormwater management maintenance plan has been prepared in support of the Maine Department of Environmental Protection Site Law Permit amendment for the Lakeside Concrete Cutting and Abatement Professional commercial building and offices in Cumberland, Maine. The requirements of this plan shall be incorporated into the efforts associated with the development including construction and ongoing operations.

This plan was prepared by:

Curt Neufeld, P.E. #9779
Sitelines, PA
119 Purinton Road, Suite A
Brunswick, Maine 04011
207-725-1200 x18

2.0 BEST MANAGEMENT PRACTICES

2.1 Best Management Practices

During Construction, a stabilized construction entrance, sediment barrier, and/or erosion control mix, seeding, and mulching practices will be used in accordance with the Maine Department of Environmental Protection Best Management Practices (BMP) manual during construction and until a stabilized condition exists.

After Construction, stormwater BMPs will include housekeeping and physical measures described herein, including the grassed underdrained soil filters, sweeping of paved surfaces, and maintenance of storm drain pipes and outfalls.

The stormwater maintenance management for this project will be performed consistent with the two references listed below and as amended in this manual. Where standards are not consistent, the more stringent requirement shall apply.

2.2 References

The primary references for the maintenance of the BMPs were as follows:

- 1 "Stormwater Management for Maine", Maine Department of Environmental Protection No. DEPLW0738, Volume 3, May 2016.
- 2 "Maine Erosion and Sedimentation Best Management Practices", Maine Department of Environmental Protection, current edition on-line.
- 3 "Maine Erosion and Sediment Control Field Guide for Contractors", Maine Department of Environmental Protection, 2014 Revision.

This information is provided as guidance if the Owner/would like to learn more about the BMPs. Also, maintenance for these BMPs may change over time. It is not expected the Owner will have the references readily available, however, they may be available through the DEP website.

3.0 MAINTENANCE OF STORMWATER FEATURES

3.1 General Responsibilities

The Contractor will be responsible for inspecting and maintaining the stormwater features until the construction phase of the project is complete. These efforts shall include maintenance of erosion and sedimentation control measures, temporary and permanent stormwater features, and addressing interim site conditions as necessary. After completion of construction, the Applicant will be responsible for inspecting and maintaining the permanent stormwater features as shown on the plan.

The Point of Contact for the Applicant is as follows:

Mr. James Howard
Cumberland Real Estate Holdings, LLC
2 Main Street
Topsham, Maine 04086
(207) 837-6198

3.2 General Requirements

The general requirements for this stormwater maintenance management manual will meet the standards of Reference No.1, specific to the water quality feature concerned. Additional maintenance requirements are identified in the following narratives.

3.3 Specific Maintenance Requirements

The following specific maintenance requirements apply to stormwater features as follows:

3.3.1 R-Tanks

- The maintenance of the R-Tanks shall be in accordance with the manufacturer's recommendations. A copy of the Operation and Maintenance Guidelines for the Separator Row and Stormwater Management System are attached.
- Maintenance shall be performed by an appropriate service company with equipment designed for the purpose.

3.3.2 Outlet Control Structures

- The maintenance of outlet control structures shall be performed bi-annually to ensure proper function.
- Debris and trash shall be removed from the structure sump when present.
- Sediment build-up in the sump should be removed when accumulation is within 1 foot of the invert of the outlet pipe and/or snout hood is observed.

3.3.3 Storm Drain Pipes & Drainage Manholes

- Piped drainage systems shall be inspected in spring and late fall, and after heavy rains to remove any obstructions to flow; remove accumulated sediments and debris at the inlet, at the outlet, and within the conduit; and to repair any erosion damage at the culvert's inlet and outlet. Sediment should be removed when its level exceeds 20% of the pipe diameter. Hydraulic flushing or any mechanical means may accomplish sediment removal. Care shall be taken to contain the sediment at the pipe outlet.

3.3.4 Paved Surfaces

- Accumulations of winter sand along impervious areas shall be cleared at least once a year, preferably in the spring. Accumulations on pavement may be removed by pavement vacuum sweeping, or mechanical sweeping (e.g. "street-sweeper"). Accumulations of sand along the edge of paved areas may be removed by grading excess sand to the pavement edge and removing it manually or by a front-end loader.

3.3.5 Vegetative Surfaces

- For most vegetative surfaces, grass should be mowed on a regular basis so that grass height does not exceed 6 inches. Any erosion rills, gullies, or bare spots should be seeded or sodded to re-establish the turf cover.
- Buffer, screening, and decorative landscaping should be inspected for health on a regular basis. Pruning, weeding, feeding, and mulching.
- Fertilizers will only be applied once yearly, to occur in the spring, and at the lowest recommended concentration. Herbicides and pesticides will only be used in accordance with DEP recommendations.

3.3.6 Drainage Structures

- Inspect for sediment in traps/sump/bed of basin. Remove sediment if within 1 foot of outlet invert.
- Inspect frame and grate to verify grate is flush with finish grade.
- Inspect for damaged or missing pavement around frame and grate.
- Inspect structure for presence of trash or debris.
- Inspect for oil and oil adsorbent material if present.
- If applicable, inspect oil absorbent pad. Replace if necessary.

4.0 CONSTRUCTION INSPECTION AND MAINTENANCE

4.1 Maintenance Frequency

Inspections of the erosion and sedimentation control measures, and temporary and permanent stormwater features during the construction process shall be performed at least once per week and before and after each significant rainfall event. For the purposes of the inspection schedule, a significant rainfall event shall be any storm event that produces more than 0.5 inches of rainfall in a 24-hour period.

During winter construction, in the months from November to March, inspections shall be performed after each rainfall, snowstorm, or thawing, and at least once per week.

4.2 Inspection Scope

The scope of construction inspections shall include disturbed and impervious areas, material storage areas, and vehicle access points in addition to the erosion and sedimentation control measures, and temporary and permanent stormwater features.

4.3 Inspection and Maintenance Checklist

All inspection forms and documentation of corrective actions during construction shall be maintained for a minimum of three (3) years after permanent stabilization has been achieved.

4.4 Corrective Action Timeline

As part of the inspection and maintenance process, if any corrective action is warranted, it shall be started by the end of the next workday and completed within seven (7) days or before the next storm event, whichever comes first.

All required corrective actions shall be documented and maintained with the inspection forms.

4.5 Qualifications of Inspector

The person(s) responsible for inspection during construction and post-construction shall be conducted by someone with knowledge or erosion and stormwater control, including the standards and conditions of the approvals.

5.0 POST-CONSTRUCTION INSPECTION AND MAINTENANCE

5.1 Maintenance Frequency

Notwithstanding any other schedule noted, general inspections post-construction shall be conducted monthly during wet weather conditions from March to November. Inspections shall also be conducted following any significant storm events. For the purposes of the inspection schedule, a significant rainfall event shall be any storm event that produces more than 0.5 inches of rainfall in a 24-hour period. Specifically, inspections of the vegetated soil filters and pond shall be conducted following any significant storm event during the first year after construction to ensure that they drain dry within 24 to 48 hours.

5.2 Inspection and Maintenance Checklist

An inspection and maintenance log specific to this project is appended. All post-construction inspection forms and documentation of corrective actions shall be maintained for a minimum of five (5) years.

5.3 Corrective Action Timeline

As part of the inspection and maintenance process, if any corrective action is warranted, it shall be started by the end of the next workday and completed within seven (7) days or before the next storm event, whichever comes first.

All required corrective actions shall be documented and maintained with the inspection forms.

5.4 Qualifications of Inspector

The person(s) responsible for inspection during construction and post-construction shall be conducted by someone with knowledge or erosion and stormwater control, including the standards and conditions of the approvals.

6.0 RECERTIFICATION

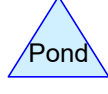
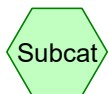
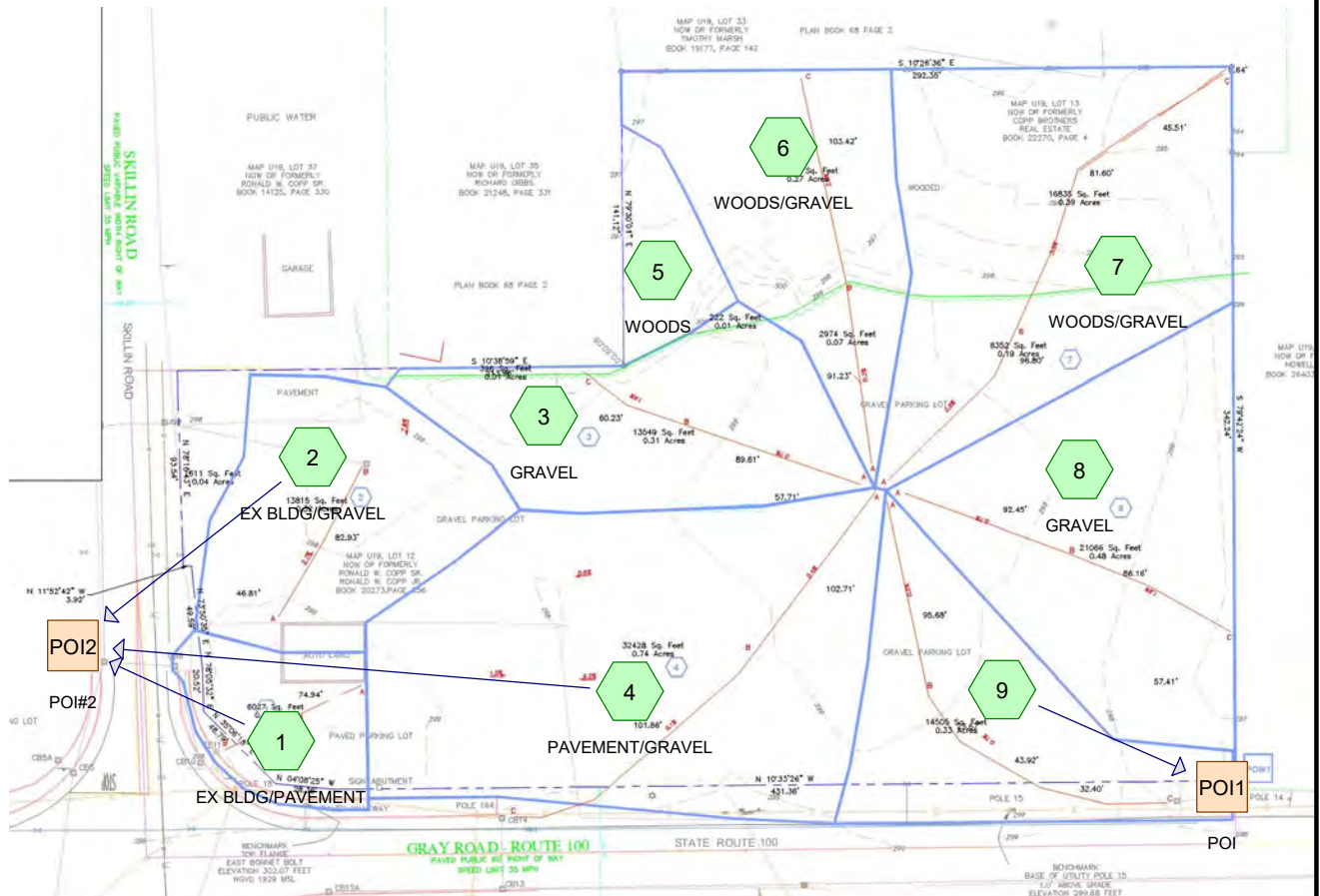
6.1 Recertification requirement

Within three months of the expiration of each five-year interval from the date of issuance of the permit, the permittee shall certify the following to the department.

- 1) All areas of the project site have been inspected for areas of erosion, and appropriate steps have been taken to permanently stabilize these areas.
- 2) All aspects of the stormwater control system are operating as approved, have been inspected for damage, wear, and malfunction, and appropriate steps have been taken to repair or replace the system, or portions of the system, as necessary.
- 3) The stormwater maintenance plan for the site is being implemented as approved by the Department, and the maintenance log is being maintained.
- 4) All proprietary systems have been maintained according to the manufacturer's recommendations. Where required by the Department, the permittee shall execute a 5-year maintenance contract with a qualified professional for the coming 5-year interval. The maintenance contract must include provisions for routine inspections, cleaning and general maintenance.
- 5) The Department may waive some or all of these recertification requirements on a case-by-case basis for permittees subject to the Department's Multi-Sector General Permit ("MSGP") and/or Maine Pollutant Discharge Elimination System ("MEPDES") programs where it is demonstrated that these programs are providing stormwater control that is at least as effective as required pursuant to this Chapter.

General Site Inspection Maintenance & Housekeeping Form			
General Information			
Project Name:	Rusty Lantern Market	Inspection Date	
Project Location:	181 Gray Road	Current Weather	
	Cumberland ME 04021	Date / Amount Last Percip.	
BMP Owner:	Cumberland Real Estate Holdings, LLC	Company Inspection:	
Owner Mailing Address:	2 Main Street	Company Mailing Address:	
	Topsham, ME 04086		
Owner Phone #:		Company Phone #:	
Owner Email:		Inspector Name	
		Inspector Email	
BMP Element	Suggested Maintenance & Recommended	Observations	Inspection Notes/Recommended
Vegetated Areas	Inspect slopes/embankments for erosion (annually)		
	Replant bare areas or areas of sparse growth (annually)		
Paved Surfaces	Clear accumulated winter sand (annually)		
	Remove sediment along edges of parking and within low spots / pockets (annually)		
Ditches/Swales	Remove obstructions/debris/sediment (monthly)		
	Inspect for erosion/repair as needed (annually)		
	Mow vegetated ditches (annually)		
Catch Basins	Remove sediment/debris from sump (annually)		
	Remove sediment/debris from inlet/outlet aprons (annually)		
Culverts	Inspect inlet/outlet aprons for erosion, repair as needed (annually)		
	Inspect, repair as needed, riprap aprons for dislodged/sparse coverage (annually)		
	Remove sediment/debris from outlet aprons (annually)		
Pipe Outlets	Inspect outlet aprons for erosion, repair as needed (annually)		
	Inspect, repair as needed, riprap aprons for dislodged/sparse coverage (annually)		
Additional Notes/Observations:			

Subsurface Sand Filter Inspection Maintenance & Housekeeping Form			
General Information			
Project Name:	Rusty Lantern Market	Inspection Date	
Project Location:	181 Gray Road	Current Weather	
	Cumberland ME 04021	Date / Amount Last Percip.	
BMP Owner:	Cumberland Real Estate Holdings, LLC	Company Inspection:	
Owner Mailing Address:	2 Main Street	Company Mailing Address:	
	Topsham, ME 04086		
Owner Phone #:		Company Phone #:	
Owner Email:		Inspector Name	
		Inspector Email	
BMP Element	Suggested Maintenance & Recommended Frequency	Observations	Inspection Notes/Recommended Action
Pre-Treatment Chamber Row	Inspect pre-treatment chamber row for presence of sediment via inspection port with a flashlight and stadia rod (annually)		
Subsurface Sand Filters	Inspect for evidence of excessive sediment deposits (annually)		
	Inspect overflow for presence of sediment and/or trash (annually)		
Catch Basins & Outlet Control Structures	Inspect for presence of sediment and/or trash (annually)		
	Inspect frame and grate to verify grate is flush with finish grade (annually)		
	Inspect for presence of trash and debris (annually)		
	Inspect oil adsorbent material (Smart Sponge). Replace per manufacturer's recommendations (annually)		
Additional Notes/Observations:			



Routing Diagram for Cumberland PreDev

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Cumberland PreDev

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Project Notes

Copied 4 events from Cumberland 24-hr S1 storm

Rainfall events imported from "Atlas-14-Rain.txt" for 1365 ME Cumberland Nw

Cumberland PreDev

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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-yr	Cumberland 24-hr S1	2-yr	Default	24.00	1	3.10	2
2	5-Year	Type III 24-hr		Default	24.00	1	3.66	2
3	10-Year	Type III 24-hr		Default	24.00	1	4.60	2
4	10-YR	Cumberland 24-hr S1	10-yr	Default	24.00	1	4.60	2
5	25-yr	Cumberland 24-hr S1	25-yr	Default	24.00	1	5.80	2

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
2.449	96	Gravel surface, HSG A (2, 3, 4, 6, 7, 8, 9)
0.138	98	Paved parking, HSG A (1)
0.743	30	Woods, Good, HSG A (5, 6, 7)
3.330	81	TOTAL AREA

Cumberland PreDev

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
3.330	HSG A	1, 2, 3, 4, 5, 6, 7, 8, 9
0.000	HSG B	
0.000	HSG C	
0.000	HSG D	
0.000	Other	
3.330		TOTAL AREA

Cumberland PreDev

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
2.449	0.000	0.000	0.000	0.000	2.449	Gravel surface	2, 3, 4, 6, 7, 8, 9
0.138	0.000	0.000	0.000	0.000	0.138	Paved parking	1
0.743	0.000	0.000	0.000	0.000	0.743	Woods, Good	5, 6, 7
3.330	0.000	0.000	0.000	0.000	3.330	TOTAL AREA	

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: EX BLDG/PAVEMENT Runoff Area=6,027 sf 100.00% Impervious Runoff Depth=2.87"
Flow Length=75' Slope=0.0090 '/' Tc=5.0 min CN=98 Runoff=0.45 cfs 0.033 af

Subcatchment 2: EX BLDG/GRAVEL Runoff Area=13,815 sf 0.00% Impervious Runoff Depth=2.65"
Flow Length=83' Slope=0.0270 '/' Tc=5.0 min CN=96 Runoff=1.00 cfs 0.070 af

Subcatchment 3: GRAVEL Runoff Area=13,549 sf 0.00% Impervious Runoff Depth=2.65"
Flow Length=150' Tc=5.0 min CN=96 Runoff=0.98 cfs 0.069 af

Subcatchment 4: PAVEMENT/GRAVEL Runoff Area=32,428 sf 0.00% Impervious Runoff Depth=2.65"
Flow Length=202' Tc=5.7 min CN=96 Runoff=2.26 cfs 0.164 af

Subcatchment 5: WOODS Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.00"
Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af

Subcatchment 6: WOODS/GRAVEL Runoff Area=14,723 sf 0.00% Impervious Runoff Depth=0.01"
Flow Length=194' Tc=5.3 min CN=43 Runoff=0.00 cfs 0.000 af

Subcatchment 7: WOODS/GRAVEL Runoff Area=25,187 sf 0.00% Impervious Runoff Depth=0.15"
Flow Length=100' Slope=0.0080 '/' Tc=5.0 min CN=52 Runoff=0.01 cfs 0.007 af

Subcatchment 8: GRAVEL Runoff Area=21,066 sf 0.00% Impervious Runoff Depth=2.65"
Flow Length=186' Tc=5.0 min CN=96 Runoff=1.52 cfs 0.107 af

Subcatchment 9: Runoff Area=14,505 sf 0.00% Impervious Runoff Depth=2.65"
Flow Length=100' Slope=0.0020 '/' Tc=5.0 min CN=96 Runoff=1.05 cfs 0.074 af

Reach POI1: POI Inflow=1.05 cfs 0.074 af
Outflow=1.05 cfs 0.074 af

Reach POI2: POI#2 Inflow=3.70 cfs 0.268 af
Outflow=3.70 cfs 0.268 af

Total Runoff Area = 3.330 ac Runoff Volume = 0.524 af Average Runoff Depth = 1.89"
95.85% Pervious = 3.192 ac 4.15% Impervious = 0.138 ac

Summary for Subcatchment 1: EX BLDG/PAVEMENT

Runoff = 0.45 cfs @ 12.02 hrs, Volume= 0.033 af, Depth= 2.87"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
6,027	98	Paved parking, HSG A
6,027		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	75	0.0090	0.91		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.4	75	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 2: EX BLDG/GRAVEL

Runoff = 1.00 cfs @ 12.02 hrs, Volume= 0.070 af, Depth= 2.65"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
13,815	96	Gravel surface, HSG A
13,815		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	83	0.0270	1.45		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.0	83	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 3: GRAVEL

Runoff = 0.98 cfs @ 12.02 hrs, Volume= 0.069 af, Depth= 2.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
13,549	96	Gravel surface, HSG A
13,549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	90	0.0070	0.86		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	60	0.0160	2.04		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.3	150	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 4: PAVEMENT/GRAVEL

Runoff = 2.26 cfs @ 12.03 hrs, Volume= 0.164 af, Depth= 2.65"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
32,428	96	Gravel surface, HSG A
32,428		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	100	0.0040	0.70		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.3	102	0.0010	0.51		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
5.7	202	Total			

Summary for Subcatchment 5: WOODS

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 6: WOODS/GRAVEL

Runoff = 0.00 cfs @ 24.00 hrs, Volume= 0.000 af, Depth= 0.01"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
11,749	30	Woods, Good, HSG A
2,974	96	Gravel surface, HSG A
14,723	43	Weighted Average
14,723		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Summary for Subcatchment 7: WOODS/GRAVEL

Runoff = 0.01 cfs @ 13.24 hrs, Volume= 0.007 af, Depth= 0.15"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
16,835	30	Woods, Good, HSG A
8,352	96	Gravel surface, HSG A
25,187	52	Weighted Average
25,187		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.8	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 8: GRAVEL

Runoff = 1.52 cfs @ 12.02 hrs, Volume= 0.107 af, Depth= 2.65"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
21,066	96	Gravel surface, HSG A
21,066		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 9:

Runoff = 1.05 cfs @ 12.02 hrs, Volume= 0.074 af, Depth= 2.65"
 Routed to Reach POI1 : POI

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
14,505	96	Gravel surface, HSG A
14,505		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.1	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach POI1: POI

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.333 ac, 0.00% Impervious, Inflow Depth = 2.65" for 2-yr event
Inflow = 1.05 cfs @ 12.02 hrs, Volume= 0.074 af
Outflow = 1.05 cfs @ 12.02 hrs, Volume= 0.074 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, 11.53% Impervious, Inflow Depth = 2.68" for 2-yr event
Inflow = 3.70 cfs @ 12.03 hrs, Volume= 0.268 af
Outflow = 3.70 cfs @ 12.03 hrs, Volume= 0.268 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: EX BLDG/PAVEMENT Runoff Area=6,027 sf 100.00% Impervious Runoff Depth=3.43"
Flow Length=75' Slope=0.0090 '/' Tc=5.0 min CN=98 Runoff=0.50 cfs 0.040 af

Subcatchment 2: EX BLDG/GRAVEL Runoff Area=13,815 sf 0.00% Impervious Runoff Depth=3.20"
Flow Length=83' Slope=0.0270 '/' Tc=5.0 min CN=96 Runoff=1.12 cfs 0.085 af

Subcatchment 3: GRAVEL Runoff Area=13,549 sf 0.00% Impervious Runoff Depth=3.20"
Flow Length=150' Tc=5.0 min CN=96 Runoff=1.10 cfs 0.083 af

Subcatchment 4: PAVEMENT/GRAVEL Runoff Area=32,428 sf 0.00% Impervious Runoff Depth=3.20"
Flow Length=202' Tc=5.7 min CN=96 Runoff=2.58 cfs 0.199 af

Subcatchment 5: WOODS Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.00"
Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af

Subcatchment 6: WOODS/GRAVEL Runoff Area=14,723 sf 0.00% Impervious Runoff Depth=0.07"
Flow Length=194' Tc=5.3 min CN=43 Runoff=0.00 cfs 0.002 af

Subcatchment 7: WOODS/GRAVEL Runoff Area=25,187 sf 0.00% Impervious Runoff Depth=0.30"
Flow Length=100' Slope=0.0080 '/' Tc=5.0 min CN=52 Runoff=0.07 cfs 0.014 af

Subcatchment 8: GRAVEL Runoff Area=21,066 sf 0.00% Impervious Runoff Depth=3.20"
Flow Length=186' Tc=5.0 min CN=96 Runoff=1.71 cfs 0.129 af

Subcatchment 9: Runoff Area=14,505 sf 0.00% Impervious Runoff Depth=3.20"
Flow Length=100' Slope=0.0020 '/' Tc=5.0 min CN=96 Runoff=1.18 cfs 0.089 af

Reach POI1: POI Inflow=1.18 cfs 0.089 af
Outflow=1.18 cfs 0.089 af

Reach POI2: POI#2 Inflow=4.20 cfs 0.323 af
Outflow=4.20 cfs 0.323 af

Total Runoff Area = 3.330 ac Runoff Volume = 0.640 af Average Runoff Depth = 2.31"
95.85% Pervious = 3.192 ac 4.15% Impervious = 0.138 ac

Summary for Subcatchment 1: EX BLDG/PAVEMENT

Runoff = 0.50 cfs @ 12.07 hrs, Volume= 0.040 af, Depth= 3.43"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
6,027	98	Paved parking, HSG A
6,027		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	75	0.0090	0.91		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.4	75	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 2: EX BLDG/GRAVEL

Runoff = 1.12 cfs @ 12.07 hrs, Volume= 0.085 af, Depth= 3.20"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
13,815	96	Gravel surface, HSG A
13,815		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	83	0.0270	1.45		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.0	83	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 3: GRAVEL

Runoff = 1.10 cfs @ 12.07 hrs, Volume= 0.083 af, Depth= 3.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
13,549	96	Gravel surface, HSG A
13,549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	90	0.0070	0.86		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	60	0.0160	2.04		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.3	150	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 4: PAVEMENT/GRAVEL

Runoff = 2.58 cfs @ 12.08 hrs, Volume= 0.199 af, Depth= 3.20"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
32,428	96	Gravel surface, HSG A
32,428		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	100	0.0040	0.70		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.3	102	0.0010	0.51		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
5.7	202	Total			

Summary for Subcatchment 5: WOODS

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 6: WOODS/GRAVEL

Runoff = 0.00 cfs @ 14.96 hrs, Volume= 0.002 af, Depth= 0.07"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
11,749	30	Woods, Good, HSG A
2,974	96	Gravel surface, HSG A
14,723	43	Weighted Average
14,723		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Summary for Subcatchment 7: WOODS/GRAVEL

Runoff = 0.07 cfs @ 12.31 hrs, Volume= 0.014 af, Depth= 0.30"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
16,835	30	Woods, Good, HSG A
8,352	96	Gravel surface, HSG A
25,187	52	Weighted Average
25,187		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.8	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 8: GRAVEL

Runoff = 1.71 cfs @ 12.07 hrs, Volume= 0.129 af, Depth= 3.20"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
21,066	96	Gravel surface, HSG A
21,066		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 9:

Runoff = 1.18 cfs @ 12.07 hrs, Volume= 0.089 af, Depth= 3.20"
 Routed to Reach POI1 : POI

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
14,505	96	Gravel surface, HSG A
14,505		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.1	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach POI1: POI

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.333 ac, 0.00% Impervious, Inflow Depth = 3.20" for 5-Year event
Inflow = 1.18 cfs @ 12.07 hrs, Volume= 0.089 af
Outflow = 1.18 cfs @ 12.07 hrs, Volume= 0.089 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, 11.53% Impervious, Inflow Depth = 3.23" for 5-Year event
Inflow = 4.20 cfs @ 12.08 hrs, Volume= 0.323 af
Outflow = 4.20 cfs @ 12.08 hrs, Volume= 0.323 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: EX BLDG/PAVEMENT Runoff Area=6,027 sf 100.00% Impervious Runoff Depth=4.36"
Flow Length=75' Slope=0.0090 '/' Tc=5.0 min CN=98 Runoff=0.63 cfs 0.050 af

Subcatchment 2: EX BLDG/GRAVEL Runoff Area=13,815 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=83' Slope=0.0270 '/' Tc=5.0 min CN=96 Runoff=1.43 cfs 0.109 af

Subcatchment 3: GRAVEL Runoff Area=13,549 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=150' Tc=5.0 min CN=96 Runoff=1.40 cfs 0.107 af

Subcatchment 4: PAVEMENT/GRAVEL Runoff Area=32,428 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=202' Tc=5.7 min CN=96 Runoff=3.29 cfs 0.257 af

Subcatchment 5: WOODS Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.00"
Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af

Subcatchment 6: WOODS/GRAVEL Runoff Area=14,723 sf 0.00% Impervious Runoff Depth=0.25"
Flow Length=194' Tc=5.3 min CN=43 Runoff=0.03 cfs 0.007 af

Subcatchment 7: WOODS/GRAVEL Runoff Area=25,187 sf 0.00% Impervious Runoff Depth=0.63"
Flow Length=100' Slope=0.0080 '/' Tc=5.0 min CN=52 Runoff=0.27 cfs 0.030 af

Subcatchment 8: GRAVEL Runoff Area=21,066 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=186' Tc=5.0 min CN=96 Runoff=2.18 cfs 0.167 af

Subcatchment 9: Runoff Area=14,505 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=100' Slope=0.0020 '/' Tc=5.0 min CN=96 Runoff=1.50 cfs 0.115 af

Reach POI1: POI Inflow=1.50 cfs 0.115 af
Outflow=1.50 cfs 0.115 af

Reach POI2: POI#2 Inflow=5.34 cfs 0.416 af
Outflow=5.34 cfs 0.416 af

Total Runoff Area = 3.330 ac Runoff Volume = 0.842 af Average Runoff Depth = 3.03"
95.85% Pervious = 3.192 ac 4.15% Impervious = 0.138 ac

Summary for Subcatchment 1: EX BLDG/PAVEMENT

Runoff = 0.63 cfs @ 12.07 hrs, Volume= 0.050 af, Depth= 4.36"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
6,027	98	Paved parking, HSG A
6,027		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	75	0.0090	0.91		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.4	75	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 2: EX BLDG/GRAVEL

Runoff = 1.43 cfs @ 12.07 hrs, Volume= 0.109 af, Depth= 4.14"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
13,815	96	Gravel surface, HSG A
13,815		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	83	0.0270	1.45		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.0	83	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 3: GRAVEL

Runoff = 1.40 cfs @ 12.07 hrs, Volume= 0.107 af, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
13,549	96	Gravel surface, HSG A
13,549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	90	0.0070	0.86		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	60	0.0160	2.04		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.3	150	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 4: PAVEMENT/GRAVEL

Runoff = 3.29 cfs @ 12.08 hrs, Volume= 0.257 af, Depth= 4.14"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
32,428	96	Gravel surface, HSG A
32,428		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	100	0.0040	0.70		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.3	102	0.0010	0.51		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
5.7	202	Total			

Summary for Subcatchment 5: WOODS

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 6: WOODS/GRAVEL

Runoff = 0.03 cfs @ 12.40 hrs, Volume= 0.007 af, Depth= 0.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
11,749	30	Woods, Good, HSG A
2,974	96	Gravel surface, HSG A
14,723	43	Weighted Average
14,723		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Summary for Subcatchment 7: WOODS/GRAVEL

Runoff = 0.27 cfs @ 12.11 hrs, Volume= 0.030 af, Depth= 0.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
16,835	30	Woods, Good, HSG A
8,352	96	Gravel surface, HSG A
25,187	52	Weighted Average
25,187		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.8	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 8: GRAVEL

Runoff = 2.18 cfs @ 12.07 hrs, Volume= 0.167 af, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
21,066	96	Gravel surface, HSG A
21,066		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 9:

Runoff = 1.50 cfs @ 12.07 hrs, Volume= 0.115 af, Depth= 4.14"
 Routed to Reach POI1 : POI

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
14,505	96	Gravel surface, HSG A
14,505		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.1	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach POI1: POI

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.333 ac, 0.00% Impervious, Inflow Depth = 4.14" for 10-Year event
Inflow = 1.50 cfs @ 12.07 hrs, Volume= 0.115 af
Outflow = 1.50 cfs @ 12.07 hrs, Volume= 0.115 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, 11.53% Impervious, Inflow Depth = 4.16" for 10-Year event
Inflow = 5.34 cfs @ 12.08 hrs, Volume= 0.416 af
Outflow = 5.34 cfs @ 12.08 hrs, Volume= 0.416 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: EX BLDG/PAVEMENT Runoff Area=6,027 sf 100.00% Impervious Runoff Depth=4.36"
Flow Length=75' Slope=0.0090 '/' Tc=5.0 min CN=98 Runoff=0.67 cfs 0.050 af

Subcatchment 2: EX BLDG/GRAVEL Runoff Area=13,815 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=83' Slope=0.0270 '/' Tc=5.0 min CN=96 Runoff=1.50 cfs 0.109 af

Subcatchment 3: GRAVEL Runoff Area=13,549 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=150' Tc=5.0 min CN=96 Runoff=1.47 cfs 0.107 af

Subcatchment 4: PAVEMENT/GRAVEL Runoff Area=32,428 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=202' Tc=5.7 min CN=96 Runoff=3.41 cfs 0.257 af

Subcatchment 5: WOODS Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.00"
Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af

Subcatchment 6: WOODS/GRAVEL Runoff Area=14,723 sf 0.00% Impervious Runoff Depth=0.25"
Flow Length=194' Tc=5.3 min CN=43 Runoff=0.01 cfs 0.007 af

Subcatchment 7: WOODS/GRAVEL Runoff Area=25,187 sf 0.00% Impervious Runoff Depth=0.63"
Flow Length=100' Slope=0.0080 '/' Tc=5.0 min CN=52 Runoff=0.26 cfs 0.030 af

Subcatchment 8: GRAVEL Runoff Area=21,066 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=186' Tc=5.0 min CN=96 Runoff=2.29 cfs 0.167 af

Subcatchment 9: Runoff Area=14,505 sf 0.00% Impervious Runoff Depth=4.14"
Flow Length=100' Slope=0.0020 '/' Tc=5.0 min CN=96 Runoff=1.58 cfs 0.115 af

Reach POI1: POI Inflow=1.58 cfs 0.115 af
Outflow=1.58 cfs 0.115 af

Reach POI2: POI#2 Inflow=5.57 cfs 0.416 af
Outflow=5.57 cfs 0.416 af

Total Runoff Area = 3.330 ac Runoff Volume = 0.842 af Average Runoff Depth = 3.03"
95.85% Pervious = 3.192 ac 4.15% Impervious = 0.138 ac

Summary for Subcatchment 1: EX BLDG/PAVEMENT

Runoff = 0.67 cfs @ 12.02 hrs, Volume= 0.050 af, Depth= 4.36"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 10-yr 10-YR Rainfall=4.60"

Area (sf)	CN	Description
6,027	98	Paved parking, HSG A
6,027		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	75	0.0090	0.91		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.4	75	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 2: EX BLDG/GRAVEL

Runoff = 1.50 cfs @ 12.02 hrs, Volume= 0.109 af, Depth= 4.14"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 10-yr 10-YR Rainfall=4.60"

Area (sf)	CN	Description
13,815	96	Gravel surface, HSG A
13,815		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	83	0.0270	1.45		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.0	83	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 3: GRAVEL

Runoff = 1.47 cfs @ 12.02 hrs, Volume= 0.107 af, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 10-yr 10-YR Rainfall=4.60"

Area (sf)	CN	Description
13,549	96	Gravel surface, HSG A
13,549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	90	0.0070	0.86		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	60	0.0160	2.04		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.3	150	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 4: PAVEMENT/GRAVEL

Runoff = 3.41 cfs @ 12.03 hrs, Volume= 0.257 af, Depth= 4.14"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 10-yr 10-YR Rainfall=4.60"

Area (sf)	CN	Description
32,428	96	Gravel surface, HSG A
32,428		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	100	0.0040	0.70		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.3	102	0.0010	0.51		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
5.7	202	Total			

Summary for Subcatchment 5: WOODS

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Cumberland 24-hr S1 10-yr 10-YR Rainfall=4.60"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 6: WOODS/GRAVEL

Runoff = 0.01 cfs @ 12.53 hrs, Volume= 0.007 af, Depth= 0.25"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 10-yr 10-YR Rainfall=4.60"

Area (sf)	CN	Description
11,749	30	Woods, Good, HSG A
2,974	96	Gravel surface, HSG A
14,723	43	Weighted Average
14,723		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Summary for Subcatchment 7: WOODS/GRAVEL

Runoff = 0.26 cfs @ 12.05 hrs, Volume= 0.030 af, Depth= 0.63"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 10-yr 10-YR Rainfall=4.60"

Area (sf)	CN	Description
16,835	30	Woods, Good, HSG A
8,352	96	Gravel surface, HSG A
25,187	52	Weighted Average
25,187		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.8	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 8: GRAVEL

Runoff = 2.29 cfs @ 12.02 hrs, Volume= 0.167 af, Depth= 4.14"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 10-yr 10-YR Rainfall=4.60"

Area (sf)	CN	Description
21,066	96	Gravel surface, HSG A
21,066		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 9:

Runoff = 1.58 cfs @ 12.02 hrs, Volume= 0.115 af, Depth= 4.14"
 Routed to Reach POI1 : POI

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 10-yr 10-YR Rainfall=4.60"

Area (sf)	CN	Description
14,505	96	Gravel surface, HSG A
14,505		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.1	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach POI1: POI

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.333 ac, 0.00% Impervious, Inflow Depth = 4.14" for 10-YR event
Inflow = 1.58 cfs @ 12.02 hrs, Volume= 0.115 af
Outflow = 1.58 cfs @ 12.02 hrs, Volume= 0.115 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, 11.53% Impervious, Inflow Depth = 4.16" for 10-YR event
Inflow = 5.57 cfs @ 12.03 hrs, Volume= 0.416 af
Outflow = 5.57 cfs @ 12.03 hrs, Volume= 0.416 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: EX BLDG/PAVEMENT Runoff Area=6,027 sf 100.00% Impervious Runoff Depth=5.56"
Flow Length=75' Slope=0.0090 '/' Tc=5.0 min CN=98 Runoff=0.84 cfs 0.064 af

Subcatchment 2: EX BLDG/GRAVEL Runoff Area=13,815 sf 0.00% Impervious Runoff Depth=5.33"
Flow Length=83' Slope=0.0270 '/' Tc=5.0 min CN=96 Runoff=1.91 cfs 0.141 af

Subcatchment 3: GRAVEL Runoff Area=13,549 sf 0.00% Impervious Runoff Depth=5.33"
Flow Length=150' Tc=5.0 min CN=96 Runoff=1.87 cfs 0.138 af

Subcatchment 4: PAVEMENT/GRAVEL Runoff Area=32,428 sf 0.00% Impervious Runoff Depth=5.33"
Flow Length=202' Tc=5.7 min CN=96 Runoff=4.33 cfs 0.331 af

Subcatchment 5: WOODS Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.05"
Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af

Subcatchment 6: WOODS/GRAVEL Runoff Area=14,723 sf 0.00% Impervious Runoff Depth=0.60"
Flow Length=194' Tc=5.3 min CN=43 Runoff=0.08 cfs 0.017 af

Subcatchment 7: WOODS/GRAVEL Runoff Area=25,187 sf 0.00% Impervious Runoff Depth=1.19"
Flow Length=100' Slope=0.0080 '/' Tc=5.0 min CN=52 Runoff=0.68 cfs 0.057 af

Subcatchment 8: GRAVEL Runoff Area=21,066 sf 0.00% Impervious Runoff Depth=5.33"
Flow Length=186' Tc=5.0 min CN=96 Runoff=2.91 cfs 0.215 af

Subcatchment 9: Runoff Area=14,505 sf 0.00% Impervious Runoff Depth=5.33"
Flow Length=100' Slope=0.0020 '/' Tc=5.0 min CN=96 Runoff=2.00 cfs 0.148 af

Reach POI1: POI Inflow=2.00 cfs 0.148 af
Outflow=2.00 cfs 0.148 af

Reach POI2: POI#2 Inflow=7.06 cfs 0.536 af
Outflow=7.06 cfs 0.536 af

Total Runoff Area = 3.330 ac Runoff Volume = 1.111 af Average Runoff Depth = 4.00"
95.85% Pervious = 3.192 ac 4.15% Impervious = 0.138 ac

Summary for Subcatchment 1: EX BLDG/PAVEMENT

Runoff = 0.84 cfs @ 12.02 hrs, Volume= 0.064 af, Depth= 5.56"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
6,027	98	Paved parking, HSG A
6,027		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.4	75	0.0090	0.91		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.4	75	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 2: EX BLDG/GRAVEL

Runoff = 1.91 cfs @ 12.02 hrs, Volume= 0.141 af, Depth= 5.33"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
13,815	96	Gravel surface, HSG A
13,815		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.0	83	0.0270	1.45		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.0	83	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 3: GRAVEL

Runoff = 1.87 cfs @ 12.02 hrs, Volume= 0.138 af, Depth= 5.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
13,549	96	Gravel surface, HSG A
13,549		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	90	0.0070	0.86		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.5	60	0.0160	2.04		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.3	150	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 4: PAVEMENT/GRAVEL

Runoff = 4.33 cfs @ 12.03 hrs, Volume= 0.331 af, Depth= 5.33"
 Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
32,428	96	Gravel surface, HSG A
32,428		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.4	100	0.0040	0.70		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.3	102	0.0010	0.51		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
5.7	202	Total			

Summary for Subcatchment 5: WOODS

Runoff = 0.00 cfs @ 23.96 hrs, Volume= 0.000 af, Depth= 0.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 6: WOODS/GRAVEL

Runoff = 0.08 cfs @ 12.08 hrs, Volume= 0.017 af, Depth= 0.60"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
11,749	30	Woods, Good, HSG A
2,974	96	Gravel surface, HSG A
14,723	43	Weighted Average
14,723		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

Summary for Subcatchment 7: WOODS/GRAVEL

Runoff = 0.68 cfs @ 12.04 hrs, Volume= 0.057 af, Depth= 1.19"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
16,835	30	Woods, Good, HSG A
8,352	96	Gravel surface, HSG A
25,187	52	Weighted Average
25,187		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
1.8	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 8: GRAVEL

Runoff = 2.91 cfs @ 12.02 hrs, Volume= 0.215 af, Depth= 5.33"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
21,066	96	Gravel surface, HSG A
21,066		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved Kv= 16.1 fps
2.5	186	Total, Increased to minimum Tc = 5.0 min			

Summary for Subcatchment 9:

Runoff = 2.00 cfs @ 12.02 hrs, Volume= 0.148 af, Depth= 5.33"
 Routed to Reach POI1 : POI

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
14,505	96	Gravel surface, HSG A
14,505		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
3.1	100	Total, Increased to minimum Tc = 5.0 min			

Summary for Reach POI1: POI

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.333 ac, 0.00% Impervious, Inflow Depth = 5.33" for 25-yr event
Inflow = 2.00 cfs @ 12.02 hrs, Volume= 0.148 af
Outflow = 2.00 cfs @ 12.02 hrs, Volume= 0.148 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.200 ac, 11.53% Impervious, Inflow Depth = 5.36" for 25-yr event
Inflow = 7.06 cfs @ 12.03 hrs, Volume= 0.536 af
Outflow = 7.06 cfs @ 12.03 hrs, Volume= 0.536 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Project Notes

Copied 4 events from Cumberland 24-hr S1 storm

Rainfall events imported from "Atlas-14-Rain.txt" for 1365 ME Cumberland Nw

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Rainfall Events Listing (selected events)

Event#	Event Name	Storm Type	Curve	Mode	Duration (hours)	B/B	Depth (inches)	AMC
1	2-yr	Cumberland 24-hr S1	2-yr	Default	24.00	1	3.10	2
2	5-Year	Type III 24-hr		Default	24.00	1	3.66	2
3	10-Year	Type III 24-hr		Default	24.00	1	4.60	2
4	25-yr	Cumberland 24-hr S1	25-yr	Default	24.00	1	5.80	2

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Area Listing (all nodes)

Area (acres)	CN	Description (subcatchment-numbers)
1.197	39	>75% Grass cover, Good, HSG A (1, 3, 6, 7, 8, 9, 10, 11, 30)
0.043	74	>75% Grass cover, Good, HSG C (2)
1.418	98	Paved parking, HSG A (1, 2, 3, 9, 10, 11, 30)
0.188	98	Roofs, HSG A (1, 4)
0.572	30	Woods, Good, HSG A (5, 6, 7)
3.419	66	TOTAL AREA

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Soil Listing (all nodes)

Area (acres)	Soil Group	Subcatchment Numbers
3.375	HSG A	1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 30
0.000	HSG B	
0.043	HSG C	2
0.000	HSG D	
0.000	Other	
3.419		TOTAL AREA

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Ground Covers (all nodes)

HSG-A (acres)	HSG-B (acres)	HSG-C (acres)	HSG-D (acres)	Other (acres)	Total (acres)	Ground Cover	Subcatchment Numbers
1.197	0.000	0.043	0.000	0.000	1.240	>75% Grass cover, Good	1, 2, 3, 6, 7, 8, 9, 10, 11, 30
1.418	0.000	0.000	0.000	0.000	1.418	Paved parking	1, 2, 3, 9, 10, 11, 30
0.188	0.000	0.000	0.000	0.000	0.188	Roofs	1, 4
0.572	0.000	0.000	0.000	0.000	0.572	Woods, Good	5, 6, 7
3.375	0.000	0.043	0.000	0.000	3.419	TOTAL AREA	

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: Store Roof	Runoff Area=13,303 sf 43.76% Impervious Runoff Depth=0.55" Tc=5.0 min CN=65 Runoff=0.15 cfs 0.014 af
Subcatchment 2: C-Store Parking	Runoff Area=42,253 sf 95.54% Impervious Runoff Depth=2.76" Tc=5.0 min CN=97 Runoff=3.11 cfs 0.223 af
Subcatchment 3:	Runoff Area=7,568 sf 8.39% Impervious Runoff Depth=0.02" Tc=0.0 min CN=44 Runoff=0.00 cfs 0.000 af
Subcatchment 4: (new Subcat)	Runoff Area=2,935 sf 100.00% Impervious Runoff Depth=2.87" Tc=5.0 min CN=98 Runoff=0.22 cfs 0.016 af
Subcatchment 5: Woods/Lawn	Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.00" Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment 6: Woods/Lawn	Runoff Area=14,372 sf 0.00% Impervious Runoff Depth=0.00" Flow Length=194' Tc=5.3 min CN=34 Runoff=0.00 cfs 0.000 af
Subcatchment 7: Woods/Lawn	Runoff Area=23,678 sf 0.00% Impervious Runoff Depth=0.00" Flow Length=100' Slope=0.0080 '/' Tc=1.8 min CN=34 Runoff=0.00 cfs 0.000 af
Subcatchment 8: Lawn	Runoff Area=6,349 sf 0.00% Impervious Runoff Depth=0.00" Flow Length=186' Tc=2.5 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment 9:	Runoff Area=6,505 sf 28.90% Impervious Runoff Depth=0.25" Flow Length=100' Slope=0.0020 '/' Tc=3.1 min CN=56 Runoff=0.01 cfs 0.003 af
Subcatchment 10:	Runoff Area=6,660 sf 14.29% Impervious Runoff Depth=0.06" Tc=5.0 min CN=47 Runoff=0.00 cfs 0.001 af
Subcatchment 11: Drive Entrance	Runoff Area=6,048 sf 60.75% Impervious Runoff Depth=1.03" Tc=5.0 min CN=75 Runoff=0.17 cfs 0.012 af
Subcatchment 30: Bank Parking	Runoff Area=15,466 sf 88.46% Impervious Runoff Depth=2.16" Tc=5.0 min CN=91 Runoff=0.96 cfs 0.064 af
Reach POI1: POI#1	Inflow=0.45 cfs 0.290 af Outflow=0.45 cfs 0.290 af
Reach POI2: POI#2	Inflow=0.17 cfs 0.013 af Outflow=0.17 cfs 0.013 af
Pond 3P: SSSF1	Peak Elev=10.76' Storage=2,303 cf Inflow=3.11 cfs 0.223 af Outflow=0.32 cfs 0.223 af
Pond 5P: Roof Infiltration	Peak Elev=295.23' Storage=66 cf Inflow=0.15 cfs 0.014 af Outflow=0.04 cfs 0.014 af

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Pond 6P: SSSF2

Peak Elev=294.42' Storage=561 cf Inflow=0.96 cfs 0.064 af
Outflow=0.13 cfs 0.064 af

Pond 7P: CB

Inflow=0.45 cfs 0.287 af
Primary=0.45 cfs 0.287 af

Total Runoff Area = 3.419 ac Runoff Volume = 0.333 af Average Runoff Depth = 1.17"
53.03% Pervious = 1.813 ac 46.97% Impervious = 1.606 ac

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Summary for Subcatchment 1: Store Roof

Runoff = 0.15 cfs @ 12.04 hrs, Volume= 0.014 af, Depth= 0.55"
Routed to Pond 5P : Roof Infiltration

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
5,262	98	Roofs, HSG A
784	39	>75% Grass cover, Good, HSG A
6,698	39	>75% Grass cover, Good, HSG A
559	98	Paved parking, HSG A
13,303	65	Weighted Average
7,482		56.24% Pervious Area
5,821		43.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 2: C-Store Parking

Runoff = 3.11 cfs @ 12.02 hrs, Volume= 0.223 af, Depth= 2.76"
Routed to Pond 3P : SSSF1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
40,368	98	Paved parking, HSG A
136	74	>75% Grass cover, Good, HSG C
1,560	74	>75% Grass cover, Good, HSG C
189	74	>75% Grass cover, Good, HSG C
42,253	97	Weighted Average
1,885		4.46% Pervious Area
40,368		95.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 3:

[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 0.00 cfs @ 23.96 hrs, Volume= 0.000 af, Depth= 0.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
281	39	>75% Grass cover, Good, HSG A
635	98	Paved parking, HSG A
6,652	39	>75% Grass cover, Good, HSG A
7,568	44	Weighted Average
6,933		91.61% Pervious Area
635		8.39% Impervious Area

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Summary for Subcatchment 4: (new Subcat)

Runoff = 0.22 cfs @ 12.02 hrs, Volume= 0.016 af, Depth= 2.87"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
2,935	98	Roofs, HSG A
2,935		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 5: Woods/Lawn

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 6: Woods/Lawn

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
8,326	30	Woods, Good, HSG A
6,046	39	>75% Grass cover, Good, HSG A
14,372	34	Weighted Average
14,372		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

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Summary for Subcatchment 7: Woods/Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
12,831	30	Woods, Good, HSG A
10,847	39	>75% Grass cover, Good, HSG A
23,678	34	Weighted Average
23,678		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.00"

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Summary for Subcatchment 8: Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
6,349	39	>75% Grass cover, Good, HSG A
6,349		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces $n=0.011$ $P2=3.00"$
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved $K_v=16.1$ fps
2.5	186	Total			

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Cumberland 24-hr S1 2-yr Rainfall=3.10"

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Summary for Subcatchment 9:[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.01 cfs @ 12.12 hrs, Volume= 0.003 af, Depth= 0.25"
 Routed to Reach POI1 : POI#1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
 Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
4,245	39	>75% Grass cover, Good, HSG A
1,652	98	Paved parking, HSG A
380	39	>75% Grass cover, Good, HSG A
228	98	Paved parking, HSG A
6,505	56	Weighted Average
4,625		71.10% Pervious Area
1,880		28.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B Smooth surfaces $n=0.011$ $P2=3.00"$

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Summary for Subcatchment 10:

Runoff = 0.00 cfs @ 23.24 hrs, Volume= 0.001 af, Depth= 0.06"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
3,751	39	>75% Grass cover, Good, HSG A
1,957	39	>75% Grass cover, Good, HSG A
444	98	Paved parking, HSG A
139	98	Paved parking, HSG A
369	98	Paved parking, HSG A
6,660	47	Weighted Average
5,708		85.71% Pervious Area
952		14.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 11: Drive Entrance

Runoff = 0.17 cfs @ 12.03 hrs, Volume= 0.012 af, Depth= 1.03"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
832	39	>75% Grass cover, Good, HSG A
1,321	39	>75% Grass cover, Good, HSG A
221	39	>75% Grass cover, Good, HSG A
3,674	98	Paved parking, HSG A
6,048	75	Weighted Average
2,374		39.25% Pervious Area
3,674		60.75% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 30: Bank Parking

Runoff = 0.96 cfs @ 12.03 hrs, Volume= 0.064 af, Depth= 2.16"
Routed to Pond 6P : SSSF2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 2-yr Rainfall=3.10"

Area (sf)	CN	Description
13,681	98	Paved parking, HSG A
969	39	>75% Grass cover, Good, HSG A
240	39	>75% Grass cover, Good, HSG A
380	39	>75% Grass cover, Good, HSG A
196	39	>75% Grass cover, Good, HSG A
15,466	91	Weighted Average
1,785		11.54% Pervious Area
13,681		88.46% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Reach POI1: POI#1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.474 ac, 87.08% Impervious, Inflow Depth = 2.36" for 2-yr event
Inflow = 0.45 cfs @ 12.52 hrs, Volume= 0.290 af
Outflow = 0.45 cfs @ 12.52 hrs, Volume= 0.290 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.292 ac, 36.40% Impervious, Inflow Depth = 0.52" for 2-yr event
Inflow = 0.17 cfs @ 12.03 hrs, Volume= 0.013 af
Outflow = 0.17 cfs @ 12.03 hrs, Volume= 0.013 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Summary for Pond 3P: SSSF1

Inflow Area = 0.970 ac, 95.54% Impervious, Inflow Depth = 2.76" for 2-yr event
 Inflow = 3.11 cfs @ 12.02 hrs, Volume= 0.223 af
 Outflow = 0.32 cfs @ 12.62 hrs, Volume= 0.223 af, Atten= 90%, Lag= 35.7 min
 Primary = 0.32 cfs @ 12.62 hrs, Volume= 0.223 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 10.76' @ 12.62 hrs Surf.Area= 4,163 sf Storage= 2,303 cf

Plug-Flow detention time= 43.4 min calculated for 0.223 af (100% of inflow)
 Center-of-Mass det. time= 43.4 min (816.0 - 772.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	10.00'	2,374 cf	74.87'W x 55.61'L x 2.69'H Field A 11,214 cf Overall - 5,279 cf Embedded = 5,934 cf x 40.0% Voids
#2A	10.25'	5,015 cf	ACF R-Tank HD 1 x 1188 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 1188 Chambers in 54 Rows
7,389 cf			Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	10.00'	2.410 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 8.00'

Primary OutFlow Max=0.32 cfs @ 12.62 hrs HW=10.76' (Free Discharge)
 ↑ **1=Exfiltration** (Controls 0.32 cfs)

Pond 3P: SSSF1 - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

22 Chambers/Row x 2.35' Long = 51.61' Row Length +24.0" End Stone x 2 = 55.61' Base Length

54 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 74.87' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

1,188 Chambers x 4.2 cf = 5,015.5 cf Chamber Storage

1,188 Chambers x 4.4 cf = 5,279.5 cf Displacement

11,213.7 cf Field - 5,279.5 cf Chambers = 5,934.2 cf Stone x 40.0% Voids = 2,373.7 cf Stone Storage

Chamber Storage + Stone Storage = 7,389.2 cf = 0.170 af

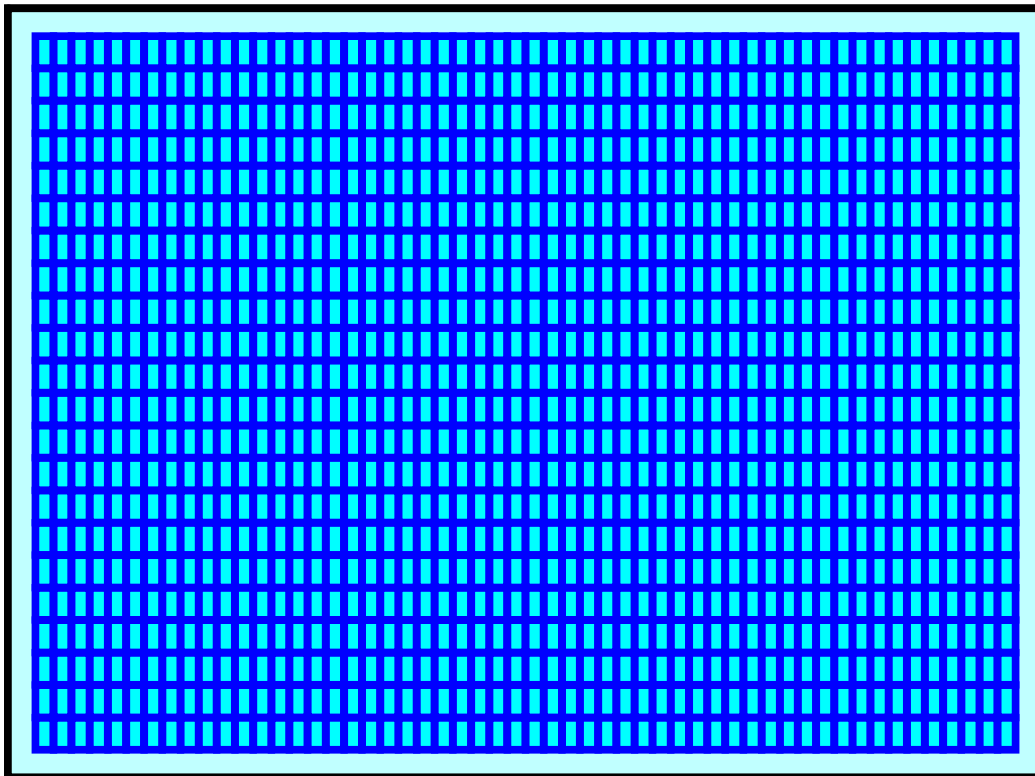
Overall Storage Efficiency = 65.9%

Overall System Size = 55.61' x 74.87' x 2.69'

1,188 Chambers

415.3 cy Field

219.8 cy Stone



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Summary for Pond 5P: Roof Infiltration

Inflow Area = 0.305 ac, 43.76% Impervious, Inflow Depth = 0.55" for 2-yr event
 Inflow = 0.15 cfs @ 12.04 hrs, Volume= 0.014 af
 Outflow = 0.04 cfs @ 12.00 hrs, Volume= 0.014 af, Atten= 74%, Lag= 0.0 min
 Discarded = 0.04 cfs @ 12.00 hrs, Volume= 0.014 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 295.23' @ 12.38 hrs Surf.Area= 719 sf Storage= 66 cf

Plug-Flow detention time= 8.6 min calculated for 0.014 af (100% of inflow)
 Center-of-Mass det. time= 8.6 min (961.4 - 952.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	295.00'	476 cf	22.37'W x 32.15'L x 2.69'H Field A 1,937 cf Overall - 747 cf Embedded = 1,191 cf x 40.0% Voids
#2A	295.25'	709 cf	ACF R-Tank HD 1 x 168 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 168 Chambers in 14 Rows
		1,186 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	295.00'	2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.04 cfs @ 12.00 hrs HW=295.05' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.04 cfs)

Pond 5P: Roof Infiltration - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

12 Chambers/Row x 2.35' Long = 28.15' Row Length +24.0" End Stone x 2 = 32.15' Base Length

14 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 22.37' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

168 Chambers x 4.2 cf = 709.3 cf Chamber Storage

168 Chambers x 4.4 cf = 746.6 cf Displacement

1,937.4 cf Field - 746.6 cf Chambers = 1,190.8 cf Stone x 40.0% Voids = 476.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,185.6 cf = 0.027 af

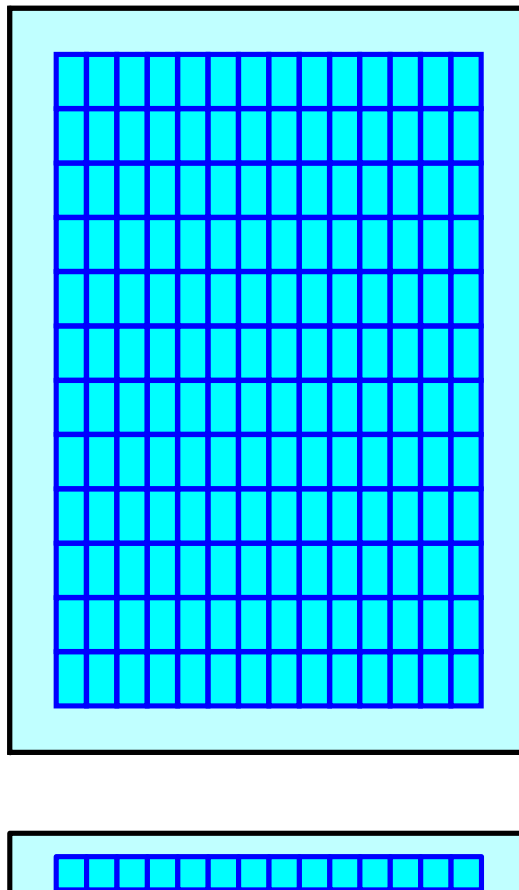
Overall Storage Efficiency = 61.2%

Overall System Size = 32.15' x 22.37' x 2.69'

168 Chambers

71.8 cy Field

44.1 cy Stone



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Summary for Pond 6P: SSSF2

Inflow Area = 0.355 ac, 88.46% Impervious, Inflow Depth = 2.16" for 2-yr event
 Inflow = 0.96 cfs @ 12.03 hrs, Volume= 0.064 af
 Outflow = 0.13 cfs @ 11.76 hrs, Volume= 0.064 af, Atten= 87%, Lag= 0.0 min
 Primary = 0.13 cfs @ 11.76 hrs, Volume= 0.064 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 294.42' @ 12.51 hrs Surf.Area= 2,299 sf Storage= 561 cf

Plug-Flow detention time= 23.0 min calculated for 0.064 af (100% of inflow)
 Center-of-Mass det. time= 23.0 min (846.0 - 823.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	294.00'	1,268 cf	38.12'W x 60.30'L x 2.04'H Field A 4,683 cf Overall - 1,513 cf Embedded = 3,171 cf x 40.0% Voids
#2A	294.25'	1,437 cf	ACF R-Tank SD 1 x 624 Inside #1 Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf 624 Chambers in 26 Rows
		2,705 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	294.00'	2.410 in/hr Exfiltration over Surface area

Primary OutFlow Max=0.13 cfs @ 11.76 hrs HW=294.02' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.13 cfs)

Pond 6P: SSSF2 - Chamber Wizard Field A**Chamber Model = ACF R-Tank SD 1 (ACF Environmental R-Tank SD)**

Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf

Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf

24 Chambers/Row x 2.35' Long = 56.30' Row Length +24.0" End Stone x 2 = 60.30' Base Length

26 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 38.12' Base Width

3.0" Stone Base + 9.4" Chamber Height + 12.0" Stone Cover = 2.04' Field Height

624 Chambers x 2.3 cf = 1,436.9 cf Chamber Storage

624 Chambers x 2.4 cf = 1,512.6 cf Displacement

4,683.3 cf Field - 1,512.6 cf Chambers = 3,170.7 cf Stone x 40.0% Voids = 1,268.3 cf Stone Storage

Chamber Storage + Stone Storage = 2,705.2 cf = 0.062 af

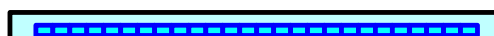
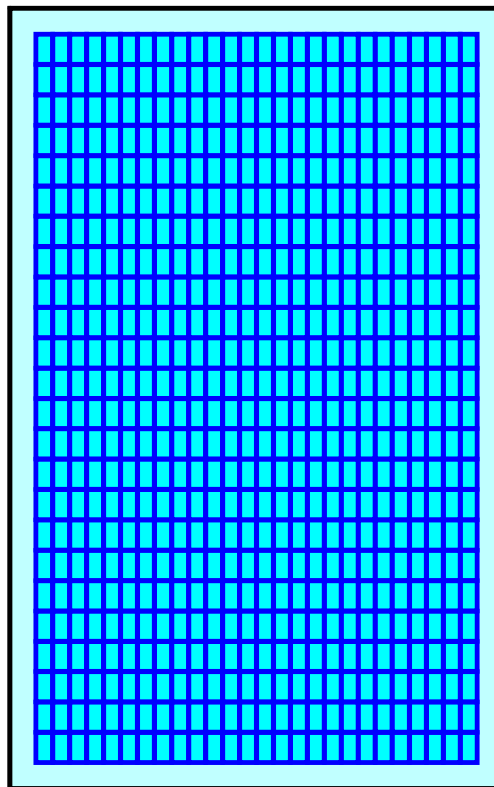
Overall Storage Efficiency = 57.8%

Overall System Size = 60.30' x 38.12' x 2.04'

624 Chambers

173.5 cy Field

117.4 cy Stone



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Summary for Pond 7P: CB

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.325 ac, 93.64% Impervious, Inflow Depth = 2.60" for 2-yr event
Inflow = 0.45 cfs @ 12.62 hrs, Volume= 0.287 af
Primary = 0.45 cfs @ 12.62 hrs, Volume= 0.287 af, Atten= 0%, Lag= 0.0 min
Routed to Reach POI1 : POI#1

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: Store Roof	Runoff Area=13,303 sf 43.76% Impervious Runoff Depth=0.84" Tc=5.0 min CN=65 Runoff=0.26 cfs 0.021 af
Subcatchment 2: C-Store Parking	Runoff Area=42,253 sf 95.54% Impervious Runoff Depth=3.31" Tc=5.0 min CN=97 Runoff=3.49 cfs 0.268 af
Subcatchment 3:	Runoff Area=7,568 sf 8.39% Impervious Runoff Depth=0.09" Tc=0.0 min CN=44 Runoff=0.00 cfs 0.001 af
Subcatchment 4: (new Subcat)	Runoff Area=2,935 sf 100.00% Impervious Runoff Depth=3.43" Tc=5.0 min CN=98 Runoff=0.25 cfs 0.019 af
Subcatchment 5: Woods/Lawn	Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.00" Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment 6: Woods/Lawn	Runoff Area=14,372 sf 0.00% Impervious Runoff Depth=0.00" Flow Length=194' Tc=5.3 min CN=34 Runoff=0.00 cfs 0.000 af
Subcatchment 7: Woods/Lawn	Runoff Area=23,678 sf 0.00% Impervious Runoff Depth=0.00" Flow Length=100' Slope=0.0080 '/' Tc=1.8 min CN=34 Runoff=0.00 cfs 0.000 af
Subcatchment 8: Lawn	Runoff Area=6,349 sf 0.00% Impervious Runoff Depth=0.02" Flow Length=186' Tc=2.5 min CN=39 Runoff=0.00 cfs 0.000 af
Subcatchment 9:	Runoff Area=6,505 sf 28.90% Impervious Runoff Depth=0.44" Flow Length=100' Slope=0.0020 '/' Tc=3.1 min CN=56 Runoff=0.05 cfs 0.005 af
Subcatchment 10:	Runoff Area=6,660 sf 14.29% Impervious Runoff Depth=0.16" Tc=5.0 min CN=47 Runoff=0.01 cfs 0.002 af
Subcatchment 11: Drive Entrance	Runoff Area=6,048 sf 60.75% Impervious Runoff Depth=1.42" Tc=5.0 min CN=75 Runoff=0.23 cfs 0.016 af
Subcatchment 30: Bank Parking	Runoff Area=15,466 sf 88.46% Impervious Runoff Depth=2.69" Tc=5.0 min CN=91 Runoff=1.12 cfs 0.080 af
Reach POI1: POI#1	Inflow=0.53 cfs 0.353 af Outflow=0.53 cfs 0.353 af
Reach POI2: POI#2	Inflow=0.23 cfs 0.018 af Outflow=0.23 cfs 0.018 af
Pond 3P: SSSF1	Peak Elev=11.26' Storage=4,138 cf Inflow=3.49 cfs 0.268 af Outflow=0.38 cfs 0.268 af
Pond 5P: Roof Infiltration	Peak Elev=295.57' Storage=255 cf Inflow=0.26 cfs 0.021 af Outflow=0.04 cfs 0.021 af

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Pond 6P: SSSF2Peak Elev=294.73' Storage=1,169 cf Inflow=1.12 cfs 0.080 af
Outflow=0.13 cfs 0.080 af**Pond 7P: CB**Inflow=0.51 cfs 0.348 af
Primary=0.51 cfs 0.348 af**Total Runoff Area = 3.419 ac Runoff Volume = 0.413 af Average Runoff Depth = 1.45"**
53.03% Pervious = 1.813 ac 46.97% Impervious = 1.606 ac

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Summary for Subcatchment 1: Store Roof

Runoff = 0.26 cfs @ 12.09 hrs, Volume= 0.021 af, Depth= 0.84"
Routed to Pond 5P : Roof Infiltration

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
5,262	98	Roofs, HSG A
784	39	>75% Grass cover, Good, HSG A
6,698	39	>75% Grass cover, Good, HSG A
559	98	Paved parking, HSG A
13,303	65	Weighted Average
7,482		56.24% Pervious Area
5,821		43.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 2: C-Store Parking

Runoff = 3.49 cfs @ 12.07 hrs, Volume= 0.268 af, Depth= 3.31"
Routed to Pond 3P : SSSF1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
40,368	98	Paved parking, HSG A
136	74	>75% Grass cover, Good, HSG C
1,560	74	>75% Grass cover, Good, HSG C
189	74	>75% Grass cover, Good, HSG C
42,253	97	Weighted Average
1,885		4.46% Pervious Area
40,368		95.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 3:

[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 0.00 cfs @ 14.62 hrs, Volume= 0.001 af, Depth= 0.09"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
281	39	>75% Grass cover, Good, HSG A
635	98	Paved parking, HSG A
6,652	39	>75% Grass cover, Good, HSG A
7,568	44	Weighted Average
6,933		91.61% Pervious Area
635		8.39% Impervious Area

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Summary for Subcatchment 4: (new Subcat)

Runoff = 0.25 cfs @ 12.07 hrs, Volume= 0.019 af, Depth= 3.43"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
2,935	98	Roofs, HSG A
2,935		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 5-Year Rainfall=3.66"

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Summary for Subcatchment 5: Woods/Lawn

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 6: Woods/Lawn

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
8,326	30	Woods, Good, HSG A
6,046	39	>75% Grass cover, Good, HSG A
14,372	34	Weighted Average
14,372		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

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Summary for Subcatchment 7: Woods/Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
12,831	30	Woods, Good, HSG A
10,847	39	>75% Grass cover, Good, HSG A
23,678	34	Weighted Average
23,678		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"

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Type III 24-hr 5-Year Rainfall=3.66"

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Summary for Subcatchment 8: Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.00 cfs @ 21.20 hrs, Volume= 0.000 af, Depth= 0.02"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
6,349	39	>75% Grass cover, Good, HSG A
6,349		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces $n=0.011$ $P2=3.00"$
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved $K_v=16.1$ fps
2.5	186	Total			

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Type III 24-hr 5-Year Rainfall=3.66"

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Summary for Subcatchment 9:[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.05 cfs @ 12.09 hrs, Volume= 0.005 af, Depth= 0.44"
 Routed to Reach POI1 : POI#1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
 Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
4,245	39	>75% Grass cover, Good, HSG A
1,652	98	Paved parking, HSG A
380	39	>75% Grass cover, Good, HSG A
228	98	Paved parking, HSG A
6,505	56	Weighted Average
4,625		71.10% Pervious Area
1,880		28.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B Smooth surfaces $n=0.011$ $P2=3.00"$

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Summary for Subcatchment 10:

Runoff = 0.01 cfs @ 12.45 hrs, Volume= 0.002 af, Depth= 0.16"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
3,751	39	>75% Grass cover, Good, HSG A
1,957	39	>75% Grass cover, Good, HSG A
444	98	Paved parking, HSG A
139	98	Paved parking, HSG A
369	98	Paved parking, HSG A
6,660	47	Weighted Average
5,708		85.71% Pervious Area
952		14.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 5-Year Rainfall=3.66"

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Summary for Subcatchment 11: Drive Entrance

Runoff = 0.23 cfs @ 12.08 hrs, Volume= 0.016 af, Depth= 1.42"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
832	39	>75% Grass cover, Good, HSG A
1,321	39	>75% Grass cover, Good, HSG A
221	39	>75% Grass cover, Good, HSG A
3,674	98	Paved parking, HSG A
6,048	75	Weighted Average
2,374		39.25% Pervious Area
3,674		60.75% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 5-Year Rainfall=3.66"

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Summary for Subcatchment 30: Bank Parking

Runoff = 1.12 cfs @ 12.07 hrs, Volume= 0.080 af, Depth= 2.69"
Routed to Pond 6P : SSSF2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 5-Year Rainfall=3.66"

Area (sf)	CN	Description
13,681	98	Paved parking, HSG A
969	39	>75% Grass cover, Good, HSG A
240	39	>75% Grass cover, Good, HSG A
380	39	>75% Grass cover, Good, HSG A
196	39	>75% Grass cover, Good, HSG A
15,466	91	Weighted Average
1,785		11.54% Pervious Area
13,681		88.46% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Reach POI1: POI#1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.474 ac, 87.08% Impervious, Inflow Depth = 2.87" for 5-Year event
Inflow = 0.53 cfs @ 12.40 hrs, Volume= 0.353 af
Outflow = 0.53 cfs @ 12.40 hrs, Volume= 0.353 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.292 ac, 36.40% Impervious, Inflow Depth = 0.76" for 5-Year event
Inflow = 0.23 cfs @ 12.08 hrs, Volume= 0.018 af
Outflow = 0.23 cfs @ 12.08 hrs, Volume= 0.018 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Summary for Pond 3P: SSSF1

Inflow Area = 0.970 ac, 95.54% Impervious, Inflow Depth = 3.31" for 5-Year event
 Inflow = 3.49 cfs @ 12.07 hrs, Volume= 0.268 af
 Outflow = 0.38 cfs @ 12.71 hrs, Volume= 0.268 af, Atten= 89%, Lag= 38.2 min
 Primary = 0.38 cfs @ 12.71 hrs, Volume= 0.268 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 11.26' @ 12.71 hrs Surf.Area= 4,163 sf Storage= 4,138 cf

Plug-Flow detention time= 85.4 min calculated for 0.268 af (100% of inflow)
 Center-of-Mass det. time= 85.3 min (847.1 - 761.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	10.00'	2,374 cf	74.87'W x 55.61'L x 2.69'H Field A 11,214 cf Overall - 5,279 cf Embedded = 5,934 cf x 40.0% Voids
#2A	10.25'	5,015 cf	ACF R-Tank HD 1 x 1188 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 1188 Chambers in 54 Rows
7,389 cf			Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	10.00'	2.410 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 8.00'

Primary OutFlow Max=0.38 cfs @ 12.71 hrs HW=11.26' (Free Discharge)
 ↑ **1=Exfiltration** (Controls 0.38 cfs)

Pond 3P: SSSF1 - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

22 Chambers/Row x 2.35' Long = 51.61' Row Length +24.0" End Stone x 2 = 55.61' Base Length

54 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 74.87' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

1,188 Chambers x 4.2 cf = 5,015.5 cf Chamber Storage

1,188 Chambers x 4.4 cf = 5,279.5 cf Displacement

11,213.7 cf Field - 5,279.5 cf Chambers = 5,934.2 cf Stone x 40.0% Voids = 2,373.7 cf Stone Storage

Chamber Storage + Stone Storage = 7,389.2 cf = 0.170 af

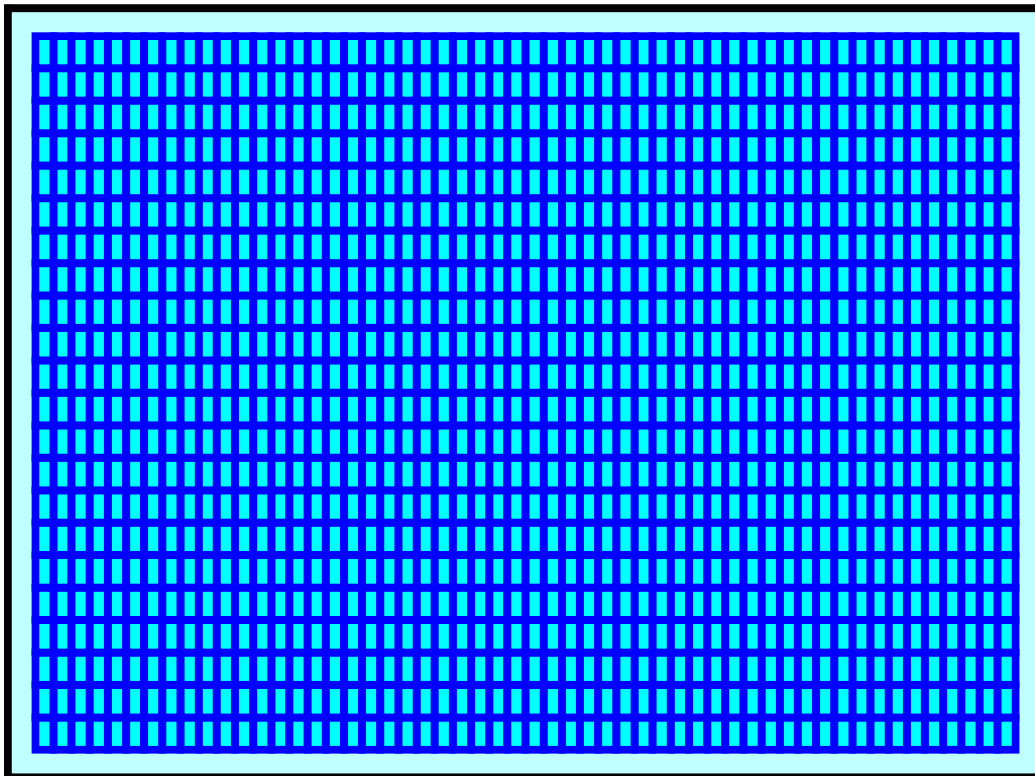
Overall Storage Efficiency = 65.9%

Overall System Size = 55.61' x 74.87' x 2.69'

1,188 Chambers

415.3 cy Field

219.8 cy Stone



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Summary for Pond 5P: Roof Infiltration

Inflow Area = 0.305 ac, 43.76% Impervious, Inflow Depth = 0.84" for 5-Year event
 Inflow = 0.26 cfs @ 12.09 hrs, Volume= 0.021 af
 Outflow = 0.04 cfs @ 11.92 hrs, Volume= 0.021 af, Atten= 85%, Lag= 0.0 min
 Discarded = 0.04 cfs @ 11.92 hrs, Volume= 0.021 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 295.57' @ 12.93 hrs Surf.Area= 719 sf Storage= 255 cf

Plug-Flow detention time= 51.8 min calculated for 0.021 af (100% of inflow)
 Center-of-Mass det. time= 51.8 min (934.0 - 882.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	295.00'	476 cf	22.37'W x 32.15'L x 2.69'H Field A 1,937 cf Overall - 747 cf Embedded = 1,191 cf x 40.0% Voids
#2A	295.25'	709 cf	ACF R-Tank HD 1 x 168 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 168 Chambers in 14 Rows
		1,186 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	295.00'	2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.04 cfs @ 11.92 hrs HW=295.03' (Free Discharge)

↑**1=Exfiltration** (Exfiltration Controls 0.04 cfs)

Pond 5P: Roof Infiltration - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

12 Chambers/Row x 2.35' Long = 28.15' Row Length +24.0" End Stone x 2 = 32.15' Base Length

14 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 22.37' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

168 Chambers x 4.2 cf = 709.3 cf Chamber Storage

168 Chambers x 4.4 cf = 746.6 cf Displacement

1,937.4 cf Field - 746.6 cf Chambers = 1,190.8 cf Stone x 40.0% Voids = 476.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,185.6 cf = 0.027 af

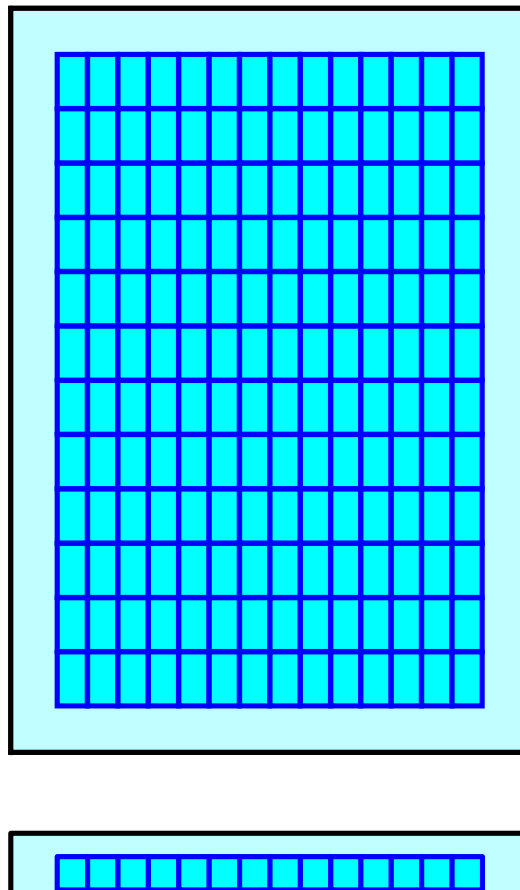
Overall Storage Efficiency = 61.2%

Overall System Size = 32.15' x 22.37' x 2.69'

168 Chambers

71.8 cy Field

44.1 cy Stone



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Summary for Pond 6P: SSSF2

Inflow Area = 0.355 ac, 88.46% Impervious, Inflow Depth = 2.69" for 5-Year event
 Inflow = 1.12 cfs @ 12.07 hrs, Volume= 0.080 af
 Outflow = 0.13 cfs @ 11.64 hrs, Volume= 0.080 af, Atten= 89%, Lag= 0.0 min
 Primary = 0.13 cfs @ 11.64 hrs, Volume= 0.080 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 294.73' @ 12.71 hrs Surf.Area= 2,299 sf Storage= 1,169 cf

Plug-Flow detention time= 65.0 min calculated for 0.080 af (100% of inflow)
 Center-of-Mass det. time= 65.0 min (861.6 - 796.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	294.00'	1,268 cf	38.12'W x 60.30'L x 2.04'H Field A 4,683 cf Overall - 1,513 cf Embedded = 3,171 cf x 40.0% Voids
#2A	294.25'	1,437 cf	ACF R-Tank SD 1 x 624 Inside #1 Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf 624 Chambers in 26 Rows
		2,705 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	294.00'	2.410 in/hr Exfiltration over Surface area

Primary OutFlow Max=0.13 cfs @ 11.64 hrs HW=294.02' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.13 cfs)

Pond 6P: SSSF2 - Chamber Wizard Field A

Chamber Model = ACF R-Tank SD 1 (ACF Environmental R-Tank SD)

Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf

Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf

24 Chambers/Row x 2.35' Long = 56.30' Row Length +24.0" End Stone x 2 = 60.30' Base Length

26 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 38.12' Base Width

3.0" Stone Base + 9.4" Chamber Height + 12.0" Stone Cover = 2.04' Field Height

624 Chambers x 2.3 cf = 1,436.9 cf Chamber Storage

624 Chambers x 2.4 cf = 1,512.6 cf Displacement

4,683.3 cf Field - 1,512.6 cf Chambers = 3,170.7 cf Stone x 40.0% Voids = 1,268.3 cf Stone Storage

Chamber Storage + Stone Storage = 2,705.2 cf = 0.062 af

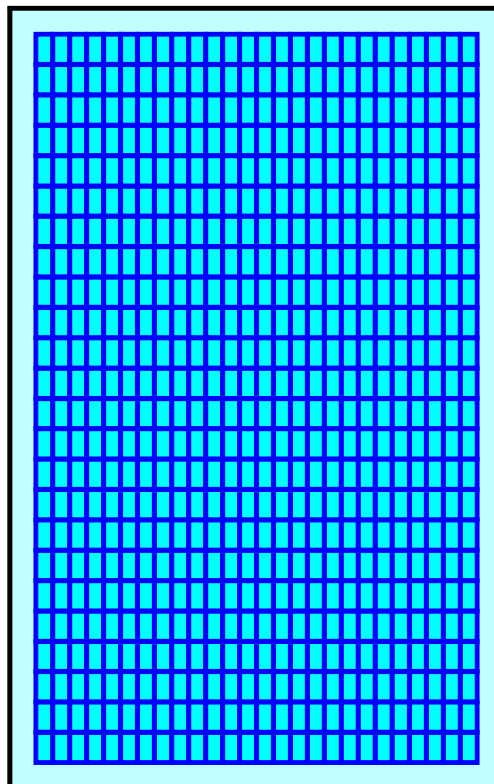
Overall Storage Efficiency = 57.8%

Overall System Size = 60.30' x 38.12' x 2.04'

624 Chambers

173.5 cy Field

117.4 cy Stone



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Summary for Pond 7P: CB

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.325 ac, 93.64% Impervious, Inflow Depth = 3.15" for 5-Year event
Inflow = 0.51 cfs @ 12.71 hrs, Volume= 0.348 af
Primary = 0.51 cfs @ 12.71 hrs, Volume= 0.348 af, Atten= 0%, Lag= 0.0 min
Routed to Reach POI1 : POI#1

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Type III 24-hr 10-Year Rainfall=4.60"

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: Store Roof	Runoff Area=13,303 sf 43.76% Impervious Runoff Depth=1.39" Tc=5.0 min CN=65 Runoff=0.48 cfs 0.035 af
Subcatchment 2: C-Store Parking	Runoff Area=42,253 sf 95.54% Impervious Runoff Depth=4.25" Tc=5.0 min CN=97 Runoff=4.41 cfs 0.343 af
Subcatchment 3:	Runoff Area=7,568 sf 8.39% Impervious Runoff Depth=0.29" Tc=0.0 min CN=44 Runoff=0.02 cfs 0.004 af
Subcatchment 4: (new Subcat)	Runoff Area=2,935 sf 100.00% Impervious Runoff Depth=4.36" Tc=5.0 min CN=98 Runoff=0.31 cfs 0.025 af
Subcatchment 5: Woods/Lawn	Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.00" Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment 6: Woods/Lawn	Runoff Area=14,372 sf 0.00% Impervious Runoff Depth=0.03" Flow Length=194' Tc=5.3 min CN=34 Runoff=0.00 cfs 0.001 af
Subcatchment 7: Woods/Lawn	Runoff Area=23,678 sf 0.00% Impervious Runoff Depth=0.03" Flow Length=100' Slope=0.0080 '/' Tc=1.8 min CN=34 Runoff=0.00 cfs 0.001 af
Subcatchment 8: Lawn	Runoff Area=6,349 sf 0.00% Impervious Runoff Depth=0.13" Flow Length=186' Tc=2.5 min CN=39 Runoff=0.00 cfs 0.002 af
Subcatchment 9:	Runoff Area=6,505 sf 28.90% Impervious Runoff Depth=0.84" Flow Length=100' Slope=0.0020 '/' Tc=3.1 min CN=56 Runoff=0.12 cfs 0.010 af
Subcatchment 10:	Runoff Area=6,660 sf 14.29% Impervious Runoff Depth=0.40" Tc=5.0 min CN=47 Runoff=0.03 cfs 0.005 af
Subcatchment 11: Drive Entrance	Runoff Area=6,048 sf 60.75% Impervious Runoff Depth=2.13" Tc=5.0 min CN=75 Runoff=0.35 cfs 0.025 af
Subcatchment 30: Bank Parking	Runoff Area=15,466 sf 88.46% Impervious Runoff Depth=3.59" Tc=5.0 min CN=91 Runoff=1.47 cfs 0.106 af
Reach POI1: POI#1	Inflow=0.60 cfs 0.460 af Outflow=0.60 cfs 0.460 af
Reach POI2: POI#2	Inflow=0.37 cfs 0.030 af Outflow=0.37 cfs 0.030 af
Pond 3P: SSSF1	Peak Elev=11.68' Storage=5,666 cf Inflow=4.41 cfs 0.343 af Outflow=0.43 cfs 0.343 af
Pond 5P: Roof Infiltration	Peak Elev=296.18' Storage=605 cf Inflow=0.48 cfs 0.035 af Outflow=0.04 cfs 0.035 af

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Pond 6P: SSSF2

Peak Elev=295.01' Storage=1,731 cf Inflow=1.47 cfs 0.106 af
Outflow=0.13 cfs 0.106 af

Pond 7P: CB

Inflow=0.56 cfs 0.450 af
Primary=0.56 cfs 0.450 af

Total Runoff Area = 3.419 ac Runoff Volume = 0.558 af Average Runoff Depth = 1.96"
53.03% Pervious = 1.813 ac 46.97% Impervious = 1.606 ac

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Summary for Subcatchment 1: Store Roof

Runoff = 0.48 cfs @ 12.09 hrs, Volume= 0.035 af, Depth= 1.39"
Routed to Pond 5P : Roof Infiltration

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
5,262	98	Roofs, HSG A
784	39	>75% Grass cover, Good, HSG A
6,698	39	>75% Grass cover, Good, HSG A
559	98	Paved parking, HSG A
13,303	65	Weighted Average
7,482		56.24% Pervious Area
5,821		43.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 2: C-Store Parking

Runoff = 4.41 cfs @ 12.07 hrs, Volume= 0.343 af, Depth= 4.25"
Routed to Pond 3P : SSSF1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
40,368	98	Paved parking, HSG A
136	74	>75% Grass cover, Good, HSG C
1,560	74	>75% Grass cover, Good, HSG C
189	74	>75% Grass cover, Good, HSG C
42,253	97	Weighted Average
1,885		4.46% Pervious Area
40,368		95.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Subcatchment 3:

[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 0.02 cfs @ 12.29 hrs, Volume= 0.004 af, Depth= 0.29"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
281	39	>75% Grass cover, Good, HSG A
635	98	Paved parking, HSG A
6,652	39	>75% Grass cover, Good, HSG A
7,568	44	Weighted Average
6,933		91.61% Pervious Area
635		8.39% Impervious Area

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 4: (new Subcat)

Runoff = 0.31 cfs @ 12.07 hrs, Volume= 0.025 af, Depth= 4.36"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
2,935	98	Roofs, HSG A
2,935		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 5: Woods/Lawn

[45] Hint: Runoff=Zero

Runoff = 0.00 cfs @ 0.00 hrs, Volume= 0.000 af, Depth= 0.00"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 6: Woods/Lawn

Runoff = 0.00 cfs @ 20.90 hrs, Volume= 0.001 af, Depth= 0.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
8,326	30	Woods, Good, HSG A
6,046	39	>75% Grass cover, Good, HSG A
14,372	34	Weighted Average
14,372		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 7: Woods/Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.00 cfs @ 20.87 hrs, Volume= 0.001 af, Depth= 0.03"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
12,831	30	Woods, Good, HSG A
10,847	39	>75% Grass cover, Good, HSG A
23,678	34	Weighted Average
23,678		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.00"

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 8: Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.00 cfs @ 14.53 hrs, Volume= 0.002 af, Depth= 0.13"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
6,349	39	>75% Grass cover, Good, HSG A
6,349		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces $n=0.011$ $P2=3.00"$
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved $K_v=16.1$ fps
2.5	186	Total			

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 9:[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.12 cfs @ 12.07 hrs, Volume= 0.010 af, Depth= 0.84"
 Routed to Reach POI1 : POI#1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
 Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
4,245	39	>75% Grass cover, Good, HSG A
1,652	98	Paved parking, HSG A
380	39	>75% Grass cover, Good, HSG A
228	98	Paved parking, HSG A
6,505	56	Weighted Average
4,625		71.10% Pervious Area
1,880		28.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B Smooth surfaces $n=0.011$ $P2=3.00"$

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 10:

Runoff = 0.03 cfs @ 12.29 hrs, Volume= 0.005 af, Depth= 0.40"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
3,751	39	>75% Grass cover, Good, HSG A
1,957	39	>75% Grass cover, Good, HSG A
444	98	Paved parking, HSG A
139	98	Paved parking, HSG A
369	98	Paved parking, HSG A
6,660	47	Weighted Average
5,708		85.71% Pervious Area
952		14.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 11: Drive Entrance

Runoff = 0.35 cfs @ 12.08 hrs, Volume= 0.025 af, Depth= 2.13"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
832	39	>75% Grass cover, Good, HSG A
1,321	39	>75% Grass cover, Good, HSG A
221	39	>75% Grass cover, Good, HSG A
3,674	98	Paved parking, HSG A
6,048	75	Weighted Average
2,374		39.25% Pervious Area
3,674		60.75% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Subcatchment 30: Bank Parking

Runoff = 1.47 cfs @ 12.07 hrs, Volume= 0.106 af, Depth= 3.59"
Routed to Pond 6P : SSSF2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Type III 24-hr 10-Year Rainfall=4.60"

Area (sf)	CN	Description
13,681	98	Paved parking, HSG A
969	39	>75% Grass cover, Good, HSG A
240	39	>75% Grass cover, Good, HSG A
380	39	>75% Grass cover, Good, HSG A
196	39	>75% Grass cover, Good, HSG A
15,466	91	Weighted Average
1,785		11.54% Pervious Area
13,681		88.46% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Reach POI1: POI#1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.474 ac, 87.08% Impervious, Inflow Depth = 3.75" for 10-Year event
Inflow = 0.60 cfs @ 12.09 hrs, Volume= 0.460 af
Outflow = 0.60 cfs @ 12.09 hrs, Volume= 0.460 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.292 ac, 36.40% Impervious, Inflow Depth = 1.22" for 10-Year event
Inflow = 0.37 cfs @ 12.08 hrs, Volume= 0.030 af
Outflow = 0.37 cfs @ 12.08 hrs, Volume= 0.030 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Type III 24-hr 10-Year Rainfall=4.60"

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Summary for Pond 3P: SSSF1

Inflow Area = 0.970 ac, 95.54% Impervious, Inflow Depth = 4.25" for 10-Year event
 Inflow = 4.41 cfs @ 12.07 hrs, Volume= 0.343 af
 Outflow = 0.43 cfs @ 12.83 hrs, Volume= 0.343 af, Atten= 90%, Lag= 45.5 min
 Primary = 0.43 cfs @ 12.83 hrs, Volume= 0.343 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 11.68' @ 12.83 hrs Surf.Area= 4,163 sf Storage= 5,666 cf

Plug-Flow detention time= 111.4 min calculated for 0.343 af (100% of inflow)
 Center-of-Mass det. time= 111.3 min (867.9 - 756.6)

Volume	Invert	Avail.Storage	Storage Description
#1A	10.00'	2,374 cf	74.87'W x 55.61'L x 2.69'H Field A 11,214 cf Overall - 5,279 cf Embedded = 5,934 cf x 40.0% Voids
#2A	10.25'	5,015 cf	ACF R-Tank HD 1 x 1188 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 1188 Chambers in 54 Rows
		7,389 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	10.00'	2.410 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 8.00'

Primary OutFlow Max=0.43 cfs @ 12.83 hrs HW=11.68' (Free Discharge)
 ↑ **1=Exfiltration** (Controls 0.43 cfs)

Pond 3P: SSSF1 - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

22 Chambers/Row x 2.35' Long = 51.61' Row Length +24.0" End Stone x 2 = 55.61' Base Length

54 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 74.87' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

1,188 Chambers x 4.2 cf = 5,015.5 cf Chamber Storage

1,188 Chambers x 4.4 cf = 5,279.5 cf Displacement

11,213.7 cf Field - 5,279.5 cf Chambers = 5,934.2 cf Stone x 40.0% Voids = 2,373.7 cf Stone Storage

Chamber Storage + Stone Storage = 7,389.2 cf = 0.170 af

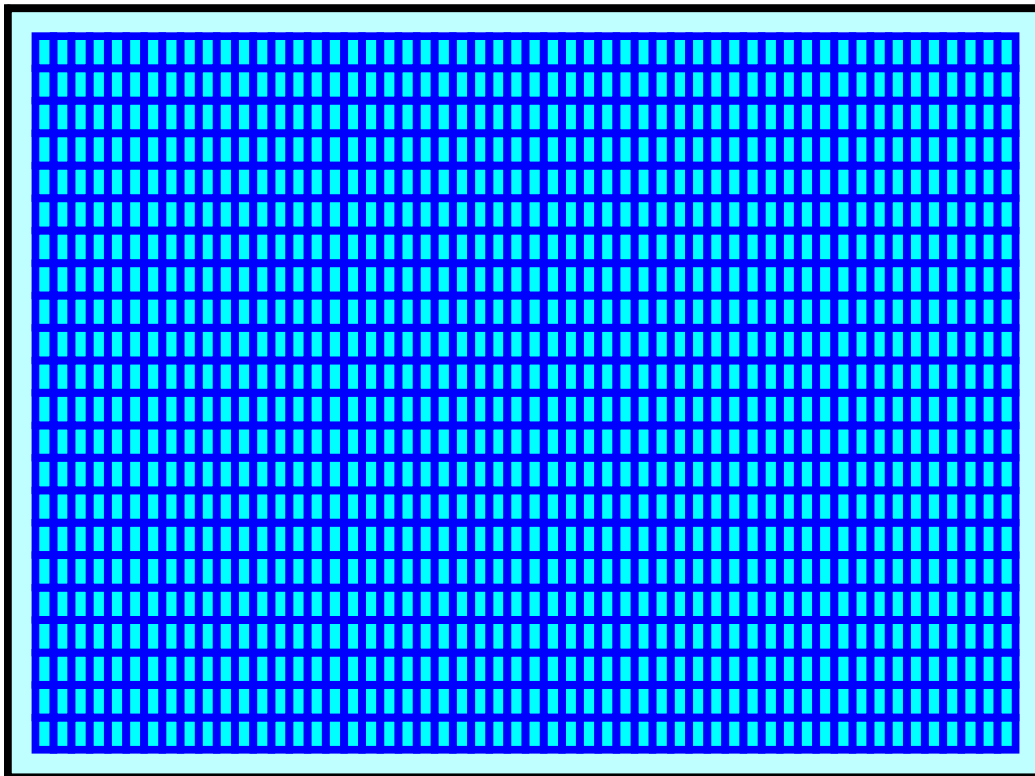
Overall Storage Efficiency = 65.9%

Overall System Size = 55.61' x 74.87' x 2.69'

1,188 Chambers

415.3 cy Field

219.8 cy Stone



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Summary for Pond 5P: Roof Infiltration

Inflow Area = 0.305 ac, 43.76% Impervious, Inflow Depth = 1.39" for 10-Year event
 Inflow = 0.48 cfs @ 12.09 hrs, Volume= 0.035 af
 Outflow = 0.04 cfs @ 11.76 hrs, Volume= 0.035 af, Atten= 92%, Lag= 0.0 min
 Discarded = 0.04 cfs @ 11.76 hrs, Volume= 0.035 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 296.18' @ 13.97 hrs Surf.Area= 719 sf Storage= 605 cf

Plug-Flow detention time= 150.4 min calculated for 0.035 af (100% of inflow)
 Center-of-Mass det. time= 150.4 min (1,015.7 - 865.3)

Volume	Invert	Avail.Storage	Storage Description
#1A	295.00'	476 cf	22.37'W x 32.15'L x 2.69'H Field A 1,937 cf Overall - 747 cf Embedded = 1,191 cf x 40.0% Voids
#2A	295.25'	709 cf	ACF R-Tank HD 1 x 168 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 168 Chambers in 14 Rows
		1,186 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	295.00'	2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.04 cfs @ 11.76 hrs HW=295.03' (Free Discharge)

↑**1=Exfiltration** (Exfiltration Controls 0.04 cfs)

Pond 5P: Roof Infiltration - Chamber Wizard Field A

Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

12 Chambers/Row x 2.35' Long = 28.15' Row Length +24.0" End Stone x 2 = 32.15' Base Length

14 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 22.37' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

168 Chambers x 4.2 cf = 709.3 cf Chamber Storage

168 Chambers x 4.4 cf = 746.6 cf Displacement

1,937.4 cf Field - 746.6 cf Chambers = 1,190.8 cf Stone x 40.0% Voids = 476.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,185.6 cf = 0.027 af

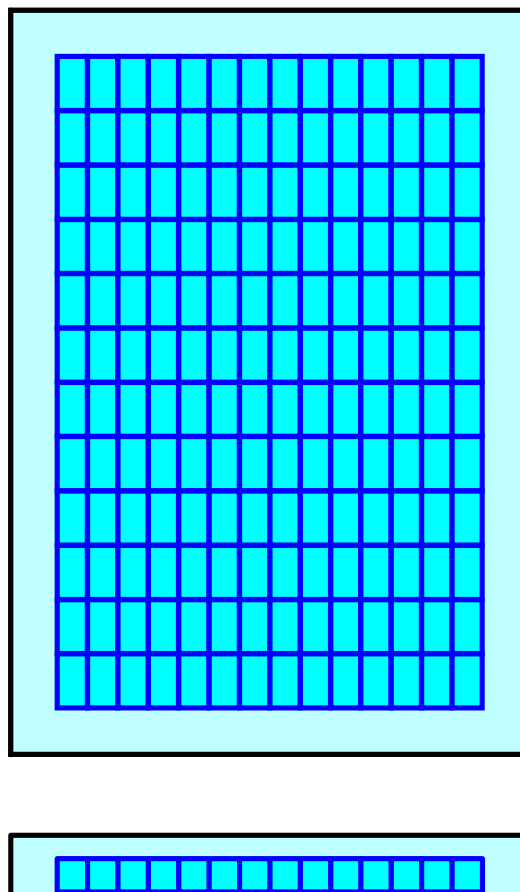
Overall Storage Efficiency = 61.2%

Overall System Size = 32.15' x 22.37' x 2.69'

168 Chambers

71.8 cy Field

44.1 cy Stone



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Summary for Pond 6P: SSSF2

Inflow Area = 0.355 ac, 88.46% Impervious, Inflow Depth = 3.59" for 10-Year event
 Inflow = 1.47 cfs @ 12.07 hrs, Volume= 0.106 af
 Outflow = 0.13 cfs @ 11.44 hrs, Volume= 0.106 af, Atten= 91%, Lag= 0.0 min
 Primary = 0.13 cfs @ 11.44 hrs, Volume= 0.106 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 295.01' @ 12.97 hrs Surf.Area= 2,299 sf Storage= 1,731 cf

Plug-Flow detention time= 103.5 min calculated for 0.106 af (100% of inflow)
 Center-of-Mass det. time= 103.5 min (892.2 - 788.7)

Volume	Invert	Avail.Storage	Storage Description
#1A	294.00'	1,268 cf	38.12'W x 60.30'L x 2.04'H Field A 4,683 cf Overall - 1,513 cf Embedded = 3,171 cf x 40.0% Voids
#2A	294.25'	1,437 cf	ACF R-Tank SD 1 x 624 Inside #1 Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf 624 Chambers in 26 Rows
		2,705 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	294.00'	2.410 in/hr Exfiltration over Surface area

Primary OutFlow Max=0.13 cfs @ 11.44 hrs HW=294.02' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.13 cfs)

Pond 6P: SSSF2 - Chamber Wizard Field A

Chamber Model = ACF R-Tank SD 1 (ACF Environmental R-Tank SD)

Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf

Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf

24 Chambers/Row x 2.35' Long = 56.30' Row Length +24.0" End Stone x 2 = 60.30' Base Length

26 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 38.12' Base Width

3.0" Stone Base + 9.4" Chamber Height + 12.0" Stone Cover = 2.04' Field Height

624 Chambers x 2.3 cf = 1,436.9 cf Chamber Storage

624 Chambers x 2.4 cf = 1,512.6 cf Displacement

4,683.3 cf Field - 1,512.6 cf Chambers = 3,170.7 cf Stone x 40.0% Voids = 1,268.3 cf Stone Storage

Chamber Storage + Stone Storage = 2,705.2 cf = 0.062 af

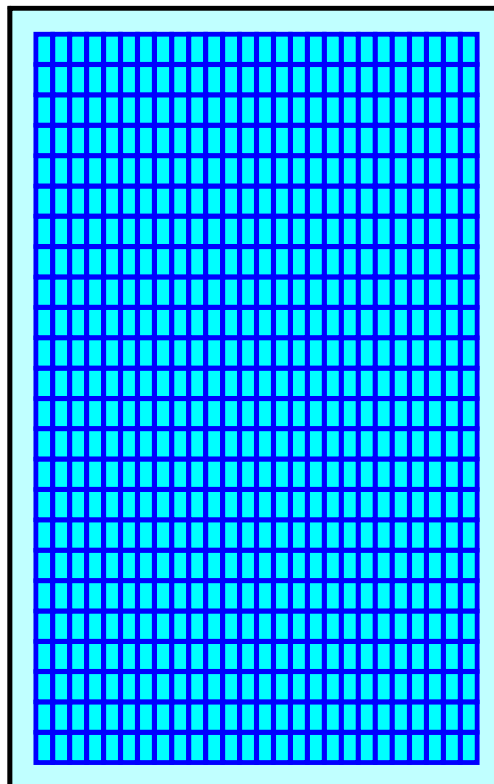
Overall Storage Efficiency = 57.8%

Overall System Size = 60.30' x 38.12' x 2.04'

624 Chambers

173.5 cy Field

117.4 cy Stone



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Summary for Pond 7P: CB

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.325 ac, 93.64% Impervious, Inflow Depth = 4.07" for 10-Year event

Inflow = 0.56 cfs @ 12.83 hrs, Volume= 0.450 af

Primary = 0.56 cfs @ 12.83 hrs, Volume= 0.450 af, Atten= 0%, Lag= 0.0 min

Routed to Reach POI1 : POI#1

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Time span=0.00-36.00 hrs, dt=0.04 hrs, 901 points
Runoff by SCS TR-20 method, UH=SCS, Weighted-CN
Reach routing by Stor-Ind+Trans method - Pond routing by Stor-Ind method

Subcatchment 1: Store Roof	Runoff Area=13,303 sf 43.76% Impervious Runoff Depth=2.21" Tc=5.0 min CN=65 Runoff=0.81 cfs 0.056 af
Subcatchment 2: C-Store Parking	Runoff Area=42,253 sf 95.54% Impervious Runoff Depth=5.44" Tc=5.0 min CN=97 Runoff=5.87 cfs 0.440 af
Subcatchment 3:	Runoff Area=7,568 sf 8.39% Impervious Runoff Depth=0.66" Tc=0.0 min CN=44 Runoff=0.07 cfs 0.010 af
Subcatchment 4: (new Subcat)	Runoff Area=2,935 sf 100.00% Impervious Runoff Depth=5.56" Tc=5.0 min CN=98 Runoff=0.41 cfs 0.031 af
Subcatchment 5: Woods/Lawn	Runoff Area=3,776 sf 0.00% Impervious Runoff Depth=0.05" Tc=5.0 min CN=30 Runoff=0.00 cfs 0.000 af
Subcatchment 6: Woods/Lawn	Runoff Area=14,372 sf 0.00% Impervious Runoff Depth=0.17" Flow Length=194' Tc=5.3 min CN=34 Runoff=0.01 cfs 0.005 af
Subcatchment 7: Woods/Lawn	Runoff Area=23,678 sf 0.00% Impervious Runoff Depth=0.17" Flow Length=100' Slope=0.0080 '/' Tc=1.8 min CN=34 Runoff=0.01 cfs 0.008 af
Subcatchment 8: Lawn	Runoff Area=6,349 sf 0.00% Impervious Runoff Depth=0.39" Flow Length=186' Tc=2.5 min CN=39 Runoff=0.01 cfs 0.005 af
Subcatchment 9:	Runoff Area=6,505 sf 28.90% Impervious Runoff Depth=1.48" Flow Length=100' Slope=0.0020 '/' Tc=3.1 min CN=56 Runoff=0.26 cfs 0.018 af
Subcatchment 10:	Runoff Area=6,660 sf 14.29% Impervious Runoff Depth=0.85" Tc=5.0 min CN=47 Runoff=0.10 cfs 0.011 af
Subcatchment 11: Drive Entrance	Runoff Area=6,048 sf 60.75% Impervious Runoff Depth=3.11" Tc=5.0 min CN=75 Runoff=0.54 cfs 0.036 af
Subcatchment 30: Bank Parking	Runoff Area=15,466 sf 88.46% Impervious Runoff Depth=4.76" Tc=5.0 min CN=91 Runoff=2.01 cfs 0.141 af
Reach POI1: POI#1	Inflow=0.73 cfs 0.599 af Outflow=0.73 cfs 0.599 af
Reach POI2: POI#2	Inflow=0.63 cfs 0.047 af Outflow=0.63 cfs 0.047 af
Pond 3P: SSSF1	Peak Elev=11.75' Storage=5,820 cf Inflow=5.87 cfs 0.440 af Outflow=0.44 cfs 0.440 af
Pond 5P: Roof Infiltration	Peak Elev=296.77' Storage=920 cf Inflow=0.81 cfs 0.056 af Outflow=0.04 cfs 0.056 af

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Cumberland 24-hr S1 25-yr Rainfall=5.80"

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Pond 6P: SSSF2

Peak Elev=295.08' Storage=1,829 cf Inflow=2.01 cfs 0.141 af

Outflow=0.13 cfs 0.141 af

Pond 7P: CB

Inflow=0.56 cfs 0.581 af

Primary=0.56 cfs 0.581 af

Total Runoff Area = 3.419 ac Runoff Volume = 0.761 af Average Runoff Depth = 2.67"
53.03% Pervious = 1.813 ac 46.97% Impervious = 1.606 ac

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Summary for Subcatchment 1: Store Roof

Runoff = 0.81 cfs @ 12.03 hrs, Volume= 0.056 af, Depth= 2.21"
Routed to Pond 5P : Roof Infiltration

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
5,262	98	Roofs, HSG A
784	39	>75% Grass cover, Good, HSG A
6,698	39	>75% Grass cover, Good, HSG A
559	98	Paved parking, HSG A
13,303	65	Weighted Average
7,482		56.24% Pervious Area
5,821		43.76% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 2: C-Store Parking

Runoff = 5.87 cfs @ 12.02 hrs, Volume= 0.440 af, Depth= 5.44"
Routed to Pond 3P : SSSF1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
40,368	98	Paved parking, HSG A
136	74	>75% Grass cover, Good, HSG C
1,560	74	>75% Grass cover, Good, HSG C
189	74	>75% Grass cover, Good, HSG C
42,253	97	Weighted Average
1,885		4.46% Pervious Area
40,368		95.54% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Cumberland Post*Cumberland 24-hr S1 25-yr Rainfall=5.80"*

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Summary for Subcatchment 3:[46] Hint: $T_c=0$ (Instant runoff peak depends on dt)

Runoff = 0.07 cfs @ 11.99 hrs, Volume= 0.010 af, Depth= 0.66"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
281	39	>75% Grass cover, Good, HSG A
635	98	Paved parking, HSG A
6,652	39	>75% Grass cover, Good, HSG A
7,568	44	Weighted Average
6,933		91.61% Pervious Area
635		8.39% Impervious Area

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Summary for Subcatchment 4: (new Subcat)

Runoff = 0.41 cfs @ 12.02 hrs, Volume= 0.031 af, Depth= 5.56"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
2,935	98	Roofs, HSG A
2,935		100.00% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 5: Woods/Lawn

Runoff = 0.00 cfs @ 23.96 hrs, Volume= 0.000 af, Depth= 0.05"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
3,776	30	Woods, Good, HSG A
3,776		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 6: Woods/Lawn

Runoff = 0.01 cfs @ 17.44 hrs, Volume= 0.005 af, Depth= 0.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
8,326	30	Woods, Good, HSG A
6,046	39	>75% Grass cover, Good, HSG A
14,372	34	Weighted Average
14,372		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
2.9	91	0.0020	0.52		Sheet Flow, A-B
					Smooth surfaces n= 0.011 P2= 3.00"
2.4	103	0.0200	0.71		Shallow Concentrated Flow, B-C
					Woodland Kv= 5.0 fps
5.3	194	Total			

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Summary for Subcatchment 7: Woods/Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.01 cfs @ 17.40 hrs, Volume= 0.008 af, Depth= 0.17"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
12,831	30	Woods, Good, HSG A
10,847	39	>75% Grass cover, Good, HSG A
23,678	34	Weighted Average
23,678		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.8	100	0.0080	0.92		Sheet Flow, A-B Smooth surfaces n= 0.011 P2= 3.00"

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Summary for Subcatchment 8: Lawn[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.01 cfs @ 12.32 hrs, Volume= 0.005 af, Depth= 0.39"

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs

Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
6,349	39	>75% Grass cover, Good, HSG A
6,349		100.00% Pervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
1.9	100	0.0070	0.88		Sheet Flow, A-B
					Smooth surfaces $n=0.011$ $P2=3.00"$
0.6	86	0.0190	2.22		Shallow Concentrated Flow, B-C
					Unpaved $K_v=16.1$ fps
2.5	186	Total			

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Summary for Subcatchment 9:[49] Hint: $T_c < 2dt$ may require smaller dt

Runoff = 0.26 cfs @ 12.01 hrs, Volume= 0.018 af, Depth= 1.48"
 Routed to Reach POI1 : POI#1

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, $dt=0.04$ hrs
 Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
4,245	39	>75% Grass cover, Good, HSG A
1,652	98	Paved parking, HSG A
380	39	>75% Grass cover, Good, HSG A
228	98	Paved parking, HSG A
6,505	56	Weighted Average
4,625		71.10% Pervious Area
1,880		28.90% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
3.1	100	0.0020	0.53		Sheet Flow, A-B Smooth surfaces $n=0.011$ $P2=3.00"$

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Summary for Subcatchment 10:

Runoff = 0.10 cfs @ 12.04 hrs, Volume= 0.011 af, Depth= 0.85"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
3,751	39	>75% Grass cover, Good, HSG A
1,957	39	>75% Grass cover, Good, HSG A
444	98	Paved parking, HSG A
139	98	Paved parking, HSG A
369	98	Paved parking, HSG A
6,660	47	Weighted Average
5,708		85.71% Pervious Area
952		14.29% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 11: Drive Entrance

Runoff = 0.54 cfs @ 12.03 hrs, Volume= 0.036 af, Depth= 3.11"
Routed to Reach POI2 : POI#2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
832	39	>75% Grass cover, Good, HSG A
1,321	39	>75% Grass cover, Good, HSG A
221	39	>75% Grass cover, Good, HSG A
3,674	98	Paved parking, HSG A
6,048	75	Weighted Average
2,374		39.25% Pervious Area
3,674		60.75% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

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Summary for Subcatchment 30: Bank Parking

Runoff = 2.01 cfs @ 12.02 hrs, Volume= 0.141 af, Depth= 4.76"
 Routed to Pond 6P : SSSF2

Runoff by SCS TR-20 method, UH=SCS, Weighted-CN, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Cumberland 24-hr S1 25-yr Rainfall=5.80"

Area (sf)	CN	Description
13,681	98	Paved parking, HSG A
969	39	>75% Grass cover, Good, HSG A
240	39	>75% Grass cover, Good, HSG A
380	39	>75% Grass cover, Good, HSG A
196	39	>75% Grass cover, Good, HSG A
15,466	91	Weighted Average
1,785		11.54% Pervious Area
13,681		88.46% Impervious Area

Tc (min)	Length (feet)	Slope (ft/ft)	Velocity (ft/sec)	Capacity (cfs)	Description
5.0					Direct Entry,

Summary for Reach POI1: POI#1

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.474 ac, 87.08% Impervious, Inflow Depth = 4.88" for 25-yr event
Inflow = 0.73 cfs @ 12.01 hrs, Volume= 0.599 af
Outflow = 0.73 cfs @ 12.01 hrs, Volume= 0.599 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Summary for Reach POI2: POI#2

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 0.292 ac, 36.40% Impervious, Inflow Depth = 1.93" for 25-yr event
Inflow = 0.63 cfs @ 12.03 hrs, Volume= 0.047 af
Outflow = 0.63 cfs @ 12.03 hrs, Volume= 0.047 af, Atten= 0%, Lag= 0.0 min

Routing by Stor-Ind+Trans method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

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Cumberland 24-hr S1 25-yr Rainfall=5.80"

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Summary for Pond 3P: SSSF1

Inflow Area = 0.970 ac, 95.54% Impervious, Inflow Depth = 5.44" for 25-yr event
 Inflow = 5.87 cfs @ 12.02 hrs, Volume= 0.440 af
 Outflow = 0.44 cfs @ 12.98 hrs, Volume= 0.440 af, Atten= 93%, Lag= 57.7 min
 Primary = 0.44 cfs @ 12.98 hrs, Volume= 0.440 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 11.75' @ 12.98 hrs Surf.Area= 4,163 sf Storage= 5,820 cf

Plug-Flow detention time= 107.6 min calculated for 0.440 af (100% of inflow)
 Center-of-Mass det. time= 107.5 min (862.2 - 754.8)

Volume	Invert	Avail.Storage	Storage Description
#1A	10.00'	2,374 cf	74.87'W x 55.61'L x 2.69'H Field A 11,214 cf Overall - 5,279 cf Embedded = 5,934 cf x 40.0% Voids
#2A	10.25'	5,015 cf	ACF R-Tank HD 1 x 1188 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 1188 Chambers in 54 Rows
7,389 cf			Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	10.00'	2.410 in/hr Exfiltration over Surface area Conductivity to Groundwater Elevation = 8.00'

Primary OutFlow Max=0.44 cfs @ 12.98 hrs HW=11.75' (Free Discharge)
 ↑ **1=Exfiltration** (Controls 0.44 cfs)

Pond 3P: SSSF1 - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

22 Chambers/Row x 2.35' Long = 51.61' Row Length +24.0" End Stone x 2 = 55.61' Base Length

54 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 74.87' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

1,188 Chambers x 4.2 cf = 5,015.5 cf Chamber Storage

1,188 Chambers x 4.4 cf = 5,279.5 cf Displacement

11,213.7 cf Field - 5,279.5 cf Chambers = 5,934.2 cf Stone x 40.0% Voids = 2,373.7 cf Stone Storage

Chamber Storage + Stone Storage = 7,389.2 cf = 0.170 af

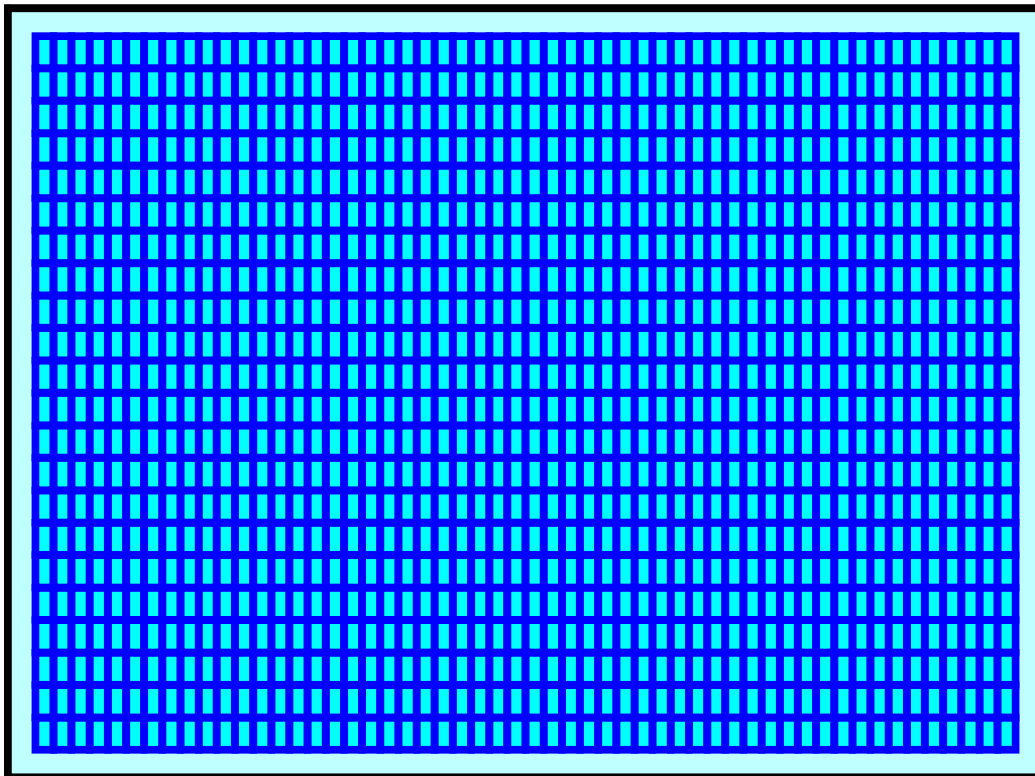
Overall Storage Efficiency = 65.9%

Overall System Size = 55.61' x 74.87' x 2.69'

1,188 Chambers

415.3 cy Field

219.8 cy Stone



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Summary for Pond 5P: Roof Infiltration

Inflow Area = 0.305 ac, 43.76% Impervious, Inflow Depth = 2.21" for 25-yr event
 Inflow = 0.81 cfs @ 12.03 hrs, Volume= 0.056 af
 Outflow = 0.04 cfs @ 11.40 hrs, Volume= 0.056 af, Atten= 95%, Lag= 0.0 min
 Discarded = 0.04 cfs @ 11.40 hrs, Volume= 0.056 af

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 296.77' @ 15.34 hrs Surf.Area= 719 sf Storage= 920 cf

Plug-Flow detention time= 250.9 min calculated for 0.056 af (100% of inflow)
 Center-of-Mass det. time= 250.9 min (1,142.1 - 891.2)

Volume	Invert	Avail.Storage	Storage Description
#1A	295.00'	476 cf	22.37'W x 32.15'L x 2.69'H Field A 1,937 cf Overall - 747 cf Embedded = 1,191 cf x 40.0% Voids
#2A	295.25'	709 cf	ACF R-Tank HD 1 x 168 Inside #1 Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf 168 Chambers in 14 Rows
		1,186 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Discarded	295.00'	2.410 in/hr Exfiltration over Surface area

Discarded OutFlow Max=0.04 cfs @ 11.40 hrs HW=295.03' (Free Discharge)

↑ **1=Exfiltration** (Exfiltration Controls 0.04 cfs)

Pond 5P: Roof Infiltration - Chamber Wizard Field A**Chamber Model = ACF R-Tank HD 1 (ACF Environmental R-Tank HD)**

Inside= 15.7"W x 17.3"H => 1.80 sf x 2.35'L = 4.2 cf

Outside= 15.7"W x 17.3"H => 1.89 sf x 2.35'L = 4.4 cf

12 Chambers/Row x 2.35' Long = 28.15' Row Length +24.0" End Stone x 2 = 32.15' Base Length

14 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 22.37' Base Width

3.0" Stone Base + 17.3" Chamber Height + 12.0" Stone Cover = 2.69' Field Height

168 Chambers x 4.2 cf = 709.3 cf Chamber Storage

168 Chambers x 4.4 cf = 746.6 cf Displacement

1,937.4 cf Field - 746.6 cf Chambers = 1,190.8 cf Stone x 40.0% Voids = 476.3 cf Stone Storage

Chamber Storage + Stone Storage = 1,185.6 cf = 0.027 af

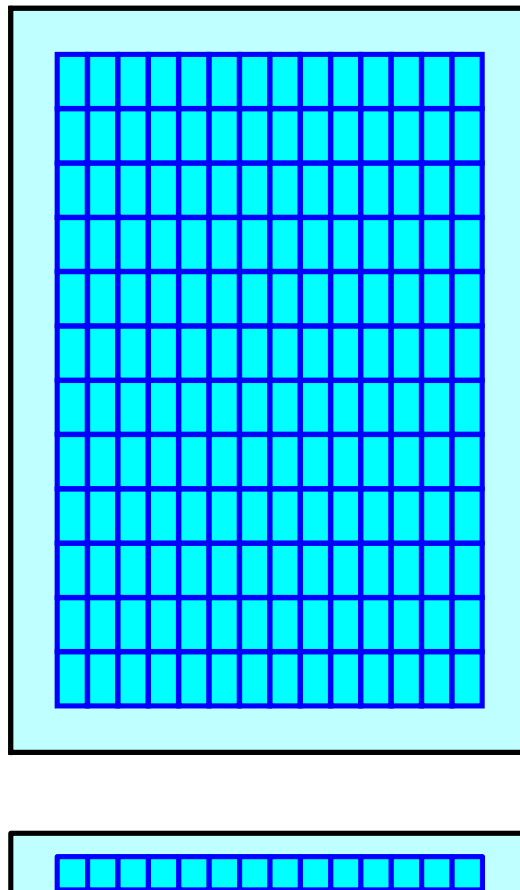
Overall Storage Efficiency = 61.2%

Overall System Size = 32.15' x 22.37' x 2.69'

168 Chambers

71.8 cy Field

44.1 cy Stone



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Cumberland 24-hr S1 25-yr Rainfall=5.80"

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Summary for Pond 6P: SSSF2

Inflow Area = 0.355 ac, 88.46% Impervious, Inflow Depth = 4.76" for 25-yr event
 Inflow = 2.01 cfs @ 12.02 hrs, Volume= 0.141 af
 Outflow = 0.13 cfs @ 11.08 hrs, Volume= 0.141 af, Atten= 94%, Lag= 0.0 min
 Primary = 0.13 cfs @ 11.08 hrs, Volume= 0.141 af
 Routed to Pond 7P : CB

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs
 Peak Elev= 295.08' @ 13.30 hrs Surf.Area= 2,299 sf Storage= 1,829 cf

Plug-Flow detention time= 102.4 min calculated for 0.141 af (100% of inflow)
 Center-of-Mass det. time= 102.3 min (895.3 - 793.0)

Volume	Invert	Avail.Storage	Storage Description
#1A	294.00'	1,268 cf	38.12'W x 60.30'L x 2.04'H Field A 4,683 cf Overall - 1,513 cf Embedded = 3,171 cf x 40.0% Voids
#2A	294.25'	1,437 cf	ACF R-Tank SD 1 x 624 Inside #1 Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf 624 Chambers in 26 Rows
		2,705 cf	Total Available Storage

Storage Group A created with Chamber Wizard

Device	Routing	Invert	Outlet Devices
#1	Primary	294.00'	2.410 in/hr Exfiltration over Surface area

Primary OutFlow Max=0.13 cfs @ 11.08 hrs HW=294.02' (Free Discharge)
 ↑ **1=Exfiltration** (Exfiltration Controls 0.13 cfs)

Pond 6P: SSSF2 - Chamber Wizard Field A**Chamber Model = ACF R-Tank SD 1 (ACF Environmental R-Tank SD)**

Inside= 15.7"W x 9.4"H => 0.98 sf x 2.35'L = 2.3 cf

Outside= 15.7"W x 9.4"H => 1.03 sf x 2.35'L = 2.4 cf

24 Chambers/Row x 2.35' Long = 56.30' Row Length +24.0" End Stone x 2 = 60.30' Base Length

26 Rows x 15.7" Wide + 24.0" Side Stone x 2 = 38.12' Base Width

3.0" Stone Base + 9.4" Chamber Height + 12.0" Stone Cover = 2.04' Field Height

624 Chambers x 2.3 cf = 1,436.9 cf Chamber Storage

624 Chambers x 2.4 cf = 1,512.6 cf Displacement

4,683.3 cf Field - 1,512.6 cf Chambers = 3,170.7 cf Stone x 40.0% Voids = 1,268.3 cf Stone Storage

Chamber Storage + Stone Storage = 2,705.2 cf = 0.062 af

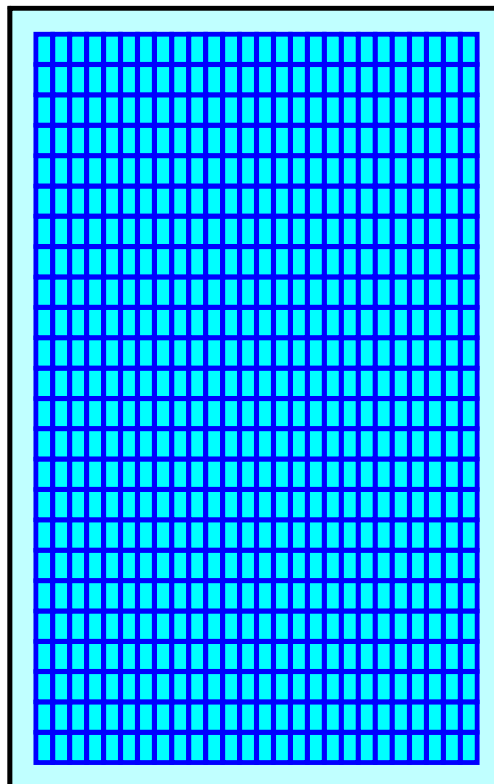
Overall Storage Efficiency = 57.8%

Overall System Size = 60.30' x 38.12' x 2.04'

624 Chambers

173.5 cy Field

117.4 cy Stone



Cumberland Post*Cumberland 24-hr S1 25-yr Rainfall=5.80"*

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Summary for Pond 7P: CB

[40] Hint: Not Described (Outflow=Inflow)

Inflow Area = 1.325 ac, 93.64% Impervious, Inflow Depth = 5.26" for 25-yr event
Inflow = 0.56 cfs @ 12.98 hrs, Volume= 0.581 af
Primary = 0.56 cfs @ 12.98 hrs, Volume= 0.581 af, Atten= 0%, Lag= 0.0 min
Routed to Reach POI1 : POI#1

Routing by Stor-Ind method, Time Span= 0.00-36.00 hrs, dt= 0.04 hrs

Attachment J
Geotechnical Report

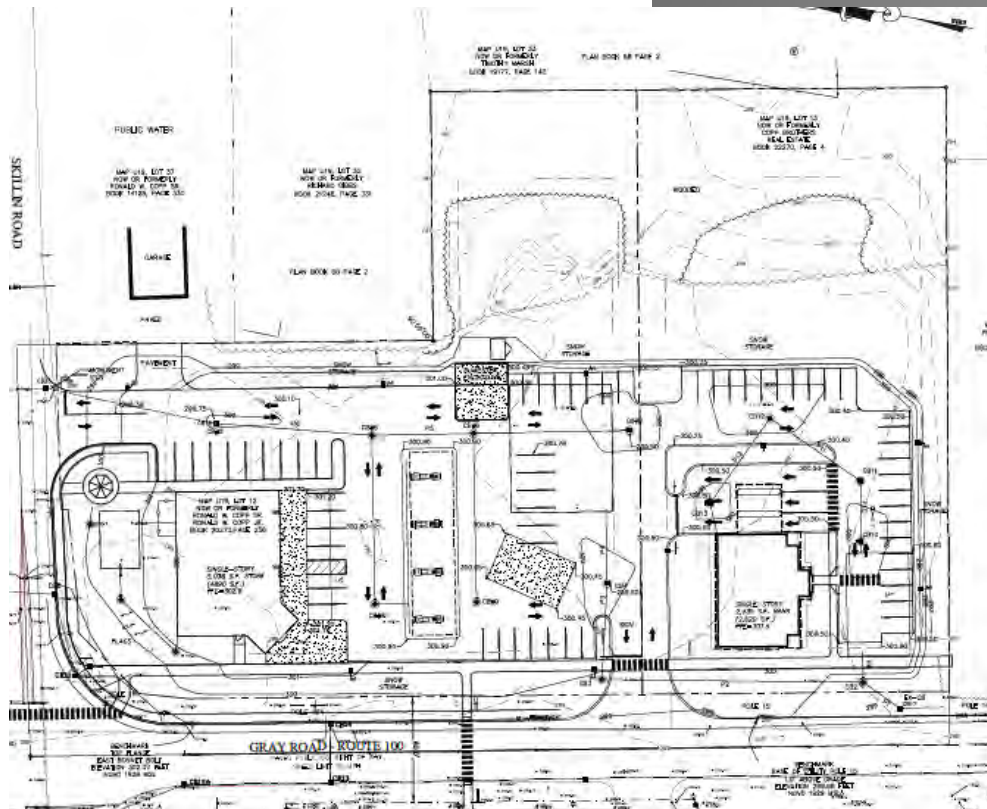
A copy of the Geotechnical Report is included for reference.

The key to success starts with a solid foundation.
ENGINEERING / EXPLORATION / EXPERIENCE

Geotechnical Report

Proposed Buildings

186 Gray Road, Cumberland, ME



Client

Priority Real Estate Group
2 Main Street
Topsham, ME 04086

Project #: 23241
Date: 12/14/2023



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December 14, 2023
SGS Project #: 23241

Priority Real Estate Group
2 Main Street
Topsham, ME 04086
Attn: Curtis Y. Neufeld

Reference: Geotechnical Report – Proposed Buildings
186 Gray Road, Cumberland, ME

Dear Curt,

Summit Geoengineering Services, Inc. (SGS) has completed a geotechnical investigation for the construction of the proposed buildings at the site referenced above. Our scope of services included the completion of borings, the installation of one observation well, laboratory testing, and the preparation of this geotechnical report summarizing our findings and providing geotechnical recommendations.

Our scope of services for this project did not include an environmental site assessment or further investigation for the presence or absence of hazardous or toxic material on, below, or around the site. Any statements in this report, or on the exploration logs, regarding odors or unusual and suspicious conditions observed are for informational purposes and are not intended to constitute an environmental assessment.

1.0 Project Description

The project consists of the construction of a new store and a new bank. The store will be single-story structure with an approximate footprint area of 5,038 square feet. The store will have a finished floor elevation of 302.0 feet. Parking lots will append the store to the east and south. A gas pump canopy will be constructed to the south of the store. The bank will be a single-story structure with an approximate footprint area of 2,935 square feet. The bank will have a finished floor elevation of 301.5 feet. Parking lots will append the bank to the east and south. An access road with a drive thru will append the building directly to the east. A shared parking lot will be present to the south of the store and to the north of the bank. Underground storage tanks will be constructed about 16 feet below the ground surface in the shared parking lot area.

The existing site is an open parking lot with an existing building to the north side of the site. Existing grades within the store range from elevation 298 to 299 feet. Based on this, up to 4 feet of fill will be required in the store footprint. Existing grades within the bank range from elevation 298.5 to 299 feet. Based on this, up to 3 feet of fill will be required in the bank footprint.

This information was referenced from a plan entitled *Grading Plan – C5* by Priority Real Estate Group, LLC dated November 22, 2023.

No structural loading was available as of the writing of this report. For our analysis, we assumed a maximum column load of 100 kips.

2.0 Explorations

Summit Geoengineering Services (SGS) observed the subsurface conditions on September 20, 2023 with the drilling of 5 borings and the installation of 1 observation well. The exploration locations were determined by SGS and marked out by others prior to drilling.

The borings were completed by SGS using a rubber tracked AMS PowerProbe 9580 VTR drill rig. The borings were drilled to depths ranging from 17.0 feet (no refusal) to 26.6 feet (refusal on dense stratum). Bottom of boring elevations ranged from approximately 271.4 to 282 feet. The borings were completed using 2 ¼-inch hollow stem augers. Standard Penetration Tests (SPT) were performed at the ground surface and in increments of 5 feet. Soils were visually classified (ASTM D2488) using SPT split spoon sampling (ASTM D1586).

One observation well was installed in B-3 (O.W.) after completion. The well was installed to 17 feet and contained 12 feet of 1-inch PVC riser overlying 5 feet of 1-inch screened PVC. Bentonite was placed near the ground surface and a road box was placed at the ground surface after the well was installed.

An exploration location plan and the exploration logs are included in *Appendix A* and *Appendix B*, respectively.

3.0 Laboratory Testing

Two grain size analyses were performed in B-3 (O.W.) from 5 to 7 feet and from 10 to 12 feet to estimate the infiltration rate of the granular material underneath the pump stations. The following table summarizes the constituents of the granular material:

GRAIN SIZE ANALYSES RESULTS					
Location	Depth (ft)	Gravel (%)	Sand (%)	Fines (%)	Moisture Content (%)
B-3 (O.W.)	5 to 7	7	90	3	6.2
B-3 (O.W.)	10 to 12	0	83.7	16.3	12.3

Detailed results of the laboratory testing can be found in *Appendix C*.

4.0 Subsurface Conditions

4.1 Soil

From the explorations, the soil at this site generally consists of the following:

- **Pavement** (encountered in B-2; 6 inches thick)
- **Fill** (1 to 5 feet thick)
- **Marine Ice Delta** (14.5 to 19.5 feet thick)

- **Glacial Marine** (1.5 to 6 feet thick)
- **Glacial Till** (very dense in every exploration; less than 1 foot of thickness explored)

The pavement is bituminous and generally less than 6 inches thick overlying a base course of sand and gravel.

The **fill** generally consists of sand with varying amounts of gravel and silt. It is generally loose to compact and humid to damp. It is 1 to 5 feet thick and is visually classified as either SP or SP-SM in accordance with the Unified Soil Classification System (USCS). SPT N-values range from 6 blows per foot (bpf) to 27 bpf and average 18 bpf.

The **marine ice delta** generally consists of various colored sands with little to trace gravel and varying amounts of silt. It is generally very loose to compact and damp to saturated. It is 14.5 to 19.5 feet thick and is visually classified as either SP, SP-SM, or SM in accordance with the USCS. SPT N-values range from 2 bpf to 16 bpf and average 10 bpf.

The **glacial marine** generally consists of silt or clay with varying amounts of sand. It is generally very soft to very firm and wet to saturated. It is 1.5 to 6 feet thick and is visually classified as either ML or CL in accordance with the USCS. SPT N-values range from 1 bpf to 22 bpf and average 8 bpf.

The **glacial till**, sampled in B-2 and B-4, generally consists of gray or tan sand with some to little silt, little gravel, and trace clay. It is generally compact to very dense and wet. The glacial till, where explored, was less than 1 foot thick before it became very dense after penetration into the layer.

Detailed descriptions of the soil can be found in the exploration logs in *Appendix B*.

4.2 Groundwater

Groundwater was measured or estimated at the following depths and approximate elevations:

GROUNDWATER DEPTHS AND ELEVATIONS				
Location	Date	Depth (ft)	Elevation (ft +/-)	Reference
B-1	9/20/2023	15.0	283.0	Estimated in spoon samples
B-2	9/20/2023	15.0	284.0	Estimated in spoon samples
B-3 (O.W.)	9/20/2023	14.9	284.1	Measured in observation well
	9/28/2023	15.0	284.0	
	12/6/2023	15.0	284.0	
B-4	9/20/2023	15.0	284.0	Estimated in spoon samples
B-5	9/20/2023	15.0	283.5	Estimated in spoon samples

Note: O.W. = Observation Well

Groundwater was generally encountered within the marine ice delta formation at or near 15 feet with elevations ranging from 283 to 284 feet. Based on readings from the observation well in the

middle of the site, the permanent groundwater should remain consistent near this elevation, however, slight fluctuation is anticipated seasonally and with precipitation levels.

4.3 Bedrock

Refusal on dense strata were encountered in B-1 at 26.6 feet (elevation 271.4 feet), B-4 at 25.8 feet (elevation 273.2 feet), and B-5 at 22.9 feet (elevation 275.6 feet). B-4 contained weathered rock in the spoon tip after the glacial till was sampled. It cannot be determined based on the collected data if the refusal for these borings was on a dense portion of glacial till, a cobble/boulder, or on hard bedrock. Bedrock will not be encountered during construction.

5.0 Geotechnical Recommendations

5.1 Bearing Capacity and Subgrade Preparation

Based on the results of our subsurface explorations, foundations can be supported on conventional continuous or spread footing foundations. We recommend that the bottom of the footings for the proposed buildings be constructed on a minimum of 6 inches of $\frac{3}{4}$ -inch crushed stone (CS) placed over proofrolled native soil. Assuming that the recommendations below are followed, footings on soil can be proportioned using a maximum allowable bearing pressure of **3,000 pounds per square foot (psf)**. The allowable bearing pressure for both buildings is based on the following construction sequences:

- After grubbing the building footprint, proofroll the exposed soil by making a minimum of 4 passes in each of two perpendicular directions using a vibratory compactor with a minimum operating weight of 8 tons.
- Excavate to 6 inches below the proposed bottom of footing elevation. Proofroll the exposed soil by making a minimum of 4 passes using a plate compactor. Soft, wet, or unstable areas should be removed and replaced with CS.
- Place a minimum of 6 inches of CS directly on the proofrolled soil. CS should be compacted to lock the particles together. The footings can be constructed directly on the compacted CS. In no case shall footings be constructed in standing water or frozen soil.
- SGS should observe the footing subgrade conditions after proofrolling and prior to the placement of the CS.

5.2 Frost Protection

The design air freezing index for the Cumberland, Maine area is approximately 1,190-degree F days (10-year, 90% probability). Based on this, exterior footings and other footings exposed to freezing temperatures should be placed at a minimum depth of **4 feet** in order to provide adequate frost protection. We recommend that all foundations exposed to freezing temperatures be backfilled with Granular Borrow (GB).

5.3 Seismic Design

Based on the discovered soils, this site can be classified as **Seismic Site Class D** in accordance with ASCE 7-10 and 7-16. The following seismic design coefficients should be used:

SUBGRADE SITE SEISMIC DESIGN COEFFICIENTS – ASCE 7		
Seismic Coefficient	ASCE 7-10 (Class D)	ASCE 7-16 (Class D)
S_s	0.248	0.290
S_1	0.080	0.073
S_{MS}	0.396	0.454
S_{M1}	0.192	0.176
S_{DS}	0.264	0.303
S_{D1}	0.128	0.118
PGA_m	0.206 g	0.251 g

No liquefiable soils were encountered in our explorations.

5.4 Underdrains and Exterior Grading

Groundwater was encountered within the middle portions of the marine ice delta formation. Groundwater is anticipated to be below the proposed bottom of footing elevations. Based on these conditions, underdrains are not strictly necessary, however, it is generally good practice to install underdrains along the exterior and interior foundations of the building to account for any local or regional changes in the hydrogeology and to control infiltration of rainfall adjacent to the foundation walls.

Underdrains, if used, should consist of 4-inch rigid PVC or flexible ADS pipe surrounded by 6 inches of $\frac{3}{4}$ -inch crushed stone (CS) which is then surrounded by Mirafi 140N or equivalent. Underdrains should be outlet to a free draining location. Where exposed at the ground surface, a screen or other device should be placed over the outlet to prevent the migration of animals into the underdrain system.

In addition, we recommend all exterior grades slope away from the building footprint to reduce runoff water from infiltrating the foundation backfill soils.

5.5 Slabs-on-Grade

All fill should be compacted to a minimum of 95% of ASTM D1557. The gradation requirements for Granular Borrow (GB), $\frac{3}{4}$ -inch crushed stone (CS), and Structural Fill (SF) can be found in *Section 6.2*.

5.5.1 Interior Slabs

All interior slabs should be constructed on either a minimum of 12 inches of SF compacted to a minimum of 95% of ASTM D1557 or 8 inches of CS compacted to lock the particles together.

Fill required to raise the grade to the bottom of the slab elevation should consist of GB or SF, placed and compacted to a minimum of 95% of ASTM D1557.

5.5.2 Exterior Slabs

For slabs in unheated entry areas, the following options should be considered for frost protection:

- Construct slab on frost wall foundation, in accordance with *Section 5.1 and 5.2*
- 6-inch slab (minimum thickness) over 2 inches of rigid insulation over 12 inches CS or SF (compacted)
- 6-inch slab (minimum thickness) over 36 inches CS or SF (compacted)

We recommend that insulation, if used, be extended 2 feet beyond the edge of the slabs and that it consist of a rigid polystyrene product.

5.6 Pavement Section Recommendations

The mean annual freezing index for the Cumberland, Maine area is estimated at 890-degree F days (2-year, 50% probability). Based on the explorations, the subgrade for the pavement sections will consist of either imported fill or existing fill soils. Based on the mean annual freezing index, the anticipated mean annual frost penetration depth is 36 inches.

For the parking lots and access road, we recommend a minimum total section thickness of **18 inches**. We further recommend that the pavement section consist of the following materials:

PAVEMENT SECTION MATERIALS AND THICKNESSES		
Material	Thickness (in)	Specifications
Asphalt Surface Course	1 1/4	MDOT 703.09 Type 9.5 mm (Light Duty) or 12.5 mm (Heavy Duty)
Asphalt Binder Course	1 3/4	MDOT 703.09 Type 19 mm
Base Soil	3	MDOT 703.06 Type A
Subbase Soil	12	MDOT 703.06 Type D

Reference: MDOT Standard Specifications, 2014

Fill beneath the subbase soil should consist of Common Borrow (CB), see *Section 6.2*, compacted to a minimum of 95% of ASTM D1557. Underdrains are not necessary beneath paved areas.

5.7 Underground Storage Tanks

Underground storage tanks are proposed to be constructed about 16 feet below the ground surface within the proposed shared parking lot. We anticipate that the underground storage tanks will bear on a concrete anchor slab. We recommend the anchor slab be constructed on a minimum of 12 inches of CS placed above the proofrolled native soil. The CS should extend a minimum of 2 feet outside the edge of the tank and should be compacted to lock the particles together.

Excavations this deep likely create unstable sidewalls. To mitigate the effects of these sidewalls potentially collapsing during construction, we recommend temporary shoring be constructed or the excavated slopes not exceed 1.5H:1V.

SGS anticipates groundwater to be encountered near the bottom of the excavations for the underground storage tanks. Dewatering techniques may be required for construction. Dewatering can be performed using shallow sumps and pumps or equivalent methods. It should be assumed that groundwater is at a minimum elevation of 285 ft (14 ft BGS) for buoyancy computations. SGS recommends excavation sidewalls that are within the limits of the groundwater table do not exceed slopes of 1.5H:1V. Backfill for the underground tanks can consist of SF or GB placed and compacted to a minimum of 95% of ASTM D1557.

6.0 Earthwork Considerations

6.1 Earthwork for Construction

All soils, existing and imported, should have an OSHA temporary excavation stability soil classification of Type C. Side slopes should not exceed 1.5H:1V. This permissible slope is for excavations less than 20 feet deep. Excavations deeper than this should be designed by a professional engineer.

De-watering in the excavations may be required if water begins to pond in the excavations. We anticipate that dewatering, if necessary, can be accomplished using shallow sump and pumps.

Adequate proof rolling of the subgrade soil is important to the success of any fill as a uniform bearing material, especially if the subgrade soil is loose in isolated areas. All foundations should be constructed on a minimum of 6 inches of compacted CS.

To the extent possible, construction should occur during periods of dry weather to minimize disturbance to excavated subgrade areas. If excavations and construction occur during wet periods, the contractor should employ the necessary measures to eliminate disturbance to the subgrade from heavy rainfall, surface water runoff, freeze/thaw softening, or any other potential weather-related cause of subgrade disturbance.

Once excavation for the footings is initiated, SGS should be contacted to observe the subgrade conditions after proofrolling and prior to the placement of the CS.

6.2 Materials

The gradation requirements reflect the portion of soil passing the 3-inch sieve size. The following table presents the recommended grain sizes for the materials to be used at the site:

GRADATION REQUIREMENTS FOR SITE MATERIALS			
Sieve Size	¹ Structural Fill (SF)	² Crushed Stone (CS)	³ Granular Borrow (GB)
3 Inch	100	---	100
2 Inch	---	---	---
1 Inch	---	100	---
³ / ₄ Inch	---	90 – 100	---
¹ / ₂ Inch	35 – 80	20 – 55	---
³ / ₈ Inch	---	0 – 15	---
¹ / ₄ Inch	25 – 65	---	---
No. 4	---	0 – 5	---
No. 40	0 – 30	---	0 – 70
No. 200	0 – 7	---	0 – 7
Maximum Particle Size	6"	1"	6"
⁴ Minimum Compaction Requirement	95%	---	95%

¹Maine DOT Specification 703.06, 2014, Type D

²Maine DOT Specification 703.13, 2020, Crushed Stone ³/₄-Inch

³Maine DOT Specification 703.19, 2020, Granular Borrow

⁴Per ASTM D1557

CS should be placed in 12-inch maximum lifts and compacted with a minimum of 4 passes with a vibratory compactor. GB should consist of a free draining, granular soil. **The upper portions of the marine ice delta <10 feet BGS will meet the requirements for GB.** Grain size analyses should be performed during construction to ensure the marine ice delta formation will meet the requirements for GB.

Common Borrow (CB) used at the site should consist of earth, suitable for embankment construction. It shall be free from frozen material, perishable rubbish, peat, and other unsuitable material including material currently or previously contaminated by chemical, radiological, or biological agents and should be able to be placed and compacted to a stable state.

6.3 Summary of Site Fill

The following table provides a summary of the proposed fill materials for the site and the requirements for use during construction:

SUMMARY OF SITE FILL			
Category	Use for Fill	Materials	Requirements/Notes
Footings	Footings Bearing Material	CS	- Minimum 6-inch thickness - Compacted to lock the particles together
	Underneath Footings Bearing Material	GB, SF, or Marine Ice Delta	- Compacted to a minimum of 95% of ASTM D1557 - Maximum particle size of 6 inches
	Exterior Backfill for Foundation Walls	GB	- Compacted to a minimum of 95% of ASTM D1557
Slabs	Slab Bearing Material	CS or SF	- 8 inches of CS compacted to lock the particles together OR - 12 inches of SF compacted to a minimum of 95% of ASTM D1557
	Underneath Slab Bearing Material	GB, SF, or Marine Ice Delta	- Compacted to a minimum of 95% of ASTM D1557 - Maximum particle size of 6 inches
Pavement	Underneath Pavement Subbase	CB	- Compacted to a minimum of 95% of ASTM D1557
Underground Storage Tanks	Anchor Slab Bearing Material	CS	- Minimum 6-inch thickness - Compacted to lock the particles together
	Backfill for Tanks	GB, SF, or Marine Ice Delta	- Compacted to a minimum of 95% of ASTM D1557 - Maximum particle size of 6 inches
Landscape Areas		CB	- Compacted to a minimum of 90% of ASTM D1557

7.0 Closure

Our recommendations are based on professional judgment, generally accepted principles of geotechnical engineering and project information provided by others. No other warranty is expressed or implied. Some changes in subsurface conditions from those presented in this report may occur. Should the subsurface conditions, finish grades, or foundation loadings differ materially from those described in this report, SGS should be notified so that we can re-evaluate our recommendations.

We recommend that a qualified third-party testing agency be retained to provide QA/QC services during construction.

SGS should be contacted to observe the footing subgrade after compaction and before the placement of the CS to ensure the subgrade conditions are sufficient to support the proposed foundations.

We appreciate the opportunity to serve you during this phase of your project. If there are any questions or if additional information is required, please do not hesitate to call.

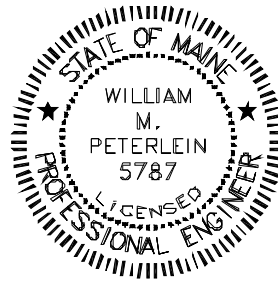
Sincerely,
Summit Geoengineering Services, Inc.



Colin M. Plante, P.E.
Geotechnical Engineer

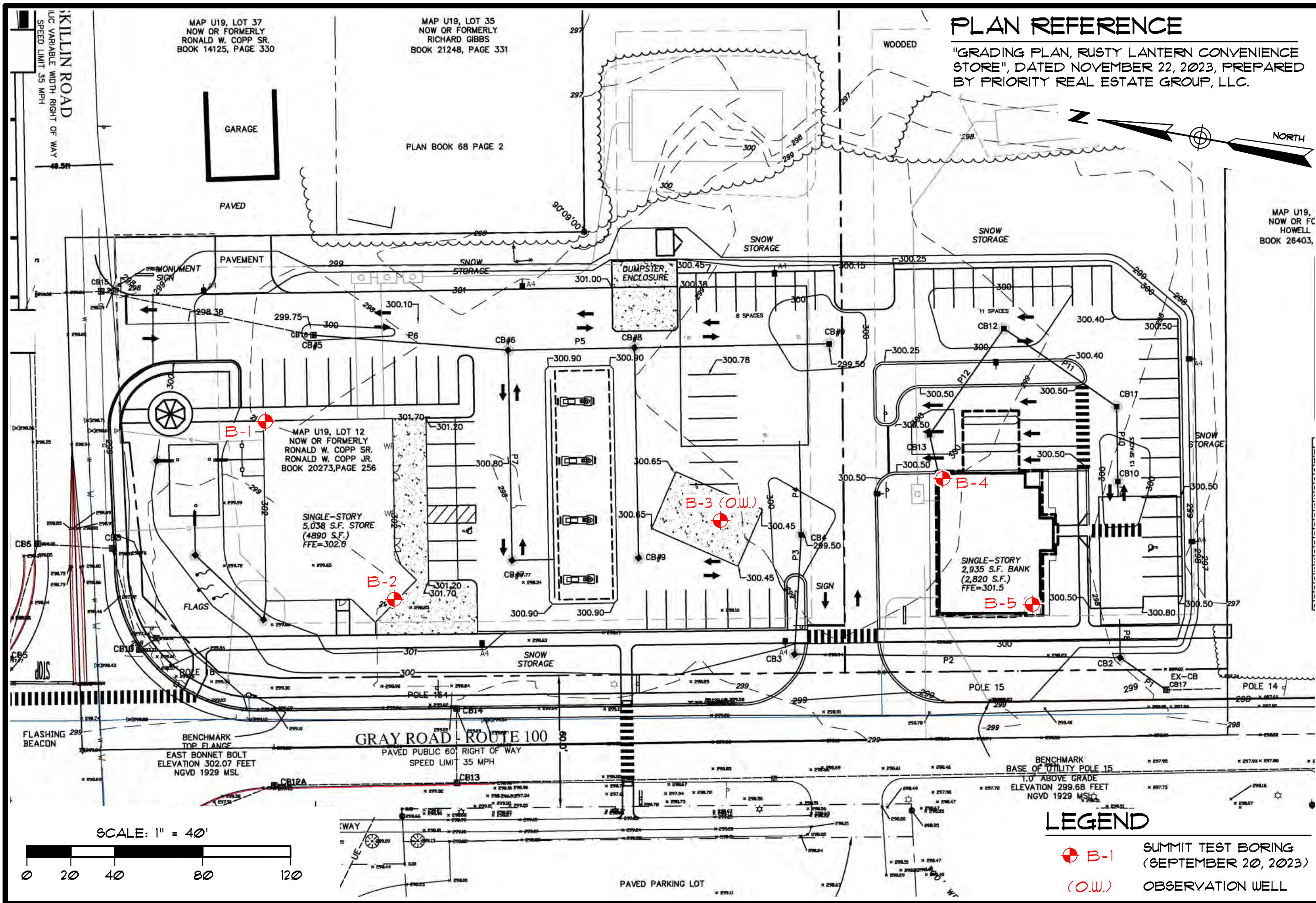


William M. Peterlein, P.E.
President & Principal Engineer



Appendix A


Figures





PROJECT:	CONVENIENCE STORE & BANK	
	181 GRAY ROAD - CUMBERLAND, MAINE	
CLIENT:	PRIORITY REAL ESTATE GROUP	
TITLE:	TEST BORING LOCATION PLAN	
SCALE: 1" = 40'	DRAWN BY: KRF	
	DATE: SEPT. 25, 2023	APPR BY: CMP
MAIL: P.O. BOX 515 FARMINGDALE, MAINE TEL: (207) 446-3360		
OFFICE: 210 MAINE AVENUE FARMINGDALE, MAINE TEL: (207) 446-3360		
SUMMIT GEOENGINEERING SERVICES		
PROJ.#: 23241		FIGURE: 1

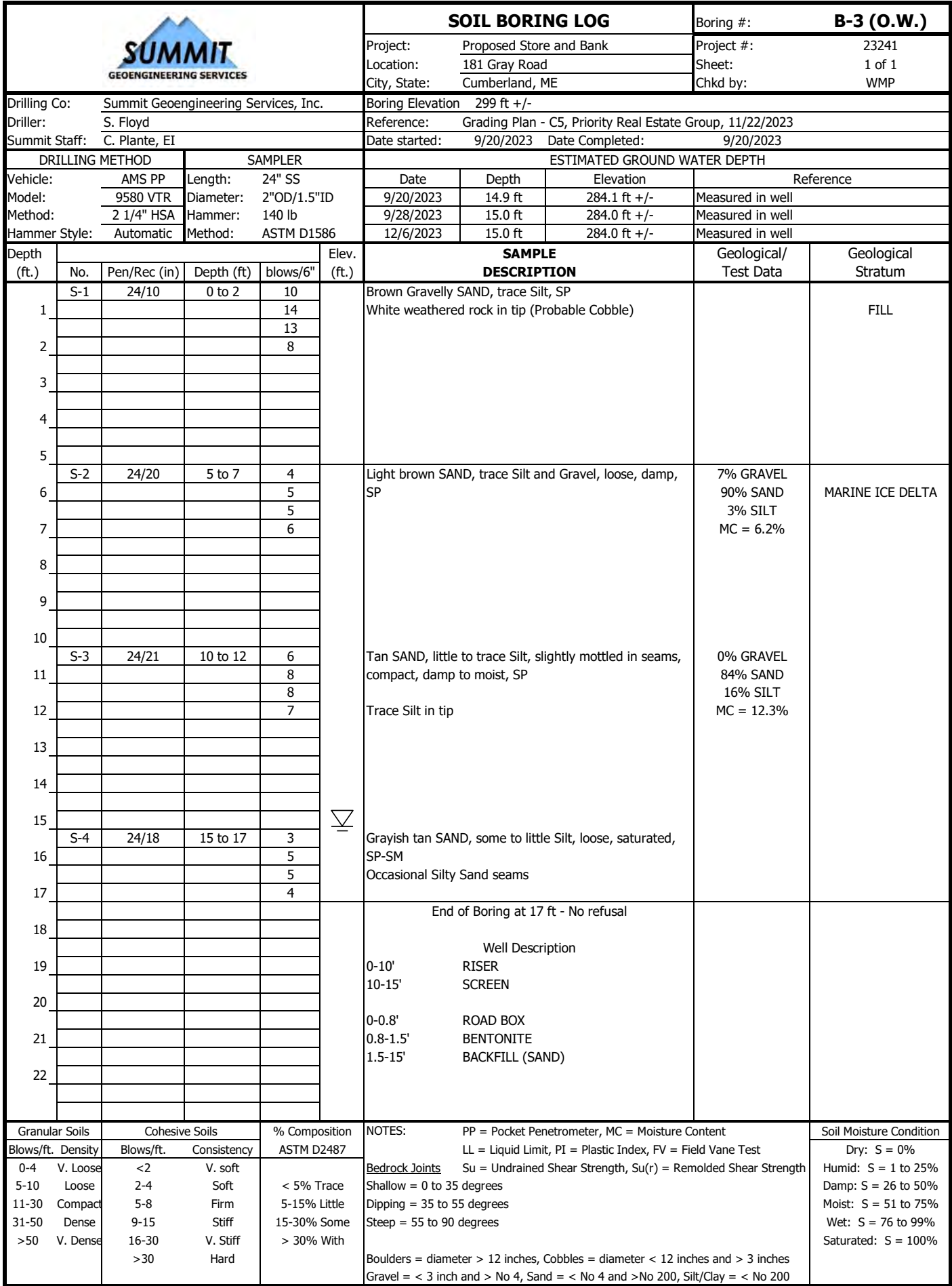
Appendix B


Exploration Logs


					SOIL BORING LOG			Boring #: B-1		
Drilling Co: Summit Geoengineering Services, Inc.					Project: Proposed Store and Bank			Project #: 23241		
Driller: S. Floyd					Location: 181 Gray Road			Sheet: 1 of 2		
Summit Staff: C. Plante, EI					City, State: Cumberland, ME			Chkd by: WMP		
Boring Elevation 298 ft +/-					Reference: Grading Plan - C5, Priority Real Estate Group, 11/22/2023					
Date started: 9/20/2023					Date Completed: 9/20/2023					
DRILLING METHOD		SAMPLER			ESTIMATED GROUND WATER DEPTH					
Vehicle: AMS PP		Length: 24" SS			Date	Depth	Elevation	Reference		
Model: 9580 VTR		Diameter: 2"OD/1.5"ID			9/20/2023	15 ft	283.0 ft +/-	Estimated in spoon samples		
Method: 2 1/4" HSA		Hammer: 140 lb								
Hammer Style: Automatic		Method: ASTM D1586								
Depth (ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	Elev. (ft.)	SAMPLE DESCRIPTION		Geological/ Test Data	Geological Stratum	
1	S-1	24/11	0 to 2	15		Black Gravelly SAND, trace Silt, compact, humid, SP			FILL	
				8		Light brown SAND, little Gravel, SP				
				6		Brown SAND, little Silt, trace Gravel, SP-SM			MARINE ICE DELTA	
2				3						
3										
4										
5										
6	S-2	24/14	5 to 7	4		Light brown SAND, trace Gravel and Silt, SP				
				6		Tan SAND, compact, damp to moist, SP				
				6		White weathered rock from 5.4 to 5.5 ft				
7				6						
8										
9										
10										
11	S-3	24/19	10 to 12	3		Tan SAND, little to trace Silt, loose, moist, SP				
				4		Some to little Silt in seams				
				4						
12				5						
13										
14										
15										
16	S-4	24/17	15 to 17	2		Light brown SAND, little to trace Silt, loose, saturated, SP				
				4						
				4						
17				5						
18						Running Sands at 18 ft				
19						Switch to casing				
20										
21	S-5	24/20	20 to 22	1		Gray brown SAND, trace Silt, very loose, saturated, SP				
				1		Brownish gray Clayey SILT, some fine Sand, slightly mottled, soft, saturated, ML		PP = 1.5 tsf	GLACIAL MARINE	
				2		Occasional fine Sandy SILT seams				
22				3						
Granular Soils		Cohesive Soils		% Composition		NOTES:			Soil Moisture Condition	
Blows/ft. Density		Blows/ft. Consistency		ASTM D2487		PP = Pocket Penetrometer, MC = Moisture Content LL = Liquid Limit, PI = Plastic Index, FV = Field Vane Test Su = Undrained Shear Strength, Su(r) = Remolded Shear Strength			Dry: S = 0%	
0-4 V. Loose		<2 V. soft		< 5% Trace		Bedrock Joints Shallow = 0 to 35 degrees			Humid: S = 1 to 25%	
5-10 Loose		2-4 Soft		5-15% Little		Dipping = 35 to 55 degrees			Damp: S = 26 to 50%	
11-30 Compact		5-8 Firm		15-30% Some		Steep = 55 to 90 degrees			Moist: S = 51 to 75%	
31-50 Dense		9-15 Stiff		> 30% With		Boulders = diameter > 12 inches, Cobbles = diameter < 12 inches and > 3 inches			Wet: S = 76 to 99%	
>50 V. Dense		16-30 V. Stiff				Gravel = < 3 inch and > No 4, Sand = < No 4 and >No 200, Silt/Clay = < No 200			Saturated: S = 100%	
		>30 Hard								

					SOIL BORING LOG			Boring #: B-1	
								Project #: 23241	
					Project: Proposed Store and Bank		Sheet: 2 of 2		
					Location: 181 Gray Road		Chkd by: WMP		
City, State: Cumberland, ME									
Drilling Co: Summit Geoengineering Services, Inc.					Boring Elevation 298 ft +/-				
Driller: S. Floyd					Reference: Grading Plan - C5, Priority Real Estate Group, 11/22/2023				
Summit Staff: C. Plante, EI					Date started: 9/20/2023 Date Completed: 9/20/2023				
DRILLING METHOD		SAMPLER			ESTIMATED GROUND WATER DEPTH				
Vehicle: AMS PP		Length: 24" SS			Date	Depth	Elevation	Reference	
Model: 9580 VTR		Diameter: 2"OD/1.5"ID			9/20/2023	15 ft	283.0 ft +/-	Estimated in spoon samples	
Method: 2 1/4" HSA		Hammer: 140 lb							
Hammer Style: Automatic		Method: ASTM D1586							
Depth (ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	Elev. (ft.)	SAMPLE DESCRIPTION		Geological/ Test Data	Geological Stratum
23						Brownish gray Clayey SILT, some fine Sand, slightly mottled, soft, saturated, ML			GLACIAL MARINE
24									
25									
26	S-6	24/24	25 to 27	WH		Gray Silty CLAY, little Sand, very soft, saturated, CL			
27				5		Gray fine Sandy SILT, some Clay, firm, saturated, ML			
28				7		Probe with spear tip and SPT hammer			GLACIAL TILL
29				50/7.5"		End of Boring at 26.6 ft - Refusal on dense stratum			
30									
31									
32									
33									
34									
35									
36									
37									
38									
39									
40									
41									
42									
43									
44									
Granular Soils		Cohesive Soils		% Composition		NOTES: PP = Pocket Penetrometer, MC = Moisture Content LL = Liquid Limit, PI = Plastic Index, FV = Field Vane Test <u>Bedrock Joints</u> Su = Undrained Shear Strength, Su(r) = Remolded Shear Strength Shallow = 0 to 35 degrees Dipping = 35 to 55 degrees Steep = 55 to 90 degrees Boulders = diameter > 12 inches, Cobbles = diameter < 12 inches and > 3 inches Gravel = < 3 inch and > No 4, Sand = < No 4 and >No 200, Silt/Clay = < No 200		Soil Moisture Condition Dry: S = 0% Humid: S = 1 to 25% Damp: S = 26 to 50% Moist: S = 51 to 75% Wet: S = 76 to 99% Saturated: S = 100%	
Blows/ft.	Density	Blows/ft.	Consistency	ASTM D2487					
0-4	V. Loose	<2	V. soft						
5-10	Loose	2-4	Soft	< 5% Trace					
11-30	Compact	5-8	Firm	5-15% Little					
31-50	Dense	9-15	Stiff	15-30% Some					
>50	V. Dense	16-30	V. Stiff	> 30% With					
		>30	Hard						

						SOIL BORING LOG		Boring #: B-2	
Project: Proposed Store and Bank						Project #:		23241	
Location: 181 Gray Road						Sheet:		1 of 1	
City, State: Cumberland, ME						Chkd by:		WMP	
Drilling Co: Summit Geoengineering Services, Inc.						Boring Elevation: 299 ft +/-			
Driller: S. Floyd						Reference: Grading Plan - C5, Priority Real Estate Group, 11/22/2023			
Summit Staff: C. Plante, EI						Date started: 9/20/2023 Date Completed: 9/20/2023			
DRILLING METHOD		SAMPLER		ESTIMATED GROUND WATER DEPTH					
Vehicle: AMS PP		Length: 24" SS		Date	Depth	Elevation	Reference		
Model: 9580 VTR		Diameter: 2"OD/1.5"ID		9/20/2023	15 ft	284.0 ft +/-	Estimated in spoon samples		
Method: 2 1/4" HSA		Hammer: 140 lb							
Hammer Style: Automatic		Method: ASTM D1586							
Depth (ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	Elev. (ft.)	SAMPLE DESCRIPTION		Geological/ Test Data	Geological Stratum
						6" Pavement			PAVEMENT
1	S-1	24/13	0 to 2	4		Brown SAND, little to trace Gravel, trace Silt, loose, damp, SP			FILL
2				3					
3				3					
4				1					
5									
6	S-2	24/16	5 to 7	1		Light brown SAND, trace Gravel, very loose, damp to moist, SP			MARINE ICE DELTA
7				1					
8				2					
9									
10									
11	S-3	24/20	10 to 12	3		Tan fine SAND, little to trace Silt, loose, damp, SP			
12				3					
13				3					
14				4					
15									
16	S-4	24/17	15 to 17	2		Tan SAND, compact, saturated, SP			
17				3					
18				10					
19				10					
20									
21	S-5	24/24	20 to 22	3		Grayish brown fine Sandy SILT, some Clay, stiff, saturated, ML		PP = 1.3 - 3.0 tsf	GLACIAL MARINE
22				3					
				6		Brownish gray SAND, some to little Silt, little Gravel, trace Clay, compact, wet, SM-SP			GLACIAL TILL
				29					
End of Boring at 22 ft - No refusal									
Granular Soils		Cohesive Soils		% Composition		NOTES:			Soil Moisture Condition
Blows/ft.	Density	Blows/ft.	Consistency	ASTM D2487		PP = Pocket Penetrometer, MC = Moisture Content LL = Liquid Limit, PI = Plastic Index, FV = Field Vane Test Su = Undrained Shear Strength, Su(r) = Remolded Shear Strength			Dry: S = 0%
0-4	V. Loose	<2	V. soft	< 5% Trace		Bedrock Joints Shallow = 0 to 35 degrees			Humid: S = 1 to 25%
5-10	Loose	2-4	Soft	5-15% Little		Dipping = 35 to 55 degrees			Damp: S = 26 to 50%
11-30	Compact	5-8	Firm	15-30% Some		Steep = 55 to 90 degrees			Moist: S = 51 to 75%
31-50	Dense	9-15	Stiff	> 30% With		Boulders = diameter > 12 inches, Cobbles = diameter < 12 inches and > 3 inches			Wet: S = 76 to 99%
>50	V. Dense	16-30	V. Stiff			Gravel = < 3 inch and > No 4, Sand = < No 4 and >No 200, Silt/Clay = < No 200			Saturated: S = 100%
		>30	Hard						



					SOIL BORING LOG			Boring #: B-4	
Drilling Co: Summit Geoengineering Services, Inc.					Project: Proposed Store and Bank			Project #: 23241	
Driller: S. Floyd					Location: 181 Gray Road			Sheet: 1 of 2	
Summit Staff: C. Plante, EI					City, State: Cumberland, ME			Chkd by: WMP	
Boring Elevation 299 ft +/-					Reference: Grading Plan - C5, Priority Real Estate Group, 11/22/2023				
Date started: 9/20/2023					Date Completed: 9/20/2023				
DRILLING METHOD		SAMPLER			ESTIMATED GROUND WATER DEPTH				
Vehicle: AMS PP		Length: 24" SS			Date	Depth	Elevation	Reference	
Model: 9580 VTR		Diameter: 2"OD/1.5"ID			9/20/2023	15 ft	284.0 ft +/-	Estimated in spoon samples	
Method: 2 1/4" HSA		Hammer: 140 lb							
Hammer Style: Automatic		Method: ASTM D1586							
Depth (ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	Elev. (ft.)	SAMPLE DESCRIPTION		Geological/ Test Data	Geological Stratum
1	S-1	24/15	0 to 2	8		Brown SAND, some to little Gravel, little to trace Silt, compact, damp, SP-SM			FILL
				11					
				4					
2				3		Dark brown SAND, some Silt, little Gravel, SM			MARINE ICE DELTA
3									
4									
5									
6	S-2	24/16	5 to 7	5		Tan SAND, trace Gravel, compact, damp, SP			
7				6					
8				7					
9				7					
10									
11	S-3	24/22	10 to 12	3		Tan fine SAND, trace Silt, loose, damp, SP			
12				5					
13				5					
14				6					
15									
16	S-4	24/18	15 to 17	2		Tan SAND, little Silt, loose, saturated, SP-SM			
17				2		Silty in seams			
18				3					
19				6					
20									
21	S-5	24/24	20 to 22	6		Brown SAND, some Silt, loose, saturated, SM			
22				4		Brownish gray fine Sandy SILT, some Clay, slightly mottled, firm, wet, ML		PP = 1.0 - 2.3 tsf	GLACIAL MARINE
				4					
				4					
Granular Soils		Cohesive Soils		% Composition		NOTES:			Soil Moisture Condition
Blows/ft.	Density	Blows/ft.	Consistency	ASTM D2487		PP = Pocket Penetrometer, MC = Moisture Content LL = Liquid Limit, PI = Plastic Index, FV = Field Vane Test Su = Undrained Shear Strength, Su(r) = Remolded Shear Strength			Dry: S = 0%
0-4	V. Loose	<2	V. soft	< 5% Trace		Bedrock Joints			Humid: S = 1 to 25%
5-10	Loose	2-4	Soft	5-15% Little		Shallow = 0 to 35 degrees			Damp: S = 26 to 50%
11-30	Compact	5-8	Firm	15-30% Some		Dipping = 35 to 55 degrees			Moist: S = 51 to 75%
31-50	Dense	9-15	Stiff	> 30% With		Steep = 55 to 90 degrees			Wet: S = 76 to 99%
>50	V. Dense	16-30	V. Stiff			Boulders = diameter > 12 inches, Cobbles = diameter < 12 inches and > 3 inches			Saturated: S = 100%
		>30	Hard			Gravel = < 3 inch and > No 4, Sand = < No 4 and >No 200, Silt/Clay = < No 200			

						SOIL BORING LOG		Boring #: B-5	
Project: Proposed Store and Bank						Project #:		23241	
Location: 181 Gray Road						Sheet:		1 of 1	
City, State: Cumberland, ME						Chkd by:		WMP	
Drilling Co: Summit Geoengineering Services, Inc.						Boring Elevation 298.5 ft +/-			
Driller: S. Floyd						Reference: Grading Plan - C5, Priority Real Estate Group, 11/22/2023			
Summit Staff: C. Plante, EI						Date started: 9/20/2023 Date Completed: 9/20/2023			
DRILLING METHOD			SAMPLER			ESTIMATED GROUND WATER DEPTH			
Vehicle: AMS PP			Length: 24" SS			Date	Depth	Elevation	Reference
Model: 9580 VTR			Diameter: 2"OD/1.5"ID			9/20/2023	15 ft	283.5 ft +/-	Estimated in spoon samples
Method: 2 1/4" HSA			Hammer: 140 lb						
Hammer Style: Automatic			Method: ASTM D1586						
Depth (ft.)	No.	Pen/Rec (in)	Depth (ft)	blows/6"	Elev. (ft.)	SAMPLE DESCRIPTION		Geological/ Test Data	Geological Stratum
1	S-1	24/17	0 to 2	10		Grayish brown SAND, some to little Gravel, trace Silt, compact, damp, SP			FILL
				10		Black SAND, SP			
				10					
2				5		Reddish brown SAND, some to little Silt, SM-SP			MARINE ICE DELTA
3									
4									
5									
6	S-2	24/15	5 to 7	5		Tan SAND, trace Gravel, compact, damp, SP			
7				7					
8				6					
9				6					
10									
11	S-3	24/18	10 to 12	3		Tan SAND, loose, damp to moist, SP			
12				5					
13				5					
14									
15									
16	S-4	24/19	15 to 17	4		Tan SAND, compact, saturated, SP			
17				9					
18				12		Light gray fine Sandy SILT, some Clay, very stiff, wet, ML			
19				10					
20									
21	S-5	24/24	20 to 22	2		Grayish brown fine Sandy SILT, some Clay, firm, saturated, ML			
22				3		Few Clayey SILT seams			
				4					
				4					
				66		Probe with spear tip and SPT hammer			
						End of Boring at 22.9 ft - Refusal in dense stratum			

Granular Soils		Cohesive Soils		% Composition ASTM D2487	NOTES: PP = Pocket Penetrometer, MC = Moisture Content LL = Liquid Limit, PI = Plastic Index, FV = Field Vane Test Su = Undrained Shear Strength, Su(r) = Remolded Shear Strength Shallow = 0 to 35 degrees Dipping = 35 to 55 degrees Steep = 55 to 90 degrees Boulders = diameter > 12 inches, Cobbles = diameter < 12 inches and > 3 inches Gravel = < 3 inch and > No 4, Sand = < No 4 and >No 200, Silt/Clay = < No 200	Soil Moisture Condition
Blows/ft.	Density	Blows/ft.	Consistency			Dry: S = 0% Humid: S = 1 to 25% Damp: S = 26 to 50% Moist: S = 51 to 75% Wet: S = 76 to 99% Saturated: S = 100%
0-4	V. Loose	<2	V. soft			
5-10	Loose	2-4	Soft	< 5% Trace		
11-30	Compact	5-8	Firm	5-15% Little		
31-50	Dense	9-15	Stiff	15-30% Some		
>50	V. Dense	16-30	V. Stiff	> 30% With		
		>30	Hard			

Appendix C

Laboratory Testing



GRAIN SIZE ANALYSIS - ASTM D6913

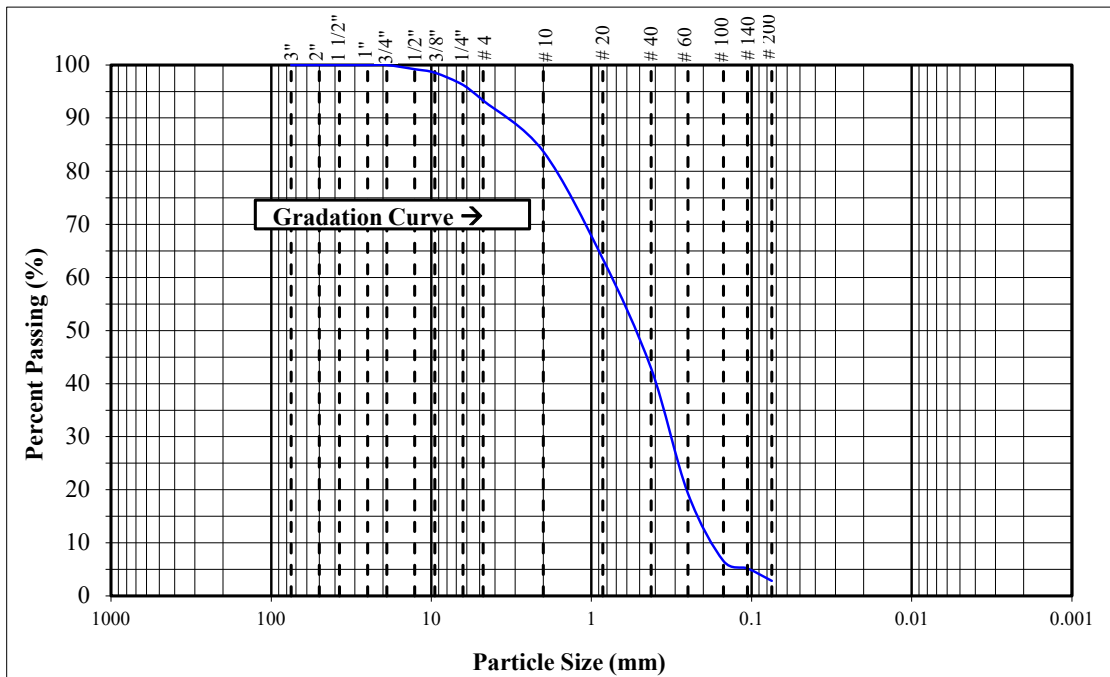
PROJECT NAME: Proposed Gas Station and Bank	PROJECT #: 23241
PROJECT LOCATION: 181 Gray Road, Cumberland, ME	EXPLORATION #: B-3
CLIENT: Priority Real Estate Group	SAMPLE #: S-2
TECHNICIAN: C. Plante, EI	SAMPLE DEPTH: 5' to 7'
SOIL DESCRIPTION: Fine-medium SAND, little Gravel, trace Silt, SP	TEST DATE: 9/25/2023

TEST PROCEDURE

Sample Source: Split Spoon	Sieve Stack: Composite	Specimen Procedure: Moist
Test Method: Method A	Separating Sieve(s): 3/8 Inch	Dispersion Type: Tap Water

DATA

<u>STANDARD SIEVE</u> DESIGNATION (mm)	<u>ALTERNATIVE SIEVE</u> DESIGNATION (in)	<u>PERCENT</u> PASSING (%)
75	(3 in)	100
50	(2 in)	100
37.5	(1-1/2 in)	100
25.0	(1 in)	100
19.0	(3/4 in)	100
12.7	(1/2 in)	99
9.5	(3/8 in)	99
6.35	(1/4 in)	96
4.75	(No. 4)	93
2.00	(No. 10)	84
0.850	(No. 20)	64
0.425	(No. 40)	43
0.250	(No. 60)	19
0.150	(No. 100)	7
0.106	(No. 140)	5
0.075	(No. 200)	3



REMARKS: Moisture Content = 6.2%

Reviewed By: ELS



GRAIN SIZE ANALYSIS - ASTM D6913

PROJECT NAME: Proposed Gas Station and Bank
 PROJECT LOCATION: 181 Gray Road, Cumberland, ME
 CLIENT: Priority Real Estate Group
 TECHNICIAN: C. Plante, EI
 SOIL DESCRIPTION: Fine SAND, some Silt, SM

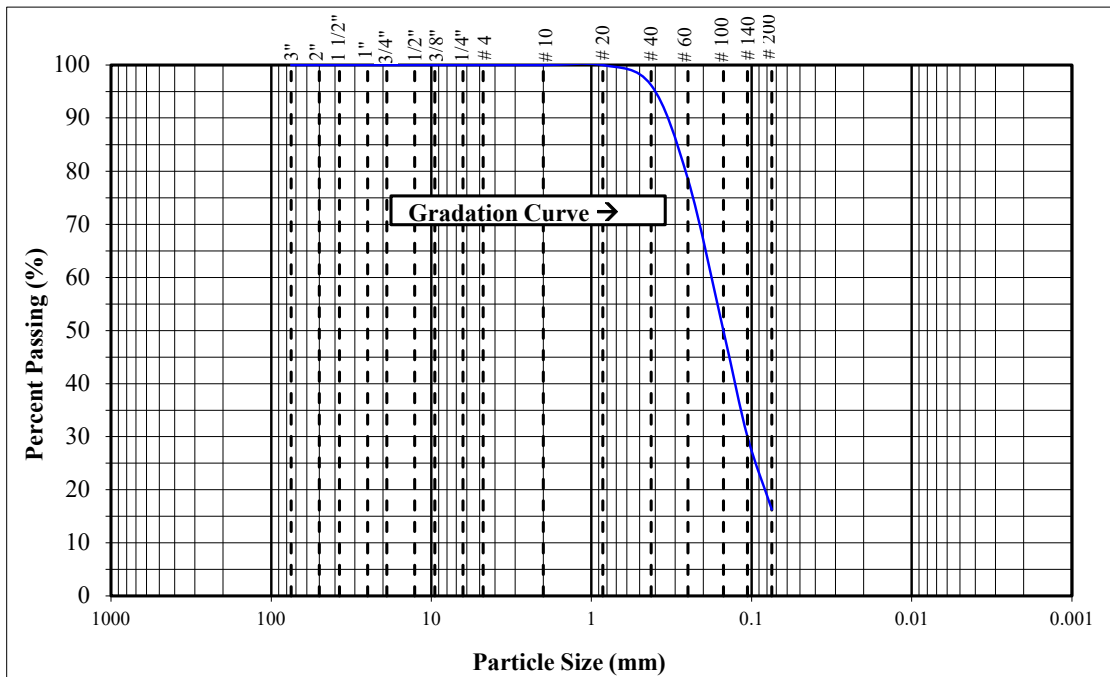
PROJECT #: 23241
 EXPLORATION #: B-3
 SAMPLE #: S-3
 SAMPLE DEPTH: 10' to 12'
 TEST DATE: 9/25/2023

TEST PROCEDURE

Sample Source: Split Spoon	Sieve Stack: Single	Specimen Procedure: Moist
Test Method: Method B	Separating Sieve(s): 3/8 Inch	Dispersion Type: Tap Water

DATA

<u>STANDARD SIEVE</u> <u>DESIGNATION (mm)</u>	<u>ALTERNATIVE SIEVE</u> <u>DESIGNATION (in)</u>	<u>PERCENT</u> <u>PASSING (%)</u>
75	(3 in)	100.0
50	(2 in)	100.0
37.5	(1-1/2 in)	100.0
25.0	(1 in)	100.0
19.0	(3/4 in)	100.0
12.7	(1/2 in)	100.0
9.5	(3/8 in)	100.0
6.35	(1/4 in)	100.0
4.75	(No. 4)	100.0
2.00	(No. 10)	100.0
0.850	(No. 20)	100.0
0.425	(No. 40)	96.2
0.250	(No. 60)	78.5
0.150	(No. 100)	49.9
0.106	(No. 140)	30.0
0.075	(No. 200)	16.3



REMARKS: Moisture Content = 12.3%

Reviewed By: ELS

Memorandum of Findings

Date: October 26, 2023

To: Curtis Neufeld, PE (Priority Real Estate Group)

From: Rodney Kelshaw, LSS, CPSS, CPESC, LSE, PWS, CWB (Flycatcher LLC)

Subject: Stormwater Test Pits: Proposed Convenience Store: Cumberland, Maine

Curtis,

This memorandum provides results and findings from a soil investigation conducted to inform siting and design of stormwater best management practices for a proposed convenience store (Project) in Cumberland. Test pits were excavated in the locations requested by Priority Real Estate Group (PREG) (Figure 1).



Figure 1. Test Pit Locations (black and white, numbered boxes).

Methods: A Maine Licensed Soil Scientist (LSS) and excavator operator from Flycatcher performed test pit observations on October 10, 2023. It should be noted that the summer and early fall of 2023 have been exceptionally wet. Three pits (TP02 – TP04) were excavated to a depth of at least 96 inches and wide enough for entrance to observe and document the soil features. Observations within the pits included color, texture, presence of redoximorphic features, presence of or depth to bedrock, firm horizons, saturation, and free water. During excavation of test pit TP01, the excavator hit an unmarked water line which flooded the pit. The excavation extended to a depth of approximately 54-inches, at which point the water line was located.

Findings: Based on aerial photograph review, the gravel area surrounding the test pit locations was filled and regraded over a period of time, beginning in the early 1990s. The elevation is at approximately 298 feet (above sea level) with a 0-3% slope across the site.

Prior to conducting the test pits, the USDA Natural Resource Conservation Service (NRCS) county soil mapping was consulted. The NRCS map for the area depicts one map unit: Hinckley loamy sand. The Hinckley series consists of very deep, excessively drained soils formed in glaciofluvial materials. Slope ranges from 0 to 6 percent. Texture in the B and C horizons ranges from sand, coarse sand, loamy sand, or loamy coarse sand.

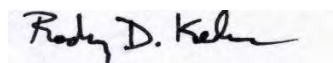
Onsite soil observations generally indicated parent materials similar to the Hinckley series as mapped by the NRCS; however, the area has had between seven and 27 inches of sandy fill imported over the native soil surface.

A summary list of accompanying observations from the test pits is provided below.

- TP01 was in a layer of pavement. There was approximately seven inches of fill below the pavement and then the soil horizons were somewhat mixed, apparently from the installation of the water line at a depth of 54 inches.
- TP02 and TP03 had variable fill materials ranging from 17 to 27 inches thick, with textures ranging from fine sandy loam to gravelly loamy sand. Additionally, debris including bottles and old apparent electrical lines were noted within the fill materials. Both pits were excavated to 96-inches with no evidence of a water table observed in either, resulting in a hydrologic soil group (HSG) classification of A.
- TP04 found evidence of the water table (redoximorphic features and soil moisture) at 80 inches.
- TP01 and TP04 have firm layers within 10-inches of the surface, due to pavement and compaction of the fill materials, resulting in a HSG classification of D. If these horizons are removed throughout the stormwater treatment area, then a HSG A classification can be substituted.

Flycatcher mapped the test pits with a mapping grade GPS unit and the locations were provided to PREG in a georeferenced CAD drawing. Please see the attached Soil Conditions Summary Table (Form E) and Soil Profile Classification Information (Form F) for detailed soil data.

Please contact me with questions and thanks again reaching out.



Rodney Kelshaw (CPSS, LSS, CPESC, LSE, PWS, CWB)
Managing Partner/Senior Scientist
C: (207) 944-6776

SOIL PROFILE / CLASSIFICATION INFORMATION

SOIL SCIENTIST DESCRIPTION OF SOIL CONDITIONS AT PROJECT SITES

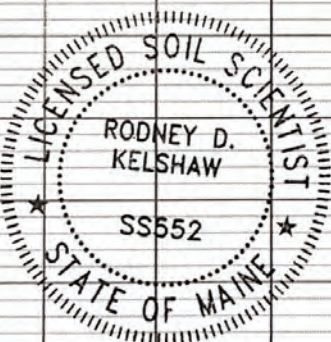
Project Name: Convenience Store

Applicant Name: **Priority Real Estate Group**

Project Location (municipality): **Cumberland**

Exploration Symbol # TP01c ☒ Test Pit ☐ Boring ☐ Probe
0 " Organic horizon thickness Ground surface elev. 298
54 " Depth: ☒ of exploration, or ☐ to refusal

	Horizon	Color	Texture	Structure	Consistence	Redox
	<u>PAVEMENT</u>					
	A ₁	dk ylt br		sbr	VFR	↑
	A ₂	v dk br	grsl	pl	F1	
10	BW ₁		grls	sbr	VFR	
	BW ₂	dk ylt br	cobls	pl	FR/FIP	
20						↓ <u>NONE OBSERVED</u>
30	B/C	lt ol br	ls		L	
40				sg		
50	C/B	pl ol	s			
60	<u>LOI 54 INCHES WATERLINE</u>					
70						
80						
90						
100						
110						
120						
130						
140						
150						



Soil Series/Phase Name: **HAHT**

Limiting Factor: ☐ Groundwater ☒ Restrictive Layer ☐ Bedrock

Drainage Class: ☒ ED ☐ SED ☐ WD ☐ MWD
☐ SPD ☐ PD ☐ VPD

Slope: 0-3 Percent Hydric Soil: ☒ No ☐ Yes Hydrologic Soil Group: D

Exploration Symbol # TP02e

0 " Organic horizon thickness Ground surface elev. 298

96 " Depth: ☒ of exploration, or ☐ to refusal

☒ Test Pit ☐ Boring ☐ Probe

0	Horizon	Color	Texture	Structure	Consistence	Redox	
10	A ₁	vd/k br	fill cobls			<div style="display: flex; align-items: center;"> <div style="flex-grow: 1; border-left: 1px solid black; position: relative;"> <div style="position: absolute; top: -10px; left: 0;">↑</div> <div style="position: absolute; bottom: -10px; left: 0;">↓</div> </div> </div>	
20				SG/GR	L		
30	A ₂	dk y/b br	fill grts				
40	Ab	blk	fsb				
50	Bs	dk br	sl	stk	FR		
60	B/C	yl br				NONE	
70	C/B	lt ol br				OBSERVED	
80			cos	SG	L		
90	C	pl ol					
100	LOI 96 INCHES						
110							
120							
130							
140							
150							

Soil Series/Phase Name: **HAHT**

Drainage Class: ☒ ED ☐ SED ☐ WD ☐ MWD
☐ SPD ☐ PD ☐ VPD

Limiting Factor: N.O. ☐ Groundwater ☐ Restrictive Layer ☐ Bedrock

Slope: 0-3 Percent Hydric Soil: ☒ No ☐ Yes Hydrologic: A Soil Group

SOIL SCIENTIST INFORMATION AND SIGNATURE

Signature
Rodney Kelshaw
Name Printed

2023-10-10
Date
552
SS License No

affix professional seal

SOIL PROFILE / CLASSIFICATION INFORMATION

SOIL SCIENTIST DESCRIPTION
OF SOIL CONDITIONS AT PROJECT SITESProject Name:
Convenience StoreApplicant Name:
Priority Real Estate GroupProject Location (municipality):
Cumberland

Exploration Symbol # TP03e ☒ Test Pit ☐ Boring ☐ Probe
 " Organic horizon thickness Ground surface elev. 298
96 " Depth: ☒ of exploration, or ☐ to refusal

Horizon	Color	Texture	Structure	Consistence	Redox
0					↑
10		fill			
20	A	dk ylb	ls	FR/FIP	
30	Ab	blk			
30	Bs	dk rd br	fst	SBK	
40	Bs	dk br	lfs	SBK/SBK	VFR
50	B/C	lt ol br	S		NONE OBSERVED
60					
70			GR	L	
80	C	pl ol	cos		
90					
100					
110					
120					
130					
140					
150					

Depth below mineral soil horizon (inches)

LOI 96 INCHES

Soil Series/Phase Name: **HAHT**

Limiting Factor ☐ Groundwater ☐ Restrictive Layer ☐ Bedrock

Depth N.O.

Drainage Class ☒ ED ☐ SED ☐ WD ☐ MWD ☐ SPD ☐ PD ☐ VPD

Slope 0-3 Percent

Hydric Soil ☒ No ☐ Yes

Hydrologic A

Soil Group

Exploration Symbol # TP04e ☒ Test Pit ☐ Boring ☐ Probe
 " Organic horizon thickness Ground surface elev. 298
96 " Depth: ☒ of exploration, or ☐ to refusal

Horizon	Color	Texture	Structure	Consistence	Redox
0					↑
10	Ap	blk	vgrls	FR	
20	Bs	br	cos	SBK	FR
30	Bw	yl br			NONE OBSERVED
40			cos		
50	B/C	lt ol br			
60			GR	L	
70	C/B	pl yl	S		
80					
90	C	pl ol	fs		st br 15%
100					
110					
120					
130					
140					
150					

Depth below mineral soil horizon (inches)

LICENSED SOIL SCIENTIST
RODNEY D. KELSHAW
SS552
STATE OF MAINE

Soil Series/Phase Name: **HAHT**

Limiting Factor ☐ Groundwater ☐ Restrictive Layer ☐ Bedrock

Depth 0

Drainage Class ☒ ED ☐ SED ☐ WD ☐ MWD ☐ SPD ☐ PD ☐ VPD

Slope 0-3 Percent

Hydric Soil ☒ No ☐ Yes

Hydrologic D

Soil Group

SOIL SCIENTIST INFORMATION AND SIGNATURE



 Signature
 Rodney Kelshaw
 Name Printed

2023-10-10

Date

552

SS License No.


affix professional seal

Attachment K
Hydrogeologic Report

K

The report from Sevee & Mahar is included here for reference.

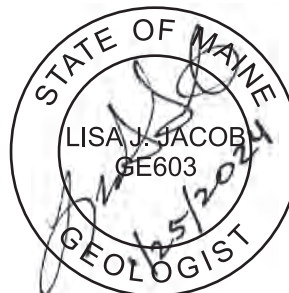
Hydrogeologic Report



HYDROGEOLOGIC EVALUATION FOR PROPOSED RUSTY LANTERN MARKET 181 GRAY ROAD, CUMBERLAND, MAINE

Prepared for

CUMBERLAND REAL ESTATE GROUP
2 MAIN STREET
TOPSHAM, MAINE



January 2024

4 Blanchard Road
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Cumberland, Maine 04021
Phone: 207.829.5016 smemaine.com

ENVIRONMENTAL • CIVIL • GEOTECHNICAL • WATER • COMPLIANCE

SME 
SEVEE & MAHER
ENGINEERS

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**HYDROGEOLOGIC EVALUATION FOR
PROPOSED RUSTY LANTERN MARKET
181 GRAY ROAD, CUMBERLAND, MAINE**

1.0 INTRODUCTION

Rusty Lantern Markets proposes to develop the properties at 173 and 181 Gray Road in Cumberland, Maine as a new Rusty Lantern Market and gas station site (hereinafter called the Site). The Site location is shown on Figure 1-1. Cumberland Real Estate Group (CREG) of Topsham, Maine are the lead engineers for the project. CREG has retained Sevee & Maher Engineers, Inc. (SME) to assist with hydrogeologic evaluation services to characterize the geology and groundwater flow conditions at and surrounding the Site.

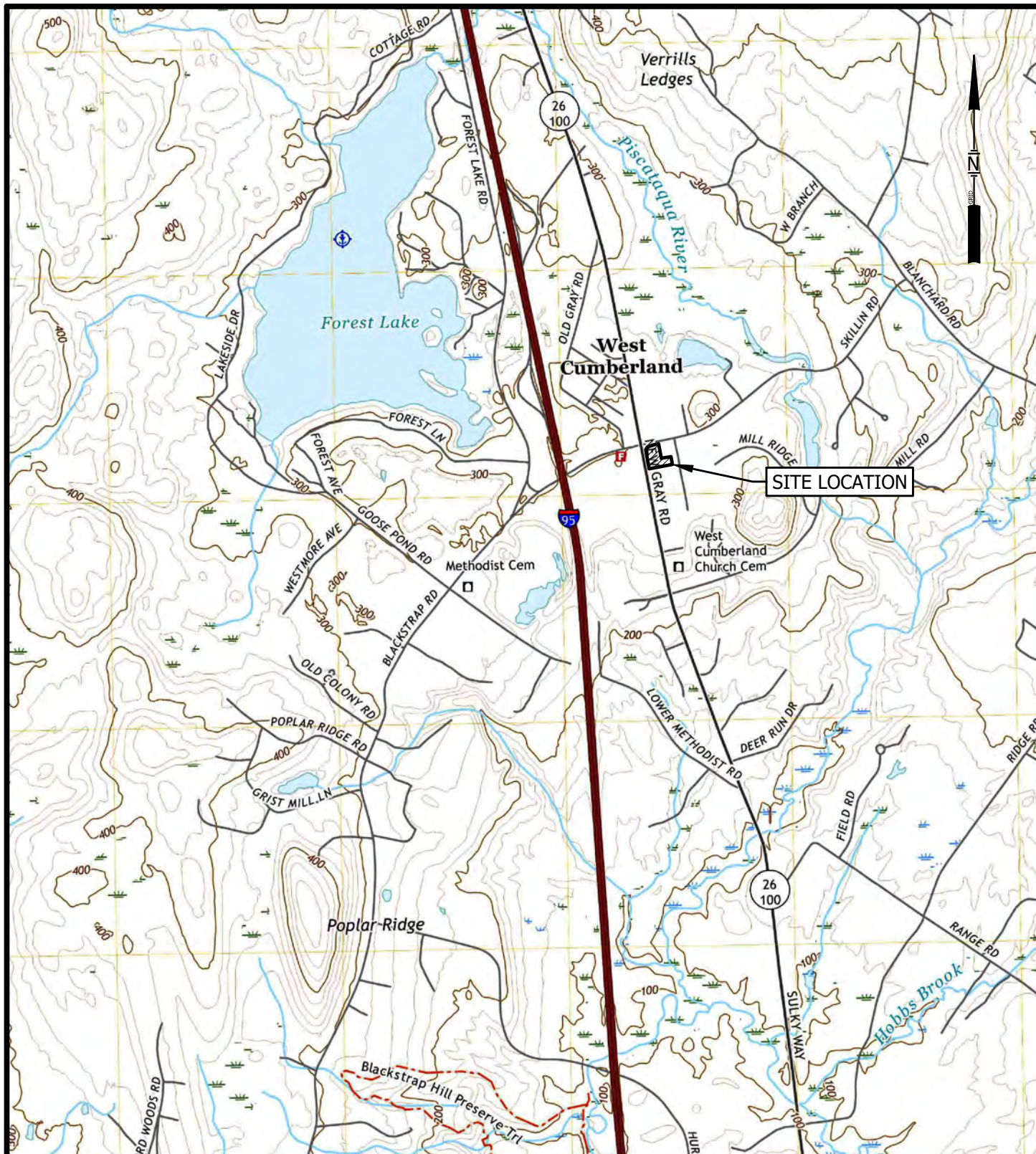
The Site is located in an area designated by the Town of Cumberland, Maine (Town) as an Aquifer Protection Zone.¹ Section § 315-36, Regulations of Article V, Aquifer Protection from the Town's Code indicates that storage of petroleum or other refined petroleum products (not including storage of petroleum products for residential purposes) shall only be allowed based upon a positive finding by the Town Planning Board that the proposed use, with any conditions imposed by the Board, will not adversely affect the quality of groundwater.² SME's hydrogeologic evaluation for the Site is intended to provide information to the Town Planning Board, supplemental to the Site design and protective engineering controls provided by others, to make a determination for the suitability of the Site for installation of an Underground Oil Storage Tank (UST) for the gas station proposed for the Site.

Based on the information provided in this report, it is SME's opinion that, with the Site's commercial zoning and existing hydrogeologic setting, and the stringent UST design standards imposed for Site development by the Maine Department of Environmental Protection (MEDEP) for a proposed UST site located in a significant sand and gravel aquifer, the Site is suitable for the proposed storage of refined petroleum products.

Background information for the Site is described in Section 2.0. As discussed in Section 2.5, SME submitted a work plan for a proposed hydrogeologic evaluation for the Site to MEDEP in November 2023 to support a variance for the prohibition of UST facilities located on significant sand and gravel aquifers with moderate yield. Based on the Site background information provided in the work plan, the MEDEP waived the requirement of the hydrogeologic evaluation and stated that the project can be transitioned into the purview of engineering for the Site to ensure compliance with design standards.

¹ Website: https://www.cumberlandmaine.com/sites/g/files/vyhlf9216/f/uploads/aquifer_map.pdf

² Town of Cumberland, Maine Code. Chapter 315, Zoning. Article V, Aquifer Protection. § Section 315-36, Regulations.



BASE MAP ADAPTED FROM 7.5 MIN USGS TOPO QUADS
CUMBERLAND CENTER, ME - 2021

FIGURE 1-1
SITE LOCATION MAP
PROPOSED RUSTY LANTERN MARKET
181 GRAY ROAD
CUMBERLAND, MAINE



SME's hydrogeologic evaluation for the Site, which was completed in December 2023 and January 2024 to provide Site specific hydrogeologic information to CREG, Rusty Lantern Market, and the Town Planning Board, is described in Section 3.0.

2.0 BACKGROUND INFORMATION

2.1 Site Location

The Site is proposed to be located at 181 Gray Road in Cumberland, Maine and a portion of 173 Gray Road in Cumberland, Maine. The existing site conditions are illustrated on Figure 2-1. The property at 181 Gray Road in Cumberland Maine is identified as Lot 12 on Tax Map U19 and is hereinafter referred to as Lot 12. Lot 12 is reported to have a size of 0.93 acres. The property at 173 Gray Road in Cumberland, Maine is identified as Lot 13 on Tax Map U19 and is hereinafter referred to as Lot 13. A reconfiguration of the common property boundary for Lots 12 and 13 is proposed to accommodate the 1.27-acre area proposed for Site development (see Figure 2-1).

There is one building located on the northwest corner of Lot 12, which is currently used as an auto sales and service business. The area surrounding the existing building is paved and there is also a small, paved area on the northeast corner of the Site. The unpaved portion of this parcel consists of a compacted gravel driving surface. There are no buildings currently located on the property located at Lot 13. The majority of the Site has an unpaved gravel surface which appears to be used for temporary truck and trailer parking.

The Site is located at the south side of the intersection of Route 100 (Gray Road) and Skillin Road. Among other utilities, water and natural gas utilities are accessible to the Site. The existing building at Lot 12 currently uses the water utility but is heated using No. 2 oil rather than using the natural gas utility. The existing building at the Site uses a private subsurface wastewater disposal system.

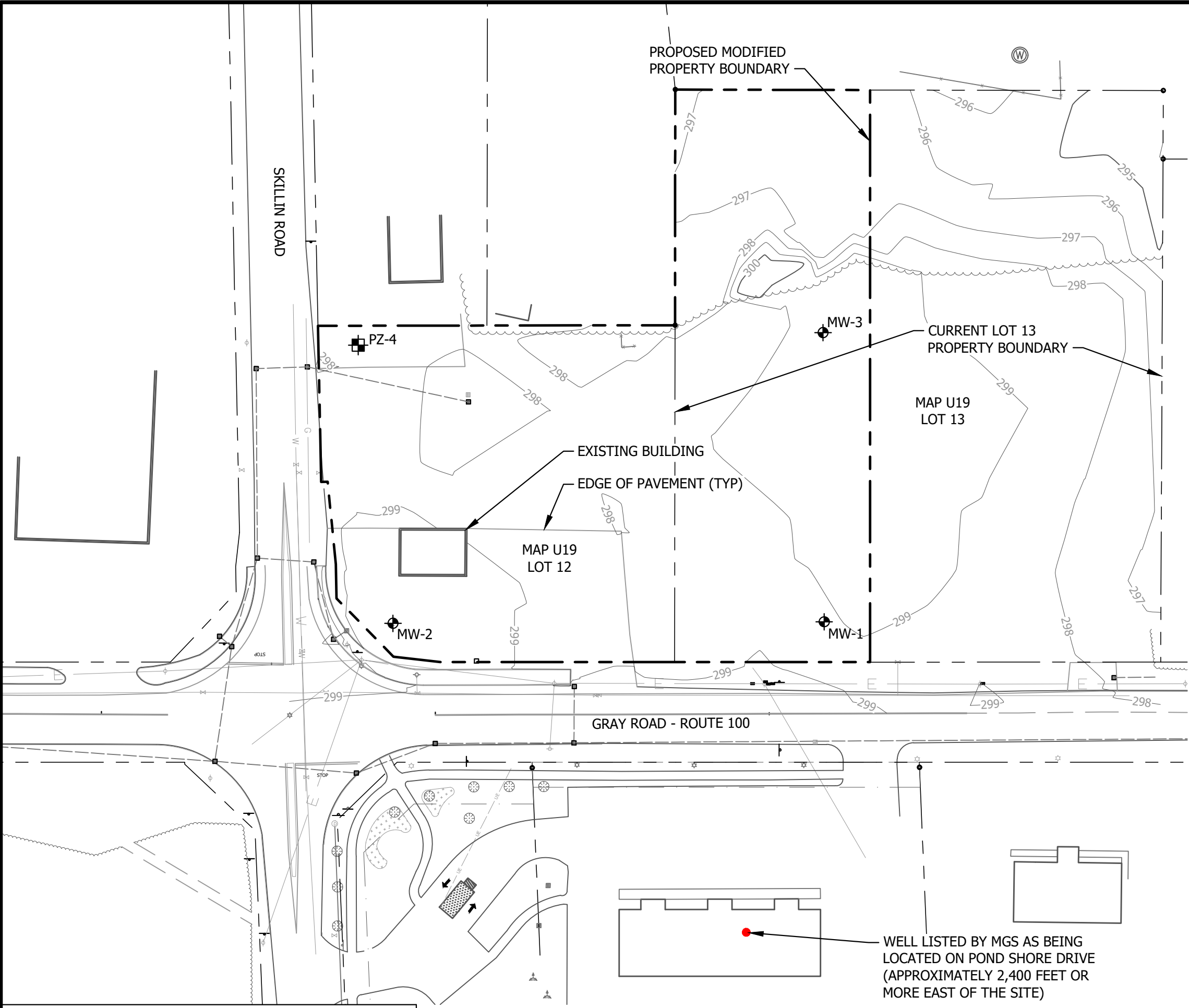
The Site is located within the Town's *Village Center Commercial* zone.³ The Site is abutted to the north, south, and west by commercial properties. The east side of the Site (i.e., the rear side of the property) abuts homes located along Skillin Road and Kathy Lane that are zoned as *Rural Residential 2*. As will be discussed in Section 3.3, the residential area homes along Kathy Lane are located in a direction that is hydraulically upgradient from the Site.

SME directed the drilling and installation of three groundwater monitoring wells and one temporary groundwater piezometer at the Site by New England Boring Contractors of Derry, New Hampshire (NEBC) on December 14 and 15, 2023. These monitoring locations are included as part of the existing Site conditions on Figure 2-1.





³ Website:

https://www.cumberlandmaine.com/sites/g/files/vyhlif9216/f/uploads/official_zoning_map_11x17_june_2022.pdf

\\SERVER\cts\Cumberland Real Estate Group\Rusty Lantern_Cumberland\Acad\Plans\BASE.dwg, FIG 2-1 - EXCON, 1/25/2024 9:44:30 AM, jrl



LEGEND

-  GROUNDWATER MONITORING WELL
-  TEMPORARY GROUNDWATER PIEZOMETER
-  PRIVATE WATER SUPPLY WELL
-  MAINE GEOLOGICAL SURVEY MAPPED WATER SUPPLY WELL

NOTES:

1. THIS PLAN SHOWS EXISTING SITE CONDITIONS AND GROUNDWATER MONITORING LOCATIONS FOR PROPOSED NEW UST FACILITY.
2. MAINE GEOLOGICAL SURVEY (MGS) MAPPED WATER SUPPLY WELL DATABASE IS UNDERSTOOD TO SHOW APPROXIMATE LOCATIONS AND NOT TO INCLUDE ALL WATER SUPPLY WELLS.
3. EXISTING AND PROPOSED PROPERTY BOUNDARIES SHOWN ARE APPROXIMATE.



FIGURE 2-1
EXISTING SITE CONDITIONS
PROPOSED RUSTY LANTERN MARKET
181 GRAY ROAD
CUMBERLAND, MAINE



2.2 Historical Site Use

As discussed further in Section 3.2, SME observed signs of historical Site petroleum-product-related contamination near the northwest corner of Lot 12 on December 14, 2023 during our hydrogeologic investigation. During soil drilling, a petroleum odor was observed in soils above the water table and in soil and groundwater at the water table. SME discussed these observations with CREG. Our observations prompted discussion between CREG and the current owner of the parcel. Based on anecdotal information provided by the current owner of Lot 12, the property was developed as a gas station in 1957 and operated as a gas station under different owners until 1989, at which time the tanks were removed. The property is also understood to have been used for an auto maintenance garage for several years prior to the current auto sales and service business located at the Site.

SME has been retained by CREG to provide a Phase 1 investigation for the Site, which is underway at the time of this reporting. Preliminary findings of the Phase 1 investigation include a UST facility registration for the former gas station located at Lot 12 and two spill reports. The UST facility registration indicates that there were previously four 4,000-gallon unleaded gasoline USTs, one 250-gallon kerosene UST, one 1,000-gallon diesel UST, and one 250-gallon waste oil UST located at the Site. All USTs are reported to have been removed from the Site. Significant soil contamination was reported to have been observed when at least two of the USTs were removed in 1989.

SME has been retained by CREG to characterize the baseline groundwater quality at the Site with respect to concentrations of volatile organic compounds (VOCs) and volatile petroleum hydrocarbons (VPH) at monitoring well MW-2, where apparent soil and groundwater contamination occurred. Groundwater samples will also be obtained hydraulically upgradient from MW-2 at monitoring well MW-3. SME is currently scheduled to sample the wells in early February 2024. The samples will be delivered to Alpha Analytical of Westborough, Massachusetts for laboratory analyses.

Based on information provided to SME by CREG, Lot 13 is not known to historically have had a permanent structure and has been used in the past for pre-manufactured cabins and sheds.

2.3 Area Groundwater Uses

The Site is located within a Town designated Aquifer Protection Zone for an aquifer with a yield of 10 to 50 gallons per minute (gpm). There are no Maine Department of Health and Human Services (MEDHHS) Drinking Water Program public drinking water supply wells mapped within the extents of the subject aquifer. The nearest public drinking water supply well to the Site is located approximately 2 miles to the north.

Area groundwater supply uses were assessed using the Maine Geological Survey (MGS) water well database. It is important to note that the MGS water well database is understood to provide approximations of well locations and to not be a complete representation of existing groundwater wells in the vicinity of the Site. In some cases, as discussed in more detail below, the locations of wells from the database appear to be incorrect.

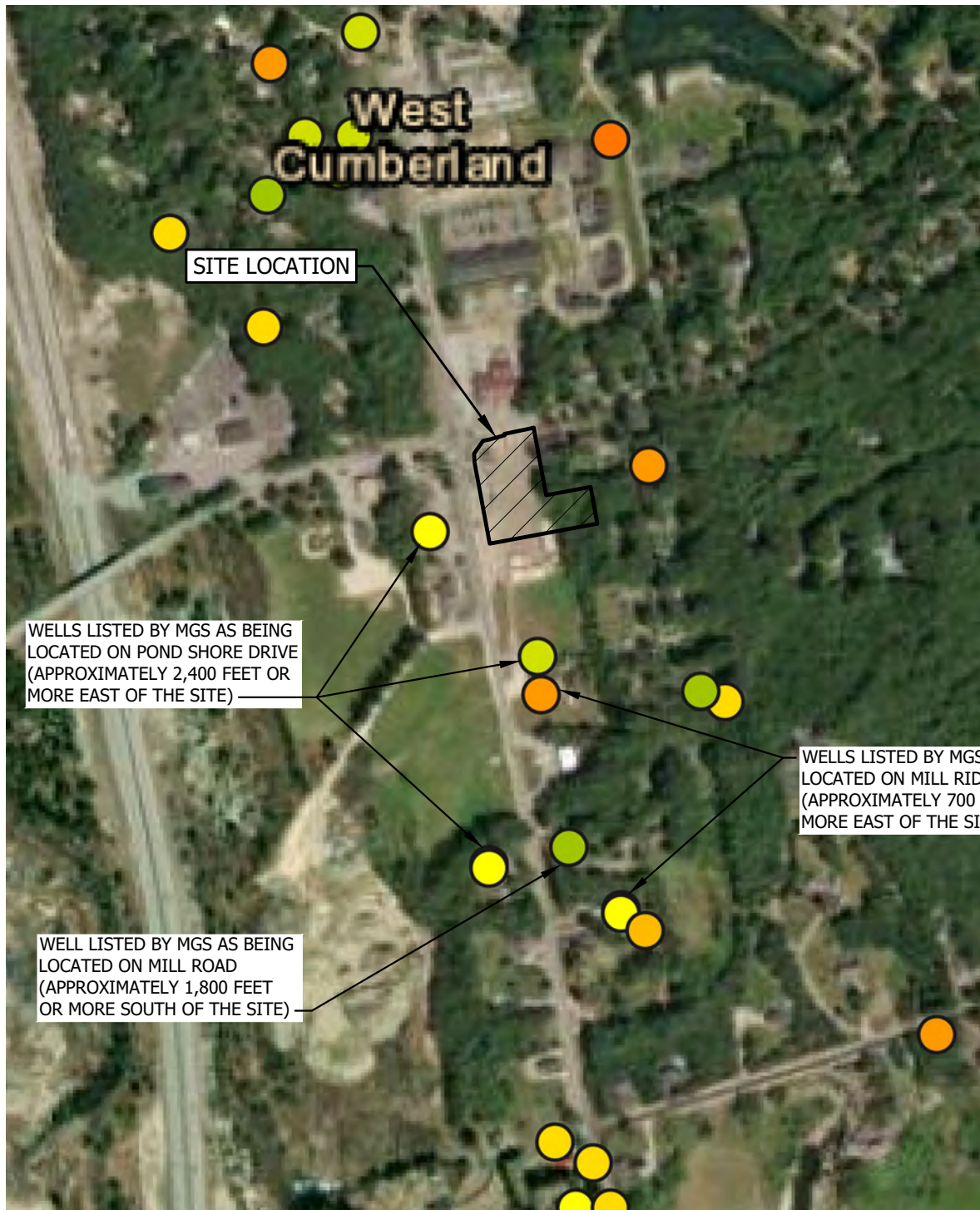
Figure 2-2 shows well locations in the vicinity of the Site that are included in the MGS water well database. Review of the database information for the wells included on Figure 2-2 indicate that multiple wells are located incorrectly based on the reported addresses for wells. Specifically, there are eight wells included on Figure 2-2 that are shown to be located along Route 100, south of the intersections with Skillin Road and Blackstrap Road, that appear to be located incorrectly. Four of these wells have addresses listed along Pond Shore Drive, which is located approximately 2,400 feet or more east of the Site. Three wells have address listed along Mill Ridge Road, which is located approximately 700 feet or more east of the Site. One of the wells has an address listed along Mill Road, which is located approximately 1,800 feet or more south of the Site. Route 100 (Gray Road) has a water utility line in the areas of these apparently mislocated wells.

It is probable that additional groundwater drinking water supply wells are located in the vicinity of the Site that are not included in the MGS water well database. The MEDEP rules for siting of oil storage facilities specifies wellhead protection zones of: (1) 300 feet from USTs for private drinking water wells; and (2) the greater of 1,000 feet from USTs to a public drinking water well or outside of the source water protection area of the well if mapped by the Maine Department of Health and Human Services.⁴

As discussed earlier in this section, the nearest public drinking water supply well is located approximately 2 miles north of the Site and the proposed UST is not located within a source water protection area designated by the MEDHHS drinking water program.

Based on information provided to SME by CREG, there are no private drinking water supply wells located on the subject properties (i.e., Lots 12 and 13). The nearest verified drinking water supply well location based on Site plan information provided to SME by CREG is located at 15 Kathy Lane (Tax Map U19, Lot 33). The drinking water supply well at 15 Kathy Lane is located more than 314 feet from the proposed UST location. SME recommends that locations of all potential drinking water supply wells on parcels located within 300 feet of the proposed UST location be verified with their respective property owners. This appears to include 7 Kathy Lane (Tax Map U19, Lot 35), 15 Kathy Lane (Tax Map U19, Lot 33), 5 Skillin Road (Tax Map U19, Lot 37), 169 Gray Road (Tax Map U19, Lot 14), 172 Gray Road (Tax Map U19, Lot 9), 176 Gray Road (Tax Map U19, Lot 10), 121 Blackstrap Road (Tax Map U19, Lot 11), and 115 Blackstrap

⁴ Maine Department of Environmental Protection. 06-096 CMR Chapter 692. Siting of Oil Storage Facilities. Effective Date: August 7, 2019 – filing 2019-116.



BASE MAP ADAPTED FROM MAINE GEOLOGICAL SURVEY (MGS) WATER WELL DATABASE

NOTE:

1. MAINE GEOLOGICAL SURVEY (MGS) MAPPED WATER SUPPLY WELL DATABASE IS UNDERSTOOD TO SHOW APPROXIMATE LOCATIONS AND NOT TO INCLUDE ALL WATER SUPPLY WELLS.



DWG: FIGURES

LMN: SOILS

CTB: SME-STD

REV: 1/23/2024

FIGURE 2-2
MAINE GEOLOGICAL SURVEY
WATER WELL DATABASE
PROPOSED RUSTY LANTERN MARKET
181 GRAY ROAD
CUMBERLAND, MAINE

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Road (Map R07, Lot 34A). It is possible that several of these properties do not have private drinking water wells since they have access to a water supply utility.

2.4 Area USTs

Based on the MEDHHS Drinking Water Program database, there are currently two sites within the same aquifer of the Site with active registered USTs. Budd's Gulf is located approximately 700 feet south of the Site at 161 Gray Road, Cumberland, Maine. There are currently two active registered USTs at Budd's Gulf, which have capacities of 8,000 gallons and 10,000 gallons. There are four 10,000-gallon active registered USTs located approximately 1,700 feet northwest of the Site at the Maine Turnpike southbound Mile 56 Service Area. Figure 2-3 shows the approximate locations of the USTs located at Budd's Gulf and at the Maine Turnpike southbound Mile 56 Service Area.


2.5 MEDEP UST Permitting

The MEDEP rules for the siting of oil storage facilities, Section 4, specifies a prohibition on facilities located on significant sand and gravel aquifers mapped by the MGS. As further discussed in Section 3.1, the Site is located in an area mapped by the MGS to be a moderate yield significant sand and gravel aquifer (i.e., generally yielding 10 or more gpm but no more than 50 gpm). The MEDEP rules for the siting of oil storage facilities, Section 4.D., indicates that a variance may be granted by MEDEP from the prohibition of USTs proposed in areas mapped as moderate yield significant sand and gravel aquifers provided that: (1) a MEDEP approved hydrogeologic evaluation demonstrates that the aquifer at the proposed facility generally yields 10 or more gpm but no more than 50 gpm; and (2) the proposed UST facility meets the design standards of Section 5 of the MEDEP rules for siting of oil facilities.

SME submitted a work plan to MEDEP in November 2023 for a hydrogeologic evaluation to assess the yield of the aquifer. Based on the Site background information provided in the work plan, the MEDEP waived the requirement of the hydrogeologic evaluation and stated that the project can be transitioned into the purview of engineering for the Site to ensure compliance with design standards. The December 6, 2023 correspondence between SME and MEDEP indicating the waiver for the requirement of the hydrogeologic evaluation is included in Appendix A.



BASE MAP ADAPTED FROM 7.5 MIN USGS TOPO QUADS
CUMBERLAND CENTER, ME - 2021

 APPROXIMATE LOCATION OF ACTIVE REGISTERED
UNDERGROUND OIL STORAGE TANK (MODIFIED FROM MAINE
DRINKING WATER DATABASE FOR ILLUSTRATIVE PURPOSES)



DWG: SITELOC

LMN: UST

CTB: SME-STD

REV: 1/24/2024

FIGURE 2-3
AREA USTs
PROPOSED RUSTY LANTERN MARKET
181 GRAY ROAD
CUMBERLAND, MAINE

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3.0 HYDROGEOLOGIC EVALUATION

SME's hydrogeologic evaluation for the Site is based on: (1) review of available data from literature and mapping in the vicinity of the Site; (2) a subsurface exploration program that included soil boring observations and well installations at four locations at the Site; and (3) measurements of groundwater levels and characteristics of the Site hydrogeology (e.g., hydraulic conductivity, saturated thickness of soils, groundwater flow direction, etc.). The general purpose of the evaluation is to provide Site specific information to develop an understanding of the volumetric rate, speed, and direction of groundwater flowing toward and away from the Site's proposed UST. The location proposed for the UST for the Site is shown on Figure 3-1.

3.1 MGS and USDA Mapping

Soils in the area of the proposed UST are classified as Hinkley loamy sand by the United States Department of Agriculture (USDA), as shown on Figure 3-2. Hinkley soils consist of deep, excessively drained, moderately coarse to coarse textured soils that form in glacial outwash deposits.⁵ The Maine Geological Survey (MGS) classifies the soils in the vicinity of the proposed UST as marine ice-contact delta deposits, which consist primarily of sorted and stratified sand and gravel, as shown on Figure 3-3.⁶ The proposed UST is located within an MGS mapped moderate yield significant sand and gravel aquifer, as shown on Figure 3-4.⁷

The bedrock underlying the Site and its vicinity are mapped by MGS as fine-grained to medium-grained biotite-quartz granofels. The MGS bedrock mapping at and in the vicinity of the Site is illustrated on Figure 3-5.⁸ There were no bedrock outcrops identified at the site.

3.2 Subsurface Explorations and Well Installations

Soil borings and well installations were completed at the Site at four locations by NEBC under the direction of SME on December 14 and 15, 2023. Groundwater monitoring wells MW-1, MW-2, and MW-3 were installed at three of the soil boring locations and temporary groundwater piezometer PZ-4 was installed at one of the soil boring locations. The locations of MW-1, MW-2, MW-3, and PZ-4 are shown on Figure 3-1. The locations of the soils borings and well installations are near the four corners of the cleared (i.e., deforested) portion of the proposed modified property boundaries (as approximately shown on Figure 3-1).

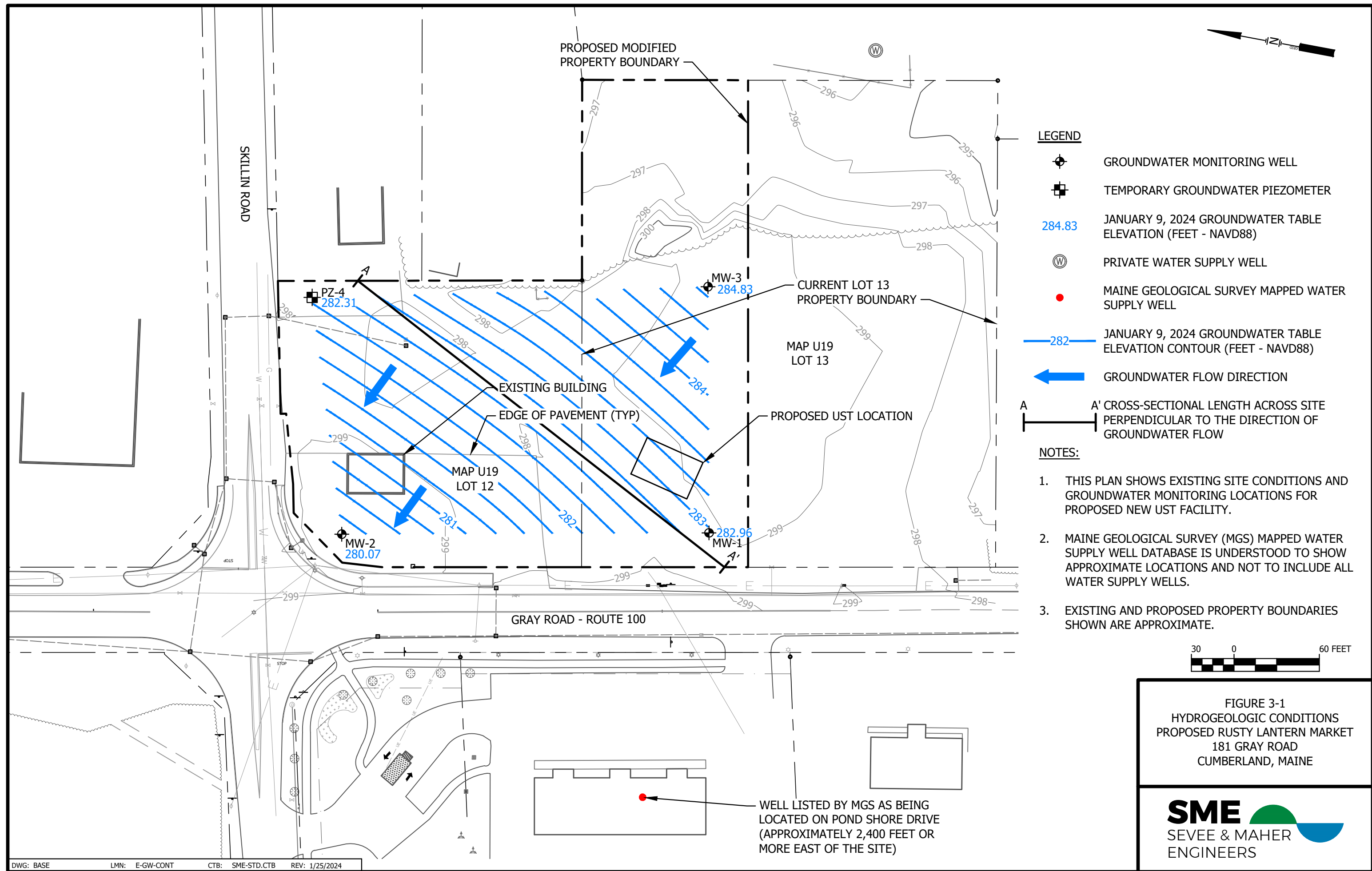
⁵ USDA, et. al. 1974. Soil Survey of Cumberland County, Maine.

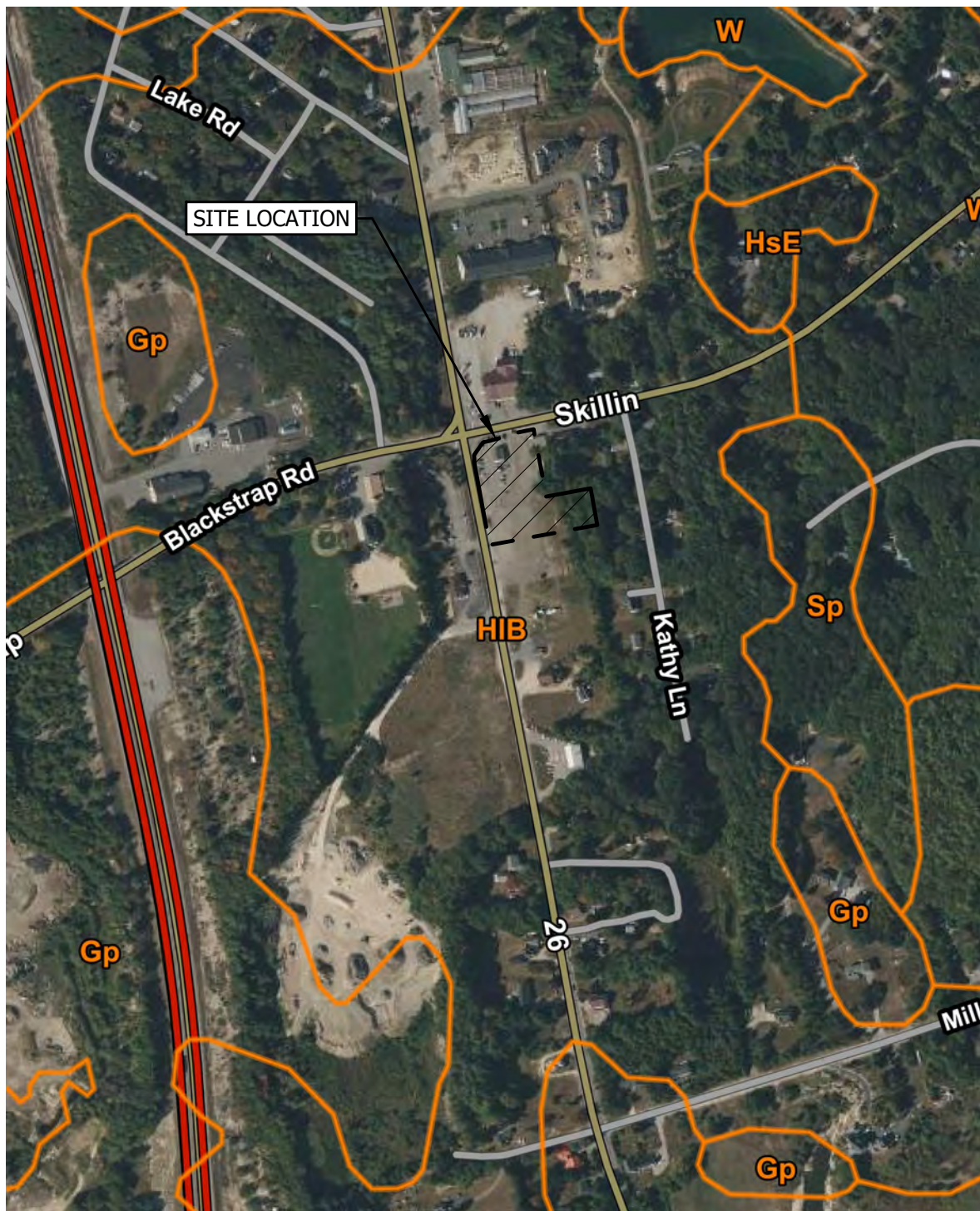
⁶ Retelle, Michael J. et. al., 1999. Surficial geology of the Cumberland Center quadrangle, Maine: Maine Geological Survey, Open-File Map 99-81, map, scale 1:24,000.

⁷ Neil, Craig D., et. al., 1999. Significant sand and gravel aquifers in the Cumberland Center quadrangle, Maine: Maine Geological Survey, Open-File Map 99-27, map, scale 1:24,000.

⁸ Engelman, Matthew R., Creasy, John W., and Berry, Henry N., IV, 2023. Bedrock geology of the Cumberland Center quadrangle, Maine: Maine Geological Survey, Open-File Map 23-14, map, scale 1:24,000.

\\nservet\cumberland Real Estate Group\Rusty Lantern_Cumberland\AcadPlans\BASE.dwg, FIG 3-1 - GW CONT, 1/25/2024 12:58:51 PM, jrl





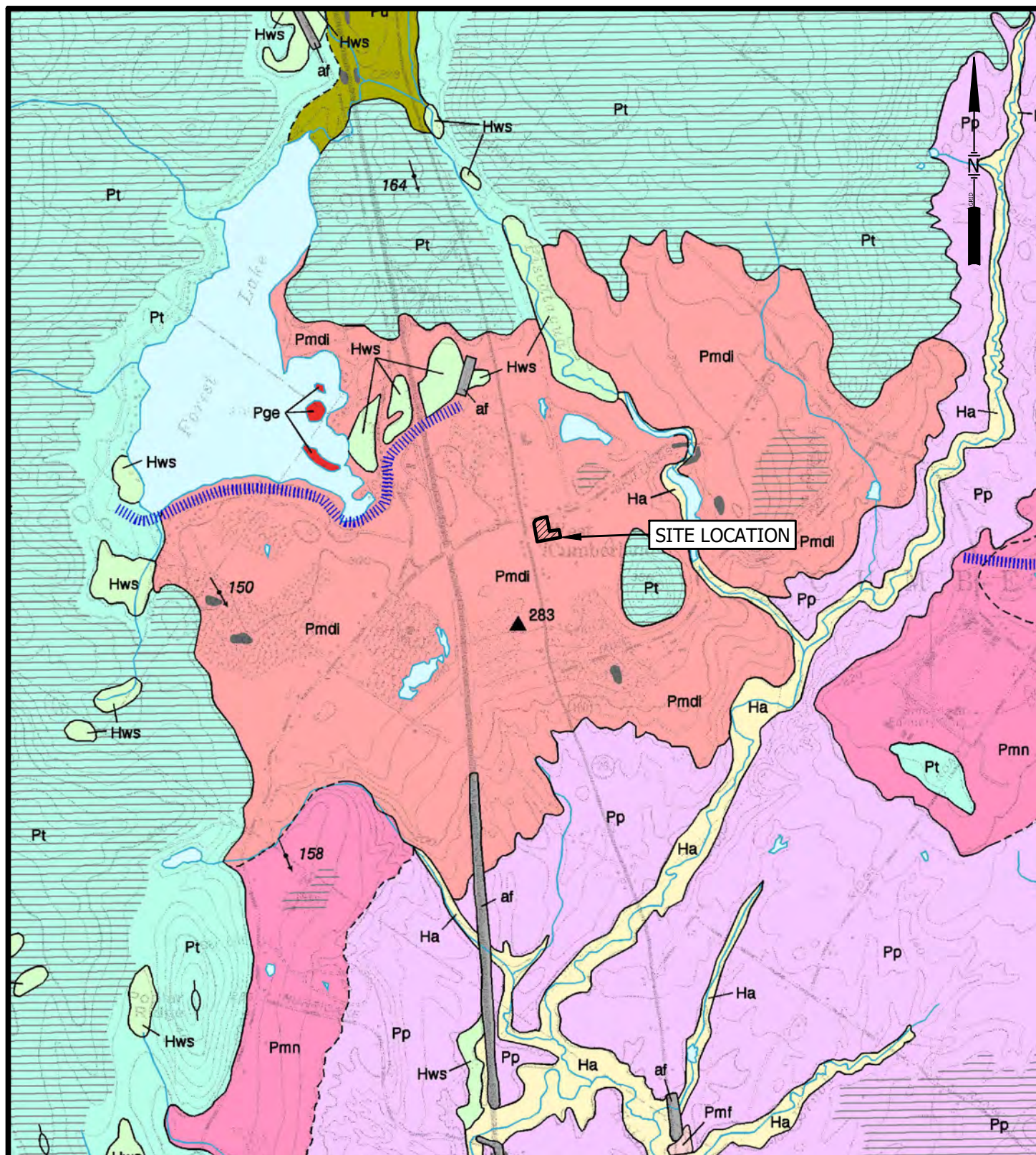
BASE MAP ADAPTED FROM WEB SOIL SURVEY SOILS MAPS

Gp - GRAVEL PITS
HIB - HINKLEY LOAMY SAND (8-15% SLOPES)
HsE - LYMAN-ABRAM COMPLEX (15-35% SLOPES, VERY ROCKY)
SP - SEBAGO MUCKY PEAT
W - WATER

FIGURE 3-2
USDA SOIL MAP
PROPOSED RUSTY LANTERN MARKET
181 GRAY ROAD
CUMBERLAND, MAINE



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ENGINEERS



Marine ice-contact delta - Ice-contact delta composed primarily of sorted and stratified sand and gravel. Deposit was graded to surface of late-glacial sea and is distinguished by flat top and foreset and topset beds.

BASE MAP ADAPTED FROM 7.5 MIN MGS SURFICIAL GEOLOGY QUAD
CUMBERLAND CENTER, ME - 1999



DWG: FIGURES

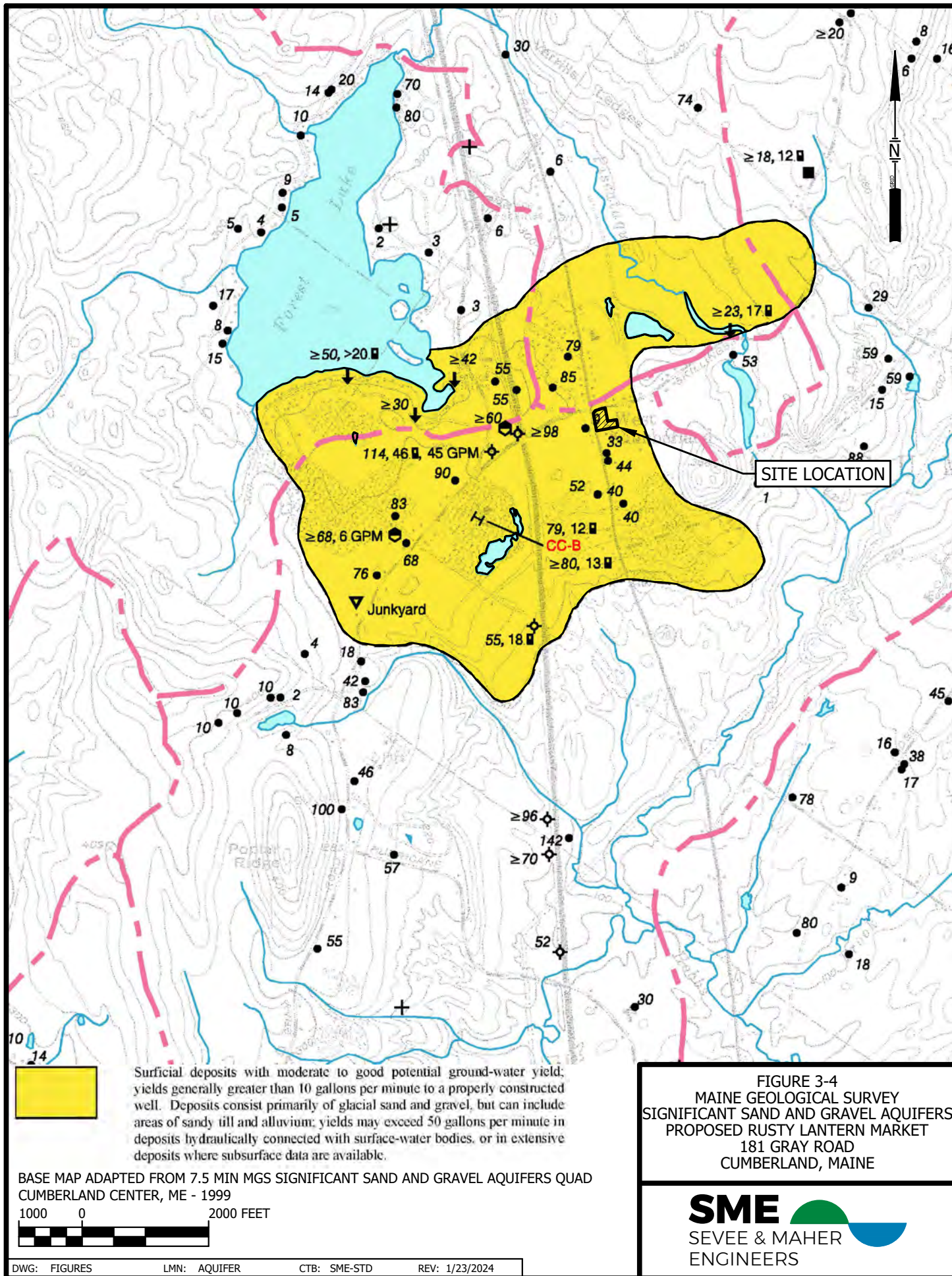
LMN: GEOLOGY

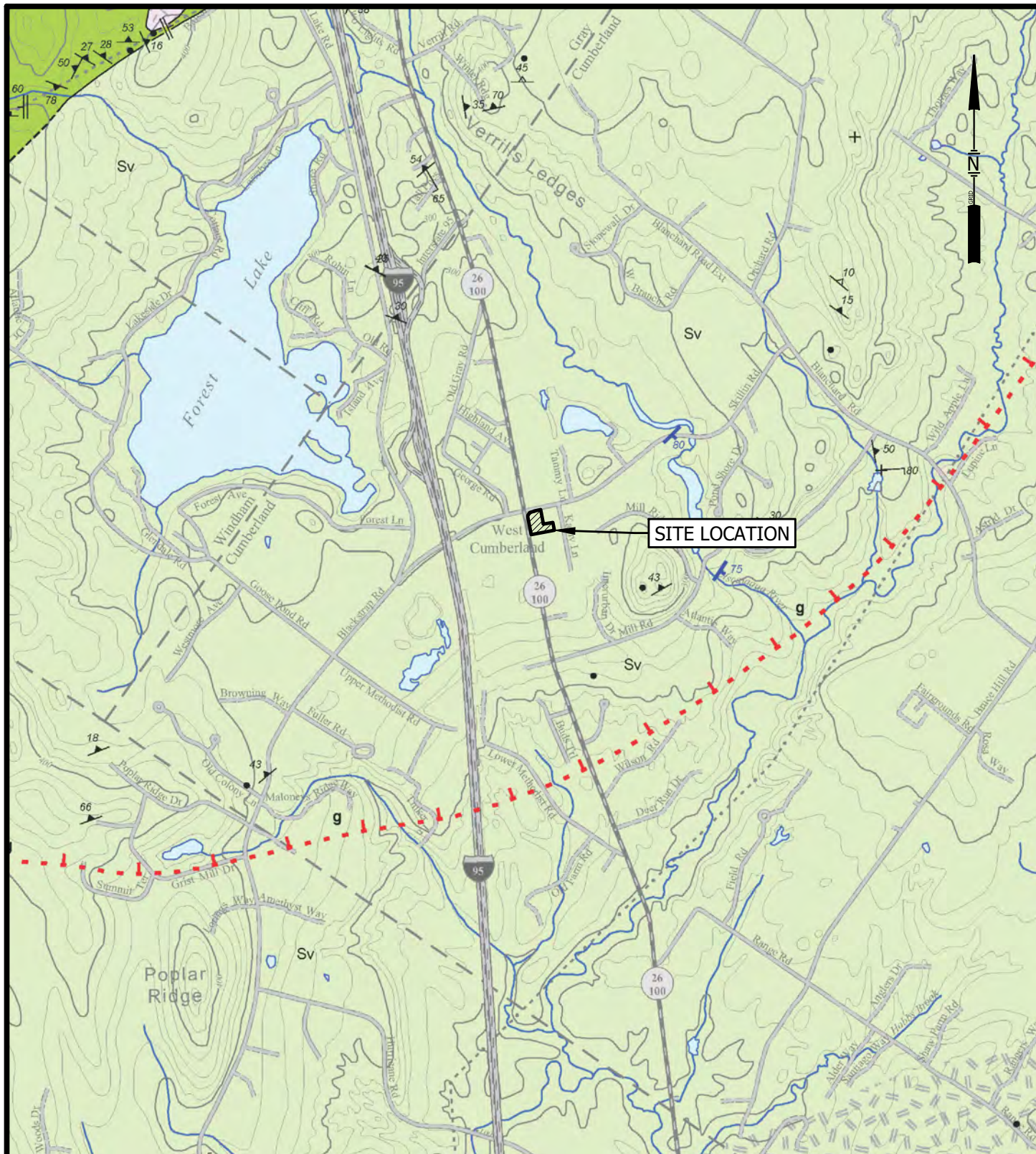
CTB: SME-STD

REV: 1/23/2024

FIGURE 3-3
MAINE GEOLOGICAL SURVEY SURFICIAL GEOLOGY
PROPOSED RUSTY LANTERN MARKET
181 GRAY ROAD
CUMBERLAND, MAINE

SME 
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ENGINEERS





STRATIFIED ROCKS

Silurian(?) [S]



Granofels, undifferentiated. Dark gray to medium gray, bluish gray or purplish gray, fine-grained to medium-grained biotite-quartz-feldspar granofels, interlayered with subordinate thin layers of light green to dark greenish-gray diopside calc-silicate granofels and dark gray, medium-grained biotite schist. The proportion of biotite schist is variable, from absent up to several meters in thickness. Layering in the granofels is generally well developed in thin to medium beds 3-20 centimeters (cm) thick. Where the rock is more highly migmatitic, and especially in the region of gneissic structure, the granofels is coarser grained.

BASE MAP ADAPTED FROM 7.5 MIN MGS BEDROCK QUAD
CUMBERLAND CENTER, ME - 2023



FIGURE 3-5
MAINE GEOLOGICAL SURVEY BEDROCK GEOLOGY
PROPOSED RUSTY LANTERN MARKET
181 GRAY ROAD
CUMBERLAND, MAINE

SME
SEVEE & MAHER
ENGINEERS

The soil borings were advanced using the drive and wash method with 4-inch diameter steel casing. Standard penetration test (SPT) sampling was completed generally at a frequency of every five feet.⁹ The soil observations across the Site were generally consistent with a compact gravelly sand surficial fill overlying loose sand and gravel soils. Silty clay lenses were observed in the saturated portion of the soil borings.

Explorations were completed to a depth of 27 feet below ground surface (ft-bgs) at MW-2 and MW-3 and 25 ft-bgs at PZ-4 without encountering bedrock refusal. Bedrock refusal was encountered at MW-1 at a depth of 22 ft-bgs.

Groundwater monitoring wells were installed in the borings that were completed for MW-1, MW-2, and MW-3 using 2-inch-diameter PVC screen and riser pipes. Filter sand was placed surrounding the well screens and bentonite seals were placed above the well screens. The tops of the monitoring wells were completed below ground surface and protected by the installation of road boxes. A temporary groundwater piezometer was installed for the boring complete for PZ-4 using 1-inch diameter PVC screen and riser pipe. Filter sand was placed surrounding the temporary groundwater piezometer and native gravelly sand backfill was placed surrounding the riser pipe.

The soil boring and well installation logs for MW-1, MW-2, MW-3, and PZ-4 are included as Appendix B.

SME surveyed the locations, ground surface elevations, and monitoring point (i.e., top of PVC riser pipe) elevations of the monitoring locations on December 20, 2023.

Table 3-1 provides a summary of the well installations.

TABLE 3-1
SUMMARY OF WELL INSTALLATIONS

ID	Easting (ft-NAD83)	Northing (ft-NAD83)	Ground Surface Elevation (ft-NAVD88)	Monitoring Point Elevation (ft-NAVD88)	Screen Bottom Depth (ft-bgs)	Screen Length (feet)	Screen Bottom Elevation (ft-NAVD88)	Screen Top Elevation (ft-NAVD88)
MW-1	2914057.68	357716.38	298.60	298.26	21.95	15	276.65	291.65
MW-2	2914009.44	357970.09	299.00	298.78	25.00	15	274.00	289.00
MW-3	2914227.8	357748.74	299.39	299.19	24.87	15	274.52	289.52
PZ-4	2914169.44	358021.13	297.77	297.63	22.62	10	275.15	285.15
Notes: ft-NAD83 – Maine State Plane Coordinate System West 1802 Zone NAD A121983 ft-NAVD88 – elevation in feet relative to the North American Vertical Datum of 1988 ft-bgs – feet below ground surface								

⁹ SPT sampling at MW-1 and MW-3 was started at a depth interval of 15 to 17 feet below ground surface since the Site groundwater table is at a depth of approximately 15 feet or more below ground surface.

As discussed earlier in Section 2.2, SME observed signs of Site petroleum product related contamination near the northwest corner of Lot 12 in the boring for MW-2 on December 14, 2023. During soil drilling, a petroleum odor was observed in soil from the SPT sample collected at 15 to 17 ft-bgs in the boring associated with MW-2. The odor was also observed in the drilling wash water. Upon making these observations, SME coordinated the delivery of soil and water containers and a photoionization detector (PID) for screening soil samples for the potential presence of VOCs in the airspace surrounding soil samples.

The airspace surrounding the soil samples collected at MW-2 were screened using the PID and the results included a detection of 1,268 parts per million (ppm) of compounds that are likely associated with the petroleum-like odor observed while drilling. The PID results for MW-2, as well as screening completed for MW-1, MW-3, and PZ-4, are included on the soil boring and well installation logs included in Appendix B. There were no PID detections observed in the airspace surrounding the soil samples from MW-1, MW-3, and PZ-4 (as discussed in Section 3.3, MW-2 is located at a corner of the property that is the most hydraulically downgradient of soil boring locations).

Soil cuttings and drilling wash water from the monitoring well MW-2 boring were contained in 55-gallon steel drums that are Department of Transportation (DOT) approved for transportation. The drums are labeled and are currently stored at the Site awaiting sampling and characterization by laboratory analyses, after which time they be properly disposed.

The source of the soil and groundwater contamination at monitoring well MW-2 appears to be from historical use of USTs at the Site for a gas station between 1957 and 1989. As discussed in Section 2.2, additional investigation into the Site's historical use and characterization of existing groundwater quality at the Site is in progress.

3.3 Groundwater Table Surface and Saturated Soil Summary

Static groundwater levels were measured by SME at groundwater monitoring wells MW-1, MW-2, and MW-3 and temporary groundwater piezometer PZ-4 on January 9, 2024. Table 3-2 provides a summary of the measured groundwater levels as well as the saturated soil conditions on January 9, 2024.

TABLE 3-2
SUMMARY OF JANUARY 9, 2024 GROUNDWATER ELEVATIONS AND SATURATED SOILS

ID	Depth to Groundwater from Monitoring Point (feet)	Depth of Groundwater Below Ground (ft-bgs)	Groundwater Elevation (ft-NAVD88)	Monitoring Point Elevation (ft-NAVD88)	Saturated Thickness of Screened Soil (feet)	Approximate Thickness of Saturated Silty Clay (feet)	Approximate Thickness of Saturated Sand & Gravel (feet)
MW-1	15.30	15.64	282.96	298.26	6.31	2.0	4.3
MW-2	18.71	18.93	280.07	298.78	6.07	0.9	5.2
MW-3	14.36	14.56	284.83	299.19	10.31	5.8	4.5
PZ-4	15.32	15.46	282.31	297.63	7.16	3.0	4.2
<u>Notes:</u> ft-NAVD88 – elevation in feet relative to the North American Vertical Datum of 1988 ft-bgs – feet below ground surface							

The groundwater elevations at monitoring locations MW-1, MW-2, MW-3, and PZ-4 were used to develop an interpreted groundwater table elevation contour map, which is shown on Figure 3-1. The groundwater is interpreted to flow across the Site from the southeast to the northwest. The hydraulic gradient (i.e., the slope of the groundwater table surface) is measured to be approximately 1.67 percent.

Based on the interpreted groundwater table elevation contours, the residences along Kathy Lane are in a direction that is hydraulically upgradient from the proposed UST location. Based on the MGS water well database mapping (see Figure 2-2) and our interpreted groundwater table elevation contours, the nearest residential wells in a down- or cross-gradient direction appear to be located northwest of the Site in an area zoned as Village Medium Density Residential by the Town. The nearest drinking water well in this area mapped on the MGS water well database is roughly 1,900 feet from the proposed UST location; however, it is important to remember that the MGS water well database is understood to be incomplete and there may be closer wells located hydraulically downgradient from the proposed UST.

The information from this hydrogeologic evaluation that was used to interpret the groundwater flow direction is limited to on-Site groundwater level measurements. It is probable that groundwater continues to flow away from the Site to the northwest proximate to the Site. Review of the MGS mapped surface water drainage divides (shown as dashed pink lines on Figure 3-4) suggest that the groundwater flow direction might shift to the northeast with greater distance from the Site since surface water drainage divides generally correlate with groundwater flow divides. If the groundwater flow direction does shift to the northeast with greater distance from the Site, then the groundwater discharge location would likely

be to the Piscataqua River at some location northeast of the intersection of Gray Road and Skillin Road. Additional exploration would be required to verify groundwater flow directions at greater distances from the Site.

3.4 Hydraulic Conductivity Testing (Slug Tests)

On January 9, 2024, SME conducted three rising head slug tests each at MW-1, MW-2, MW-3, and PZ-4. The groundwater level recoveries were measured at one-second to half-second intervals using pressure transducers. The slug test data were analyzed using the Bouwer & Rice method.¹⁰ The slug test groundwater level recovery data and analysis results are included in Appendix C. The slug test results are summarized in Table 3-3.

TABLE 3-3
SUMMARY OF SLUG TEST ANALYSES RESULTS

Well ID	Hydraulic Conductivity (ft/day)			
	Test 1	Test 2	Test 3	Average
MW-1	41.3	45.4	43.0	43.2
MW-2	32.8	32.2	32.0	32.3
MW-3	13.1	13.4	13.8	13.4
PZ-4	57.2	60.4	51.0	56.2
Average of All Results = 36.3 ft/day				
Notes: ft/day – feet per day				

The estimated hydraulic conductivity measurements in the area of investigation range from an average of 13.4 feet per day (ft/day) at MW-3 to 56.2 ft/day at PZ-4. The average hydraulic conductivity on a Site-wide basis is 36.3 ft/day.

3.5 Groundwater Flow

The average groundwater flow across the Site under static groundwater level conditions on January 9, 2024 is estimated using Darcy's law, which is an equation that describes the flow of a fluid through a porous medium.¹¹ Darcy's law is expressed as follows:

$$Q = KiA$$

where,

¹⁰ Bouwer, H. and Rice, P.C., 1976. A slug test method for determining hydraulic conductivity of unconfined aquifers with completely or partially penetrating wells, *Water Resources Research*, vol. 12, no. 3, pp. 423-428.

¹¹ Fetter, 1994. *Applied Hydrogeology*, 3rd Edition. *Prentice Hall*. p. 142

Q = volume of groundwater flow (cubic length per time)

K = hydraulic conductivity (length per time)

i = hydraulic gradient (length per length)

A = cross-sectional area of flow (square length)

As described in Section 3.4, the average estimated hydraulic conductivity across the Site, as determined from the results of slug test analyses, is 36.3 ft/day. The hydraulic gradient across the Site is 1.67 percent (0.0167 feet/feet), as described in Section 3.3.

The cross-sectional area of flow is estimated based on the length across the Site in a direction perpendicular to groundwater flow and the saturated thicknesses of the sand and gravel soil deposits observed at the borings associated with monitoring locations MW-1, MW-2, MW-3, and PZ-4. The length across the Site in a direction perpendicular to groundwater flow is illustrated on Figure 3-1 to be 327 feet along cross-sectional profile A-A'. The average of saturated thicknesses of sand and gravel deposits (excluding thicknesses of silt and clay lenses) at these monitoring locations is approximately 4.6 feet see Table 3-2). Thus, the estimated cross-sectional area of flow across the Site is estimated to be approximately 1,500 square feet (ft²).

Based on the observations and measurements from SME's hydrogeologic evaluation for the Site, the average groundwater flow across the Site under the static groundwater level conditions on January 9, 2024 is estimated using Darcy's law as follows:

$$Q = 36.3 \text{ ft/day} * 0.0167 \text{ feet/feet} * 1,500 \text{ ft}^2 = 909 \text{ cubic feet per day (ft}^3\text{/day) or 6,800 gallons per day (gpd)}$$

The average linear velocity of groundwater moving across the Site under the static groundwater level conditions observed on January 9, 2024 is estimated using the following equation:¹²

$$v = Ki/n_e$$

where,

v = average linear velocity (length per time)

K = hydraulic conductivity (length per time)

i = hydraulic gradient (length per length)

n_e = effective porosity (cubic length per cubic length)

¹² Fetter, 1994. Applied Hydrogeology, 3rd Edition. *Prentice Hall*. p. 142

The average estimated hydraulic conductivity and estimated hydraulic gradient across the Site are described above. The average effective porosity of the Site's sand and gravel deposits is estimated to be 0.25 (i.e., 25 percent).¹³ The average linear velocity of groundwater moving across the Site under the static groundwater level conditions on January 9, 2024 is estimated as follows:

$$v = (36.3 \text{ ft/day} * 0.0167 \text{ feet/feet}) / (0.25) = 2.4 \text{ ft/day}$$

Baseline knowledge of the volumetric flow rate and average linear velocity of groundwater movement in the area of the proposed UST is of value for current and/or future planning for protection of groundwater users located hydraulically downgradient from the proposed UST. An estimate of the average linear groundwater velocity in the area of the proposed UST can be used for establishing an appropriate frequency for detection groundwater quality monitoring that is protective of hydraulically downgradient groundwater users.

¹³ Fetter, 1994. Applied Hydrogeology, 3rd Edition. *Prentice Hall*. p. 91

4.0 SUMMARY, RECOMMENDATIONS, AND CONCLUSION

4.1 Summary

A summary of key points presented in this hydrogeologic evaluation for the proposed UST at the Site is provided below:

- MEDEP has waived the requirement for a hydrogeologic evaluation for a proposed UST located in a moderate yield significant sand and gravel aquifer and stated that the project can be transitioned into the purview of engineering for the Site to ensure compliance with design standards. The waiver was based on Site background information provided in a work plan for a hydrogeologic evaluation submitted to MEDEP in November 2023. The design standards required by MEDEP (from the MEDEP rules for siting an oil storage facility) for a variance from the prohibition of USTs located in a moderate yield significant sand and gravel aquifer require that the facility must be designed, installed, operated, and monitored with a combination of leak detection and spill prevention equipment, discharge monitoring equipment, or other engineering, operational and monitoring measurements that collectively are more stringent than state and federal requirements to minimize the risk of oil discharges and future groundwater contamination.
- There are existing USTs located within the subject aquifer northwest of the Site at the Maine Turnpike southbound Mile 56 Service Area and south of the Site at 161 Gray Road in Cumberland, Maine. Additionally, the proposed UST is in a location that is reportedly very close to a former gas station that used seven USTs that have since been removed. The existing presence of USTs in this area, as well as the historical use of USTs at the Site, suggest a low potential for this area of the aquifer as a public drinking water supply source area.
- SME's hydrogeologic evaluation provides a baseline understanding of the volumetric flow rate, average linear velocity, and direction of groundwater movement in the area of the UST, which is of value for current and/or future planning for protection of groundwater users located hydraulically downgradient from the proposed UST. The evaluation has indicated that groundwater moves away from the proposed UST location to the northwest at an average linear velocity of 2.4 ft/day. An estimate of the average linear groundwater velocity in the area of the proposed UST can be used for establishing an appropriate frequency for detection groundwater quality monitoring that is protective of hydraulically downgradient groundwater users.
- The MEDEP rules for siting of oil storage facilities specifies wellhead protection zones of: (1) 300 feet from USTs for private drinking water wells; and (2) the greater of 1,000 feet from USTs to a public drinking water well or outside of the source water protection area of the well if mapped by the Maine Department of Health and Human Services. The nearest public drinking water supply well is located approximately 2 miles north of the Site and the proposed UST is not located within a source water protection area designated by the MEDHHS drinking water program. The nearest

verified drinking water supply well location based on Site plan information provided to SME by CREG is located at 15 Kathy Lane (Tax Map U19, Lot 33). The drinking water supply well at 15 Kathy Lane is located more than 314 feet from the proposed UST location in a hydraulically upgradient direction.

4.2 Recommendations

SME recommends that locations of all potential drinking water supply wells on parcels located within 300 feet of the proposed UST location be verified with their respective property owners.

Based on the MGS water well database mapping (see Figure 2-2) and our interpreted groundwater table elevation contours, the nearest residential wells in a down- or cross-gradient direction appear to be located northwest of the Site in an area zoned as Village Medium Density Residential by the Town. The nearest drinking water well in this area mapped on the MGS water well database is roughly 1,900 feet from the proposed UST location; however, it is important to remember that the MGS water well database is understood to be incomplete and there may be closer wells located hydraulically downgradient from the proposed UST. SME recommends verification of the actual nearest hydraulically downgradient private drinking water supply well, which is likely to be located in the vicinity of the intersection of George and Blackstrap Roads.

4.3 Conclusion

Based on the information provided in this report, it is SME's opinion that, with the Site's commercial zoning and existing hydrogeologic setting, and the stringent UST design standards imposed for Site development by the Maine Department of Environmental Protection (MEDEP) for a proposed UST site located in a significant sand and gravel aquifer, the Site is suitable for the proposed storage of refined petroleum products.

APPENDIX A

MEDEP CORRESPONDENCE

Andrew Gobeil

From: Wehr, Daniel J <Daniel.J.Wehr@maine.gov>
Sent: Wednesday, December 6, 2023 4:30 PM
To: Lisa Jacob
Subject: FW: Scope of work for hydrogeologic evaluation

Hi Lisa,

Below is our evalua. on of the scope of work you provided last Wednesday. Please let us know what course SME decides to take.

Respectfully,

Dan J. Wehr, USCG Ret.

Environmental Specialist II
Maine Department of Environmental Protection
Bureau of Remediation and Waste Management
Marquardt Building 3rd floor
17 State House Station
Augusta, ME 04333
Office: 207-287-3547
<https://www.maine.gov/dep/>

From: Rodda, Charles I <Charles.I.Rodda@maine.gov>
Sent: Wednesday, December 6, 2023 1:51 PM
To: Wehr, Daniel J <Daniel.J.Wehr@maine.gov>; Dougherty, Sean <Sean.Dougherty@maine.gov>
Cc: Smith, Autumn G <Autumn.G.Smith@maine.gov>
Subject: RE: Scope of work for hydrogeologic evaluation

Good Afternoon, Dan.

I've reviewed the SME plan for work in support of a variance for UST installation over a sand and gravel aquifer at 161 Gray Rd. in Cumberland, ME. That area is currently mapped as a moderate yield aquifer and I see no reason to suspect that the current mapping is incorrect.

I see two options forward. First, the client can accept the moderate-yield-aquifer mapping, and agree to build the facility in a manner that meets design standards in Maine Chapter 692, Section 5. In that case, the proposed hydrogeologic evaluation scheduled for next week would be unnecessary, and this project can transition into the purview of engineering to ensure Section 5 compliance.

In the second option, the client may elect to go ahead with the hydrogeologic evaluation. If they do this, three outcomes are possible.

1. The evaluation indicates less-than-moderate potential yield. In that case, the Section 5 standards would not apply, and normal design standards could be used.
2. The evaluation indicates moderate yield, as mapped. In that case, they would need to use the Section 5 design standards, as mentioned above.
3. The evaluation indicates high potential yield. In that case, the variance they are requesting would be denied.

Please let me know if you want this evaluation submitted in a letter, if this email is sufficient for your needs, or something else. I wanted to put these thoughts in front of you quickly so that the client has time to cancel drilling, or make some other decision in a timely manner.

Feel free to reach out, or direct any of those involved in the project my way if anyone has further questions.

Cheers,
-Charles

From: Lisa Jacob <LJJ@smemaine.com>
Sent: Wednesday, November 29, 2023 5:14 PM
To: Wehr, Daniel J <Daniel.J.Wehr@maine.gov>
Cc: cneufeld@priorityrealestategroup.com; Andrew Gobeil <apg@smemaine.com>
Subject: Scope of work for hydrogeologic evaluation

EXTERNAL: This email originated from outside of the State of Maine Mail System. Do not click links or open attachments unless you recognize the sender and know the content is safe.

Hello Dan,

As discussed, we are providing the attached scope of work for a hydrogeological evaluation at the site of a proposed gasoline station in Cumberland, Maine. The proposed business is located within a significant sand and gravel aquifer as mapped by the Maine Geological Survey. The scope of work is intended to provide information to support a variance application for a new UST facility located over sand and gravel aquifers.

We understand that you will provide a review of this scope of work and we look forward to hearing from you. If we can answer any questions, please don't hesitate to contact me or Andrew Gobeil.

Thank you very much.

Regards,
Lisa

Lisa J. Jacob, L.G.
Principal/Senior Geologist



Sevee & Maher Engineers, Inc.

4 Blanchard Road, P.O. Box 85A

Cumberland, ME 04021

Office: 207.829.5016

Cell: 207.272.2275

Fax: 207.829.5692

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APPENDIX B

SOIL BORING AND WELL INSTALLATION LOGS

PROJECT: Proposed Rusty Lantern Market, Cumberland, Maine			JOB NO.: 231411		BORING NO. MW-1		
DATE STARTED: 12/15/2023		DATE FINISHED: 12/15/2023		DRILLING METHOD: Drive & Wash w/4" Casing (HSA to 15 feet BGS)			
GROUND SURFACE ELEVATION (FT): 298.60 ft-NAVD88		DRILLING CONTRACTOR: NE Boring Contractors			LOGGED BY: Sevee & Maher (APG)		
BOREHOLE DIA.: 4-inch		WELL SCREEN/RISER DIA.: 2-inch			SHEET 1 OF 1		
DEPTH (FT)	SAMPLE NO./PID	MATERIAL DESCRIPTION	Blows per 0.5 feet on Sampler	Recovery (ft/ft)		WELL LOG	DEPTH (FT)
0						Road Box	0
	0-5 feet BGS Auger Cuttings 0.0 ppm	0.0 to 2.0 feet: dark brown, loose, well sorted, fine to coarse sand (Fill) 2.0 to 5.0 feet: yellowish brown, loose, well sorted, fine to coarse sand				TOC 0.34 ft-BGS Below Ground	
	5-10 feet BGS Auger Cuttings 0.0 ppm	5.0 to 10.0 feet: dull yellowish brown, loose, well sorted, fine to coarse sand				Filter Sand	
10						Bentonite Seal (5.0 to 2.0 ft-BGS)	
	10-15 feet BGS Auger Cuttings 0.0 ppm	10.0 to 15.0 feet: light grayish brown, loose, well sorted, fine sand, some medium sand, little silt				2" Dia. Sch. 40 PVC Riser	10
	1D 0.0 ppm	15.0 to 17.0 feet: light grayish brown, loose, well sorted, fine sand	3-3-4-9	1.6/2.0		Filter Sand (22.4 to 5.0 ft-BGS)	
20		Clay in wash water at 19 feet BGS				2" Dia. Sch. 40 PVC Screen, No. 10 Slot, L=15 ft (22.4 to 7.4 ft-BGS)	20
	2D 0.0 ppm	20.0 to 22.0 feet: top 0.7 feet gray, medium stiff, silty clay; bottom 0.7 feet brown, medium dense, poorly sorted, gravelly medium to coarse sand	4-12-16-36	1.4/2.0			
		Rollercone from 22.0 to 22.4 feet into granofels bedrock					
		End of Exploration at 22.4 feet					
30							30
40							40
50							50

NOTES:

Monitoring point elevation for MW-1 = 298.26 feet NAVD88 (top of PVC casing)

Water level measured on 1/9/2024 at 12:24 PM: MW-1 = 15.30 feet below top PVC, 282.96 feet NAVD88 elevation

Soil Key

Fill

Stratified Sand and Gravel Deposits

Marine Silt and Clay


Bedrock

PROJECT: Proposed Rusty Lantern Market, Cumberland, Maine				JOB NO.: 231411		BORING NO. MW-2	
DATE STARTED: 12/14/2023		DATE FINISHED: 12/14/2023		DRILLING METHOD: Drive & Wash w/4" Casing			
GROUND SURFACE ELEVATION (FT): 299.00 ft-NAVD88		DRILLING CONTRACTOR: NE Boring Contractors			LOGGED BY: Sevee & Maher (JAP)		
BOREHOLE DIA.: 4-inch		WELL SCREEN/RISER DIA.: 2-inch			SHEET 1 OF 1		
DEPTH (FT)	SAMPLE NO./PID	MATERIAL DESCRIPTION	Blows per 0.5 feet on Sampler	Recovery (ft/ft)		WELL LOG	DEPTH (FT)
0						Road Box	0
		0.0-1.0 feet: auger through asphalt and base gravel				TOC 0.38 feet Below Ground	
	1D 0.1ppm	1.0-3.0 feet: brown to light brown, loose, poorly sorted, fine to medium sand, some gravel, trace silt	4-4-4-6	1.6/2.0		Filter Sand	
						Bentonite Seal (8.0 to 3.0 ft-BGS)	
	2D 0.1ppm	5.0-7.0 feet: top 0.2 feet same as above; bottom 1.6 feet loose, light yellowish born, well sorted, fine to medium sand	5-6-8-8	1.8/2.0		2" Dia. Sch. 40 PVC Riser	
10							10
	3D 0.2ppm	10.0-12.0 feet: top 0.2 feet light brown, loose, well sorted, coarse sand; bottom 0.8 feet light yellowish brown, loose, well sorted, very fine sand	4-5-7-8	1.0/2.0		Filter Sand (25.0 to 8.0 ft-BGS)	
	4D 1268ppm	15.0-17.0 feet: light brown-yellow orange, loose, well ported, very fine sand, thinly stratified, petroleum odor	6-7-8-11	1.4/2.0		2" Dia. Sch. 40 PVC Screen, No. 10 Slot, L=15 ft (25.0 to 10.0 ft-BGS)	
20							20
	5D 309ppm	20.0 to 22.0 feet: light brown-yellow orange, loose, well sorted, very fine sand, petroleum odor	8-10-13-12	1.2/2.0			
	6D 5.9ppm	25.0-27.0 feet: top 0.8 feet gray, medium dense, poorly sorted, very fine sand, silt, and clay; mid 0.9 feet greenish gray clay; bottom 0.1 feet light brown, loose, well sorted, fine sand	8-9-4-11	1.8/2.0			
		End of Exploration at 27 feet					
30							30

PROJECT: Proposed Rusty Lantern Market, Cumberland, Maine				JOB NO.: 231411		BORING NO. PZ-4		
DATE STARTED: 12/15/2023		DATE FINISHED: 12/15/2023		DRILLING METHOD: Drive & Wash w/4" Casing				
GROUND SURFACE ELEVATION (FT): 297.77 ft-NAVD88		DRILLING CONTRACTOR: NE Boring Contractors			LOGGED BY: Sevee & Maher (APG)			
BOREHOLE DIA.: 4-inch		WELL SCREEN/RISER DIA.: 1-inch			SHEET 1 OF 1			
DEPTH (FT)	SAMPLE NO./PID	MATERIAL DESCRIPTION		Blows per 0.5 feet on Sampler	Recovery (ft/ft)		WELL LOG	DEPTH (FT)
0								0
	1D 0.0 ppm	0.0 to 2.0 feet: top 0.8 feet dark brown, compact, well sorted, loamy sand (Fill); bottom 0.2 feet reddish brown, loose, poorly sorted, gravelly sandy loam		5-4-8-8	1.0/2.0		TOC 0.14 ft-BGS Below Ground	
							Native Sand Backfill	
	2D 0.0 ppm	5.0 to 7.0 feet: light brown, loose, poorly sorted, medium to coarse gravelly sand		5-5-4-4	1.1/2.0			
							1" Dia. Sch. 40 PVC Riser	
10								10
	3D 0.0 ppm	10.0 to 12.0 feet: top 0.5 feet brown, loose, well sorted, fine sand; bottom 1.5 feet light brown, loose, well sorted, very fine sand, little silt		4-4-4-5	1.8/2.0			
							Filter Sand (23.0 to 13.0 ft-BGS)	
	4D 0.0 ppm	15.0 to 17.0 feet: top 0.5 feet light brown, loose, well sorted, silty sand; bottom 1.2 feet light brown, loose, well sorted, fine to medium sand		4-8-8-10	1.7/2.0			
							1" Dia. Sch. 40 PVC Screen, No. 10 Slot, L=10 ft (23.0 to 13.0 ft-BGS)	
20		Clay in wash water at 20 feet						20
	5D 0.0 ppm	23.0 to 25.0 feet: gray, soft, silty clay		3-2-5-5	1.6/2.0			
		End of Exploration at 25.0 feet						
30								30
40								40
50								50
NOTES:				Soil Key				
Monitoring point elevation for PZ-4 = 297.63 feet NAVD88 (top of PVC casing)				<div><div></div> Fill</div>				
Water level measured on 1/9/2024 at 11:56 AM: PZ-4 = 15.46 feet below top PVC, 282.31 feet NAVD88 elevation				<div><div></div> Stratified Sand and Gravel Deposits</div>				
				<div><div></div> Marine Silt and Clay</div>				
				<div><div></div> Bedrock</div>				

APPENDIX C

SLUG TEST ANALYSES RESULTS

<div>  <div> Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine </div> </div>			<div> <div>Slug Test - Water Level Data</div> <div>Page 1 of 2</div> </div>	
			Project: Rusty Lantern Market	
			Number: 231411	
			Client: Cumberland Real Estate Group	
Location: 181 Gray Road, Cumberland		Slug Test: MW-1 Test 1		Test Well: MW-1
Test Conducted by: APG		Test Date: 1/9/2024		
Water level at t=0 [ft]: 1.64		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 1.64
	Time [s]	Water Level [ft]	WL Change [ft]	
1	0.744	1.6424	1.6424	
2	1	0.7785	0.7785	
3	1.747	1.3144	1.3144	
4	2	1.2243	1.2243	
5	2.748	0.9748	0.9748	
6	3	0.9101	0.9101	
7	3.779	0.7277	0.7277	
8	4	0.6838	0.6838	
9	4.792	0.5521	0.5521	
10	5	0.5151	0.5151	
11	5.794	0.4274	0.4274	
12	6	0.4042	0.4042	
13	6.812	0.3326	0.3326	
14	7	0.3188	0.3188	
15	7.5	0.2864	0.2864	
16	8	0.2495	0.2495	
17	8.5	0.2287	0.2287	
18	9	0.2056	0.2056	
19	9.5	0.1894	0.1894	
20	10	0.1732	0.1732	
21	10.5	0.1663	0.1663	
22	11	0.1525	0.1525	
23	11.5	0.1478	0.1478	
24	12	0.1386	0.1386	
25	12.5	0.134	0.134	
26	13	0.1247	0.1247	
27	13.5	0.1201	0.1201	
28	14	0.1132	0.1132	
29	14.5	0.1086	0.1086	
30	15	0.104	0.104	
31	15.5	0.1016	0.1016	
32	16	0.0947	0.0947	
33	16.5	0.0901	0.0901	
34	17	0.0901	0.0901	
35	17.5	0.0855	0.0855	
36	18.028	0.0809	0.0809	
37	18.5	0.0809	0.0809	
38	19	0.0762	0.0762	
39	19.5	0.0716	0.0716	
40	20	0.067	0.067	
41	20.5	0.067	0.067	
42	21	0.0647	0.0647	
43	21.5	0.0601	0.0601	
44	22	0.0578	0.0578	
45	22.5	0.0578	0.0578	
46	23	0.0531	0.0531	
47	23.5	0.0554	0.0554	
48	24	0.0508	0.0508	
49	24.5	0.0485	0.0485	
50	25	0.0462	0.0462	
51	25.5	0.0462	0.0462	
52	26	0.0439	0.0439	
53	26.5	0.0439	0.0439	



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Slug Test - Water Level Data

Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

	Time [s]	Water Level [ft]	WL Change [ft]
54	27	0.0416	0.0416
55	27.5	0.037	0.037
56	28	0.0347	0.0347
57	28.5	0.0347	0.0347
58	29	0.0323	0.0323
59	29.5	0.0323	0.0323
60	30	0.03	0.03
61	30.5	0.0254	0.0254
62	31	0.03	0.03
63	31.5	0.0254	0.0254
64	32	0.0231	0.0231
65	32.5	0.0231	0.0231
66	33	0.0231	0.0231
67	33.5	0.0208	0.0208
68	34	0.0185	0.0185
69	34.5	0.0185	0.0185
70	35.002	0.0185	0.0185
71	35.5	0.0185	0.0185
72	36.005	0.0185	0.0185
73	36.5	0.0139	0.0139
74	37.008	0.0162	0.0162
75	37.5	0.0162	0.0162
76	38.011	0.0139	0.0139
77	38.5	0.0139	0.0139
78	39.014	0.0139	0.0139
79	39.5	0.0139	0.0139
80	40.032	0.0092	0.0092
81	40.5	0.0139	0.0139



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

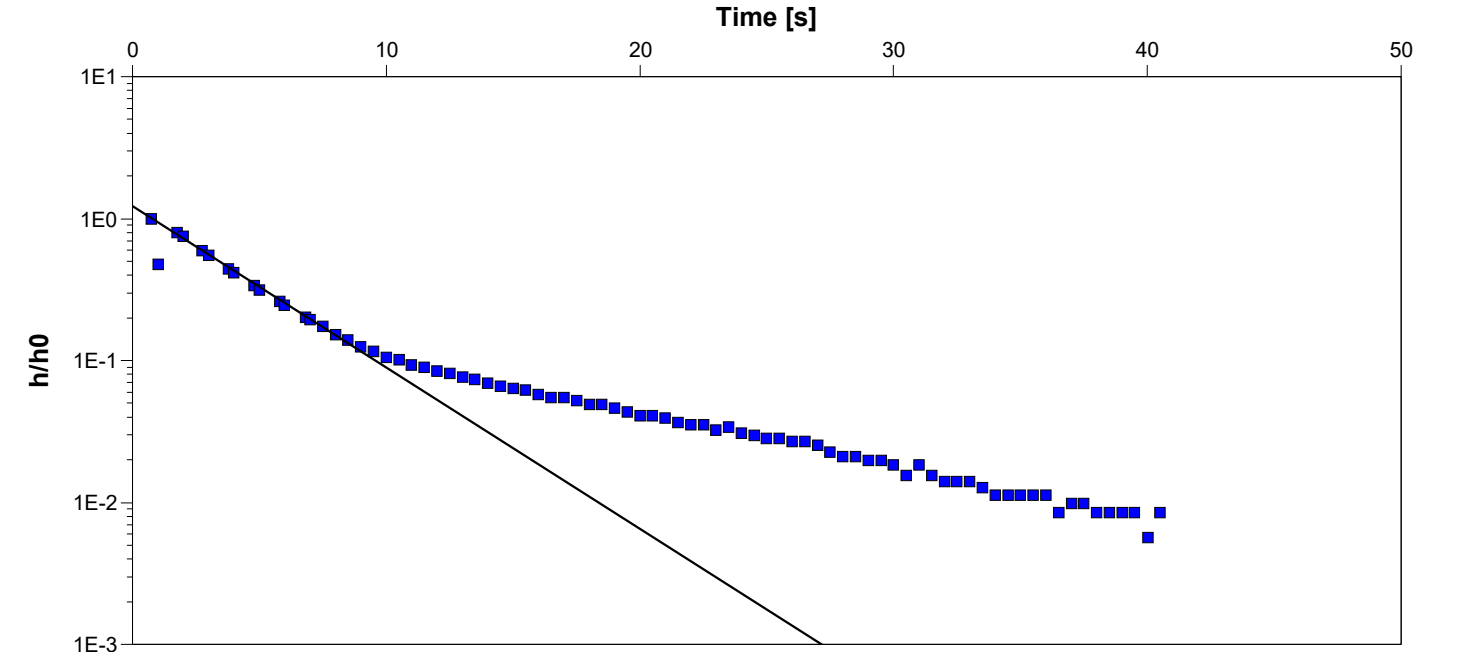
Slug Test Analysis Report

Project: Rusty Lantern Market


Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: MW-1 Test 1	Test Well: MW-1
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	MW-1 Test 1	Analysis Date: 1/21/2024
Aquifer Thickness: 6.31 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
MW-1	4.13×10^1	

<div>  <div> Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine </div> </div>			Slug Test - Water Level Data <div>Page 1 of 3</div>	
			Project: Rusty Lantern Market	
			Number: 231411	
			Client: Cumberland Real Estate Group	
Location: 181 Gray Road, Cumberland		Slug Test: MW-1 Test 2		Test Well: MW-1
Test Conducted by: APG		Test Date: 1/9/2024		
Water level at t=0 [ft]: 1.29		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 1.29
	Time [s]	Water Level [ft]	WL Change [ft]	
1	0.341	1.2913	1.2913	
2	1.005	1.0349	1.0349	
3	1.341	0.9309	0.9309	
4	1.998	0.7623	0.7623	
5	2.341	0.6768	0.6768	
6	3.001	0.5683	0.5683	
7	3.341	0.5151	0.5151	
8	4.003	0.432	0.432	
9	4.341	0.3927	0.3927	
10	5.022	0.3303	0.3303	
11	5.341	0.3119	0.3119	
12	6.04	0.2587	0.2587	
13	6.341	0.2449	0.2449	
14	7.043	0.2171	0.2171	
15	7.341	0.2056	0.2056	
16	8.045	0.1871	0.1871	
17	8.341	0.1825	0.1825	
18	9.049	0.1686	0.1686	
19	9.341	0.164	0.164	
20	10.05	0.1502	0.1502	
21	10.341	0.1502	0.1502	
22	11.069	0.1409	0.1409	
23	11.341	0.1363	0.1363	
24	12.09	0.1317	0.1317	
25	12.341	0.1271	0.1271	
26	13.103	0.1224	0.1224	
27	13.341	0.1201	0.1201	
28	14.106	0.1132	0.1132	
29	14.341	0.1109	0.1109	
30	15.116	0.1063	0.1063	
31	15.341	0.1063	0.1063	
32	16.132	0.0993	0.0993	
33	16.341	0.0993	0.0993	
34	17.156	0.0924	0.0924	
35	17.341	0.0924	0.0924	
36	18.159	0.0878	0.0878	
37	18.341	0.0855	0.0855	
38	19.162	0.0832	0.0832	
39	19.341	0.0832	0.0832	
40	20.165	0.0785	0.0785	
41	20.341	0.0762	0.0762	
42	20.841	0.0785	0.0785	
43	21.341	0.0716	0.0716	
44	21.841	0.067	0.067	
45	22.341	0.067	0.067	
46	22.841	0.067	0.067	
47	23.341	0.067	0.067	
48	23.841	0.0624	0.0624	
49	24.341	0.0624	0.0624	
50	24.841	0.0578	0.0578	
51	25.341	0.0578	0.0578	
52	25.841	0.0554	0.0554	
53	26.341	0.0554	0.0554	

	Time [s]	Water Level [ft]	WL Change [ft]
54	26.841	0.0554	0.0554
55	27.341	0.0554	0.0554
56	27.841	0.0485	0.0485
57	28.341	0.0508	0.0508
58	28.841	0.0462	0.0462
59	29.341	0.0462	0.0462
60	29.841	0.0462	0.0462
61	30.341	0.0462	0.0462
62	30.841	0.0462	0.0462
63	31.341	0.0416	0.0416
64	31.841	0.0416	0.0416
65	32.341	0.0416	0.0416
66	32.841	0.0416	0.0416
67	33.341	0.0416	0.0416
68	33.841	0.037	0.037
69	34.341	0.0416	0.0416
70	34.841	0.037	0.037
71	35.341	0.0347	0.0347
72	35.841	0.037	0.037
73	36.341	0.03	0.03
74	36.841	0.0323	0.0323
75	37.341	0.0347	0.0347
76	37.841	0.0323	0.0323
77	38.341	0.0323	0.0323
78	38.841	0.03	0.03
79	39.341	0.03	0.03
80	39.841	0.0323	0.0323
81	40.341	0.03	0.03
82	40.841	0.0277	0.0277
83	41.341	0.0277	0.0277
84	41.841	0.0254	0.0254
85	42.341	0.0254	0.0254
86	42.841	0.0277	0.0277
87	43.341	0.0231	0.0231
88	43.841	0.0277	0.0277
89	44.341	0.0231	0.0231
90	44.841	0.0231	0.0231
91	45.341	0.0254	0.0254
92	45.841	0.0254	0.0254
93	46.341	0.0231	0.0231
94	46.841	0.0231	0.0231
95	47.341	0.0231	0.0231
96	47.841	0.0231	0.0231
97	48.341	0.0231	0.0231
98	48.841	0.0208	0.0208
99	49.341	0.0208	0.0208
100	49.841	0.0208	0.0208
101	50.341	0.0185	0.0185
102	50.841	0.0231	0.0231
103	51.341	0.0162	0.0162
104	51.841	0.0162	0.0162
105	52.341	0.0185	0.0185
106	52.841	0.0162	0.0162
107	53.347	0.0139	0.0139
108	53.841	0.0185	0.0185
109	54.366	0.0162	0.0162
110	54.841	0.0185	0.0185
111	55.368	0.0185	0.0185



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

	Time [s]	Water Level [ft]	WL Change [ft]
112	55.841	0.0162	0.0162
113	56.378	0.0162	0.0162
114	56.841	0.0139	0.0139
115	57.397	0.0139	0.0139
116	57.841	0.0162	0.0162
117	58.399	0.0139	0.0139
118	58.841	0.0139	0.0139
119	59.402	0.0139	0.0139
120	59.841	0.0139	0.0139
121	60.405	0.0139	0.0139
122	60.841	0.0139	0.0139
123	61.429	0.0139	0.0139
124	61.841	0.0139	0.0139
125	62.448	0.0116	0.0116
126	62.841	0.0116	0.0116
127	63.45	0.0139	0.0139
128	63.841	0.0116	0.0116
129	64.453	0.0116	0.0116
130	64.841	0.0139	0.0139
131	65.472	0.0116	0.0116
132	65.841	0.0139	0.0139
133	66.491	0.0116	0.0116
134	66.841	0.0116	0.0116



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Slug Test Analysis Report

Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland

Slug Test: MW-1 Test 2

Test Well: MW-1

Test Conducted by: APG

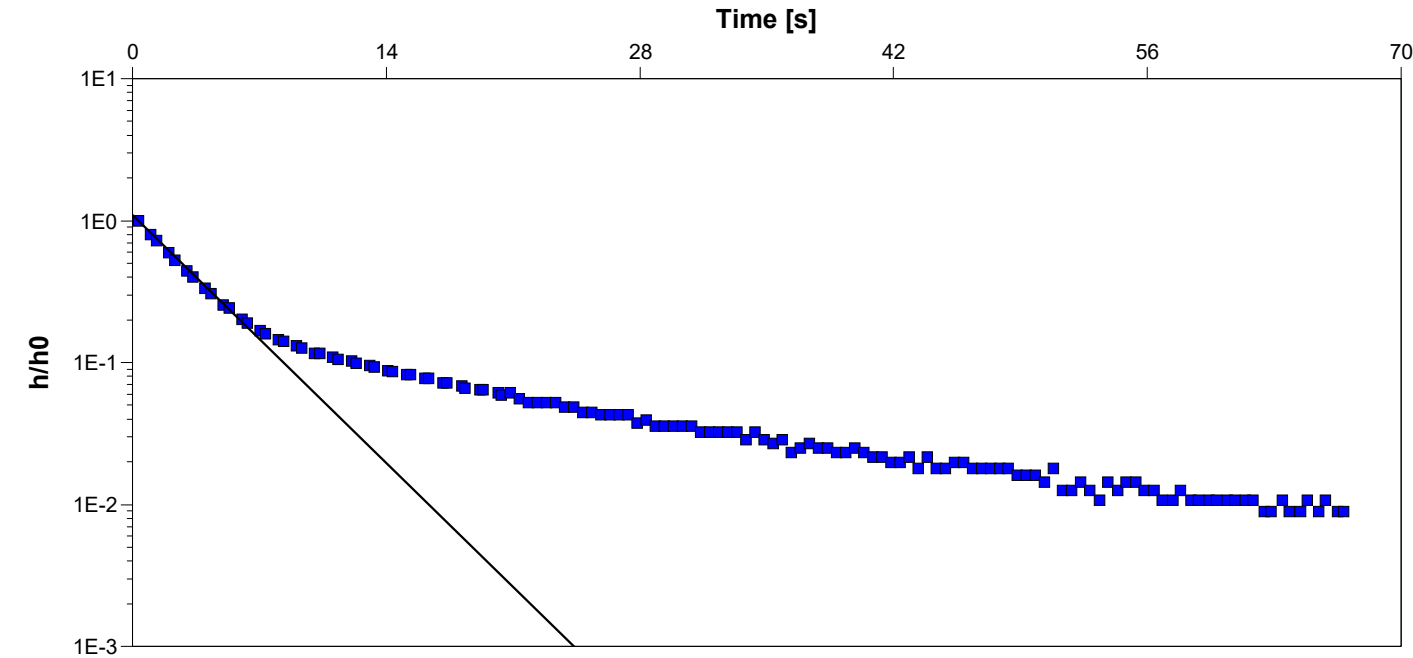
Test Date: 1/9/2024

Analysis Performed by: APG

MW-1 Test 2

Analysis Date: 1/21/2024

Aquifer Thickness: 6.31 ft




Calculation using Bouwer & Rice

Observation Well

Hydraulic Conductivity
[ft/d]

MW-1

4.54×10^1

<div>  <div> Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine </div> </div>			Slug Test - Water Level Data <div>Page 1 of 3</div>	
			Project: Rusty Lantern Market	
			Number: 231411	
			Client: Cumberland Real Estate Group	
Location: 181 Gray Road, Cumberland		Slug Test: MW-1 Test 3		Test Well: MW-1
Test Conducted by: APG		Test Date: 1/9/2024		
Water level at t=0 [ft]: 2.24		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 2.24
	Time [s]	Water Level [ft]	WL Change [ft]	
1	0.282	2.2384	2.2384	
2	1.002	1.2451	1.2451	
3	1.282	1.1296	1.1296	
4	2.021	0.9009	0.9009	
5	2.282	0.827	0.827	
6	3.026	0.6607	0.6607	
7	3.282	0.6168	0.6168	
8	4.029	0.5013	0.5013	
9	4.282	0.4666	0.4666	
10	5.03	0.3742	0.3742	
11	5.282	0.3534	0.3534	
12	6.032	0.298	0.298	
13	6.282	0.2795	0.2795	
14	7.036	0.2402	0.2402	
15	7.282	0.2287	0.2287	
16	8.039	0.2033	0.2033	
17	8.282	0.201	0.201	
18	9.058	0.1802	0.1802	
19	9.282	0.1779	0.1779	
20	10.06	0.1594	0.1594	
21	10.282	0.1571	0.1571	
22	11.062	0.1478	0.1478	
23	11.282	0.1432	0.1432	
24	12.065	0.1363	0.1363	
25	12.282	0.1317	0.1317	
26	13.084	0.1247	0.1247	
27	13.282	0.1224	0.1224	
28	14.087	0.1132	0.1132	
29	14.282	0.1132	0.1132	
30	15.089	0.1063	0.1063	
31	15.282	0.104	0.104	
32	16.1	0.0993	0.0993	
33	16.282	0.0947	0.0947	
34	16.782	0.0947	0.0947	
35	17.282	0.0901	0.0901	
36	18.095	0.0855	0.0855	
37	18.282	0.0878	0.0878	
38	18.782	0.0832	0.0832	
39	19.282	0.0832	0.0832	
40	19.782	0.0762	0.0762	
41	20.282	0.0762	0.0762	
42	20.782	0.0739	0.0739	
43	21.282	0.0693	0.0693	
44	21.782	0.0693	0.0693	
45	22.282	0.0647	0.0647	
46	22.782	0.0624	0.0624	
47	23.282	0.0624	0.0624	
48	23.783	0.0624	0.0624	
49	24.282	0.0554	0.0554	
50	24.782	0.0554	0.0554	
51	25.282	0.0578	0.0578	
52	25.782	0.0531	0.0531	
53	26.282	0.0508	0.0508	



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Slug Test - Water Level Data

Page 2 of 3

Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

	Time [s]	Water Level [ft]	WL Change [ft]
54	26.782	0.0485	0.0485
55	27.282	0.0485	0.0485
56	27.782	0.0508	0.0508
57	28.282	0.0485	0.0485
58	28.782	0.0462	0.0462
59	29.282	0.0462	0.0462
60	29.782	0.0439	0.0439
61	30.282	0.0439	0.0439
62	30.782	0.0416	0.0416
63	31.282	0.037	0.037
64	31.782	0.0393	0.0393
65	32.282	0.0393	0.0393
66	32.782	0.0347	0.0347
67	33.282	0.037	0.037
68	33.782	0.0393	0.0393
69	34.282	0.0347	0.0347
70	34.782	0.0323	0.0323
71	35.282	0.0323	0.0323
72	35.782	0.0347	0.0347
73	36.282	0.03	0.03
74	36.782	0.0347	0.0347
75	37.282	0.0323	0.0323
76	37.782	0.03	0.03
77	38.282	0.03	0.03
78	38.782	0.03	0.03
79	39.282	0.03	0.03
80	39.782	0.03	0.03
81	40.282	0.0254	0.0254
82	40.782	0.0231	0.0231
83	41.282	0.0254	0.0254
84	41.782	0.0254	0.0254
85	42.282	0.0208	0.0208
86	42.782	0.0254	0.0254
87	43.282	0.0254	0.0254
88	43.782	0.0277	0.0277
89	44.282	0.0254	0.0254
90	44.782	0.0208	0.0208
91	45.282	0.0208	0.0208
92	45.782	0.0231	0.0231
93	46.282	0.0185	0.0185
94	46.782	0.0208	0.0208
95	47.282	0.0185	0.0185
96	47.782	0.0185	0.0185
97	48.282	0.0185	0.0185
98	48.782	0.0208	0.0208
99	49.282	0.0185	0.0185
100	49.782	0.0162	0.0162
101	50.282	0.0162	0.0162
102	50.782	0.0162	0.0162
103	51.282	0.0185	0.0185
104	51.782	0.0162	0.0162
105	52.282	0.0185	0.0185
106	52.782	0.0162	0.0162
107	53.282	0.0185	0.0185
108	53.782	0.0162	0.0162
109	54.282	0.0162	0.0162
110	54.782	0.0139	0.0139
111	55.282	0.0185	0.0185



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

	Time [s]	Water Level [ft]	WL Change [ft]
112	55.782	0.0162	0.0162
113	56.282	0.0139	0.0139
114	56.782	0.0116	0.0116
115	57.282	0.0139	0.0139
116	57.782	0.0139	0.0139
117	58.282	0.0116	0.0116
118	58.782	0.0116	0.0116
119	59.282	0.0116	0.0116
120	59.782	0.0139	0.0139
121	60.282	0.0139	0.0139
122	60.782	0.0116	0.0116
123	61.282	0.0139	0.0139
124	61.782	0.0139	0.0139
125	62.282	0.0139	0.0139
126	62.782	0.0092	0.0092
127	63.282	0.0116	0.0116
128	63.782	0.0139	0.0139
129	64.282	0.0139	0.0139
130	64.782	0.0116	0.0116



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

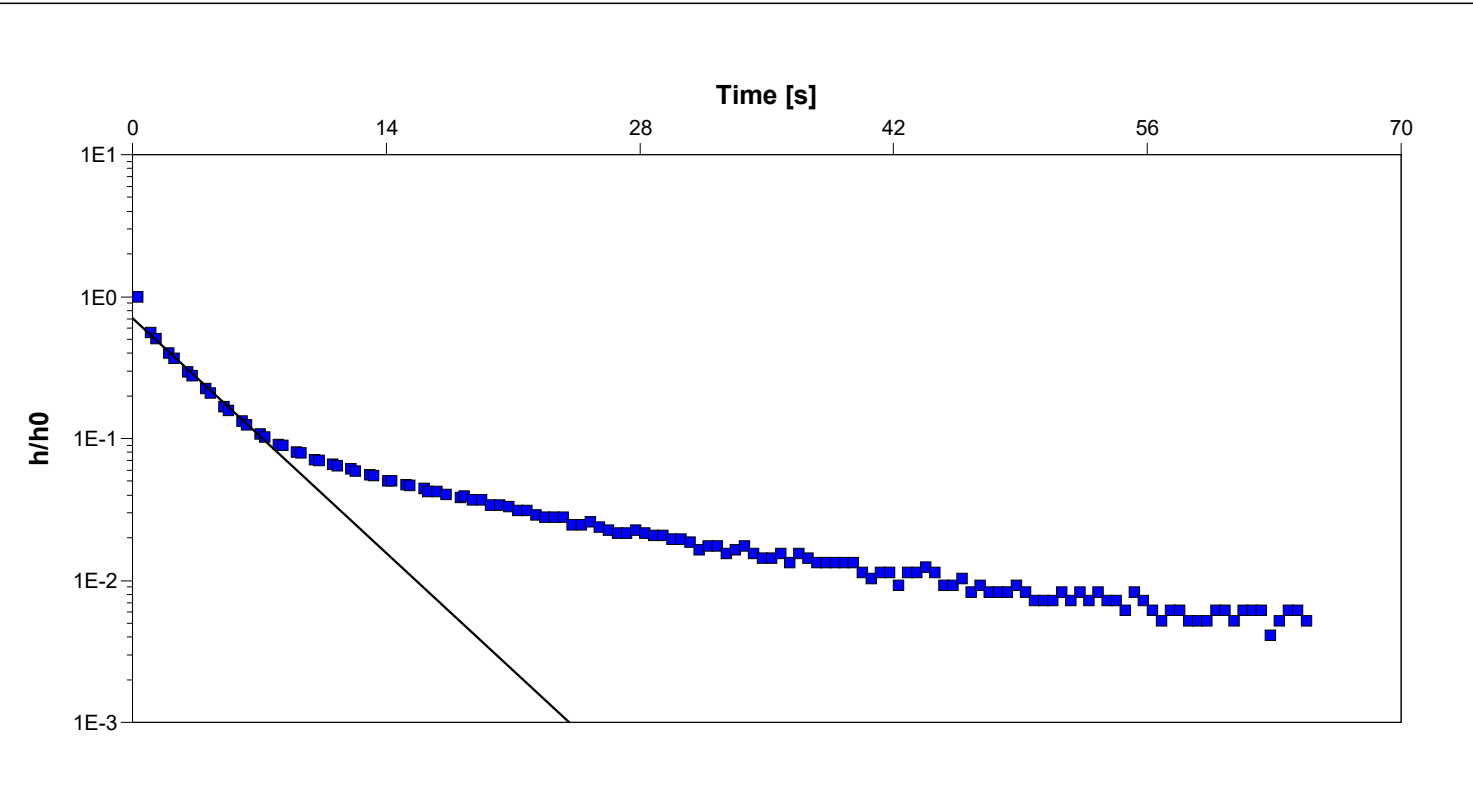
Slug Test Analysis Report

Project: Rusty Lantern Market


Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: MW-1 Test 3	Test Well: MW-1
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	MW-1 Test 3	Analysis Date: 1/21/2024
Aquifer Thickness: 6.31 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
MW-1	4.30×10^1	

<div><div></div><div>Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine</div></div>				Slug Test - Water Level Data		Page 1 of 2	
				Project: Rusty Lantern Market			
				Number: 231411			
				Client: Cumberland Real Estate Group			
Location: 181 Gray Road, Cumberland			Slug Test: MW-2 Test 1		Test Well: MW-2		
Test Conducted by: APG			Test Date: 1/9/2024				
Water level at t=0 [ft]: 0.77			Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 0.77		
	Time [s]	Water Level [ft]	WL Change [ft]				
1	0.5	0.766	0.766				
2	1	0.648	0.648				
3	1.5	0.582	0.582				
4	2	0.517	0.517				
5	2.5	0.468	0.468				
6	3	0.419	0.419				
7	3.5	0.379	0.379				
8	4	0.357	0.357				
9	4.5	0.313	0.313				
10	5	0.284	0.284				
11	5.5	0.256	0.256				
12	6	0.237	0.237				
13	6.5	0.219	0.219				
14	7	0.201	0.201				
15	7.5	0.187	0.187				
16	8	0.174	0.174				
17	8.5	0.162	0.162				
18	9	0.153	0.153				
19	9.5	0.145	0.145				
20	10	0.136	0.136				
21	10.5	0.13	0.13				
22	11	0.124	0.124				
23	11.5	0.119	0.119				
24	12	0.114	0.114				
25	12.5	0.11	0.11				
26	13	0.105	0.105				
27	13.5	0.101	0.101				
28	14	0.097	0.097				
29	14.5	0.094	0.094				
30	15.017	0.09	0.09				
31	15.5	0.087	0.087				
32	16.019	0.084	0.084				
33	16.5	0.083	0.083				
34	17.02	0.079	0.079				
35	17.5	0.075	0.075				
36	18.039	0.072	0.072				
37	18.5	0.07	0.07				
38	19.058	0.068	0.068				
39	19.5	0.067	0.067				
40	20.061	0.063	0.063				
41	20.5	0.063	0.063				
42	21.075	0.058	0.058				
43	21.5	0.056	0.056				
44	22.095	0.053	0.053				
45	22.5	0.051	0.051				
46	23.097	0.047	0.047				
47	23.5	0.047	0.047				
48	24.1	0.043	0.043				
49	24.5	0.043	0.043				
50	25.119	0.039	0.039				
51	25.5	0.039	0.039				
52	26.122	0.037	0.037				
53	26.5	0.035	0.035				



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Slug Test - Water Level Data

Page 2 of 2

Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

	Time [s]	Water Level [ft]	WL Change [ft]
54	27.125	0.034	0.034
55	27.5	0.032	0.032
56	28.129	0.031	0.031
57	28.5	0.031	0.031
58	29.131	0.029	0.029
59	29.5	0.028	0.028
60	30.152	0.027	0.027
61	30.5	0.027	0.027
62	31.155	0.026	0.026
63	31.5	0.025	0.025
64	32.153	0.024	0.024
65	32.5	0.023	0.023
66	33.164	0.023	0.023
67	33.5	0.022	0.022
68	34.184	0.021	0.021
69	34.5	0.021	0.021
70	35.186	0.02	0.02
71	35.5	0.02	0.02
72	36.189	0.018	0.018
73	36.5	0.019	0.019
74	37.192	0.018	0.018
75	37.5	0.018	0.018
76	38.218	0.017	0.017
77	38.5	0.018	0.018
78	39.221	0.018	0.018
79	39.5	0.016	0.016
80	40.223	0.016	0.016
81	40.5	0.016	0.016
82	41.225	0.016	0.016
83	41.5	0.015	0.015
84	42.229	0.014	0.014
85	42.5	0.015	0.015
86	43.233	0.015	0.015
87	43.5	0.015	0.015
88	44.25	0.013	0.013
89	44.5	0.013	0.013
90	45.252	0.013	0.013



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

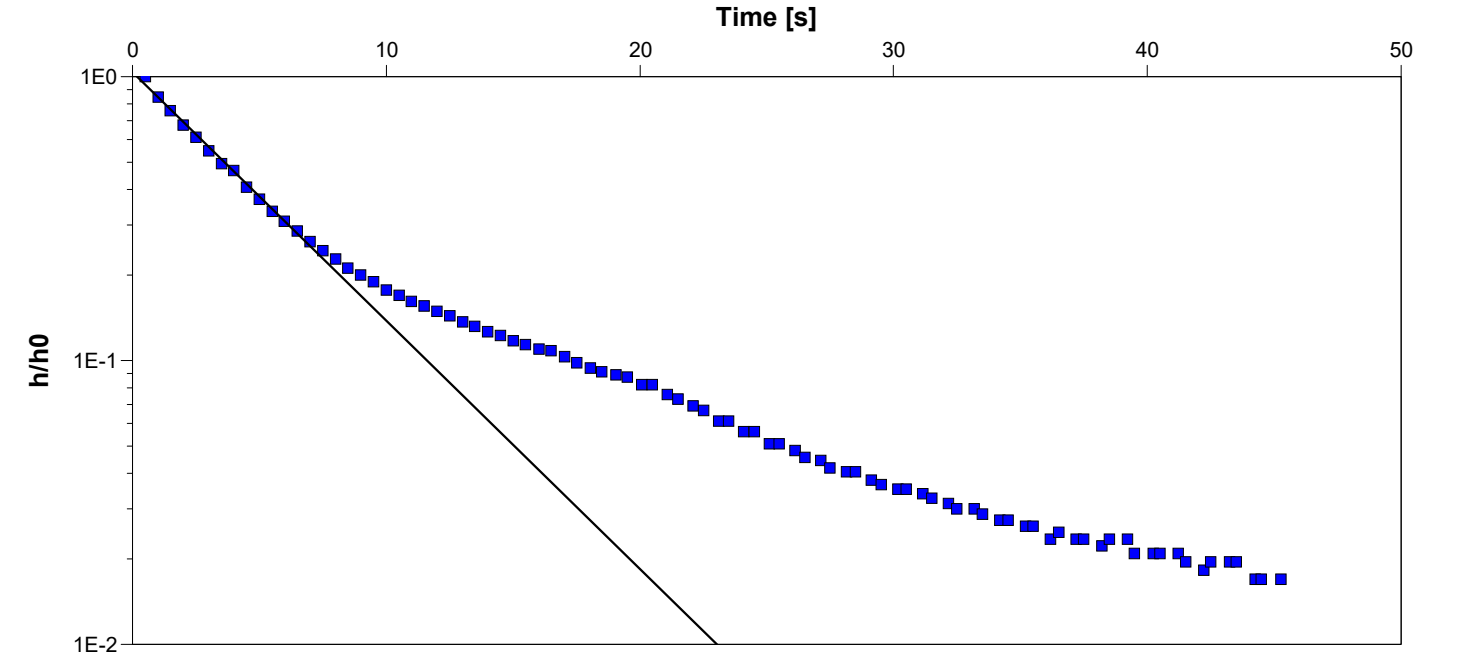
Slug Test Analysis Report

Project: Rusty Lantern Market


Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: MW-2 Test 1	Test Well: MW-2
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	MW-2 Test 1	Analysis Date: 1/21/2024
Aquifer Thickness: 6.07 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
MW-2	3.28×10^1	

<div>  <div> Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine </div> </div>				Slug Test - Water Level Data <div> Page 1 of 2 Project: Rusty Lantern Market Number: 231411 Client: Cumberland Real Estate Group </div>	
Location: 181 Gray Road, Cumberland		Slug Test: MW-2 Test 2		Test Well: MW-2	
Test Conducted by: APG		Test Date: 1/9/2024			
Water level at t=0 [ft]: 0.96		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 0.96	
	Time [s]	Water Level [ft]	WL Change [ft]		
1	0.5	0.955	0.955		
2	1	0.74	0.74		
3	1.5	0.619	0.619		
4	2	0.553	0.553		
5	2.5	0.495	0.495		
6	3	0.451	0.451		
7	3.5	0.402	0.402		
8	4	0.36	0.36		
9	4.5	0.325	0.325		
10	5	0.29	0.29		
11	5.5	0.266	0.266		
12	6	0.24	0.24		
13	6.5	0.225	0.225		
14	7	0.205	0.205		
15	7.5	0.19	0.19		
16	8	0.176	0.176		
17	8.506	0.168	0.168		
18	9	0.157	0.157		
19	9.5	0.145	0.145		
20	10	0.139	0.139		
21	10.503	0.13	0.13		
22	11	0.123	0.123		
23	11.505	0.12	0.12		
24	12	0.113	0.113		
25	12.508	0.11	0.11		
26	13	0.105	0.105		
27	13.527	0.102	0.102		
28	14	0.10	0.10		
29	14.529	0.095	0.095		
30	15	0.092	0.092		
31	15.533	0.088	0.088		
32	16	0.087	0.087		
33	16.528	0.083	0.083		
34	17	0.079	0.079		
35	17.542	0.076	0.076		
36	18	0.075	0.075		
37	18.544	0.07	0.07		
38	19	0.068	0.068		
39	19.563	0.065	0.065		
40	20	0.062	0.062		
41	20.555	0.058	0.058		
42	21	0.055	0.055		
43	21.574	0.053	0.053		
44	22	0.052	0.052		
45	22.576	0.048	0.048		
46	23	0.047	0.047		
47	23.58	0.044	0.044		
48	24	0.043	0.043		
49	24.583	0.041	0.041		
50	25	0.039	0.039		
51	25.608	0.039	0.039		
52	26	0.037	0.037		
53	26.627	0.036	0.036		



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Slug Test - Water Level Data

Page 2 of 2

Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

	Time [s]	Water Level [ft]	WL Change [ft]
54	27	0.036	0.036
55	27.63	0.033	0.033
56	28	0.032	0.032
57	28.649	0.032	0.032
58	29	0.031	0.031
59	29.677	0.03	0.03
60	30	0.028	0.028
61	30.698	0.028	0.028
62	31	0.029	0.029
63	31.701	0.027	0.027
64	32	0.026	0.026
65	32.704	0.025	0.025
66	33	0.026	0.026
67	33.707	0.025	0.025
68	34	0.025	0.025
69	34.732	0.024	0.024
70	35	0.024	0.024
71	35.751	0.023	0.023
72	36	0.024	0.024
73	36.754	0.022	0.022
74	37	0.023	0.023
75	37.771	0.023	0.023
76	38	0.021	0.021
77	38.789	0.021	0.021
78	39	0.021	0.021
79	39.793	0.02	0.02
80	40	0.021	0.021
81	40.797	0.02	0.02
82	41	0.02	0.02
83	41.794	0.02	0.02
84	42	0.019	0.019
85	42.797	0.019	0.019
86	43	0.018	0.018
87	43.8	0.019	0.019
88	44	0.017	0.017
89	44.802	0.017	0.017
90	45	0.018	0.018
91	45.821	0.017	0.017
92	46	0.018	0.018
93	46.5	0.017	0.017
94	47	0.017	0.017
95	47.5	0.016	0.016



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

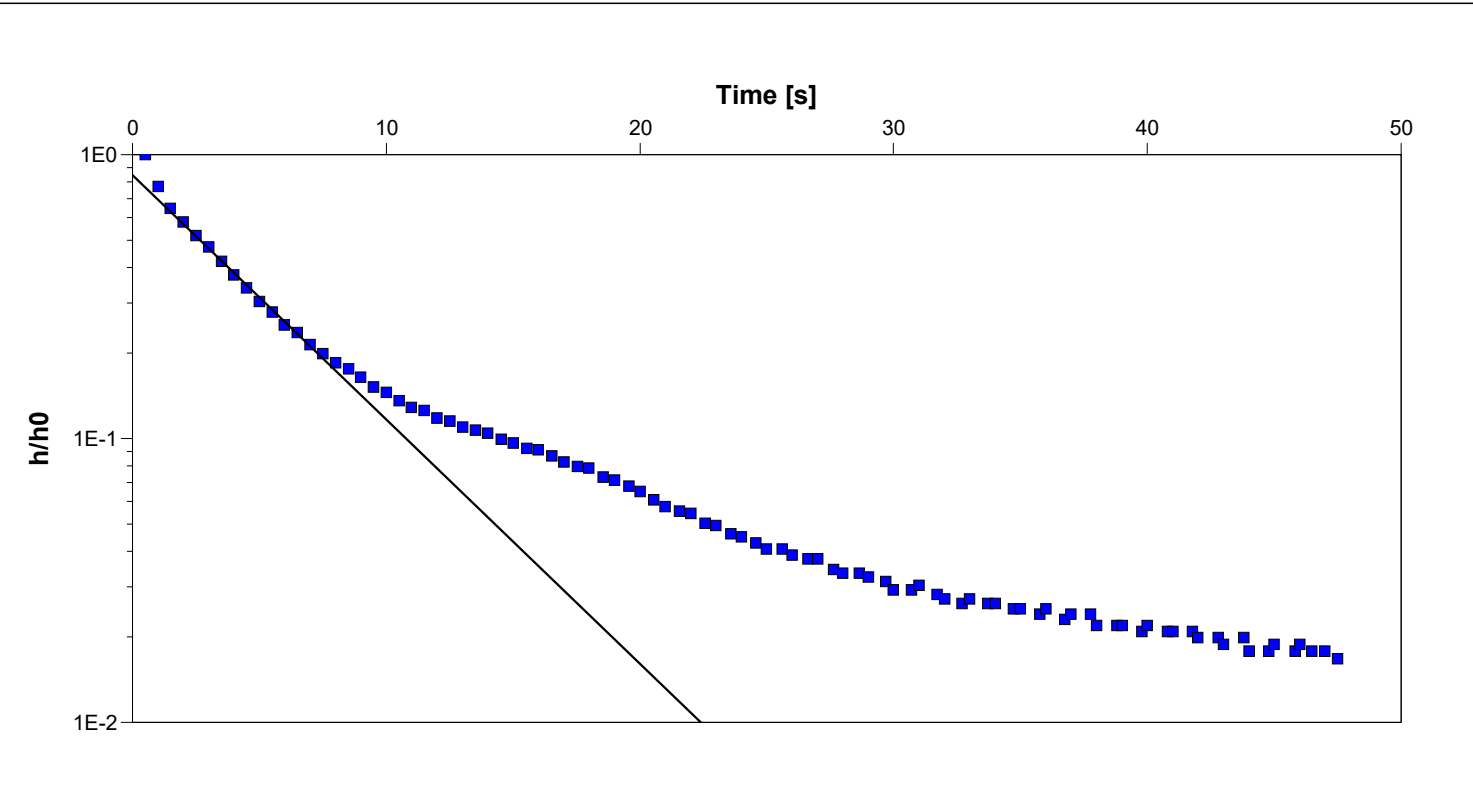
Slug Test Analysis Report

Project: Rusty Lantern Market


Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: MW-2 Test 2	Test Well: MW-2
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	MW-2 Test 2	Analysis Date: 1/21/2024
Aquifer Thickness: 6.07 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
MW-2	3.22×10^1	

<div>  <div> Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine </div> </div>			Slug Test - Water Level Data <div>Page 1 of 3</div>	
			Project: Rusty Lantern Market	
			Number: 231411	
			Client: Cumberland Real Estate Group	
Location: 181 Gray Road, Cumberland		Slug Test: MW-2 Test 3		Test Well: MW-2
Test Conducted by: APG		Test Date: 1/9/2024		
Water level at t=0 [ft]: 0.89		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 0.89
	Time [s]	Water Level [ft]	WL Change [ft]	
1	0.5	0.886	0.886	
2	1	0.763	0.763	
3	1.5	0.632	0.632	
4	2	0.561	0.561	
5	2.5	0.504	0.504	
6	3	0.451	0.451	
7	3.5	0.402	0.402	
8	4.001	0.36	0.36	
9	4.5	0.325	0.325	
10	5	0.297	0.297	
11	5.5	0.273	0.273	
12	6.016	0.248	0.248	
13	6.5	0.224	0.224	
14	7.05	0.205	0.205	
15	7.5	0.193	0.193	
16	8.067	0.178	0.178	
17	8.5	0.17	0.17	
18	9.069	0.155	0.155	
19	9.5	0.146	0.146	
20	10.073	0.137	0.137	
21	10.5	0.132	0.132	
22	11.076	0.123	0.123	
23	11.5	0.119	0.119	
24	12.101	0.113	0.113	
25	12.5	0.109	0.109	
26	13.137	0.105	0.105	
27	13.5	0.102	0.102	
28	14.141	0.098	0.098	
29	14.5	0.095	0.095	
30	15.159	0.091	0.091	
31	15.5	0.089	0.089	
32	16.162	0.084	0.084	
33	16.5	0.081	0.081	
34	17.164	0.077	0.077	
35	17.5	0.075	0.075	
36	18.18	0.071	0.071	
37	18.5	0.069	0.069	
38	19.177	0.065	0.065	
39	19.5	0.064	0.064	
40	20.18	0.057	0.057	
41	20.5	0.057	0.057	
42	21.184	0.053	0.053	
43	21.5	0.053	0.053	
44	22.202	0.05	0.05	
45	22.5	0.048	0.048	
46	23.22	0.045	0.045	
47	23.5	0.045	0.045	
48	24.223	0.042	0.042	
49	24.5	0.041	0.041	
50	25.225	0.039	0.039	
51	25.5	0.039	0.039	
52	26.228	0.037	0.037	
53	26.5	0.036	0.036	



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Slug Test - Water Level Data

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Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

	Time [s]	Water Level [ft]	WL Change [ft]
54	27.232	0.034	0.034
55	27.5	0.035	0.035
56	28.251	0.032	0.032
57	28.5	0.033	0.033
58	29.254	0.031	0.031
59	29.5	0.032	0.032
60	30.273	0.03	0.03
61	30.5	0.03	0.03
62	31.295	0.028	0.028
63	31.5	0.028	0.028
64	32.295	0.028	0.028
65	32.5	0.028	0.028
66	33.298	0.027	0.027
67	33.5	0.026	0.026
68	34.31	0.025	0.025
69	34.5	0.025	0.025
70	35	0.025	0.025
71	35.5	0.026	0.026
72	36	0.024	0.024
73	36.5	0.025	0.025
74	37	0.023	0.023
75	37.5	0.024	0.024
76	38	0.023	0.023
77	38.5	0.023	0.023
78	39	0.022	0.022
79	39.5	0.022	0.022
80	40	0.022	0.022
81	40.5	0.021	0.021
82	41	0.022	0.022
83	41.5	0.02	0.02
84	42	0.02	0.02
85	42.5	0.02	0.02
86	43	0.021	0.021
87	43.5	0.02	0.02
88	44	0.02	0.02
89	44.5	0.019	0.019
90	45	0.019	0.019
91	45.5	0.019	0.019
92	46	0.019	0.019
93	46.5	0.018	0.018
94	47	0.019	0.019
95	47.5	0.018	0.018
96	48	0.018	0.018
97	48.5	0.019	0.019
98	49	0.018	0.018
99	49.5	0.018	0.018
100	50	0.018	0.018
101	50.5	0.017	0.017
102	51	0.018	0.018
103	51.5	0.017	0.017
104	52	0.017	0.017
105	52.5	0.017	0.017
106	53	0.015	0.015
107	53.5	0.017	0.017
108	54	0.016	0.016
109	54.5	0.016	0.016
110	55	0.017	0.017
111	55.5	0.017	0.017



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

	Time [s]	Water Level [ft]	WL Change [ft]
112	56	0.016	0.016
113	56.5	0.016	0.016
114	57	0.016	0.016
115	57.501	0.016	0.016
116	58	0.015	0.015
117	58.5	0.015	0.015
118	59	0.015	0.015



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

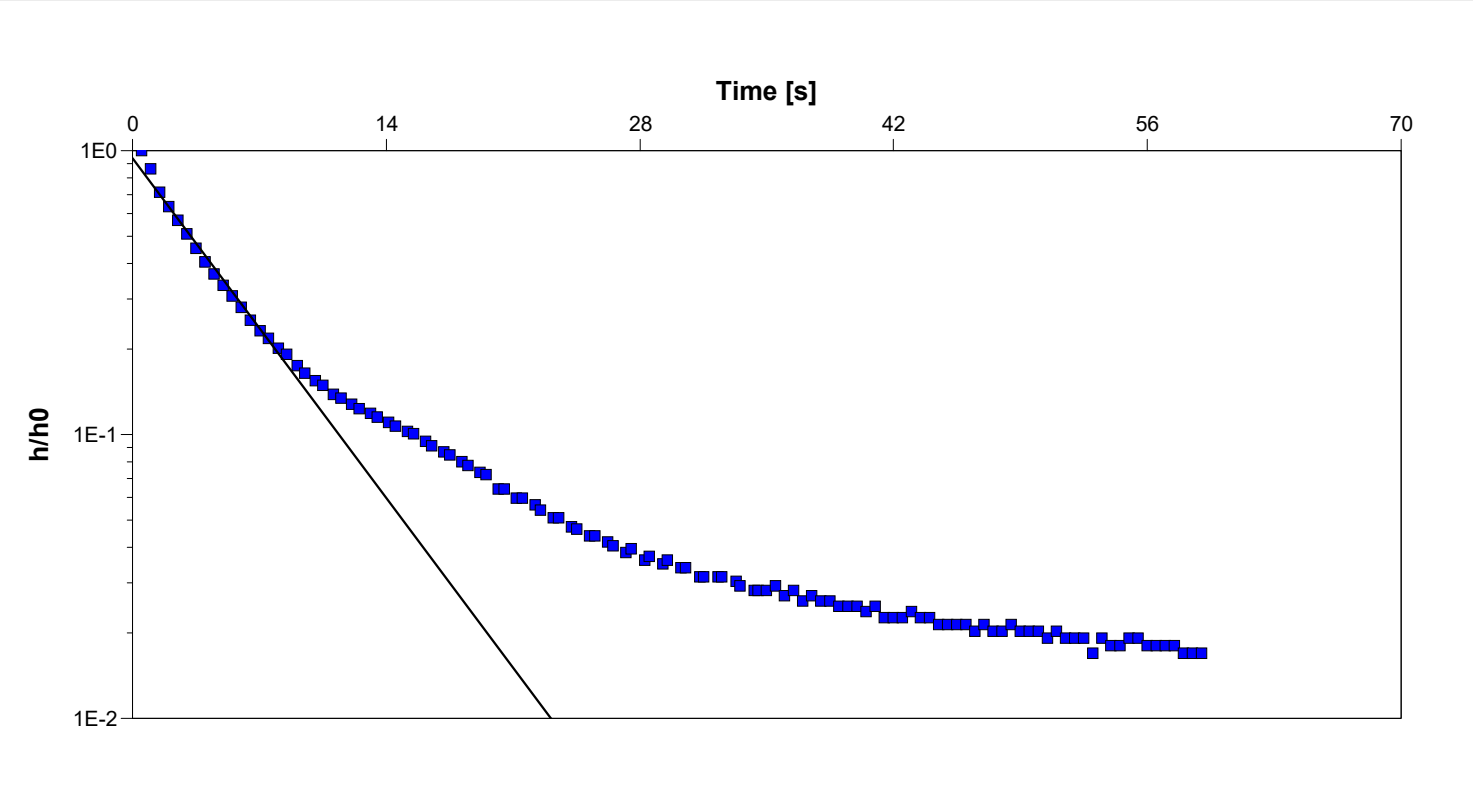
Slug Test Analysis Report

Project: Rusty Lantern Market


Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: MW-2 Test 3	Test Well: MW-2
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	MW-2 Test 3	Analysis Date: 1/21/2024
Aquifer Thickness: 6.07 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
MW-2	3.20×10^1	

Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine 			Slug Test - Water Level Data		Page 1 of 3
			Project: Rusty Lantern Market		
			Number: 231411		
			Client: Cumberland Real Estate Group		
Location: 181 Gray Road, Cumberland		Slug Test: MW-3 Test 1		Test Well: MW-3	
Test Conducted by: APG		Test Date: 1/9/2024			
Water level at t=0 [ft]: 0.68		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 0.68	
	Time [s]	Water Level [ft]	WL Change [ft]		
1	0.667	0.68	0.68		
2	1	0.663	0.663		
3	1.667	0.614	0.614		
4	2	0.584	0.584		
5	2.686	0.539	0.539		
6	3	0.519	0.519		
7	3.69	0.472	0.472		
8	4	0.459	0.459		
9	4.693	0.42	0.42		
10	5	0.404	0.404		
11	5.697	0.373	0.373		
12	6	0.353	0.353		
13	6.7	0.335	0.335		
14	7	0.317	0.317		
15	7.718	0.295	0.295		
16	8	0.285	0.285		
17	8.72	0.265	0.265		
18	9	0.257	0.257		
19	9.723	0.241	0.241		
20	10	0.234	0.234		
21	10.727	0.219	0.219		
22	11	0.214	0.214		
23	11.729	0.203	0.203		
24	12	0.198	0.198		
25	12.748	0.189	0.189		
26	13	0.185	0.185		
27	13.774	0.177	0.177		
28	14	0.174	0.174		
29	14.777	0.167	0.167		
30	15	0.164	0.164		
31	15.779	0.157	0.157		
32	16	0.155	0.155		
33	16.781	0.149	0.149		
34	17	0.148	0.148		
35	17.801	0.143	0.143		
36	18	0.141	0.141		
37	18.804	0.137	0.137		
38	19	0.137	0.137		
39	19.807	0.131	0.131		
40	20	0.131	0.131		
41	20.5	0.128	0.128		
42	21	0.126	0.126		
43	21.5	0.124	0.124		
44	22	0.122	0.122		
45	22.5	0.121	0.121		
46	23	0.117	0.117		
47	23.5	0.116	0.116		
48	24	0.114	0.114		
49	24.5	0.112	0.112		
50	25	0.111	0.111		
51	25.5	0.109	0.109		
52	26	0.107	0.107		
53	26.5	0.106	0.106		



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Slug Test - Water Level Data

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Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

	Time [s]	Water Level [ft]	WL Change [ft]
54	27	0.104	0.104
55	27.5	0.104	0.104
56	28	0.102	0.102
57	28.5	0.10	0.10
58	29	0.10	0.10
59	29.5	0.097	0.097
60	30	0.096	0.096
61	30.5	0.096	0.096
62	31	0.094	0.094
63	31.5	0.093	0.093
64	32	0.092	0.092
65	32.5	0.091	0.091
66	33	0.091	0.091
67	33.5	0.089	0.089
68	34	0.088	0.088
69	34.5	0.088	0.088
70	35	0.086	0.086
71	35.5	0.085	0.085
72	36	0.084	0.084
73	36.5	0.084	0.084
74	37	0.082	0.082
75	37.5	0.081	0.081
76	38	0.082	0.082
77	38.5	0.081	0.081
78	39	0.08	0.08
79	39.5	0.078	0.078
80	40	0.078	0.078
81	40.5	0.078	0.078
82	41	0.076	0.076
83	41.5	0.075	0.075
84	42	0.074	0.074
85	42.5	0.075	0.075
86	43	0.073	0.073
87	43.5	0.074	0.074
88	44	0.072	0.072
89	44.5	0.071	0.071
90	45	0.072	0.072
91	45.5	0.071	0.071
92	46	0.07	0.07
93	46.5	0.07	0.07
94	47	0.07	0.07
95	47.5	0.069	0.069
96	48	0.068	0.068
97	48.5	0.068	0.068
98	49	0.067	0.067
99	49.5	0.067	0.067
100	50	0.066	0.066
101	50.5	0.065	0.065
102	51	0.066	0.066
103	51.5	0.065	0.065
104	52	0.065	0.065
105	52.5	0.065	0.065
106	53.038	0.062	0.062
107	53.5	0.063	0.063
108	54	0.063	0.063
109	54.5	0.063	0.063
110	55	0.062	0.062
111	55.5	0.063	0.063



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Slug Test - Water Level Data

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Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

	Time [s]	Water Level [ft]	WL Change [ft]
112	56	0.061	0.061
113	56.5	0.061	0.061
114	57	0.061	0.061
115	57.5	0.06	0.06
116	58	0.06	0.06
117	58.5	0.061	0.061
118	59	0.059	0.059
119	59.5	0.059	0.059
120	60	0.059	0.059
121	60.5	0.058	0.058
122	61	0.058	0.058
123	61.5	0.058	0.058
124	62	0.057	0.057
125	62.5	0.057	0.057
126	63.002	0.056	0.056
127	63.5	0.057	0.057
128	64	0.055	0.055
129	64.5	0.055	0.055
130	65	0.055	0.055
131	65.5	0.056	0.056
132	66	0.055	0.055
133	66.5	0.055	0.055
134	67.01	0.054	0.054
135	67.5	0.053	0.053
136	68.028	0.053	0.053
137	68.5	0.053	0.053
138	69.047	0.055	0.055
139	69.5	0.054	0.054
140	70.051	0.054	0.054
141	70.5	0.053	0.053
142	71.054	0.052	0.052
143	71.5	0.051	0.051
144	72.073	0.052	0.052
145	72.5	0.052	0.052
146	73.075	0.052	0.052
147	73.5	0.052	0.052
148	74.079	0.051	0.051
149	74.5	0.051	0.051
150	75.083	0.052	0.052
151	75.5	0.051	0.051
152	76.102	0.049	0.049
153	76.5	0.051	0.051
154	77.12	0.049	0.049
155	77.5	0.05	0.05
156	78.115	0.051	0.051
157	78.5	0.05	0.05
158	79.134	0.049	0.049
159	79.5	0.05	0.05
160	80.152	0.049	0.049
161	80.5	0.05	0.05
162	81.155	0.049	0.049
163	81.5	0.05	0.05
164	82.158	0.049	0.049
165	82.5	0.05	0.05
166	83.161	0.048	0.048
167	83.5	0.049	0.049
168	84.179	0.049	0.049
169	84.5	0.048	0.048



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

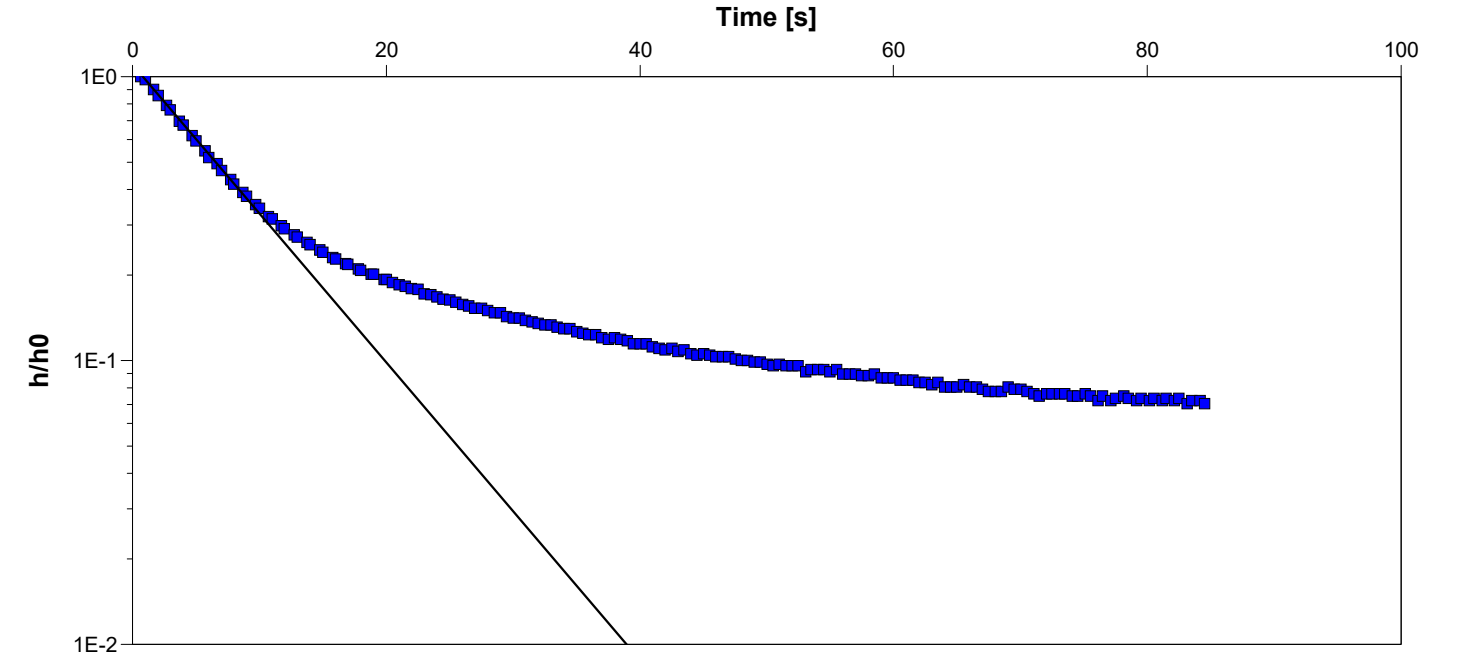
Slug Test Analysis Report

Project: Rusty Lantern Market


Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: MW-3 Test 1	Test Well: MW-3
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	MW-3 Test 1	Analysis Date: 1/22/2024
Aquifer Thickness: 10.31 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
MW-3	1.31×10^1	

<div>  <div> Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine </div> </div>			Slug Test - Water Level Data <div>Page 1 of 3</div>	
			Project: Rusty Lantern Market	
			Number: 231411	
			Client: Cumberland Real Estate Group	
Location: 181 Gray Road, Cumberland		Slug Test: MW-3 Test 2		Test Well: MW-3
Test Conducted by: APG		Test Date: 1/9/2024		
Water level at t=0 [ft]: 0.69		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 0.69
	Time [s]	Water Level [ft]	WL Change [ft]	
1	0.288	0.688	0.688	
2	1.003	0.631	0.631	
3	1.288	0.608	0.608	
4	2.005	0.555	0.555	
5	2.288	0.527	0.527	
6	3.009	0.485	0.485	
7	3.288	0.47	0.47	
8	4.027	0.426	0.426	
9	4.288	0.415	0.415	
10	5.046	0.377	0.377	
11	5.288	0.365	0.365	
12	6.048	0.33	0.33	
13	6.288	0.322	0.322	
14	7.05	0.294	0.294	
15	7.288	0.285	0.285	
16	8.067	0.261	0.261	
17	8.288	0.256	0.256	
18	9.076	0.236	0.236	
19	9.288	0.231	0.231	
20	10.094	0.214	0.214	
21	10.288	0.21	0.21	
22	11.096	0.196	0.196	
23	11.288	0.192	0.192	
24	12.098	0.181	0.181	
25	12.288	0.178	0.178	
26	13.103	0.168	0.168	
27	13.288	0.165	0.165	
28	13.788	0.162	0.162	
29	14.288	0.156	0.156	
30	14.788	0.152	0.152	
31	15.288	0.147	0.147	
32	15.788	0.142	0.142	
33	16.288	0.139	0.139	
34	16.788	0.137	0.137	
35	17.288	0.132	0.132	
36	17.788	0.13	0.13	
37	18.288	0.127	0.127	
38	18.788	0.125	0.125	
39	19.288	0.119	0.119	
40	19.788	0.118	0.118	
41	20.288	0.116	0.116	
42	20.788	0.114	0.114	
43	21.288	0.11	0.11	
44	21.788	0.109	0.109	
45	22.288	0.107	0.107	
46	22.788	0.103	0.103	
47	23.288	0.102	0.102	
48	23.788	0.10	0.10	
49	24.288	0.098	0.098	
50	24.788	0.098	0.098	
51	25.288	0.093	0.093	
52	25.788	0.092	0.092	
53	26.288	0.091	0.091	



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Slug Test - Water Level Data

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Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

	Time [s]	Water Level [ft]	WL Change [ft]
54	26.788	0.09	0.09
55	27.288	0.089	0.089
56	27.788	0.085	0.085
57	28.288	0.084	0.084
58	28.788	0.08	0.08
59	29.288	0.081	0.081
60	29.788	0.081	0.081
61	30.288	0.079	0.079
62	30.788	0.078	0.078
63	31.288	0.076	0.076
64	31.788	0.074	0.074
65	32.288	0.073	0.073
66	32.788	0.073	0.073
67	33.288	0.072	0.072
68	33.788	0.069	0.069
69	34.288	0.07	0.07
70	34.788	0.069	0.069
71	35.288	0.067	0.067
72	35.788	0.066	0.066
73	36.288	0.065	0.065
74	36.788	0.064	0.064
75	37.288	0.064	0.064
76	37.788	0.062	0.062
77	38.288	0.061	0.061
78	38.788	0.06	0.06
79	39.288	0.06	0.06
80	39.788	0.058	0.058
81	40.288	0.059	0.059
82	40.788	0.058	0.058
83	41.288	0.058	0.058
84	41.788	0.057	0.057
85	42.288	0.055	0.055
86	42.788	0.054	0.054
87	43.288	0.053	0.053
88	43.788	0.054	0.054
89	44.288	0.05	0.05
90	44.788	0.052	0.052
91	45.288	0.051	0.051
92	45.788	0.05	0.05
93	46.288	0.049	0.049
94	46.788	0.05	0.05
95	47.288	0.048	0.048
96	47.788	0.048	0.048
97	48.291	0.046	0.046
98	48.788	0.046	0.046
99	49.294	0.046	0.046
100	49.788	0.046	0.046
101	50.297	0.044	0.044
102	50.788	0.045	0.045
103	51.315	0.044	0.044
104	51.788	0.044	0.044
105	52.317	0.042	0.042
106	52.788	0.042	0.042
107	53.342	0.042	0.042
108	53.788	0.042	0.042
109	54.354	0.04	0.04
110	54.788	0.041	0.041
111	55.356	0.04	0.04



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

Slug Test - Water Level Data

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Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

	Time [s]	Water Level [ft]	WL Change [ft]
112	55.788	0.039	0.039
113	56.36	0.038	0.038
114	56.788	0.038	0.038
115	57.362	0.038	0.038
116	57.788	0.039	0.039
117	58.38	0.037	0.037
118	58.788	0.038	0.038
119	59.4	0.036	0.036
120	59.788	0.037	0.037
121	60.411	0.036	0.036
122	60.788	0.037	0.037
123	61.437	0.035	0.035
124	61.788	0.036	0.036
125	62.439	0.035	0.035
126	62.788	0.034	0.034
127	63.441	0.034	0.034
128	63.788	0.034	0.034
129	64.438	0.034	0.034
130	64.788	0.033	0.033
131	65.437	0.034	0.034
132	65.788	0.034	0.034
133	66.441	0.032	0.032
134	66.788	0.031	0.031
135	67.459	0.031	0.031
136	67.788	0.032	0.032
137	68.485	0.031	0.031
138	68.788	0.032	0.032
139	69.487	0.029	0.029
140	69.788	0.03	0.03
141	70.489	0.03	0.03
142	70.788	0.029	0.029
143	71.501	0.03	0.03
144	71.788	0.029	0.029
145	72.528	0.03	0.03
146	72.788	0.03	0.03
147	73.531	0.027	0.027
148	73.788	0.029	0.029
149	74.533	0.029	0.029
150	74.788	0.029	0.029
151	75.563	0.028	0.028
152	75.788	0.027	0.027
153	76.563	0.027	0.027
154	76.788	0.028	0.028
155	77.566	0.027	0.027
156	77.788	0.027	0.027
157	78.583	0.026	0.026
158	78.788	0.025	0.025



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

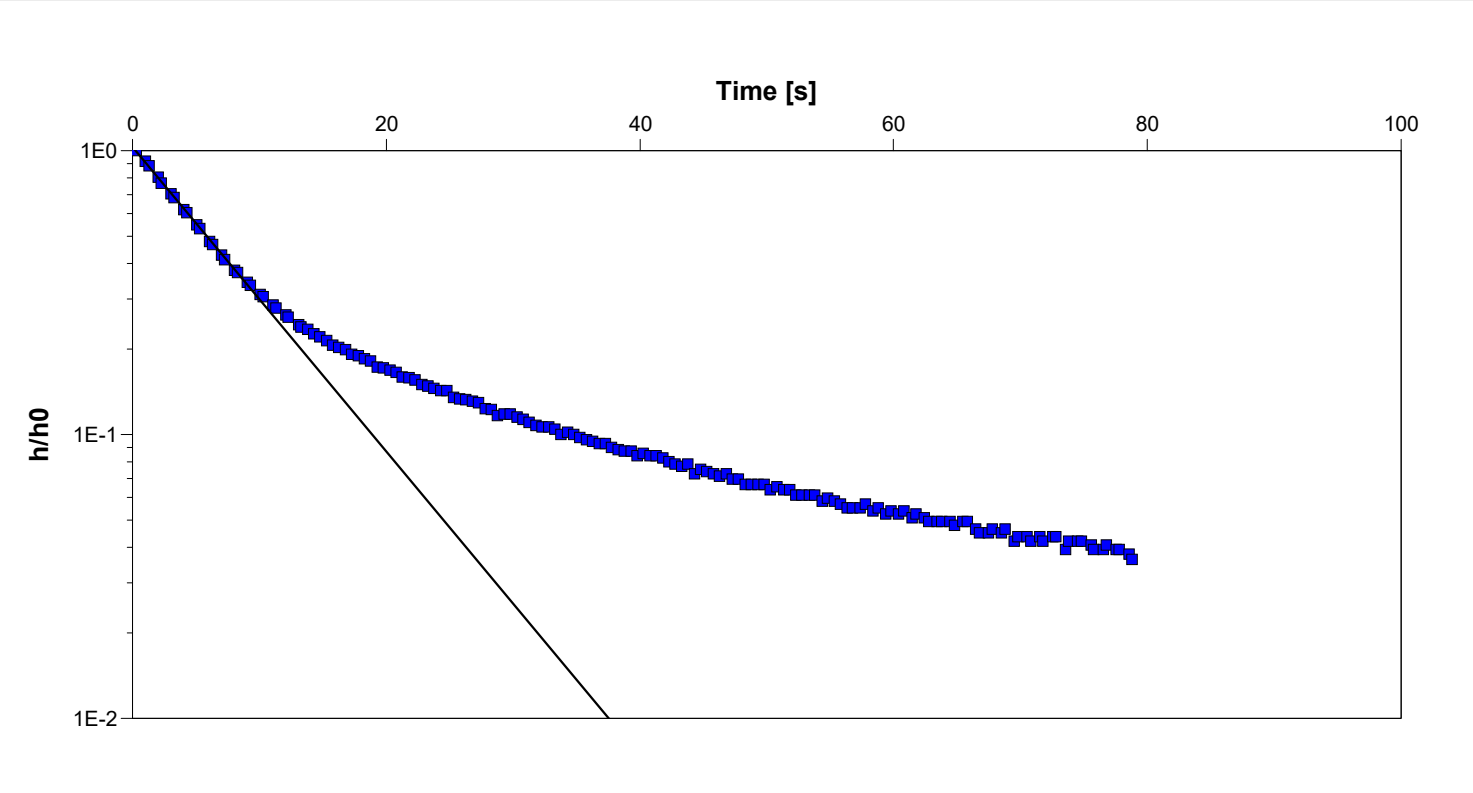
Slug Test Analysis Report

Project: Rusty Lantern Market


Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: MW-3 Test 2	Test Well: MW-3
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	MW-3 Test 2	Analysis Date: 1/22/2024
Aquifer Thickness: 10.31 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
MW-3	1.34×10^1	

<div><div></div><div>Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine</div></div>				Slug Test - Water Level Data		Page 1 of 3
				Project: Rusty Lantern Market		
				Number: 231411		
				Client: Cumberland Real Estate Group		
Location: 181 Gray Road, Cumberland		Slug Test: MW-3 Test 3		Test Well: MW-3		
Test Conducted by: APG		Test Date: 1/9/2024				
Water level at t=0 [ft]: 0.83		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 0.83		
	Time [s]	Water Level [ft]	WL Change [ft]			
1	0.424	0.831	0.831			
2	1.003	0.667	0.667			
3	1.424	0.628	0.628			
4	2.006	0.581	0.581			
5	2.424	0.553	0.553			
6	3.008	0.509	0.509			
7	3.424	0.491	0.491			
8	4.034	0.449	0.449			
9	4.424	0.432	0.432			
10	5.052	0.397	0.397			
11	5.424	0.378	0.378			
12	6.055	0.346	0.346			
13	6.424	0.33	0.33			
14	7.084	0.304	0.304			
15	7.424	0.293	0.293			
16	8.087	0.269	0.269			
17	8.424	0.26	0.26			
18	9.089	0.242	0.242			
19	9.424	0.235	0.235			
20	10.091	0.216	0.216			
21	10.424	0.21	0.21			
22	11.094	0.196	0.196			
23	11.424	0.192	0.192			
24	12.114	0.181	0.181			
25	12.424	0.176	0.176			
26	13.116	0.167	0.167			
27	13.424	0.164	0.164			
28	14.119	0.155	0.155			
29	14.424	0.151	0.151			
30	15.138	0.144	0.144			
31	15.424	0.142	0.142			
32	16.148	0.136	0.136			
33	16.424	0.135	0.135			
34	17.142	0.128	0.128			
35	17.424	0.128	0.128			
36	18.146	0.121	0.121			
37	18.424	0.12	0.12			
38	19.149	0.116	0.116			
39	19.424	0.114	0.114			
40	20.167	0.11	0.11			
41	20.424	0.11	0.11			
42	21.185	0.105	0.105			
43	21.424	0.104	0.104			
44	22.188	0.101	0.101			
45	22.424	0.099	0.099			
46	23.193	0.097	0.097			
47	23.424	0.096	0.096			
48	24.196	0.092	0.092			
49	24.424	0.091	0.091			
50	25.214	0.088	0.088			
51	25.424	0.088	0.088			
52	26.217	0.083	0.083			
53	26.424	0.083	0.083			

	Time [s]	Water Level [ft]	WL Change [ft]
54	27.22	0.08	0.08
55	27.424	0.08	0.08
56	28.224	0.077	0.077
57	28.424	0.077	0.077
58	29.222	0.075	0.075
59	29.424	0.073	0.073
60	30.229	0.071	0.071
61	30.424	0.071	0.071
62	30.924	0.07	0.07
63	31.424	0.067	0.067
64	31.924	0.067	0.067
65	32.424	0.067	0.067
66	32.924	0.064	0.064
67	33.424	0.063	0.063
68	33.924	0.062	0.062
69	34.424	0.061	0.061
70	34.924	0.06	0.06
71	35.424	0.06	0.06
72	35.924	0.057	0.057
73	36.424	0.057	0.057
74	36.924	0.055	0.055
75	37.424	0.055	0.055
76	37.924	0.055	0.055
77	38.424	0.053	0.053
78	38.924	0.052	0.052
79	39.424	0.053	0.053
80	39.924	0.049	0.049
81	40.424	0.05	0.05
82	40.924	0.049	0.049
83	41.424	0.048	0.048
84	41.924	0.047	0.047
85	42.424	0.047	0.047
86	42.924	0.046	0.046
87	43.424	0.046	0.046
88	43.924	0.045	0.045
89	44.424	0.043	0.043
90	44.924	0.043	0.043
91	45.424	0.043	0.043
92	45.924	0.043	0.043
93	46.424	0.042	0.042
94	46.924	0.041	0.041
95	47.424	0.04	0.04
96	47.924	0.04	0.04
97	48.424	0.038	0.038
98	48.924	0.037	0.037
99	49.424	0.038	0.038
100	49.924	0.038	0.038
101	50.424	0.037	0.037
102	50.924	0.037	0.037
103	51.424	0.036	0.036
104	51.924	0.037	0.037
105	52.424	0.035	0.035
106	52.924	0.035	0.035
107	53.424	0.035	0.035
108	53.924	0.034	0.034
109	54.424	0.034	0.034
110	54.924	0.033	0.033
111	55.424	0.033	0.033



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	Time [s]	Water Level [ft]	WL Change [ft]
112	55.924	0.034	0.034
113	56.424	0.033	0.033
114	56.924	0.032	0.032
115	57.424	0.03	0.03
116	57.924	0.03	0.03
117	58.424	0.031	0.031
118	58.924	0.029	0.029
119	59.424	0.029	0.029
120	59.924	0.03	0.03
121	60.424	0.03	0.03
122	60.924	0.029	0.029
123	61.424	0.027	0.027
124	61.924	0.028	0.028
125	62.424	0.028	0.028
126	62.924	0.028	0.028
127	63.424	0.026	0.026
128	63.924	0.026	0.026
129	64.424	0.025	0.025
130	64.924	0.026	0.026
131	65.424	0.025	0.025
132	65.924	0.026	0.026
133	66.438	0.026	0.026



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4 Blanchard Road
Cumberland, Maine

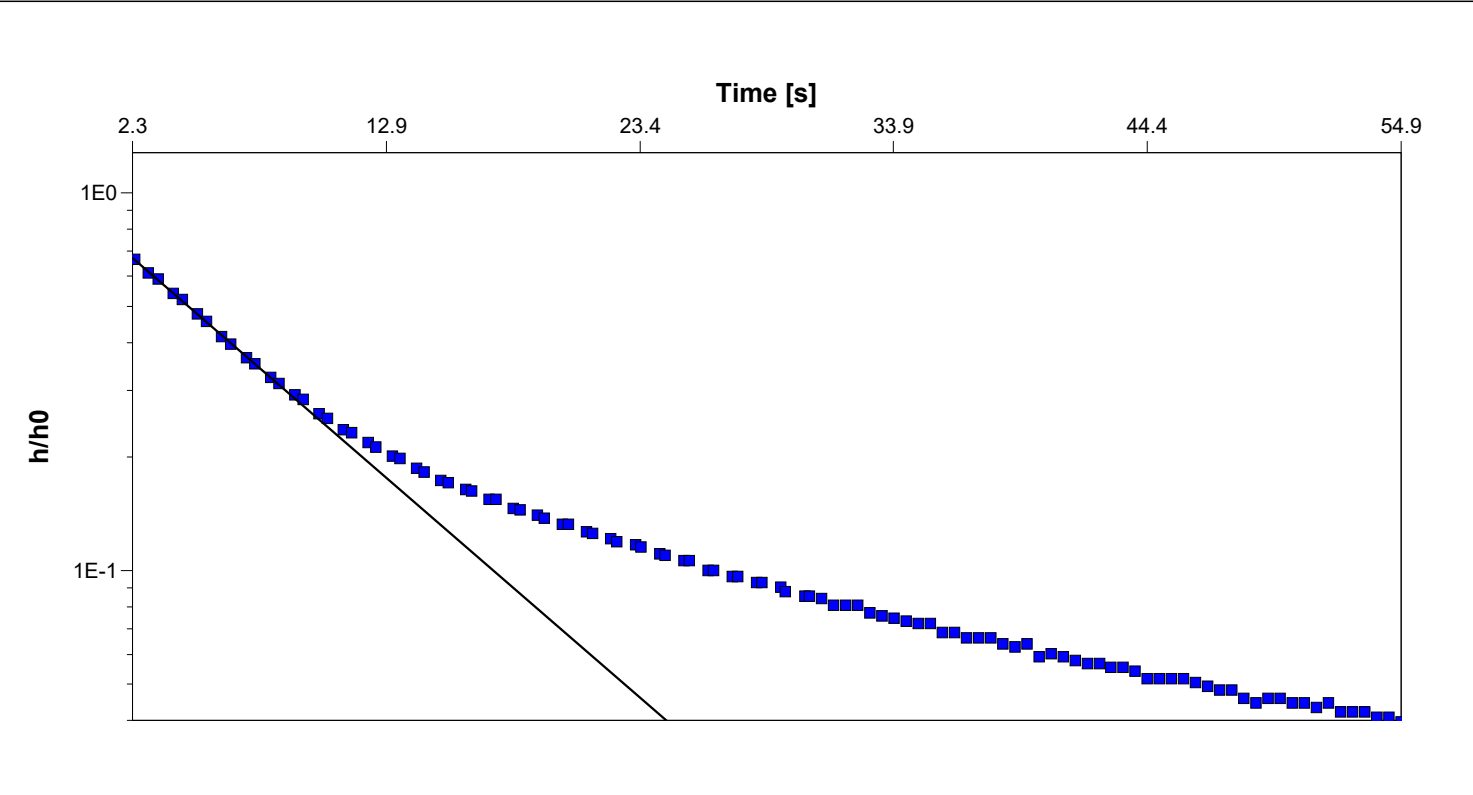
Slug Test Analysis Report

Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: MW-3 Test 3	Test Well: MW-3
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	MW-3 Test 3	Analysis Date: 1/22/2024
Aquifer Thickness: 10.31 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
MW-3	1.38×10^1	

<div><div>Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine</div><div><div>Waterloo</div><div>HYDROGEOLOGIC</div></div></div>		Slug Test - Water Level Data		Page 1 of 1
		Project: Rusty Lantern Market		
		Number: 231411		
		Client: Cumberland Real Estate Group		
Location: 181 Gray Road, Cumberland		Slug Test: PZ-4 Test 1		Test Well: PZ-4
Test Conducted by: APG		Test Date: 1/9/2024		
Water level at t=0 [ft]: 0.68		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 0.68
	Time [s]	Water Level [ft]	WL Change [ft]	
1	1	0.6771	0.6771	
2	2	0.2026	0.2026	
3	3	0.0218	0.0218	
4	4	0.0008	0.0008	
5	5	0.0034	0.0034	



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4 Blanchard Road
Cumberland, Maine

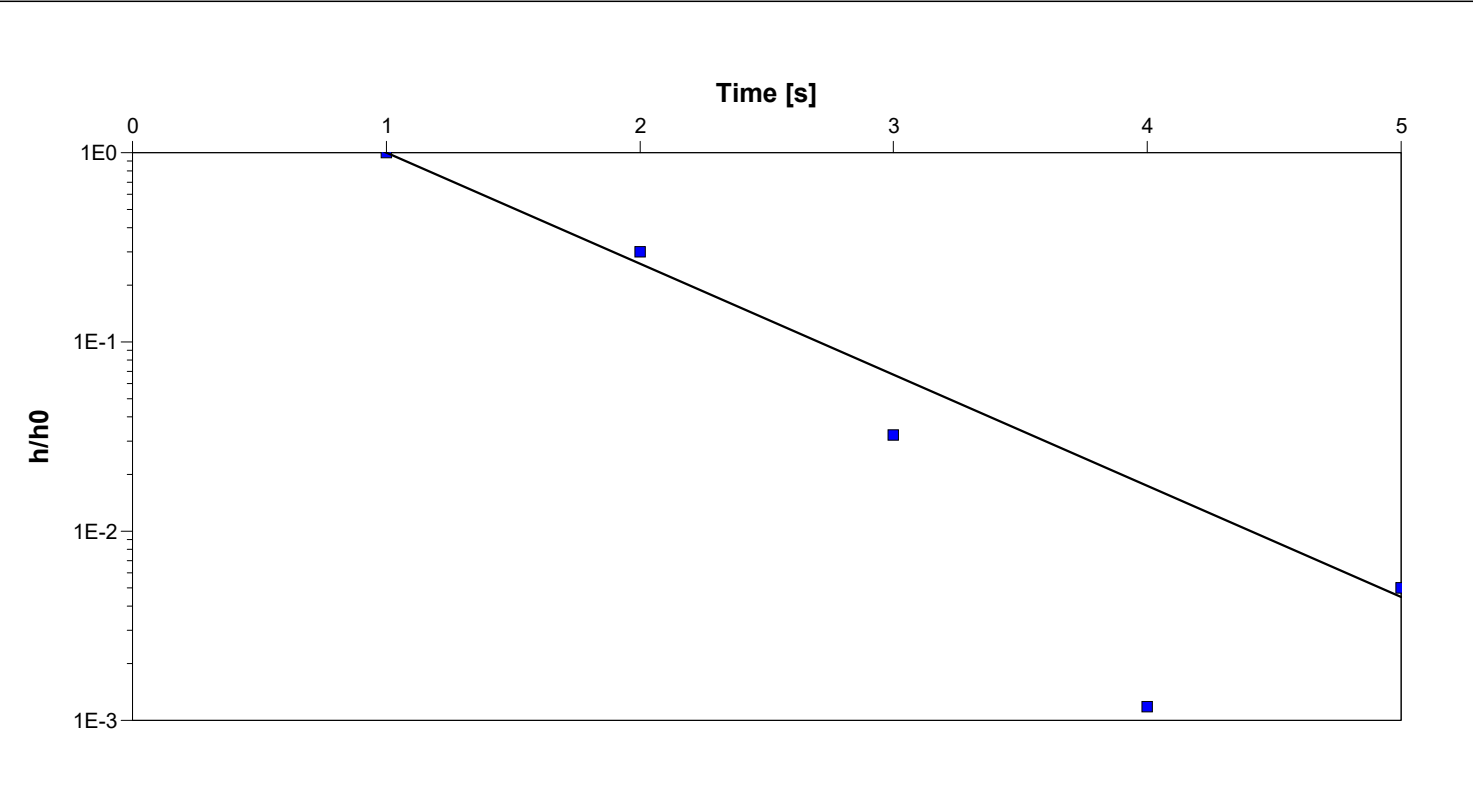
Slug Test Analysis Report

Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: PZ-4 Test 1	Test Well: PZ-4
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	PZ-4 Test 1	Analysis Date: 1/22/2024
Aquifer Thickness: 7.16 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
PZ-4	5.72×10^1	

<div><div>Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine</div><div><div>Waterloo</div><div>HYDROGEOLOGIC</div></div></div>		Slug Test - Water Level Data		Page 1 of 1
		Project: Rusty Lantern Market		
		Number: 231411		
		Client: Cumberland Real Estate Group		
Location: 181 Gray Road, Cumberland		Slug Test: PZ-4 Test 2		Test Well: PZ-4
Test Conducted by: APG		Test Date: 1/9/2024		
Water level at t=0 [ft]: 1.73		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 1.73
	Time [s]	Water Level [ft]	WL Change [ft]	
1	1	1.7309	1.7309	
2	2	0.4184	0.4184	
3	3	0.0981	0.0981	



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4 Blanchard Road
Cumberland, Maine

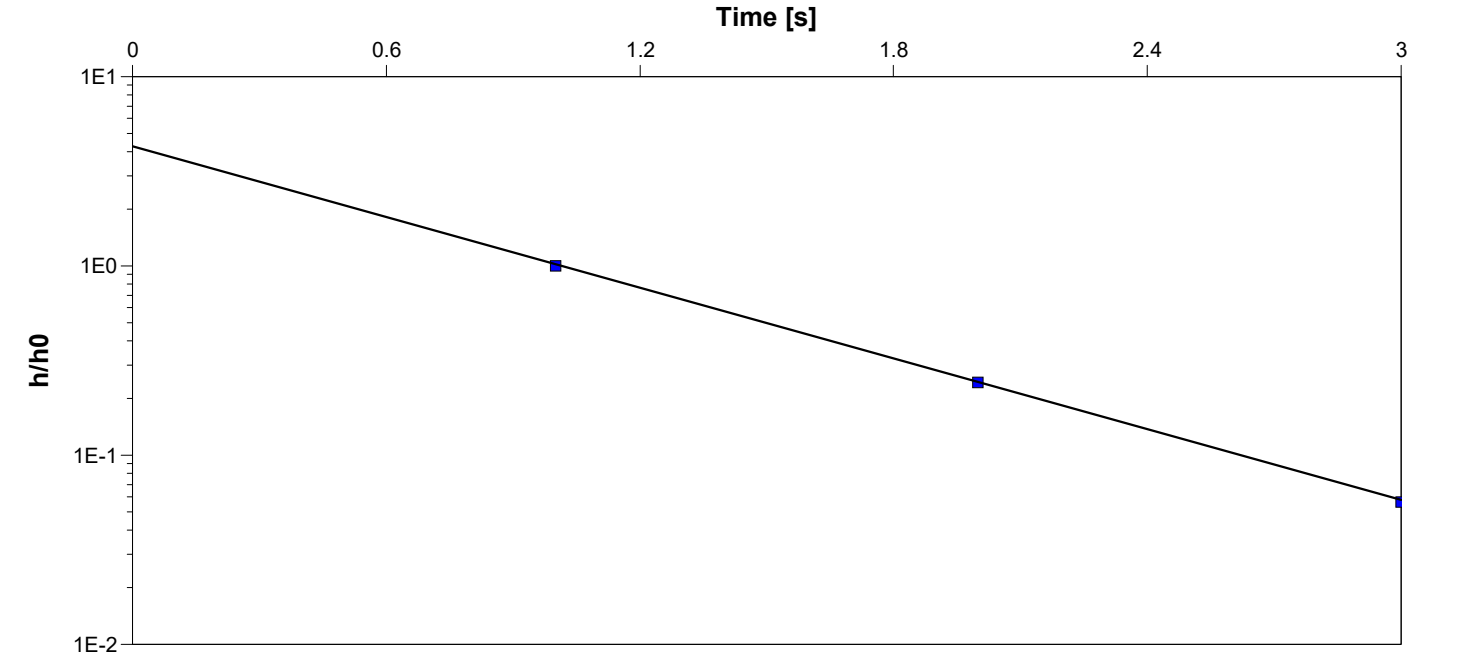
Slug Test Analysis Report

Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: PZ-4 Test 2	Test Well: PZ-4
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	PZ-4 Test 2	Analysis Date: 1/22/2024
Aquifer Thickness: 7.16 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
PZ-4	6.06×10^1	

<div><div>Sevee & Maher Engineers, Inc. 4 Blanchard Road Cumberland, Maine</div><div><div>Waterloo</div><div>HYDROGEOLOGIC</div></div></div>		Slug Test - Water Level Data		Page 1 of 1
		Project: Rusty Lantern Market		
		Number: 231411		
		Client: Cumberland Real Estate Group		
Location: 181 Gray Road, Cumberland		Slug Test: PZ-4 Test 3		Test Well: PZ-4
Test Conducted by: APG		Test Date: 1/9/2024		
Water level at t=0 [ft]: 0.61		Static Water Level [ft]: 0.00		Water level change at t=0 [ft]: 0.61
	Time [s]	Water Level [ft]	WL Change [ft]	
1	1	0.6051	0.6051	
2	2	0.2239	0.2239	
3	3	0.0466	0.0466	
4	4	0.0224	0.0224	
5	5	0.0148	0.0148	
6	6	0.013	0.013	
7	7	0.0084	0.0084	
8	8	0.0074	0.0074	
9	9	0.0052	0.0052	
10	10	0.0044	0.0044	
11	11	0.0039	0.0039	
12	12	0.0029	0.0029	



Sevee & Maher Engineers, Inc.
4 Blanchard Road
Cumberland, Maine

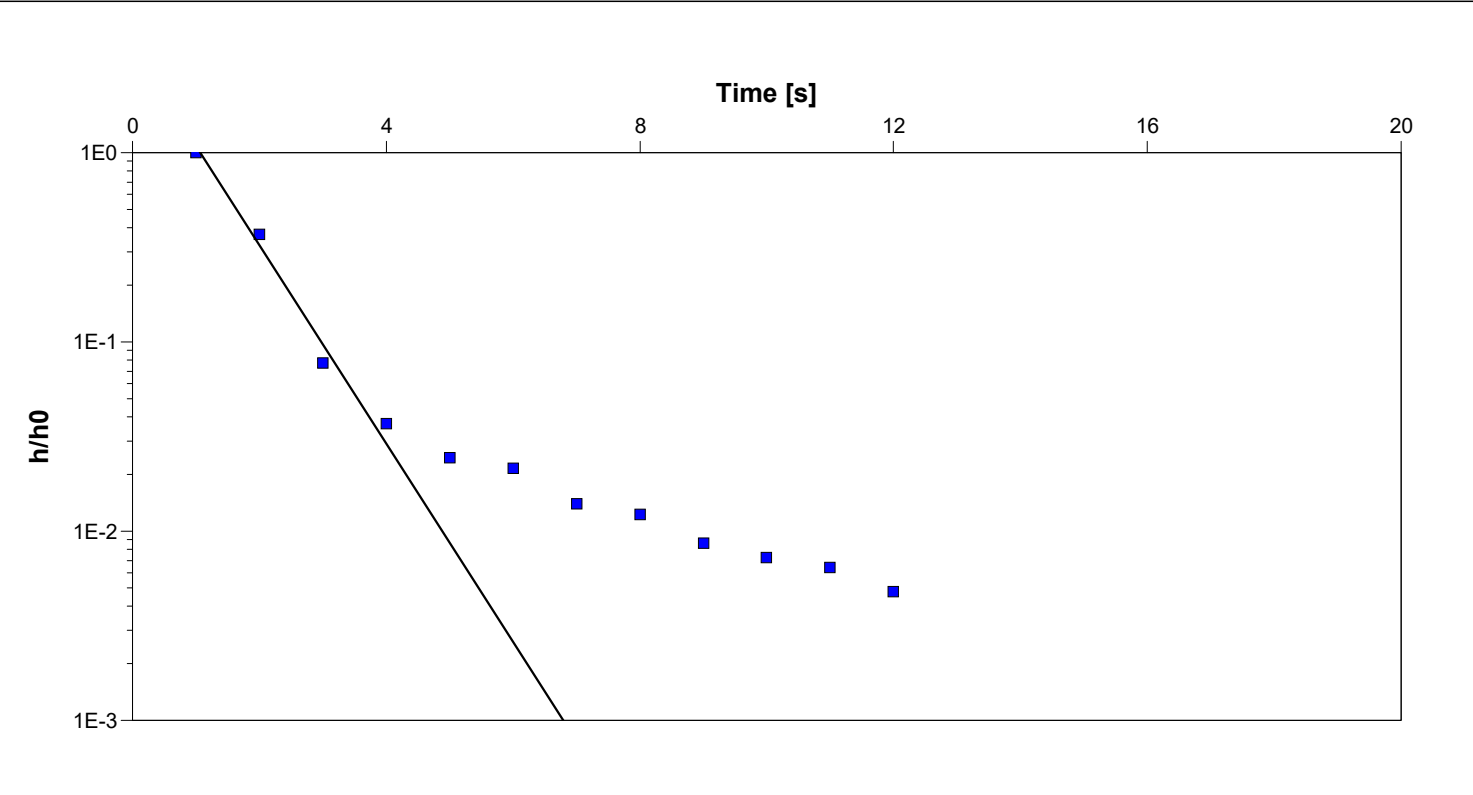
Slug Test Analysis Report

Project: Rusty Lantern Market

Number: 231411

Client: Cumberland Real Estate Group

Location: 181 Gray Road, Cumberland	Slug Test: PZ-4 Test 3	Test Well: PZ-4
Test Conducted by: APG		Test Date: 1/9/2024
Analysis Performed by: APG	PZ-4 Test 3	Analysis Date: 1/22/2024
Aquifer Thickness: 7.16 ft		



Calculation using Bouwer & Rice		
Observation Well	Hydraulic Conductivity [ft/d]	
PZ-4	5.10×10^1	

Attachment L **Architecture**



The project site plans are included for review as a separate plan set of full site documents.

Rusty Lantern Market Architectural Renderings



Rendering 1: Store Entrance



Rendering 2: Store Entrance

Rusty Lantern Market Architectural Renderings



Rendering 3: Store Entrance



Rendering 4: Store from Skillin Road Entrance

Rusty Lantern Market Architectural Renderings



Rendering 5 Store from Skillin Road Entrance



Rendering 6: Rear Façade of Store from Skillin Road

Rusty Lantern Market Architectural Renderings



Rendering 7 Rear Façade of Store from Skillin Road



Rendering 8: Rear Façade of Store from Skillin Road and Gray Road

Rusty Lantern Market Architectural Renderings



Rendering 9: Gazebo



Rendering 10: Side Façade of Store from Skillin Road and Gray Road

Rusty Lantern Market Architectural Renderings



Rendering 11: Rear Façade of Store from Skillin Road and Gray Road



Rendering 12: Gazebo

Rusty Lantern Market Architectural Renderings



Rendering 13: Entrance to Site from Skillin Road



Rendering 14: Aerial Perspective View

Rusty Lantern Market Architectural Renderings



Rendering 15 Aerial Perspective View



Rendering 16: Site Entrance from Gray Road

Rusty Lantern Market Architectural Renderings



Rendering 17: View from South End of Store Parcel



Rendering 18: View from South End of Store Parcel

Rusty Lantern Market Architectural Renderings



Rendering 19: View from Blackstrap Road

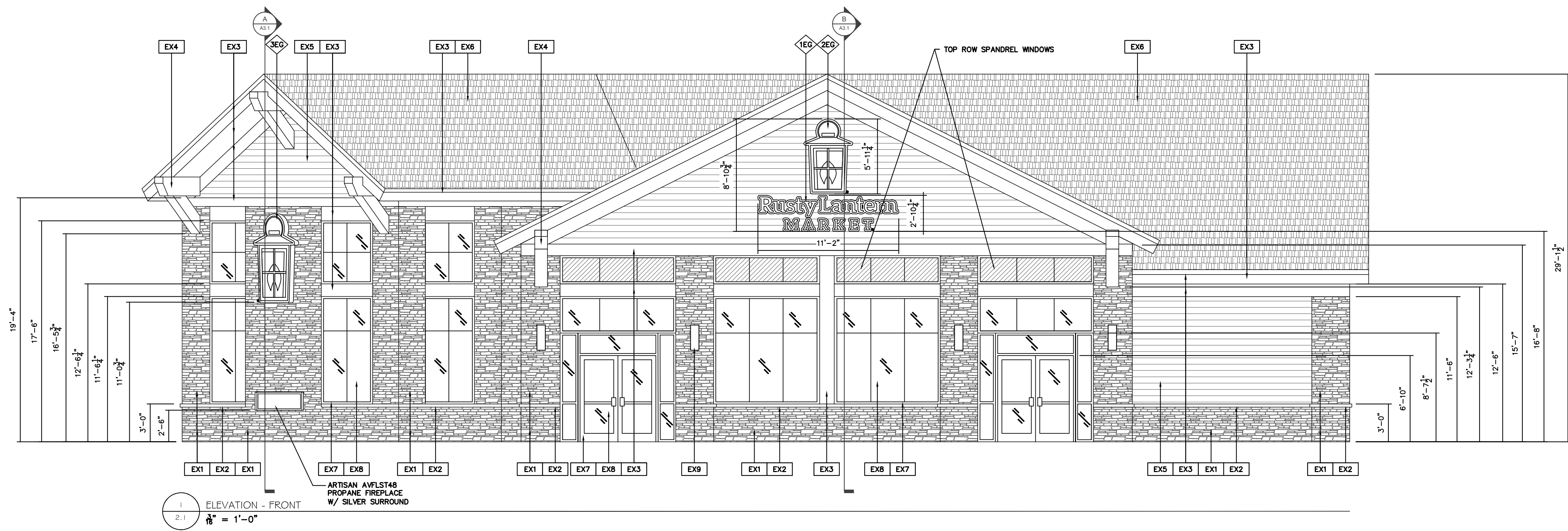


Rendering 20: View from Blackstrap Road

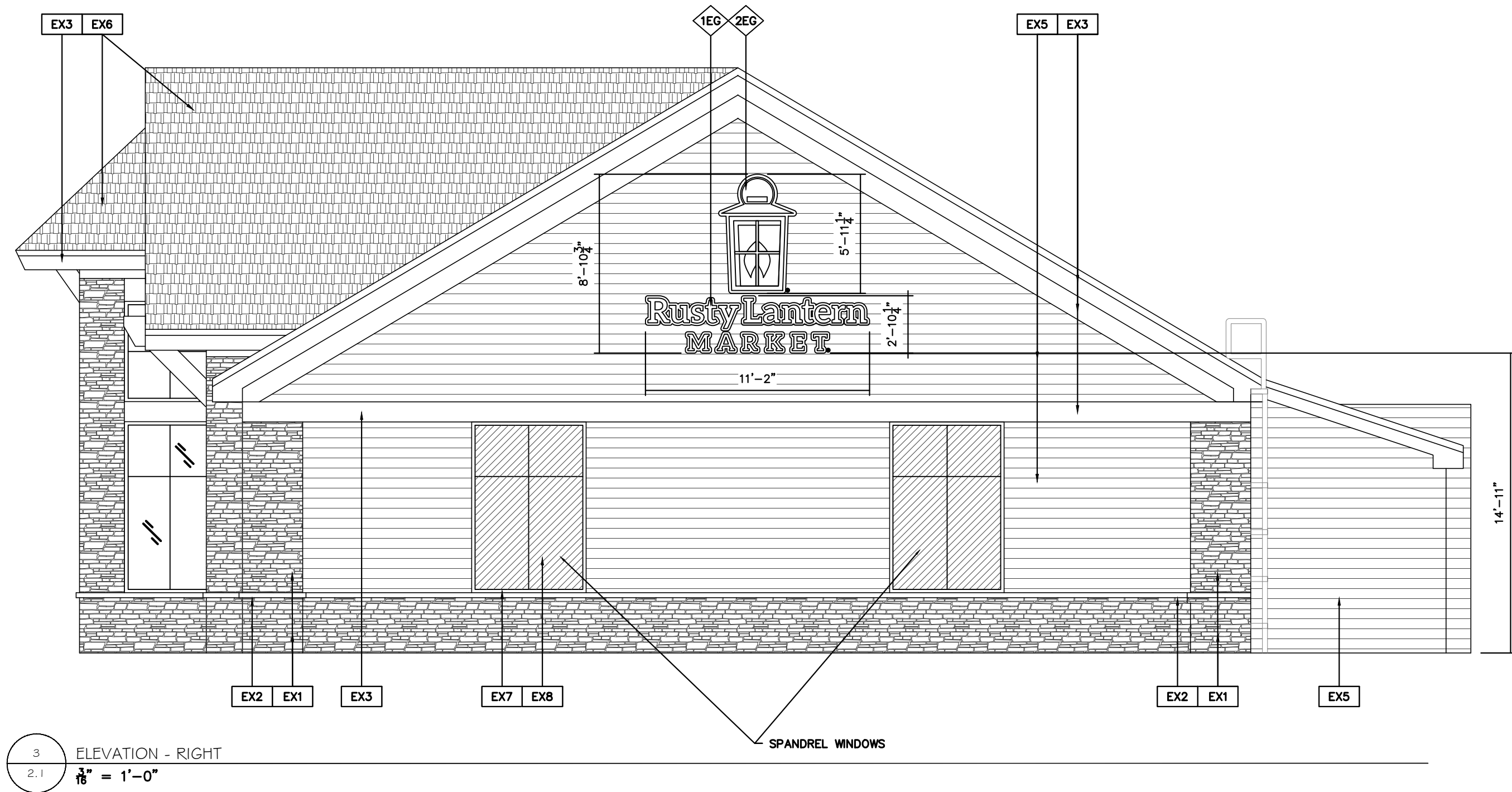
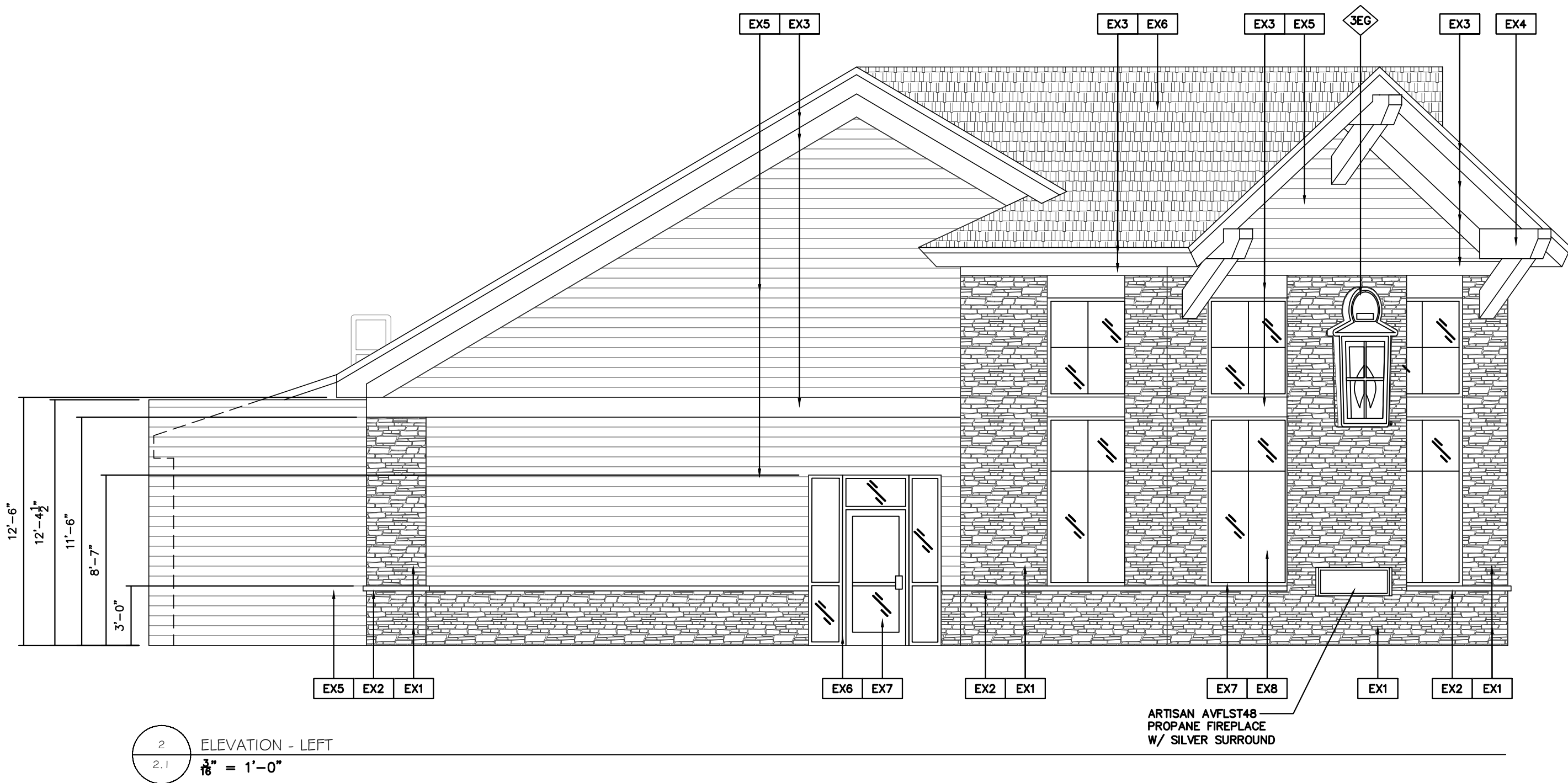
Rusty Lantern Market Architectural Renderings



Rendering 21: View from Southbound Gray Road



SEE A2.2 FOR
EXTERIOR GRAPHICS SCHEDULE AND
EXTERIOR FINISH SCHEDULE



RUSTY LANTERN MARKET- GEN 2
181 GRAY ROAD
CUMBERLAND, MAINE

JOB: 23102

ISSUE DATE	
PRELIM	04-20-2023
SFMO	06-30-2023
CD's	-
REV. 1	-
REV. 2	-
REV. 3	-

EXTERIOR ELEVATIONS

Attachment M
Site Plans

M

The project site plans are included for review as a separate plan set of full site documents.

Site Plans

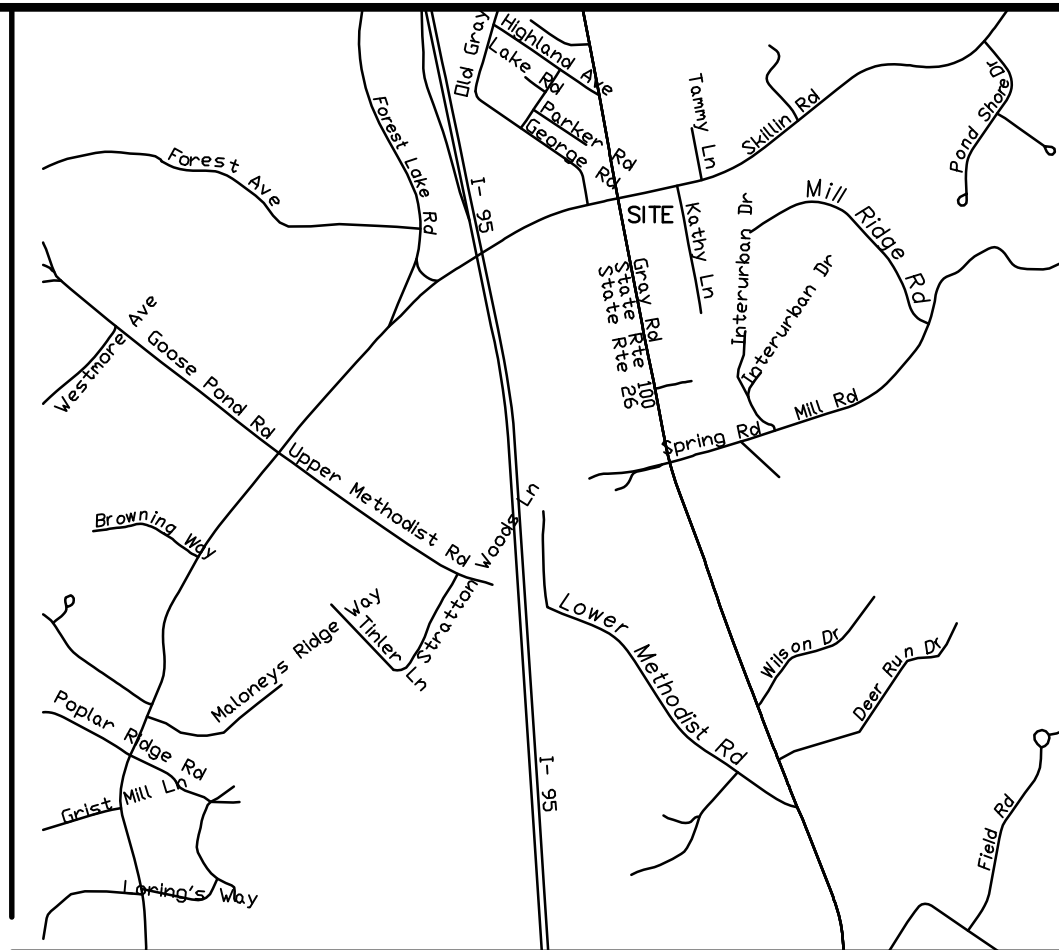
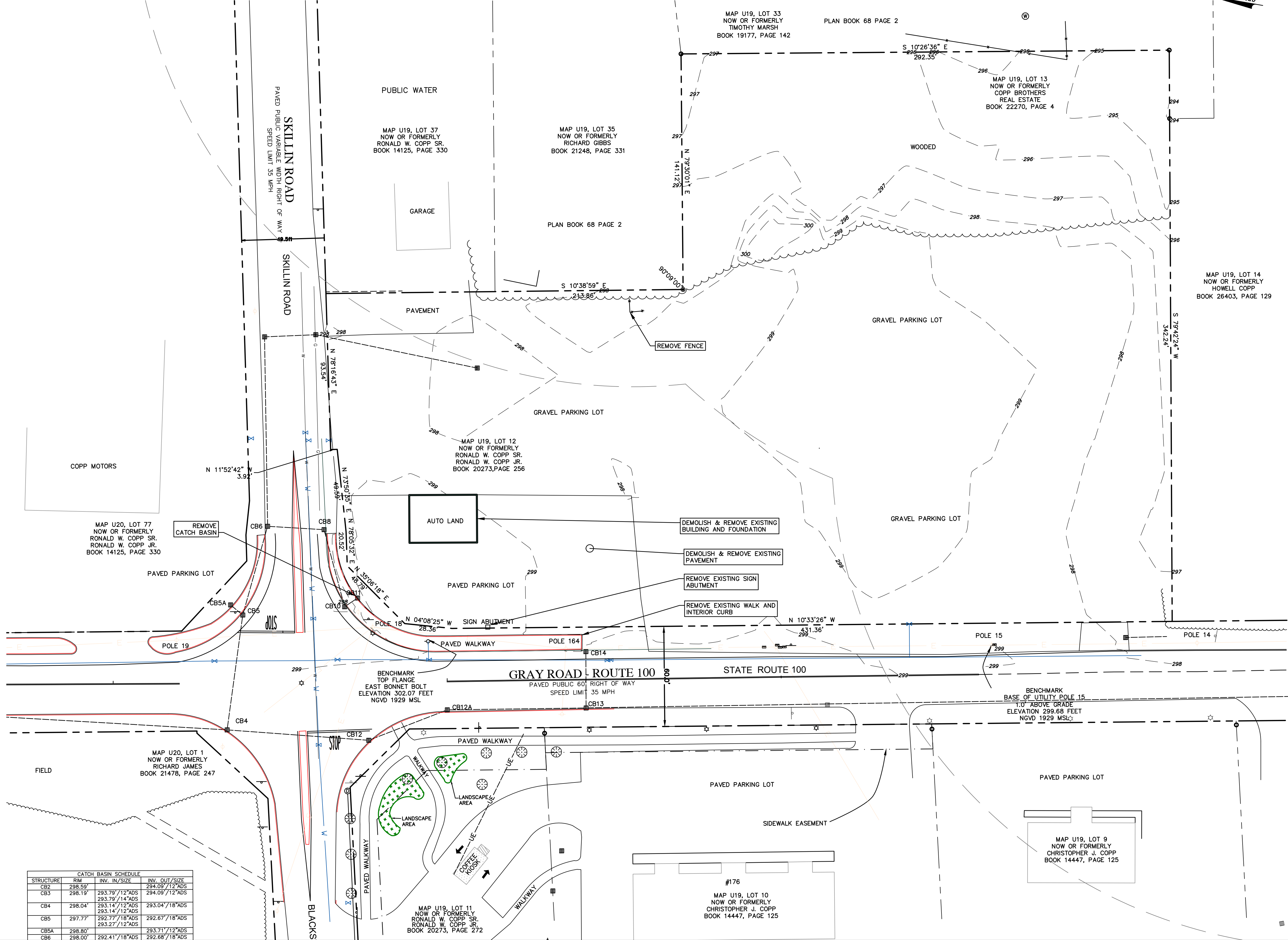
C:\USERS\CURT NEUFELD\ONE DRIVE\DOCUMENTS\PROJECTS\22-RLM-004 CUMBERLAND\DWG\22-004 SITE.DWG, C2 EX COND-DEMO, 1/30/2024 9:41 AM, CURT NEUFELD

- 1) A DEMOLITION PERMIT MUST BE OBTAINED FROM THE TOWN OF BRUNSWICK PRIOR TO COMMENCEMENT OF WORK. ALL EXISTING UTILITY DISCONNECTIONS MUST BE COORDINATED WITH RESPECTIVE UTILITY COMPANIES.
- 2) ALL DEMOLITION ACTIVITIES ARE TO BE PERFORMED IN STRICT ADHERENCE TO ALL FEDERAL, STATE AND LOCAL REGULATIONS. CONTRACTOR TO INSTALL EROSION CONTROL DEVICES IN ACCORDANCE WITH GRADING & DRAINAGE PLAN PRIOR TO BEGINNING DEMOLITION ACTIVITIES.
- 3) PROCEED WITH DEMOLITION IN A SYSTEMATIC MANNER. FROM THE TOP OF THE STRUCTURE(S) TO THE GROUND.
- 4) DEMOLISH CONCRETE IN ALL SECTIONS.
- 5) BREAK UP CONCRETE SLABS-ON-GRADE UNLESS OTHERWISE DIRECTED BY THE CONSTRUCTION MANAGER.
- 6) CONDUCT ALL DEMOLITION OPERATIONS IN A MANNER THAT WILL PREVENT INJURY, DAMAGE TO STRUCTURES, ADJACENT BUILDINGS AND ALL PERSONS.
- 7) REFRAIN FROM USING EXPLOSIVES WITHOUT PRIOR WRITTEN CONSENT OF THE DEVELOPER AND APPLICABLE GOVERNMENTAL AUTHORITIES.
- 8) CONDUCT DEMOLITION SERVICES IN SUCH A MANNER TO INSURE MINIMUM INTERFERENCE WITH ROADS, STREETS, WALKS AND OTHER ADJACENT FACILITIES. DO NOT CLOSE OR OBSTRUCT STREETS, WALKS OR OTHER OCCUPIED FACILITIES WITHOUT PRIOR WRITTEN PERMISSION OF THE DEVELOPER AND APPLICABLE GOVERNMENTAL AUTHORITIES. PROVIDE ALTERNATE ROUTES AROUND CLOSED OR OBSTRUCTED TRAFFICWAYS IF REQUIRED BY APPLICABLE GOVERNMENTAL REGULATIONS.

- 9) USE WATERING, TEMPORARY ENCLOSURES AND OTHER SUITABLE METHODS, AS NECESSARY, TO LIMIT THE AMOUNT OF DUST AND DIRT RISING AND SCATTERING IN THE AIR. CLEAN ADJACENT STRUCTURES AND SURFACES OF ALLEYS AND DRIVEWAYS OF DIRT AND DEBRIS BY DEMOLITION OPERATIONS. RETURN ALL ADJACENT AREAS TO THE CONDITIONS EXISTING PRIOR TO THE START OF WORK.
- 10) ACCOMPLISH AND PERFORM THE DEMOLITION IN SUCH A MANNER AS TO PREVENT THE UNAUTHORIZED ENTRY OF PERSONS AT ANY TIME.
- 11) COMPLETELY FILL BELOW GRADE AREAS AND VOIDS RESULTING FROM THE DEMOLITION OF STRUCTURES AND FOUNDATIONS WITH SOIL MATERIALS CONSISTING OF STONE, GRAVEL AND SAND, FREE FROM DEBRIS, TRASH, FILL, OR HAZARDOUS AND OTHER ORGANIC MATERIAL. STONES USED WILL NOT BE LARGER THAN 6 INCHES IN DIMENSION. MATERIAL FROM DEMOLITION MAY NOT BE USED AS FILL PRIOR TO PLACEMENT OF FILL MATERIALS. UNDERTAKE ALL NECESSARY ACTION IN ORDER TO INSURE THAT AREAS TO BE FILLED ARE FREE OF SUBSURFACE WATER, ALLEYS AND DRIVEWAYS TRASH, DEBRIS, PLACEMENT LAYERS NOT EXCEEDING 6 INCHES IN LOOSE DEPTH AND COMPACT EACH LAYER AT PLACEMENT TO 95% OPTIMUM DENSITY. GRADE SURFACE TO MEET ADJACENT CONTOURS AND TO PROVIDE SURFACE DRAINAGE.
- 12) REMOVE FROM THE DESIGNATED SITE, AT THE EARLIEST POSSIBLE TIME, ALL DEBRIS RUBBISH, SALVAGEABLE ITEMS, HAZARDOUS AND COMBUSTIBLE SERVICES. REMOVED MATERIALS MAY NOT BE STORED, SOLD OR BURNED ON SITE. REMOVAL OF HAZARDOUS AND COMBUSTIBLE MATERIALS SHALL BE ACCOMPLISHED IN ACCORDANCE WITH THE PROCEDURES AS AUTHORIZED BY THE FIRE DEPARTMENT OR OTHER APPROPRIATE REGULATORY AGENCIES AND DEPARTMENTS.
- 13) DISCONNECT, SHUT OFF AND SEAL ALL UTILITIES SERVING THE STRUCTURE(S) TO BE DEMOLISHED BEFORE THE DEMOLITION WORK IS INITIATED. DEMOLITION MARK FOR POSITION ALL UTILITY DRAINAGE AND SANITARY LINES AND PROTECT ALL ACTIVE LINES. CLEARLY IDENTIFY BEFORE THE COMMENCEMENT OF DEMOLITION SERVICES THE REQUIRED INTERUPTION OF ACTIVE SYSTEMS THAT MAY AFFECT OTHER PARTIES, AND NOTIFY ALL

14) PROTECT EXISTING DRAINAGE SYSTEM(S) AS NECESSARY TO PREVENT SEDIMENT FROM ENTERING DURING CONSTRUCTION. SEE DETAIL SHEETS FOR EROSION CONTROL DEVICES.

- 15) ALL WORK WITHIN ROADWAY RIGHT-OF-WAYS TO CONFORM TO TOWN OF BRUNSWICK and MaineDOT STANDARDS.
- 16) THE LIMITS OF WORK SHALL BE CLEARLY MARKED IN THE FIELD PRIOR TO THE START OF CONSTRUCTION OR SITE CLEARING.
- 17) NOTES ON THIS PLAN THAT READ "TBR" REPRESENT FEATURES TO BE REMOVED. ANY FEATURES NOT LABELED "TBR" OR "TO BE REMOVED" SHALL BE CONSIDERED EXISTING TO REMAIN.

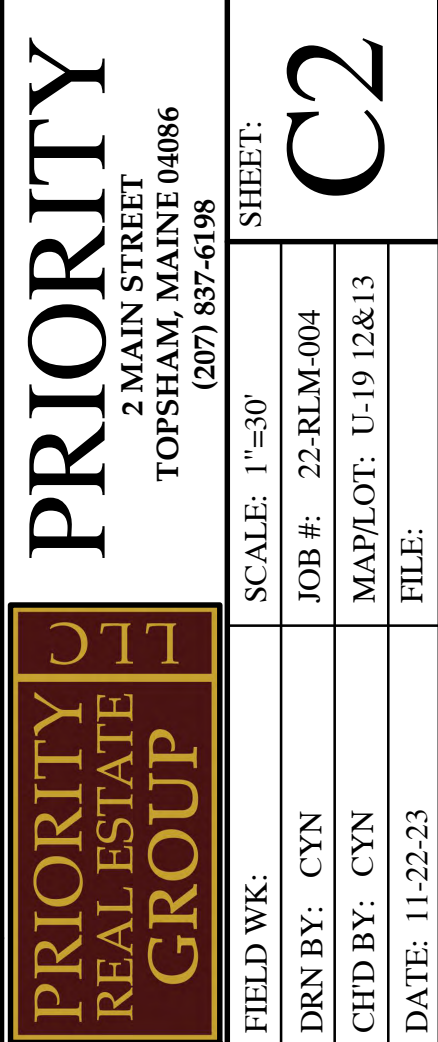


LOCATION MAP
NOT TO SCALE

THIS PLAN DEPICTS CONDITIONS FOUND AND SURVEYED BY MAIN-LAND AS OF APRIL, 2023. SUPPORTING DATA IS FROM THE INFORMATION BELOW.

1. TITLE REFERENCE FOR SURVEYED PARCEL:
BK XXX, PG XXX
BK XXX, PG XXX
2. PLAN REFERENCE(S):
a) PLAN ENTITLED, "EXISTING CONDITIONS SURVEY FOR PRIORITY REAL ESTATE GROUP OF 181 GRAY ROAD, CUMBERLAND, MAINE 04021", DATED 5-30-2023, BY MAIN-LAND, LIVERMORE FALLS. NOT RECORDED.
3. AREA INFORMATION:
XXX ACRES
4. TAX MAP REFERENCE:
TAX MAP U19, LOT 12,13
5. BASIS OF BEARINGS:
BEARINGS ARE BASED ON MAINE STATE PLANE GRID, WEST ZONE, NORTH AMERICAN DATUM 1983.
6. ROAD INFORMATION:
GRAY ROAD WIDTH IS XXX' PER PLANS REFERENCED IN NOTE 2(a) THROUGH 2(d) ABOVE. LOCATION IS BASED ON EVIDENCE FOUND.
7. UTILITY INFORMATION:

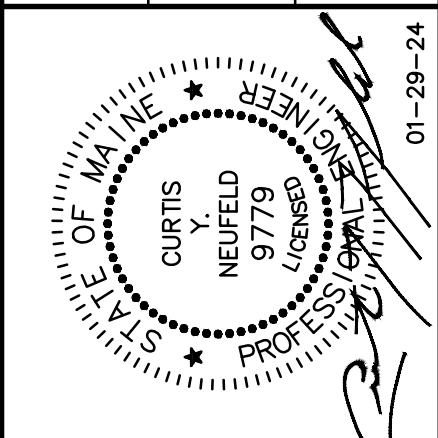
THERE MAY BE UNDERGROUND CONDUIT, WRES, CABLES AND/OR STRUCTURES NOT SHOWN ON THIS PLAN. THE LOCATIONS SHOWN ARE BASED ON SURFACE FEATURES VISIBLE AT THE TIME OF SURVEY AND POSSIBLY FROM INFORMATION PROVIDED BY THE OWNER, MUNICIPAL GIS DATA, AND/OR UTILITY COMPANIES. NO EXCAVATIONS WERE MADE DURING THE COURSE OF THE SURVEY TO VERIFY OR LOCATE ANY UNDERGROUND STRUCTURES. IT IS THE RESPONSIBILITY OF THE OWNER/CONTRACTOR TO VERIFY THE LOCATION OF ANY UNDERGROUND UTILITIES PRIOR TO EXCAVATING BY CONTACTING THE APPROPRIATE UTILITY COMPANY. STATE LAW REQUIRES DIG-SAFE BE CONTACTED PRIOR TO EXCAVATION.



EXISTING CONDITIONS PLAN

RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBER; LAND, ME 04021

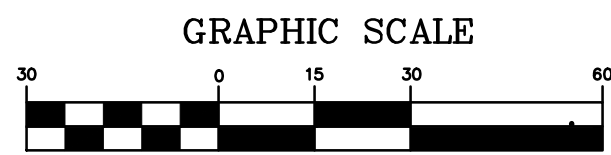
CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

[illegible]

NOT FOR CONSTRUCTION

THIS PLAN IS ISSUED FOR REVIEW AND INFORMATION PURPOSES ONLY. THIS PLAN WILL CHANGE AND IS NOT INTENDED FOR PRICING OR CONSTRUCTION.

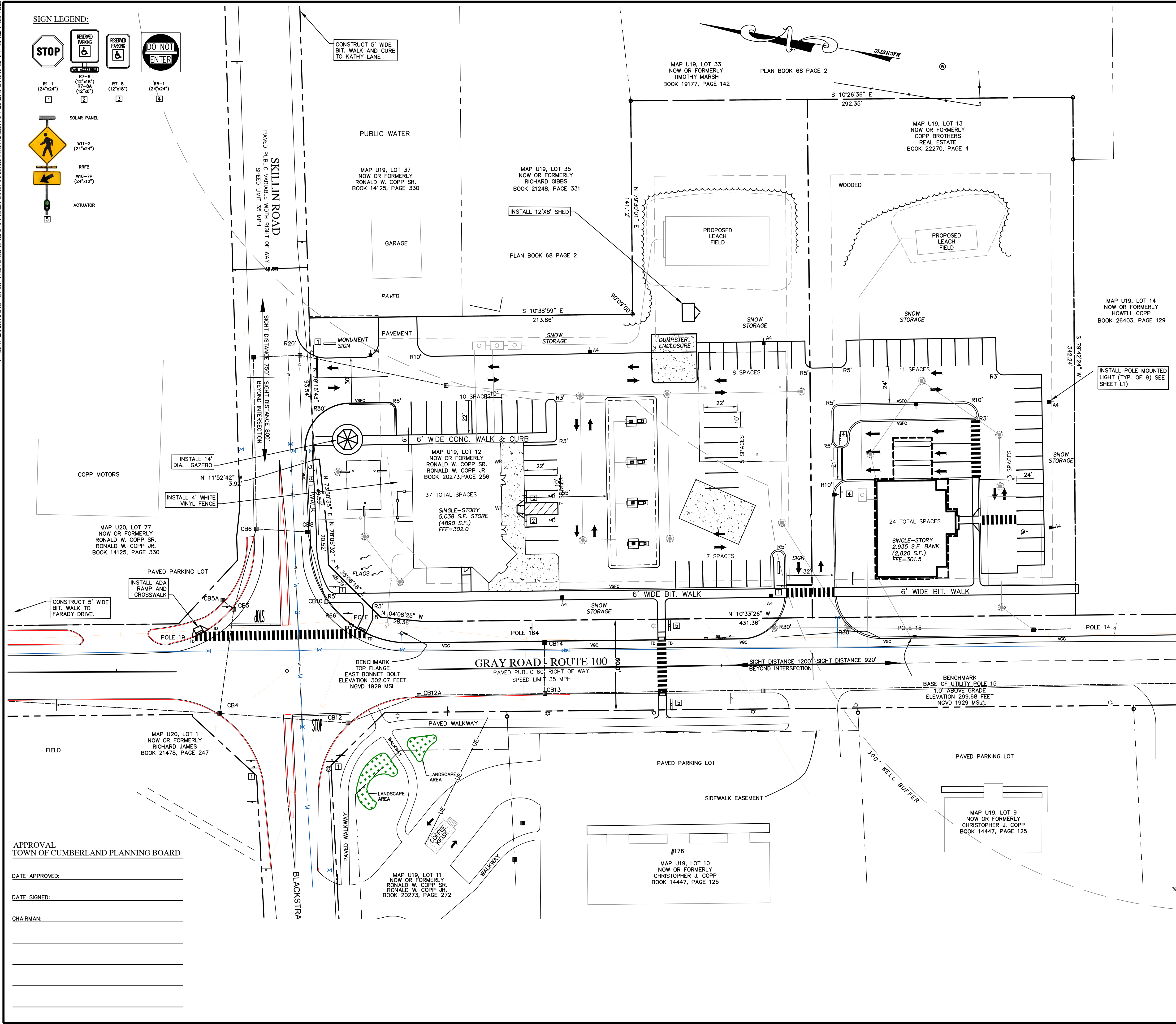
PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.



ISSUED FOR:
PERMITTING

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CUMBERLAND NEILFELD/COURT NEILFELD/PROJECTS/22-RLM-004 CUMBERLAND/02-004 SITE DWG. C3 SITE, 1/30/2024 9:41 AM, CURT NEILFELD

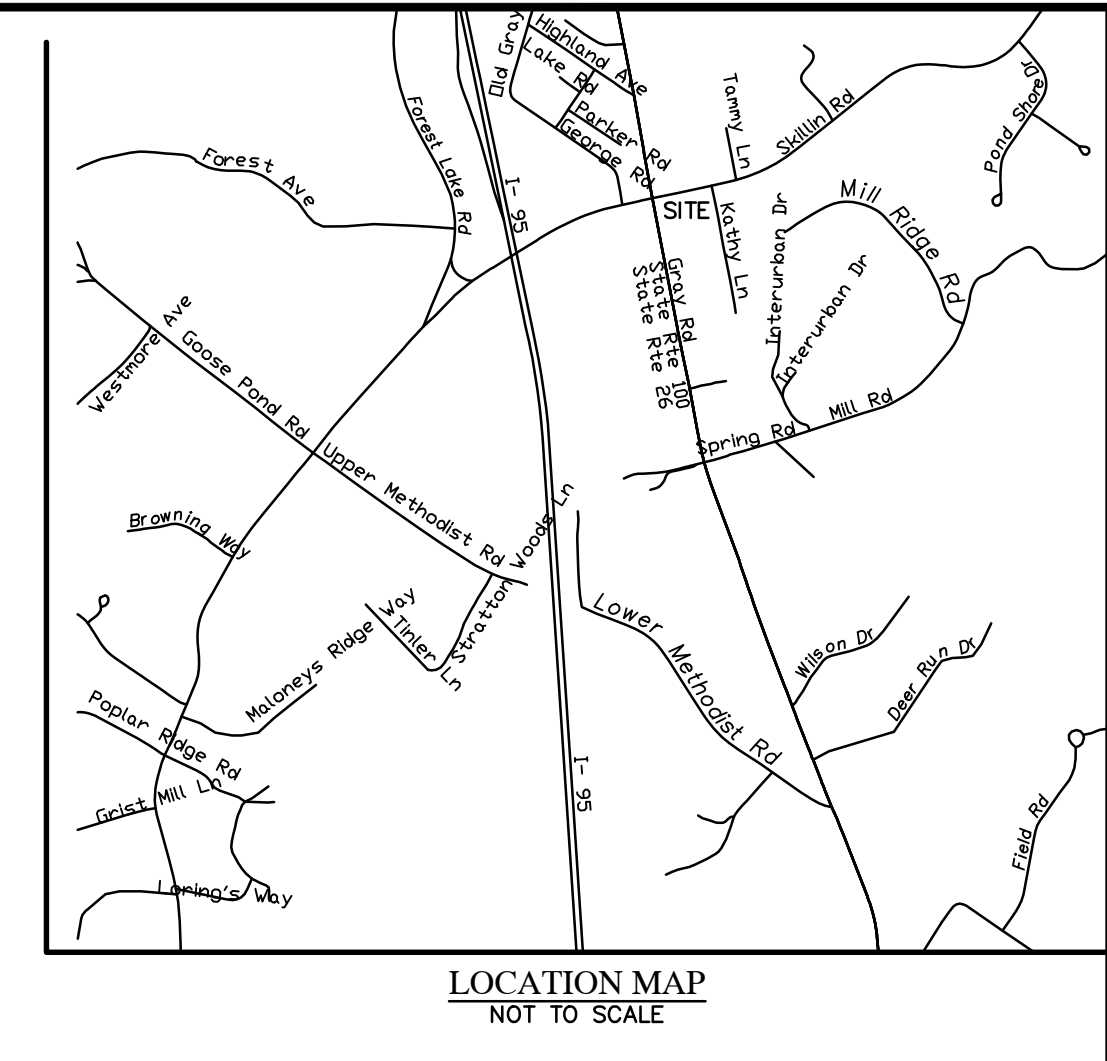


APPROVAL
TOWN OF CUMBERLAND PLANNING BOARD

DATE APPROVED: _____

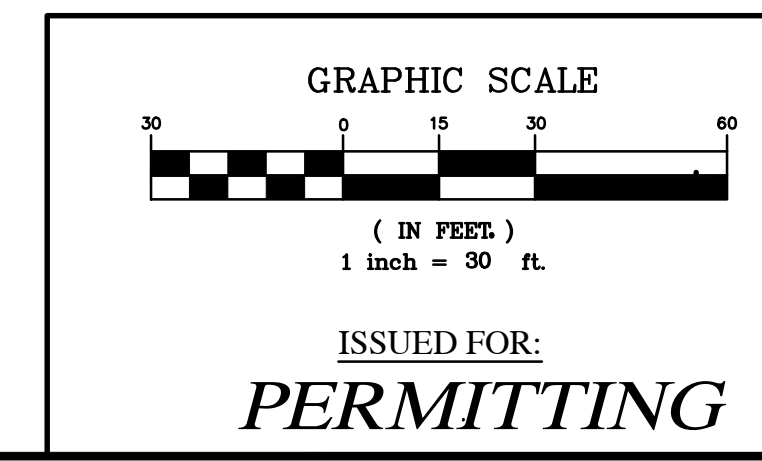
DATE SIGNED: _____

CHAIRMAN: _____



- GENERAL NOTES:**
- TITLE REFERENCE FOR SURVEYED PARCEL:**
BK 20273, PG 256 (U19-12)
BK 34640, PG 209 (U19-13)
 - PLAN REFERENCE(S):**
(1) EXISTING CONDITIONS SURVEY FOR PRIORITY REAL ESTATE GROUP OF 181 GRAY ROAD, CUMBERLAND, MAINE 04021, PREPARED BY BOUNDARY POINTS, NOT RECORDED.
 - AREA INFORMATION:**
LOT AREA: 141,116 S.F. (3.24 ACRES)
 - TAX MAP REFERENCE:**
TAX MAP U19, LOT 12 & 13.
 - BASIS OF BEARINGS:**
BEARINGS ARE MAINE STATE PLANE, WEST ZONE, NAD 83.
 - ELEVATION DATUM:**
NGVD 1929 MSL
 - FLOOD ZONE INFORMATION:**
PARCEL IS LOCATED WITHIN ZONE C (AREAS OF MINIMAL FLOODING) OF THE FLOOD INSURANCE RATE MAPS FOR CUMBERLAND COUNTY, MAINE. THE PROJECT IS LOCATED ON PANEL 15 OF 25 (COMMUNITY PANEL 230162 0015 B, EFF. DATE MAY 19, 1981)
 - IMPERVIOUS AREA:**
EXISTING IMPERVIOUS AREA: 94,773 S.F. (2.18 AC)
PROPOSED IMPERVIOUS AREA: 68,232 S.F. (1.57 AC)
NET CHANGE IN IMPERVIOUS AREA: -26,541 S.F. (0.61 AC)
- UTILITY NOTES:**
- INFORMATION REGARDING THE LOCATION OF EXISTING UNDERGROUND UTILITIES IS A COMPILATION OF THAT FOUND IN THE FIELD AND THAT SHOWN ON A PREVIOUS PLANS, AND SHALL NOT BE CONSIDERED AN AS-BUILT PLAN. CONTRACTOR SHALL BE RESPONSIBLE FOR FIELD VERIFYING UTILITY LOCATIONS PRIOR TO COMMENCING WORK. NOTIFY ENGINEER OF ANY DISCREPANCY BETWEEN UTILITIES AS SHOWN AND AS FOUND. CONTRACTOR SHALL NOTIFY DIG-SAFE PRIOR TO EXCAVATION. 1-888-344-7233

- LAYOUT NOTES:**
- ALL DIMENSIONING, UNLESS NOTED OTHERWISE, IS TO THE FACE OF CURB OR FOUNDATION.
 - BOUNDARY INFORMATION ON LAYOUT PLAN IS FOR REFERENCE ONLY. REFER TO CERTIFIED BOUNDARY PLANS FOR BOUNDARY INFORMATION.
 - ALL HANDICAP ACCESSIBLE PARKING SPACES, RAMPS AND SIDEWALKS SHALL BE CONSTRUCTED IN CONFORMANCE WITH THE AMERICANS WITH DISABILITIES ACT (ADA).
 - ALL SITE SIGNAGE AND PAVEMENT MARKINGS SHALL CONFORM TO THE MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES (MUTCD)
 - BUILDING FOUNDATION SHOWN IS NOT FOR FOUNDATION LAYOUT. COORDINATE SITE WORK WITH ARCHITECTURAL DRAWINGS INCLUDING BUILDING FEATURES AND FOUNDATION PLAN.
 - REFER TO SHEET C4 FOR GRADING AND DRAINAGE INFORMATION.
 - REFER TO SHEET L1 FOR LANDSCAPE INFORMATION.
 - REFER TO SHEET L2 FOR LIGHTING INFORMATION.



PRIORITY REAL ESTATE GROUP

SITE PLAN

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PROJECT: RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME 04021

PREPARED FOR: CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

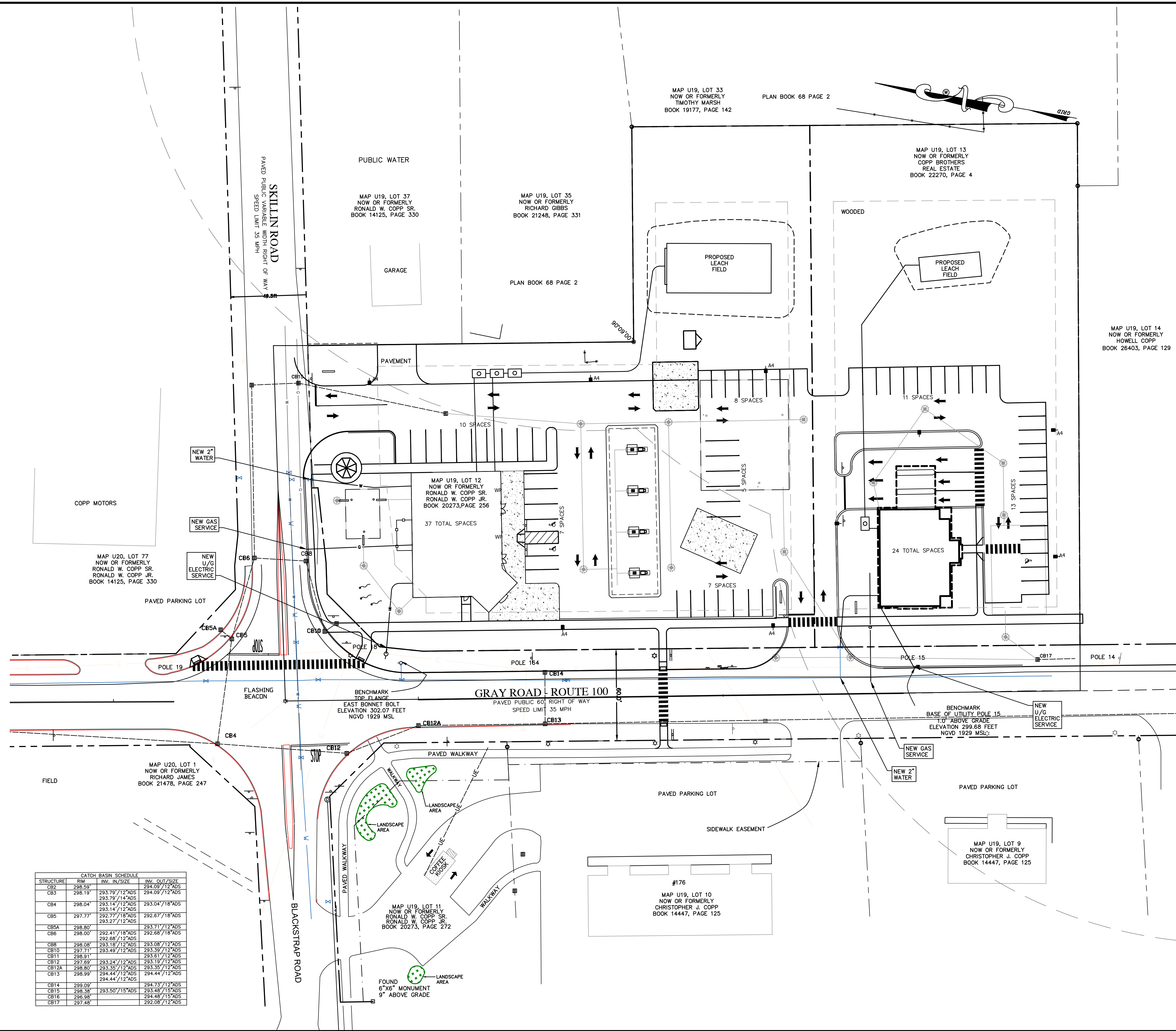
DATE: 11-22-23

FIELD WK: CYN
DRN BY: CYN
CHD BY: CYN
FILE:

SCALE: 1"=30'

JOB #: 22-RLM-004
MAP/LOT: U-19 12&13

SHEET: C3



CATCH BASIN SCHEDULE			
STRUCTURE	R/W	INV. IN/SIDE	INV. OUT/SIDE
CB2	298.50		294.09 / 12'AD
CB3	298.19	293.79 / 12'AD	294.09 / 12'AD
		293.79 / 14'AD	
CB4	298.77	293.14 / 12'AD	293.04 / 16'AD
		293.14 / 12'AD	
CB5	299.07	292.77 / 18'AD	292.67 / 16'AD
		293.27 / 12'AD	
CB5A	298.80		293.71 / 12'AD
CB6	298.00	293.41 / 18'AD	292.68 / 18'AD
		292.68 / 12'AD	
CB8	298.08	293.18 / 12'AD	293.08 / 12'AD
CB10	297.71	293.49 / 12'AD	293.39 / 12'AD
CB11	298.91		293.61 / 12'AD
		292.60 / 12'AD	
CB12A	298.80	293.25 / 12'AD	293.15 / 12'AD
CB13	298.99	294.44 / 12'AD	294.44 / 12'AD
		294.44 / 12'AD	
CB14	299.09		294.73 / 12'AD
CB15	298.36	293.70 / 15'AD	293.48 / 15'AD
CB16	298.98		293.80 / 12'AD
CB17	297.48		292.08 / 12'AD

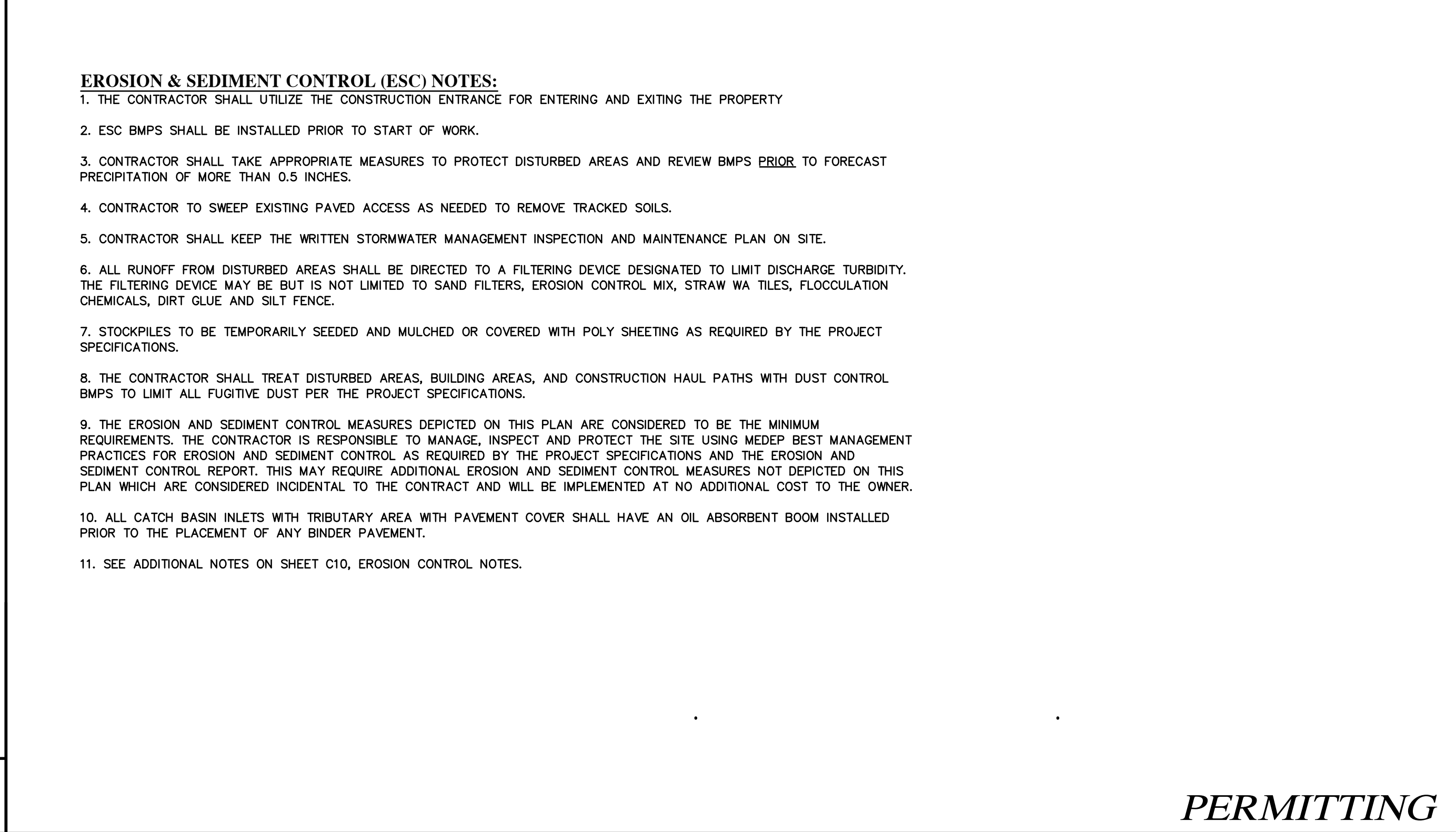
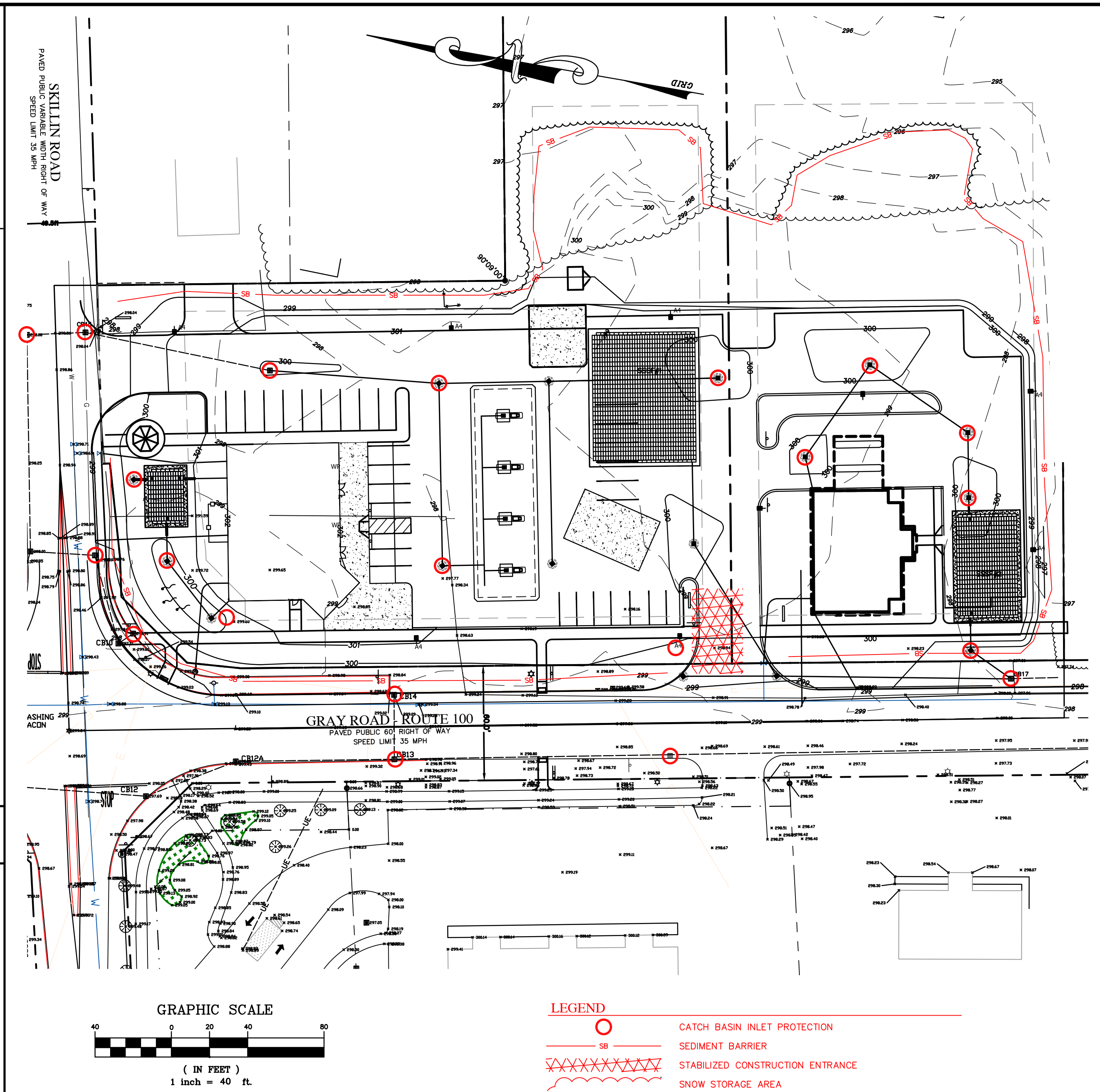
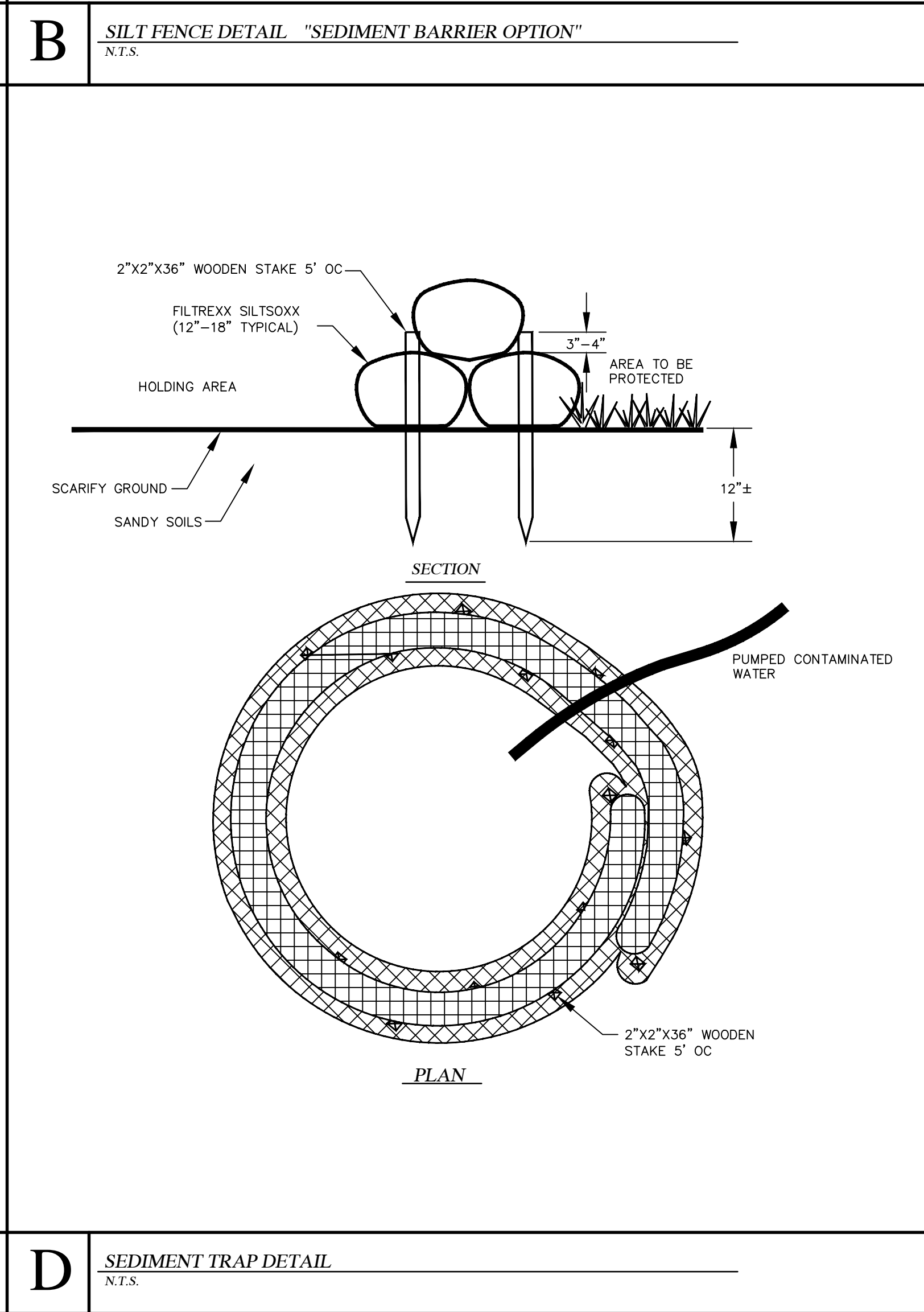
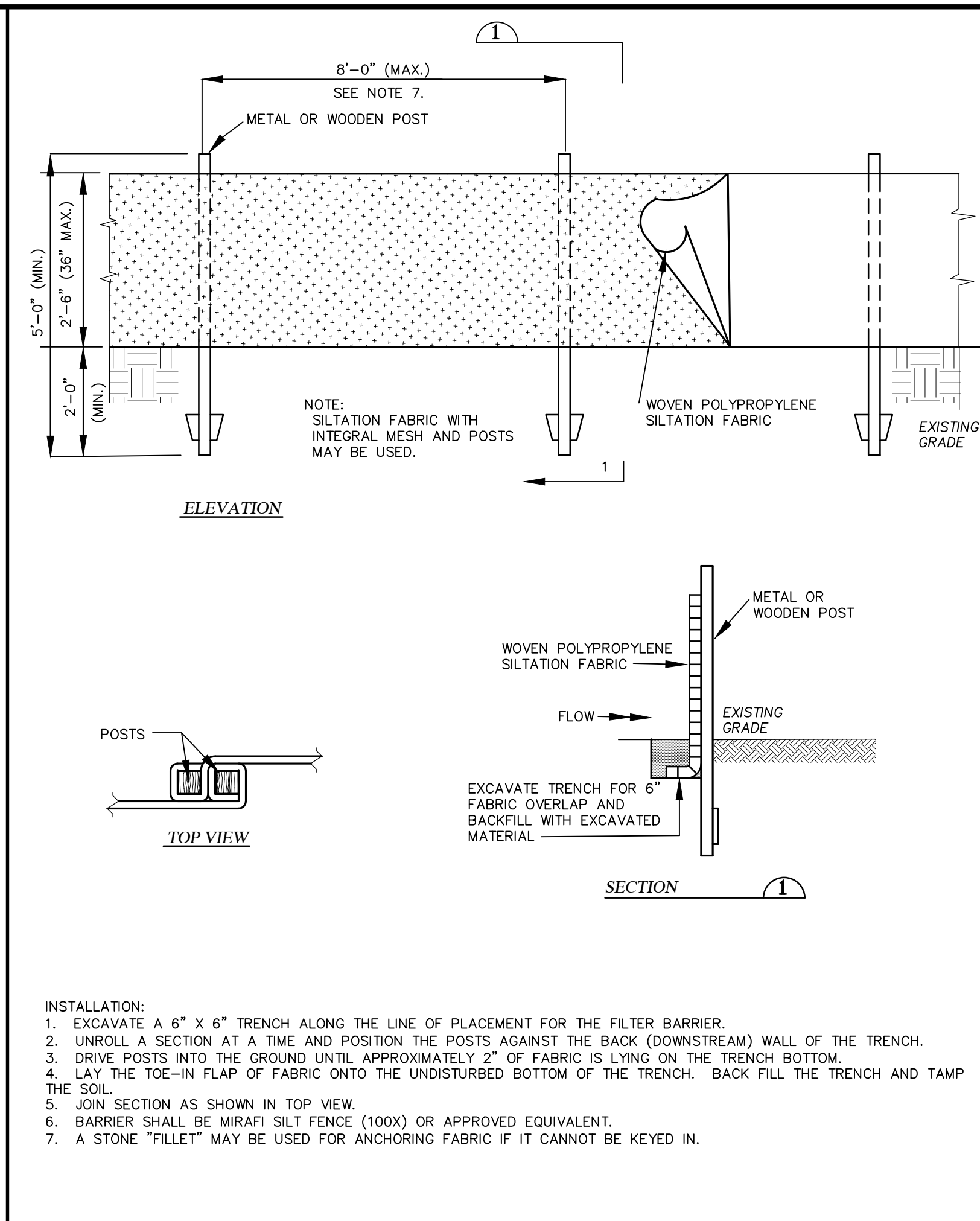
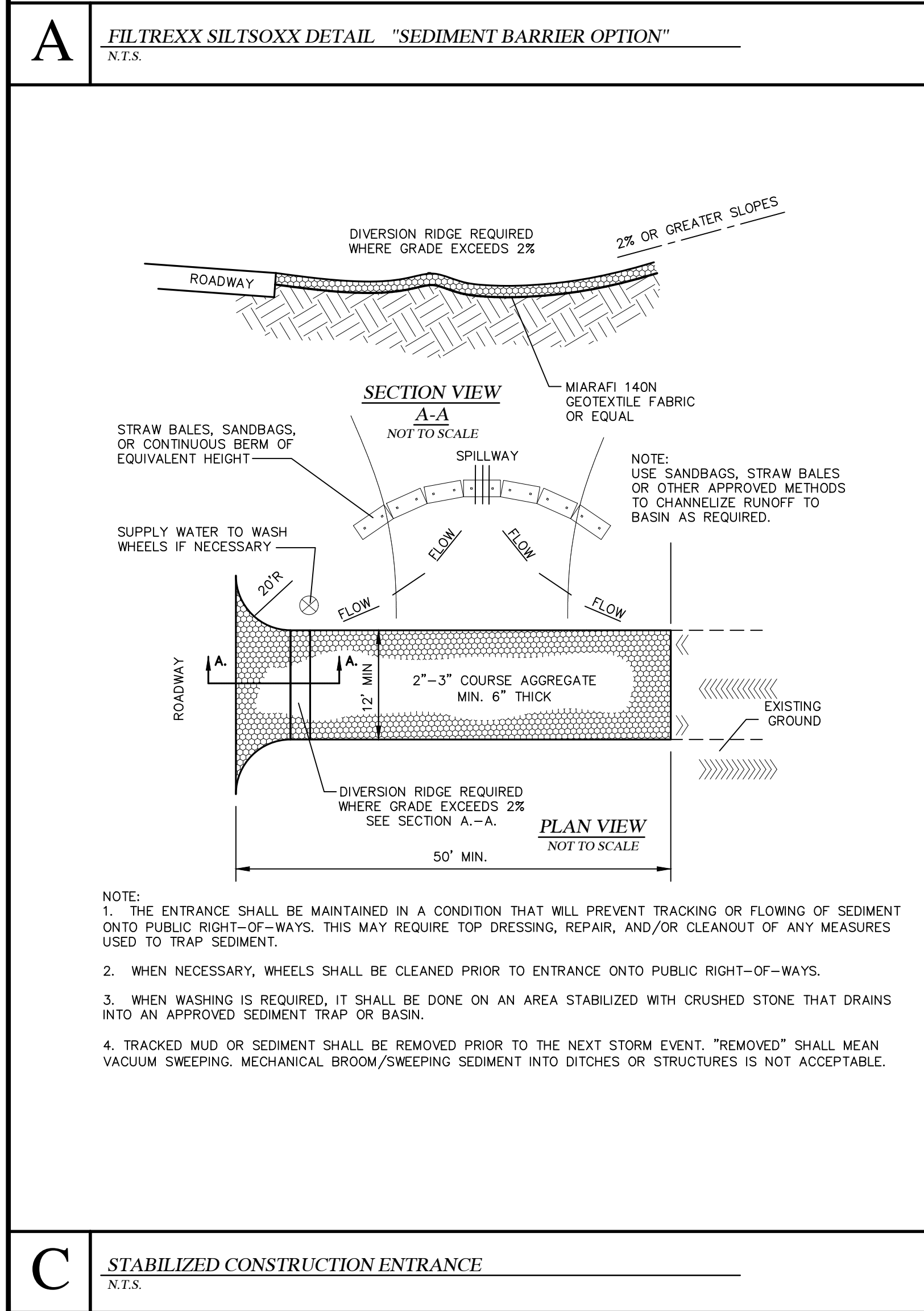
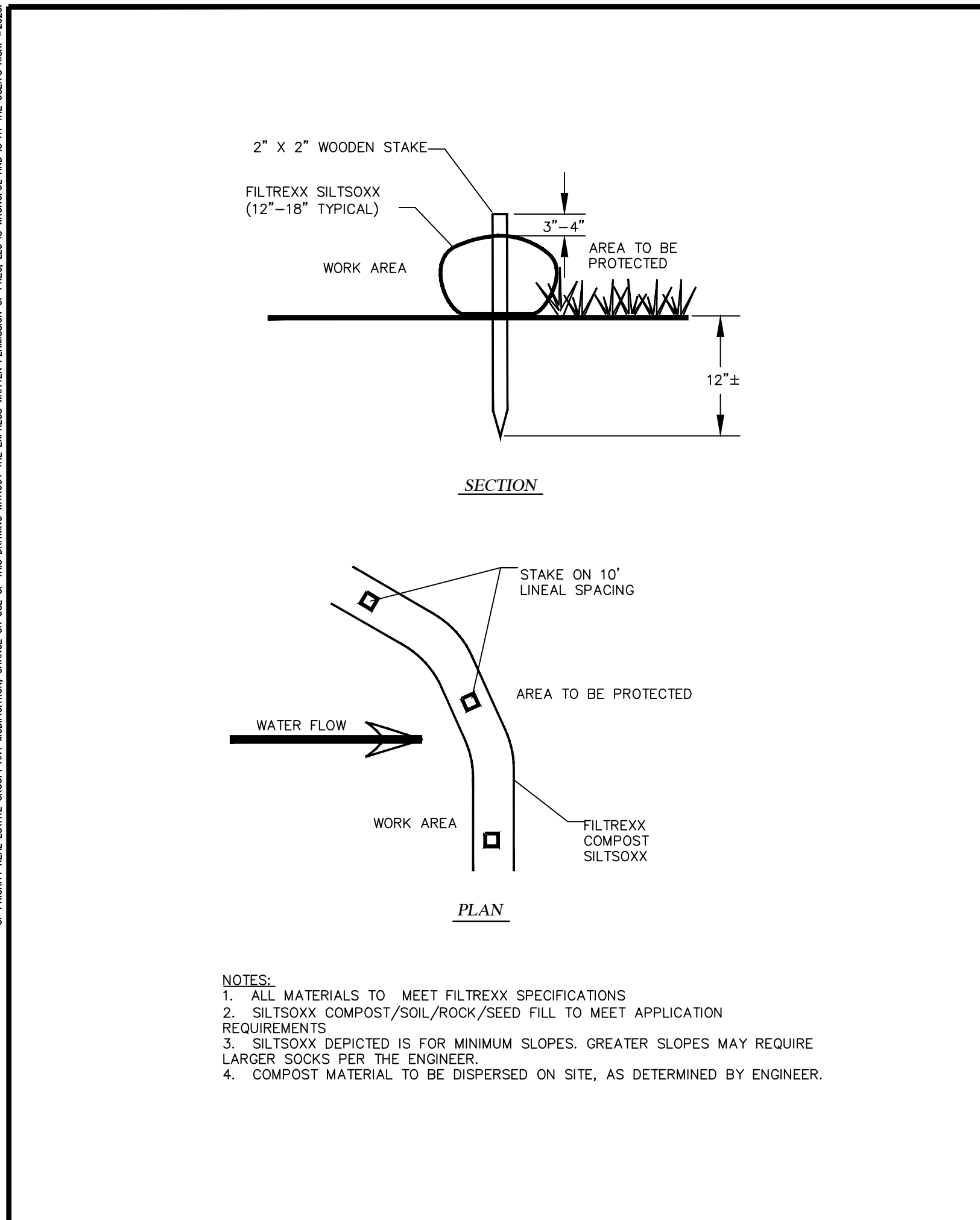
UTILITY NOTES:

1. ALL TERMINATIONS AND CONNECTIONS OF SERVICES SHALL BE IN COMPLIANCE WITH REQUIREMENTS OF THE RESPECTIVE UTILITY DISTRICT. ALL BACKFILLING AND COMPACTION OF WATER AND SEWER LINE TRENCHES SHALL BE AS APPROVED BY THE LOCAL UTILITY DISTRICT.
1. THE CONTRACTOR SHALL CONTROL DIGSAFE (888--444--7233) PRIOR TO COMMENCING EXCAVATION.
2. THE BASIS FOR PROJECT LAYOUT AND FOR CONSTRUCTION ELEVATIONS IS THE BASELINE AND BENCHMARK EXISTING ON THE SITE AND SHOWN ON THE DRAWINGS.
3. THE CONTRACTOR SHALL CONFIRM HORIZONTAL AND VERTICAL CONTROL BEFORE BEGINNING WORK.
4. SEE PLUMBING AND ELECTRICAL PLANS FOR LOCATION AND INVERTS OF SLEEVES IN FOUNDATIONS.
5. ELECTRIC SERVICE SHALL BE INSTALLED IN CONDUIT UNDER PAVEMENT AND CONCRETE.
6. CONTRACTOR SHALL SUBMIT SHOP DRAWINGS OF ALL SEWER, WATER, ELECTRICAL, AND SANITARY CONDUIT, MANHOLES, TRANSFORMERS, AND FITTINGS FOR APPROVAL.
7. CONTRACTOR SHALL VERIFY LOCATION OF EXISTING UTILITIES PRIOR TO CONSTRUCTION.
8. DUCTILE IRON PIPE SHALL MEET THE REQUIREMENTS OF AWWA C150 AND C900, CLASS 52, AND HAVE PUSH OR FLANGED JOINTS AS REQUIRED. FITTINGS SHALL HAVE MECHANICAL JOINTS WITH RETAINER GLANDS.
9. SANITARY SEWER PIPE AND FITTINGS SHALL BE SDR--35 PVC.
10. INSTALL 2" RIGID STYROFOAM INSULATION OVER SANITARY SEWER IN AREAS WHERE THERE IS LESS THAN 4' OF COVER.
11. CONNECTIONS AT MANHOLES/CATCH BASINS SHALL HAVE A FLEXIBLE BOOT CAST ONTO THE BARREL AND SECURED WITH STAINLESS STEEL BANDS.
12. SEE SHEET C4 FOR GRADING, DRAINAGE, STORM DRAIN DATA & EROSION CONTROL MEASURES.
13. BUILDING FOOTPRINT SHOWN IS NOT FOR FOUNDATION LAYOUT. REFER TO STRUCTURAL/ARCHITECTURAL DRAWINGS.
14. ALL PIPING MATERIAL TO THE BALL VALVE SHALL BE 1" OR 2" TYPE K COPPER AND ALL CONTROL VALVES SHALL BE LOCATED WITHIN THE EASEMENT AREA.
15. ALL DOMESTIC WATER SERVICES ON THE BUILDING SIDE OF THE CONTROL VALVE SHALL BE EITHER 2" TYPE K COPPER OR 2" CTS PE RATED AT 200 PSI. IF THE PE IS USED, AN 8 GAUGE WIRE SHALL BE ATTACHED TO THE PIPE WITH ONE END BROUGHT ALONGSIDE THE CURB BOX FOR LOCATING PURPOSES.
16. ANY CURB BOXES LOCATED WITHIN PAVEMENT SHALL BE INSTALLED INSIDE A GATE BOX TOP.
17. ALL MATERIALS SHOWN SHALL BE NEW AND FURNISHED BY CONTRACTOR AS PART OF CONTRACT WORK. ONLY ITEMS SPECIFICALLY IDENTIFIED TO BE SALVAGED MAY BE RE-USED WITHOUT PRIOR WRITTEN PERMISSION.
18. SEE HHE--200 FOR ALL SITE FOR DETAILS OF SUBSURFACE DISPOSAL SYSTEMS.

[illegible]

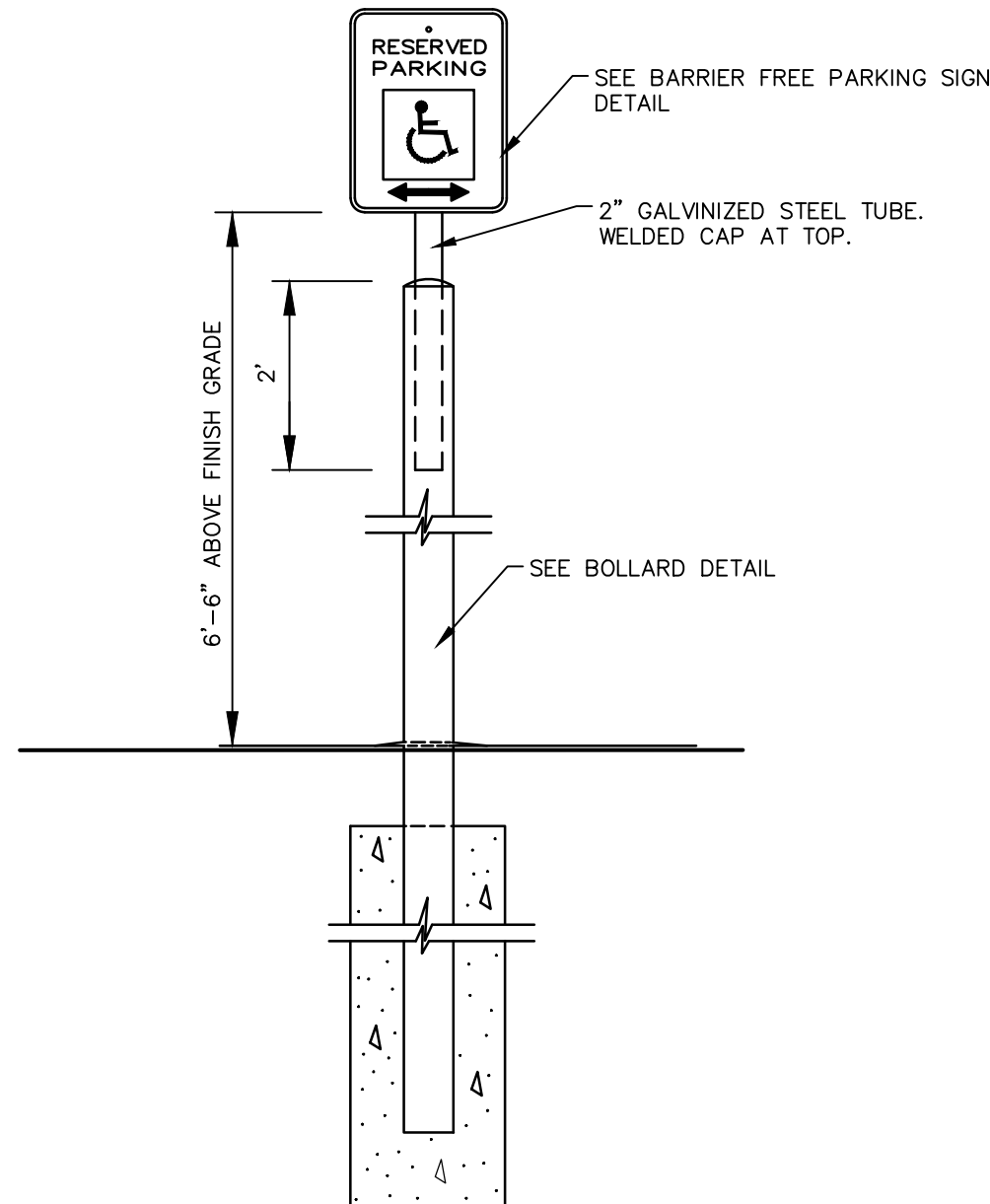
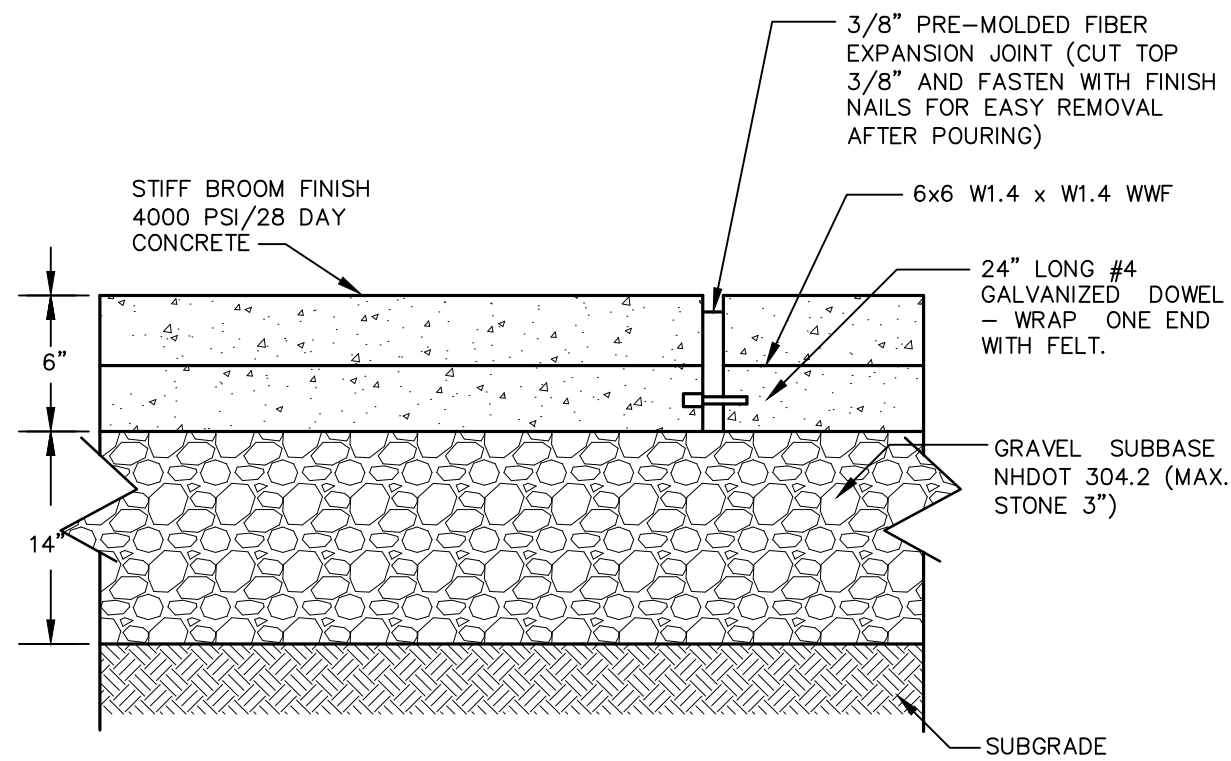
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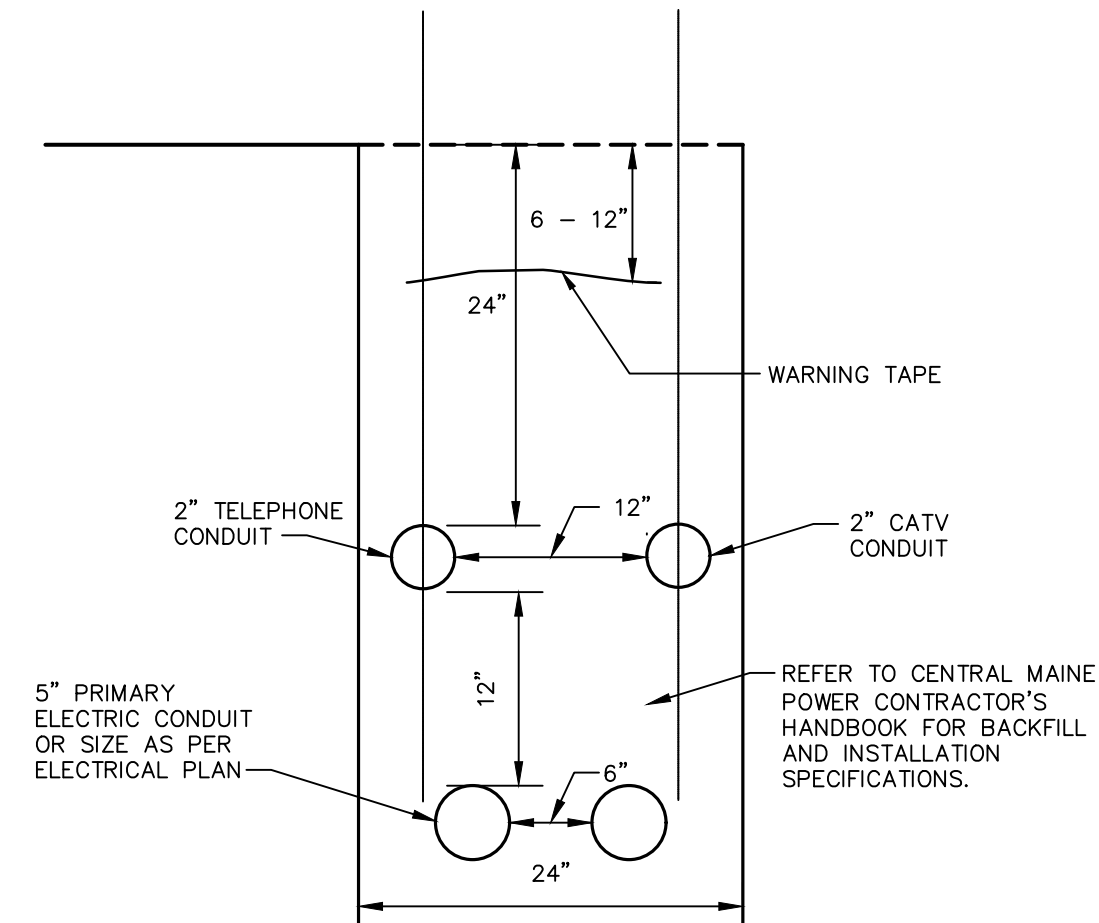
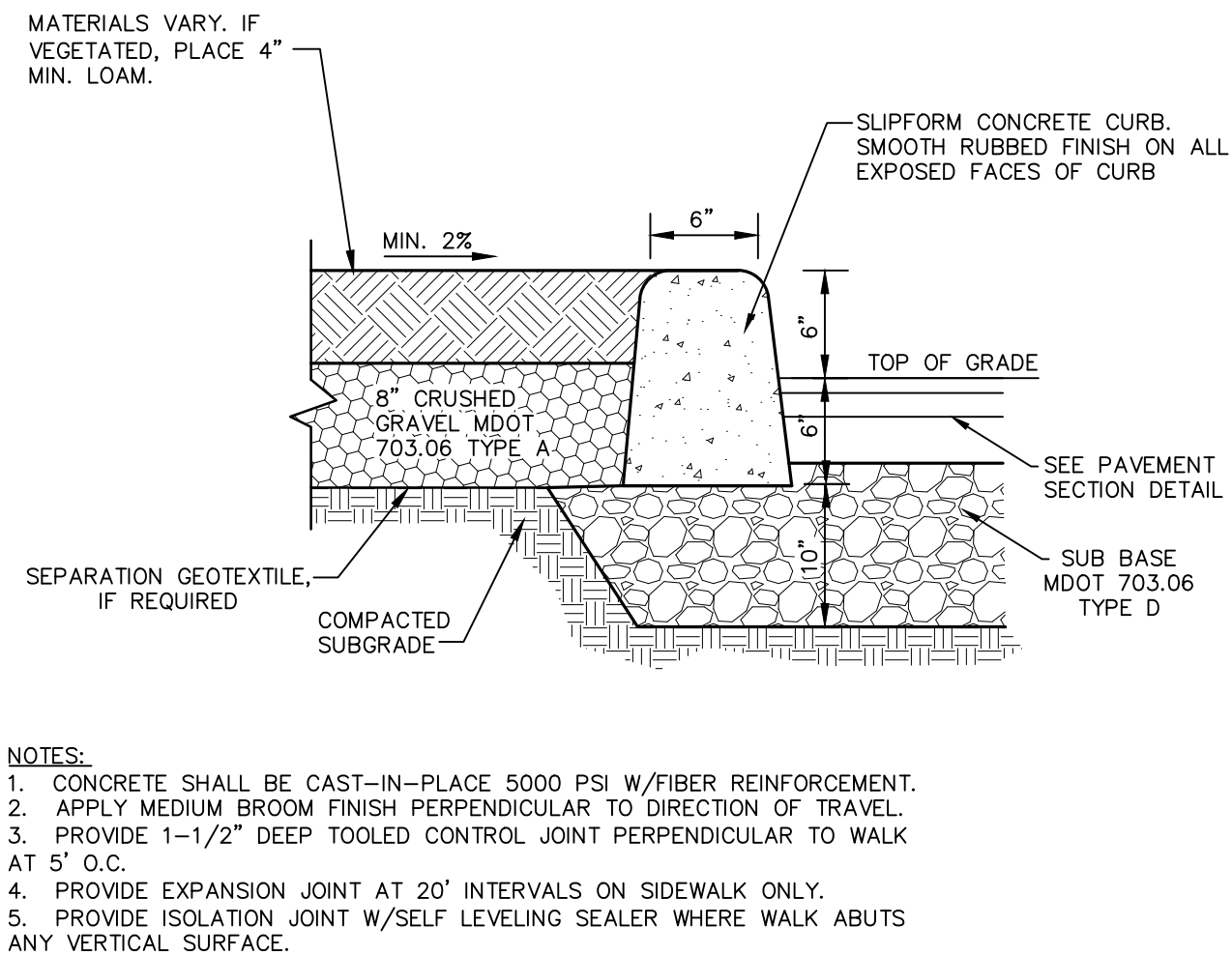


PRIORITY REAL ESTATE GROUP	PRIORITY	
	2 MAIN STREET TOPSHAM, MAINE 04086 (207) 837-6198	
FIELD WK:	SCALE:	SHEET:
DRN BY: CYN	JOB #: 22-RLM-004	C6
CHD BY: CYN	MAPLOT: U-19 12&13	
DATE: 11-22-23	FILE:	
EROSION CONTROL PLAN		
PROJECT: RUSTY LANTERN CONVENIENCE STORE 181 GRAY ROAD, CUMBERLAND, ME 04021		
PREPARED FOR: CUMBERLAND REAL ESTATE GROUP, LLC 2 MAIN STREET, TOPSHAM, ME 04086		
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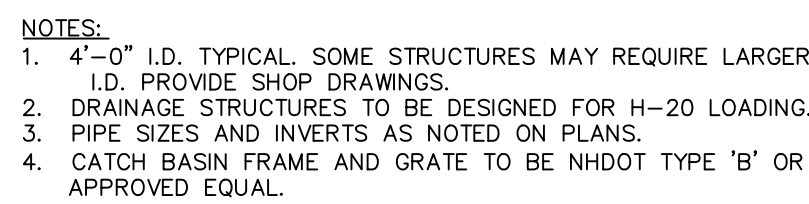
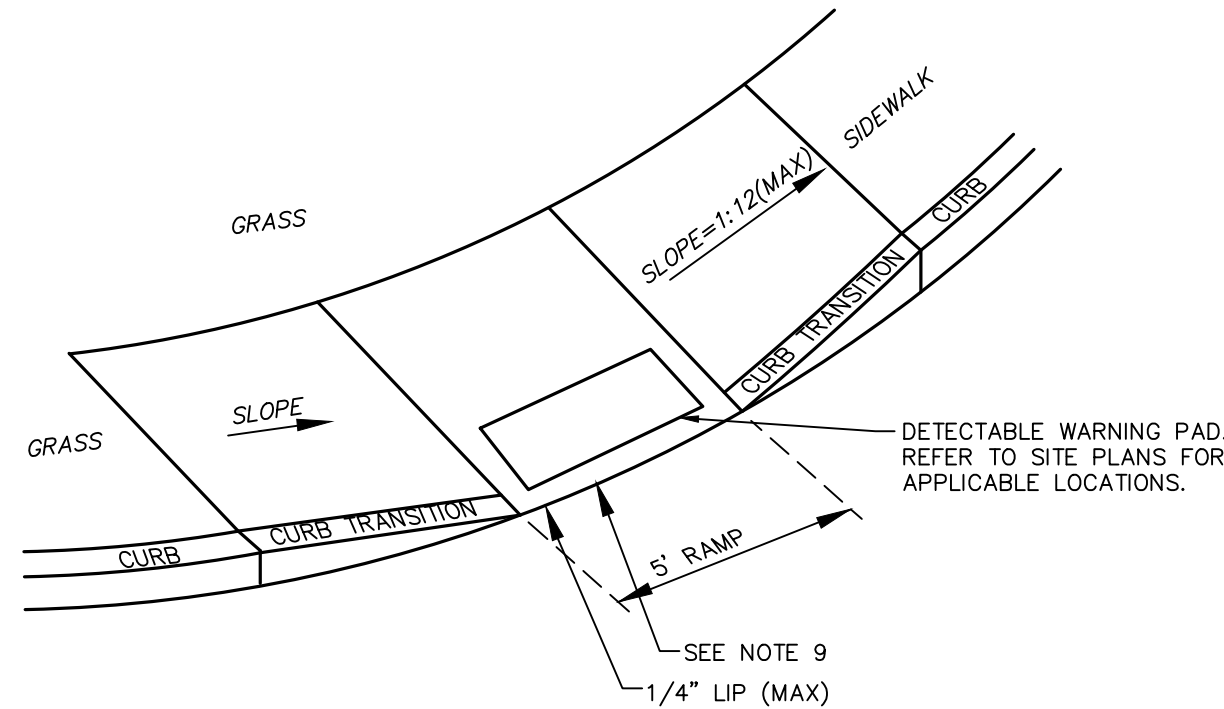
PERMITTING



D BARRIER FREE PARKING SIGN DETAIL
N.T.S.



H | PRIMARY UTILITY TRENCH
N.T.S.



K	CATCH BASIN OR DRAINAGE MANHOLE W/ SNOUT
	N.T.S.

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CIVIL DETAILS

TITLE:

A circular professional engineer seal for the State of Maine. The outer ring contains the text "STATE OF MAINE" at the top and "PROFESSIONAL ENGINEER" at the bottom, separated by two stars. The inner circle contains the text "CURTIS Y. NEUFELD", "9779", and "LICENSED". To the right of the seal, the expiration date "06-01-23" is printed. The seal is stamped over a document with handwritten notes and signatures.

[illegible]

PRIORITY
2 MAIN STREET
TOPSHAM, MAINE 04086
(207) 837-6198

**PRIORITY
REAL ESTATE
GROUP**

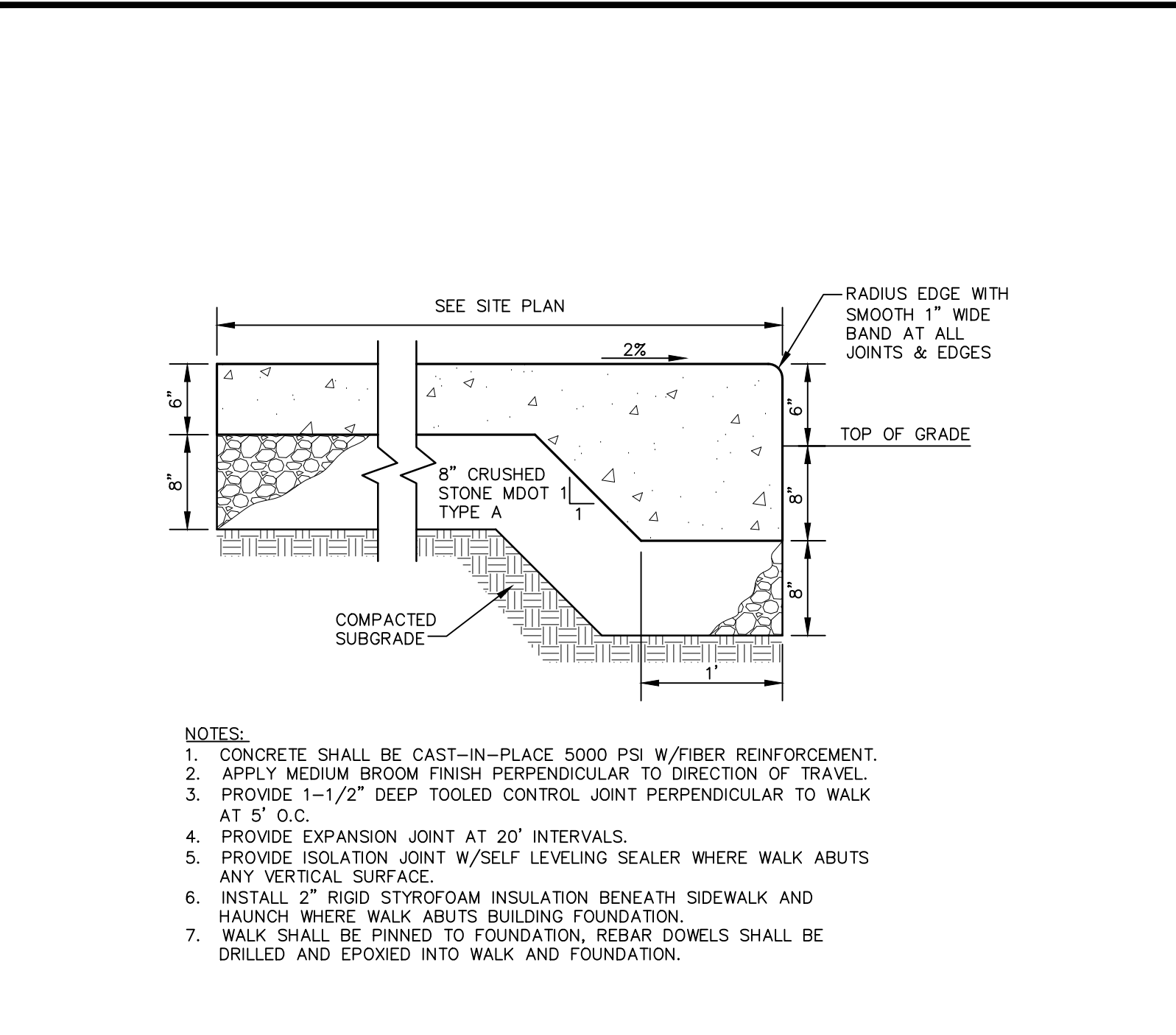
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DRN BY: CYN	JOB #: 22-RLM-004	C7
CHD BY: CYN	MAP/LOT: U-19 12&13	
DATE: 11-22-23	FILE: COV-DET	

OWNER:
181 GRAY ROAD, CUMBERLAND, ME 04021
CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

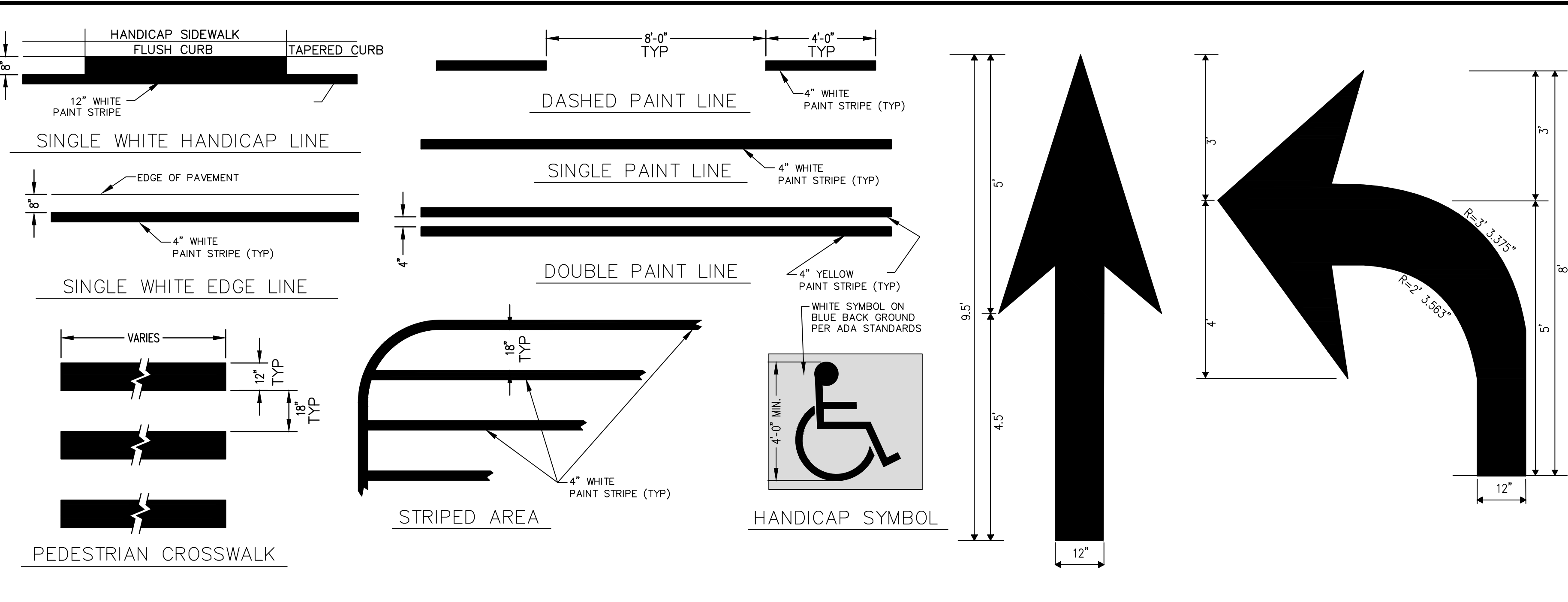
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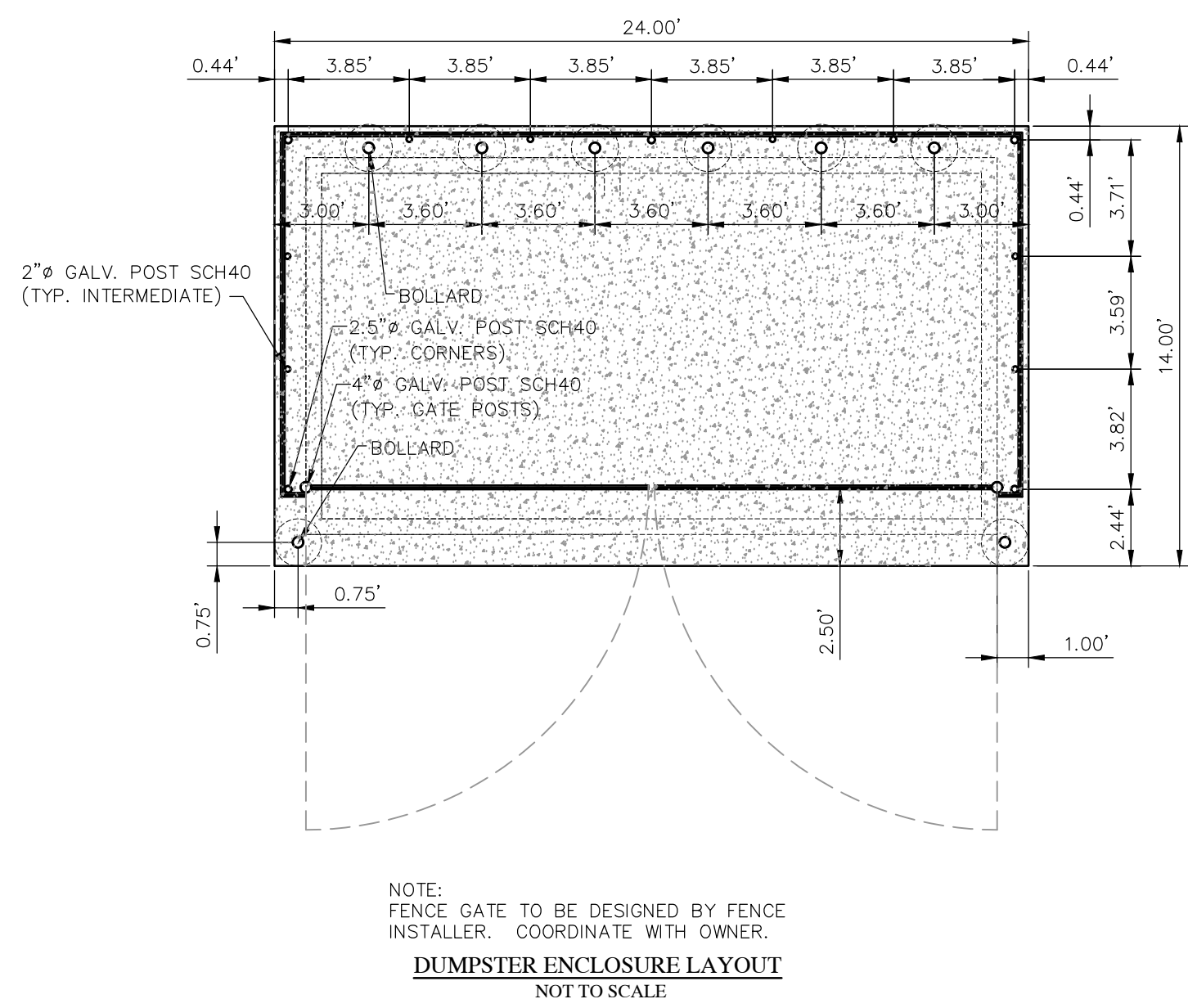
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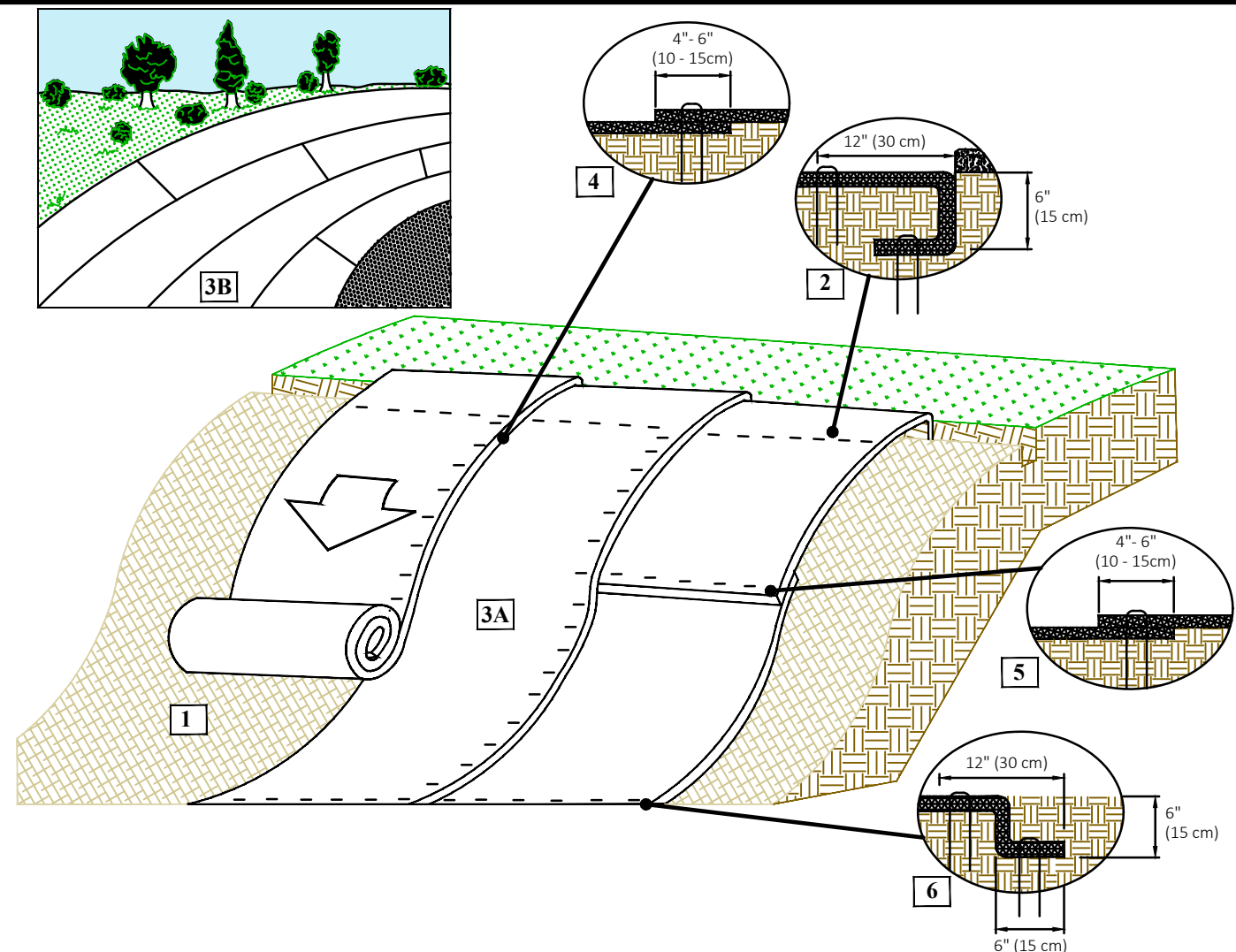
A **MONOLITHIC CONCRETE CURB AND SIDEWALK**
N.T.S.



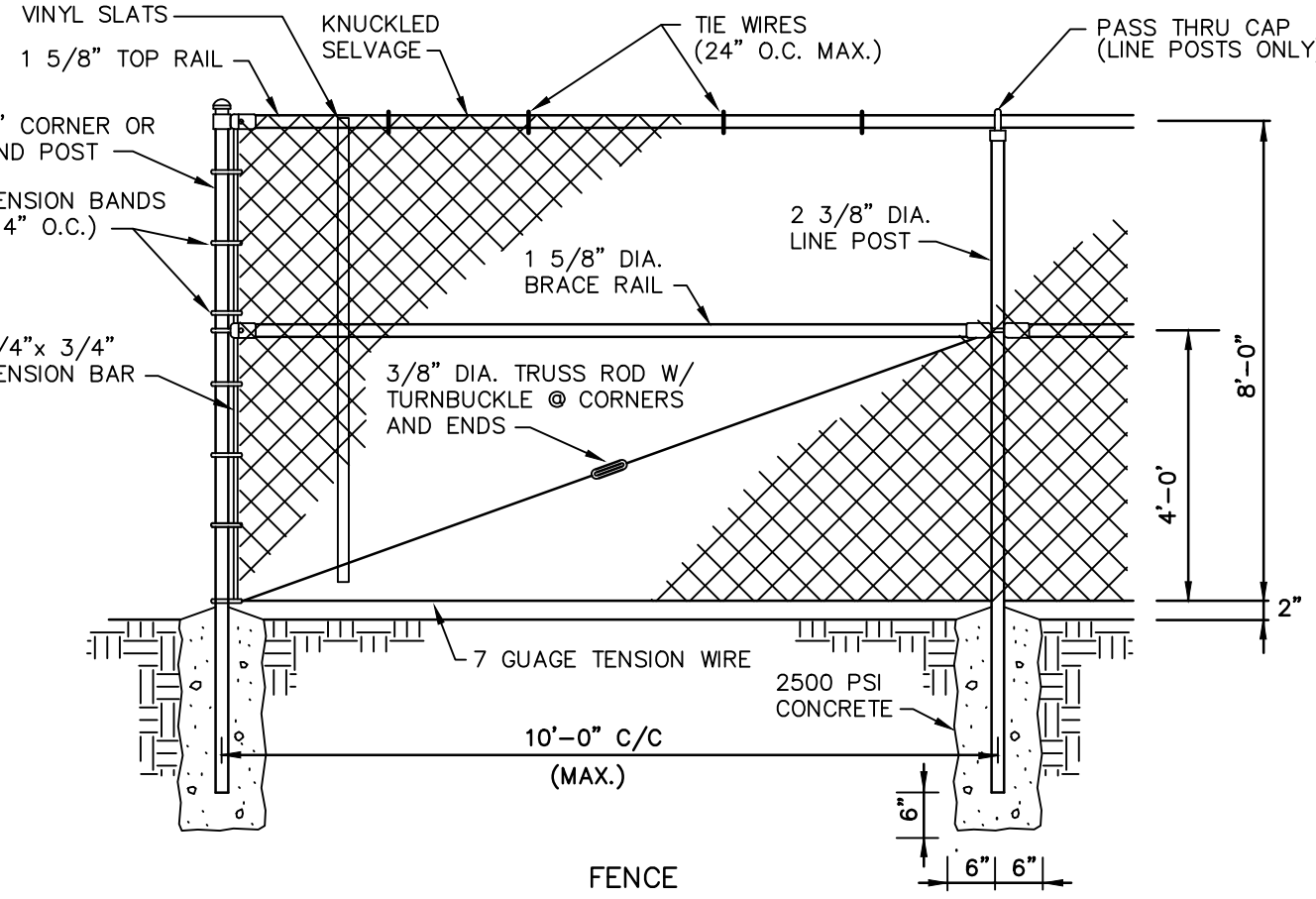
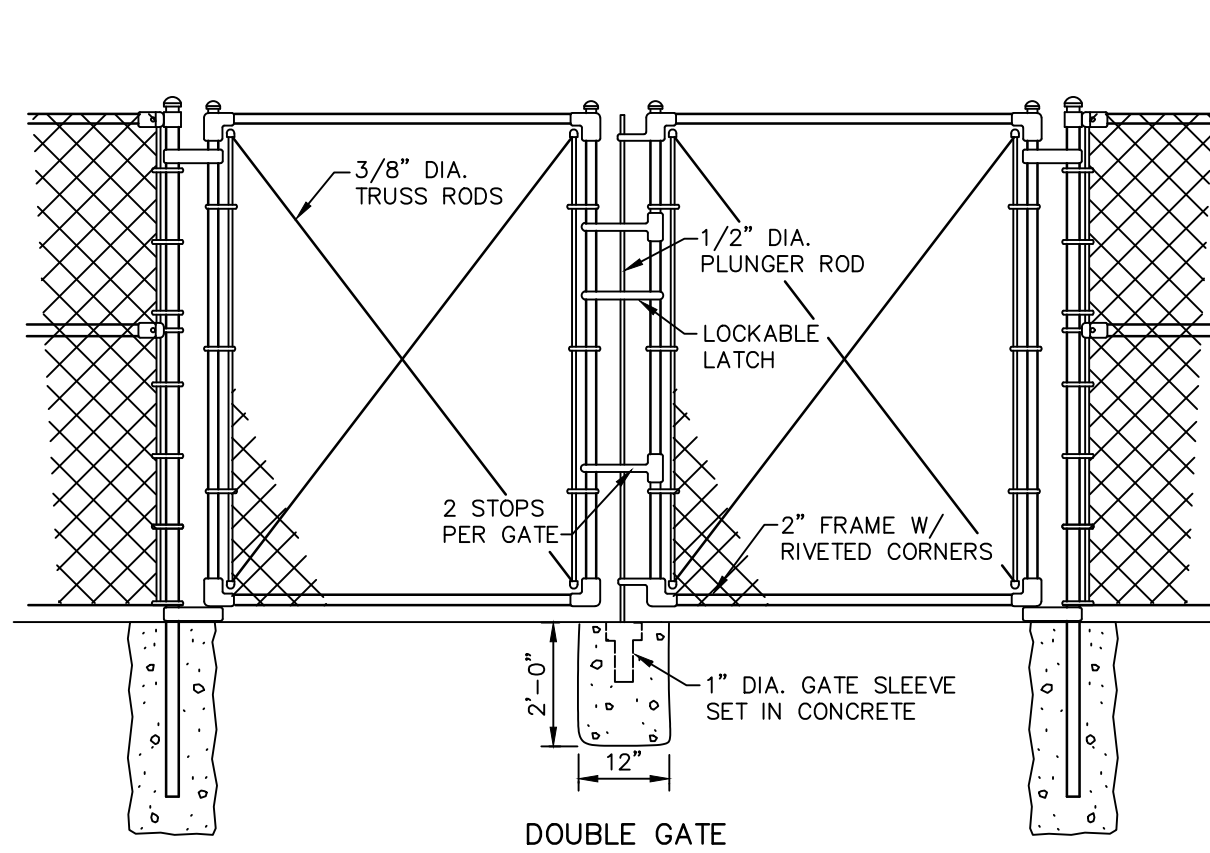
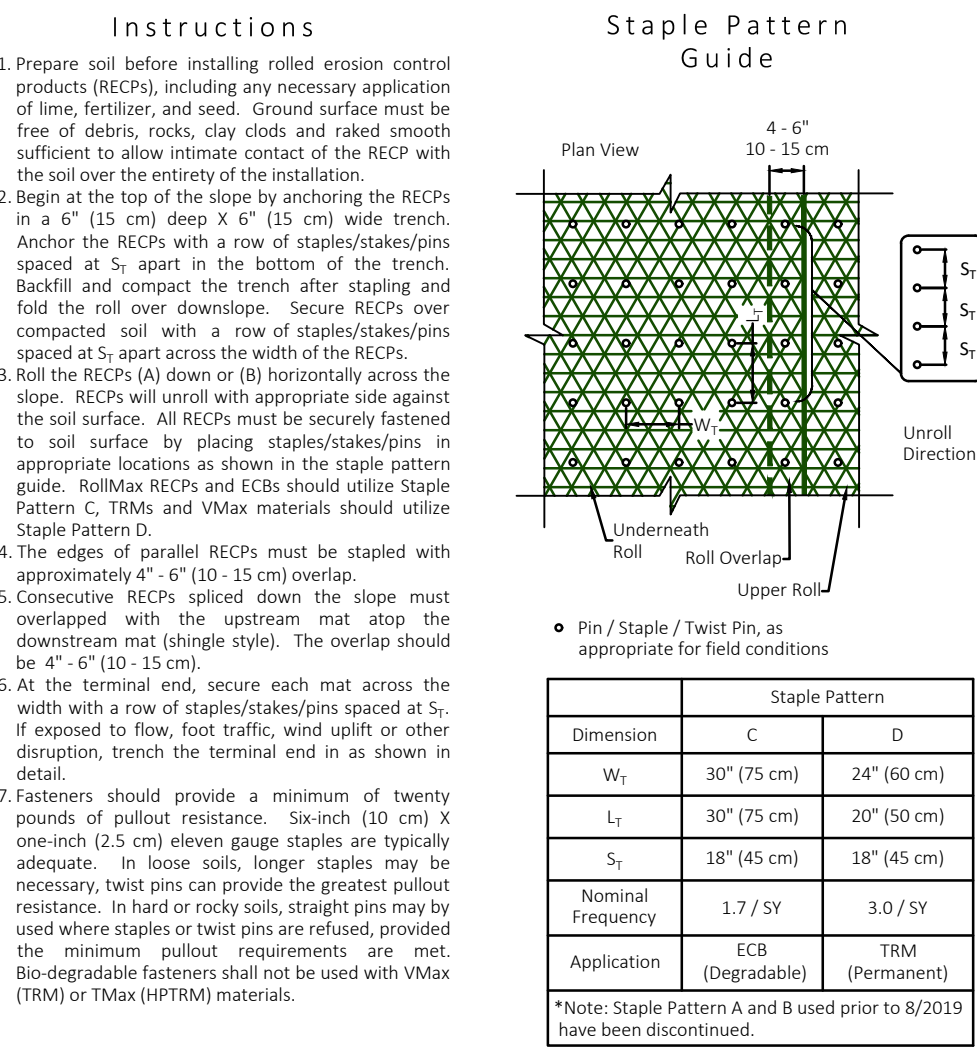
B **PAVEMENT MARKINGS**
N.T.S.



C **DUMPSTER DETAILS**
N.T.S.



D **TURF REINFORCEMENT MAT INSTALLATION**
N.T.S.



ISSUED FOR:
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PRIORITY REAL ESTATE GROUP

PRIORITY

2 MAIN STREET
TOPSHAM, MAINE 04086
(207) 837-6198

FIELD WK: CYN
DRN BY: CYN
CHD BY: CYN
DATE: 11-22-23

SCALE: 22-RLM-004
MAP/LOT: U-19 12&13
FILE: COV-DET

CIVIL DETAILS

PROJECT: RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME 04021

OWNER: CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

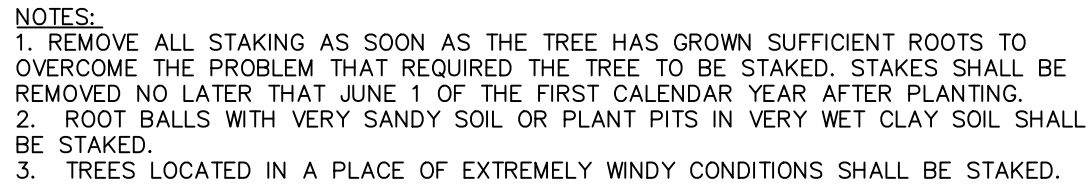
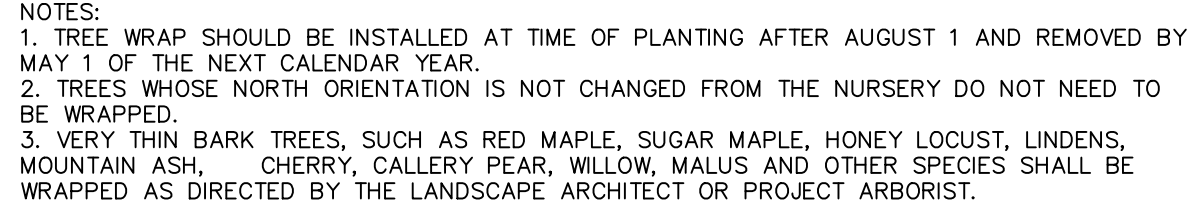
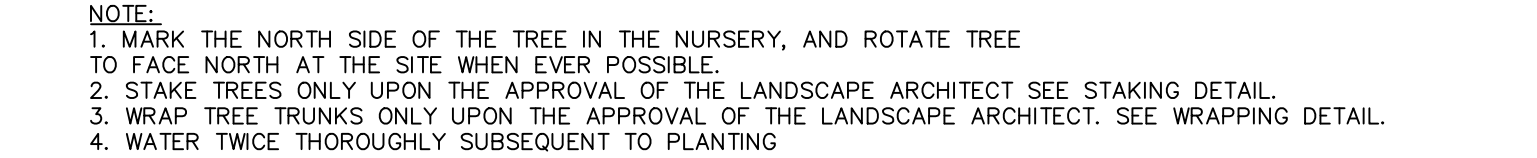
MAINE
CURTIS Y. NEUFELD
07780
REGISTERED PROFESSIONAL ENGINEER

10-06-01-23

2: 01-28-24 SUBMITTED TO TOWN OF CUMBERLAND FOR REVIEW
1: 08-11-23 SUBMITTED FOR MAINDOT REVIEW

CYN
CYN

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E	NOT USED
	N.T.S.

F	NOT USED
	N.T.S.

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1. ALL MATERIALS TO MEET FILTREXX SPECIFICATIONS
2. SILTSOXX COMPOST/SOIL/ROCK/SEED FILL TO MEET APPLICATION REQUIREMENTS
3. SILTSOXX DEPICTED IS FOR MINIMUM SLOPES. GREATER SLOPES MAY REQUIRE LARGER SOCKS PER THE ENGINEER.
4. COMPOST MATERIAL TO BE DISPERSED ON SITE, AS DETERMINED BY ENGINEER



1. EXCAVATE A 6" X 6" TRENCH ALONG THE LINE OF PLACEMENT FOR THE FILTER BARRIER.
2. UNROLL A SECTION AT A TIME AND POSITION THE POSTS AGAINST THE BACK (DOWNSTREAM) WALL OF THE TRENCH.
3. DRIVE POSTS INTO THE GROUND UNTIL APPROXIMATELY 2" OF FABRIC IS LYING ON THE TRENCH BOTTOM.
4. LAY THE TOE-IN FLAP OF FABRIC ONTO THE UNDISTURBED BOTTOM OF THE TRENCH. BACK FILL THE TRENCH AND TAMPER THE SOIL.
5. JOIN SECTION AS SHOWN IN TOP VIEW.
6. BARRIER SHALL BE MIRAFI SILT FENCE (100X) OR APPROVED EQUIVALENT.
7. A STONE "FILLET" MAY BE USED FOR ANCHORING FABRIC IF IT CANNOT BE KEED IN.

FILTREXX SILTSOXX DETAIL "SEDIMENT BARRIER OPTION"

SILT FENCE DETAIL "SEDIMENT BARRIER OPTION"

N.T.S.

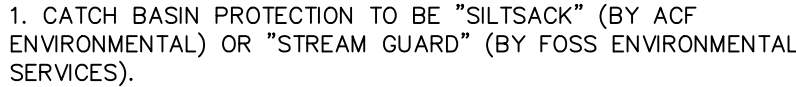
1. CONTRACTOR SHALL FOLLOW BEST MANAGEMENT PRACTICES OF THE MAINE DEP BEST MANAGEMENT PRACTICES HANDBOOK.

THE FOLLOWING EROSION SEDIMENTATION CONTROL DEVICES ARE PROPOSED FOR CONSTRUCTION ON THIS PROJECT. INSTALL THESE DEVICES AS INDICATED ON THE PLANS.

1. SEDIMENT BARRIER: SILT SOXX OR APPROVED EQUAL WILL BE INSTALLED ALONG THE DOWN GRADING EDGES OF DISTURBED AREAS TO TRAP RUNOFF BORNE SEDIMENTS UNTIL THE SITE IS STABILIZED. IN AREAS WHERE STORMWATER DISCHARGES THE SEDIMENT BARRIER WILL BE REINFORCED WITH HAY BALES TO HELP MAINTAIN THE INTEGRITY OF THE SEDIMENT BARRIER AND TO PROVIDE ADDITIONAL TREATMENT.
2. HAY BALES: HAY BALES TO BE PLACED IN LOW FLOW DRAINAGE SWALES AND PATHS TO TRAP SEDIMENTS AND REDUCE RUNOFF VELOCITIES. DO NOT PLACE HAY BALES IN FLOWING WATER OR STREAMS.
3. RIPRAP: PROVIDE RIPRAP IN AREAS WHERE CULVERTS DISCHARGE OR AS SHOWN ON THE PLANS.
4. LOAM, SEED, & MULCH: ALL DISTURBED AREAS, WHICH ARE NOT OTHERWISE TREATED, SHALL RECEIVE PERMANENT SEEDING AND MULCH TO STABILIZE THE DISTURBED AREAS. THE DISTURBED AREAS WILL BE REVEGETATED WITHIN 5 DAYS OF FINAL GRADING. SEEDING REQUIREMENTS ARE PROVIDED AT THE END OF THIS SPECIFICATION.
5. STRAW AND HAY MULCH: USED TO COVER DENUED AREAS UNTIL PERMANENT SEED OR EROSION CONTROL MEASURES ARE IN PLACE. MULCH BY ITSELF CAN BE USED ON SLOPES LESS THAN 15% IN SUMMER AND 8% IN WINTER. JUTE MESH IS TO BE USED OVER MULCH ONLY.
6. IN LIEU OF MULCH, USE EROSION CONTROL BLANKET (EQUAL TO NORTH AMERICAN GREEN SC150) TO STABILIZE AREAS OF CONCENTRATED FLOW AND DRAINAGE WAYS.

PROVIDE THE FOLLOWING TEMPORARY EROSION/SEDIMENTATION CONTROL MEASURES DURING CONSTRUCTION OF THE DEVELOPMENT:

1. SEDIMENT BARRIER ALONG THE DOWNGRADE SIDE OF THE PARKING AREAS AND OF ALL FILL SECTIONS. THE SEDIMENT BARRIER WILL REMAIN IN PLACE UNTIL THE SITE IS 85% REVEGETATED.
2. HAY BALES PLACED AT KEY LOCATIONS TO SUPPLEMENT THE SEDIMENT BARRIER.
3. PROTECT TEMPORARY STOCKPILES OF STUMPS, GRUBBINGS, OR COMMON EXCAVATION AS FOLLOWS:
 - A. SOIL STOCKPILE SIDE SLOPES SHALL NOT EXCEED 2:1.
 - B. AVOID PLACING TEMPORARY STOCKPILES IN AREAS WITH SLOPES OVER 10 PERCENT, OR NEAR DRAINAGE SWALES.
- SEE ITEM 3 FOR CONSTRUCTION PRACTICES BELOW.
4. STABILIZE STOCKPILES WITHIN 7 DAYS BY TEMPORARILY SEEDING WITH A HYDROSEED METHOD CONTAINING AN EMULSIFIED MULCH TACKIFIER OR BY COVERING THE STOCKPILE WITH MULCH.
5. D. SURROUND STOCKPILE SOIL WITH SEDIMENT BARRIER AT BASE OF PILE.
6. ALL DENUED AREAS WHICH HAVE BEEN ROUGH GRADED AND ARE NOT LOCATED WITHIN THE BUILDING PAD, OR PARKING AND DRIVEWAY SUBBASE AREA SHALL RECEIVE MULCH WITHIN 30 DAYS OF INITIAL DISTURBANCE OF SOIL OR WITHIN 7 DAYS AFTER COMPLETING THE ROUGH GRADING OPERATIONS. IN THE EVENT THE CONTRACTOR COMPLETES FINAL GRADING AND INSTALLATION OF LOAM AND SOO WITHIN THE TIME PERIODS PRESENTED ABOVE, INSTALLATION OF MULCH AND NETTING, WHERE APPLICABLE, IS NOT REQUIRED.
7. IF WORK IS CONDUCTED BETWEEN OCTOBER 15 AND APRIL 15, ALL DENUED AREAS ARE TO BE COVERED WITH HAY MULCH, APPLIED AT TWICE THE NORMAL APPLICATION RATE, AND ANCHORED WITH FABRIC NETTING. THE PERIOD BETWEEN FINAL GRADING AND MULCHING SHALL BE REDUCED TO A 15 DAY MAXIMUM.



2. INSERT TO BE EMPTIED IN AN APPROVED MANNER WHEN IT IS 1/2 FULL OF SEDIMENT.
3. INSPECT INSERT AFTER ALL RAINFALL EVENTS, REPAIR AND MAINTAIN AS REQUIRED.

TEMPORARY INLET PROTECTION DETAIL
N.T.S.

3. LONG-TERM PROVISIONS FOR PERMANENT MAINTENANCE OF ALL EROSION AND SEDIMENTATION CONTROL DEVICES AFTER ACCEPTANCE OF THE PROJECT SHALL BE THE RESPONSIBILITY OF THE OWNER.

ISSUED FOR:

PERMITTING

371

RUSTY LANTERN CONVENIENCE STORE

CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET. TOPSHAM. ME 04086

A circular professional seal for the State of Maine. The outer ring contains the text "STATE OF MAINE" on the left and "PROFESSIONAL ENGINEER" on the right, separated by two stars. The inner circle contains the text "CURTIS Y. NEUFELD" and "9779 LICENSED" below it.

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CONSIDERATIONS TO FUTURE RESEARCH

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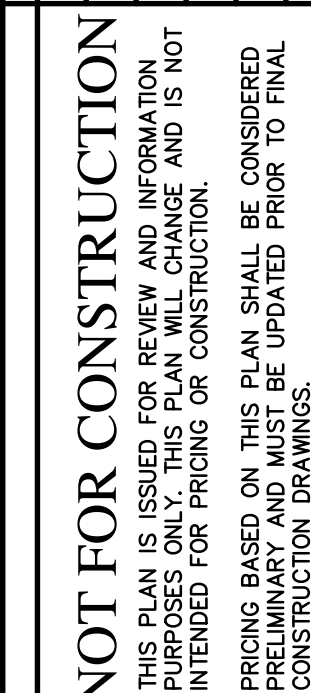
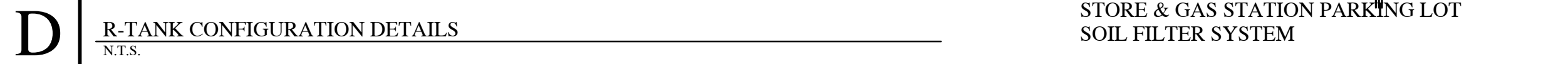
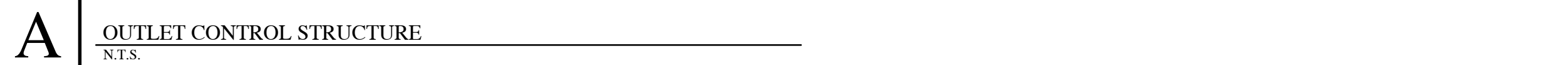
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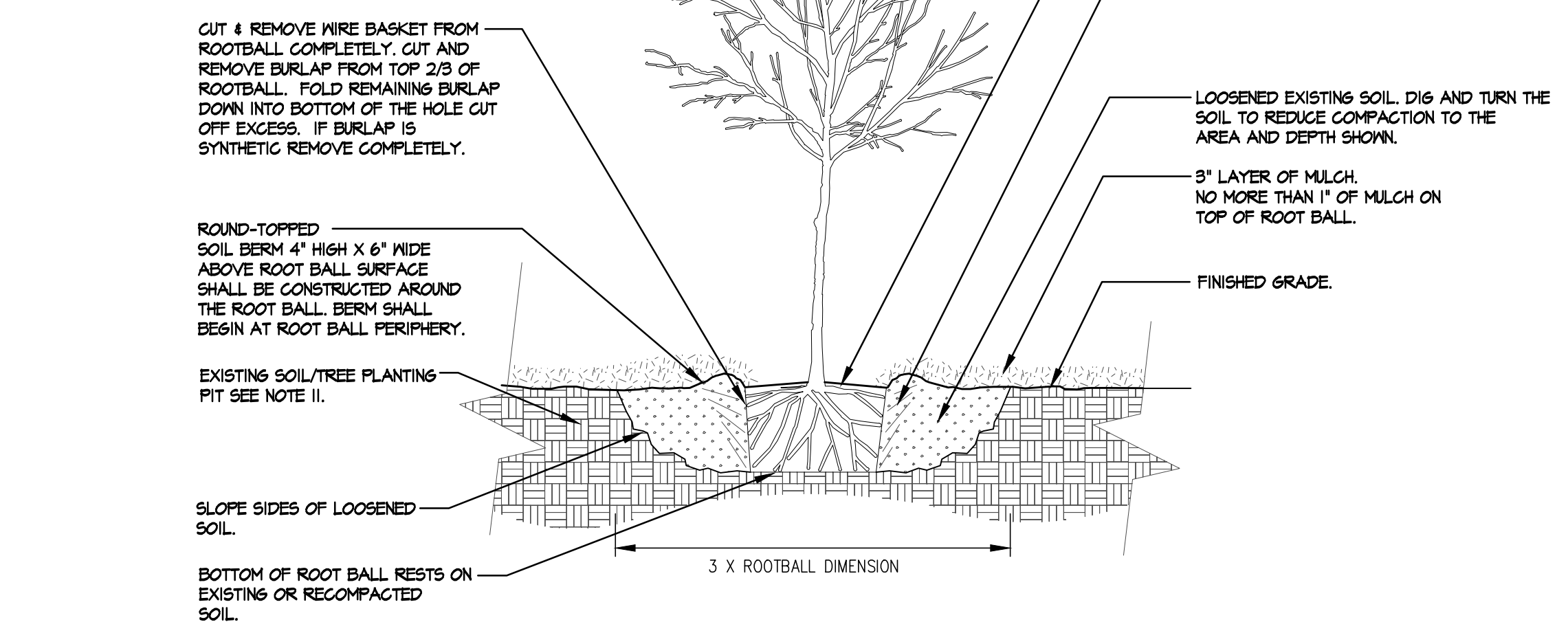
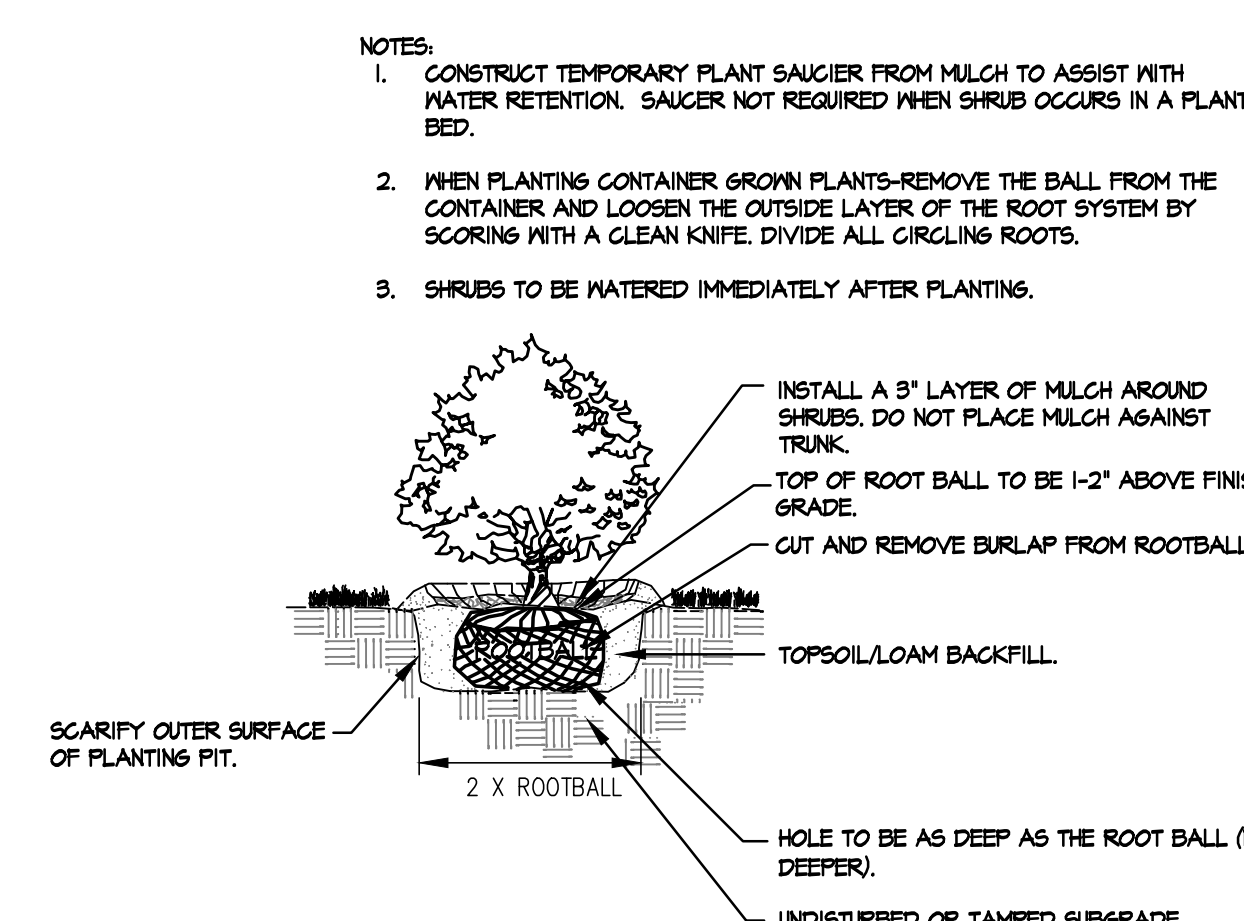
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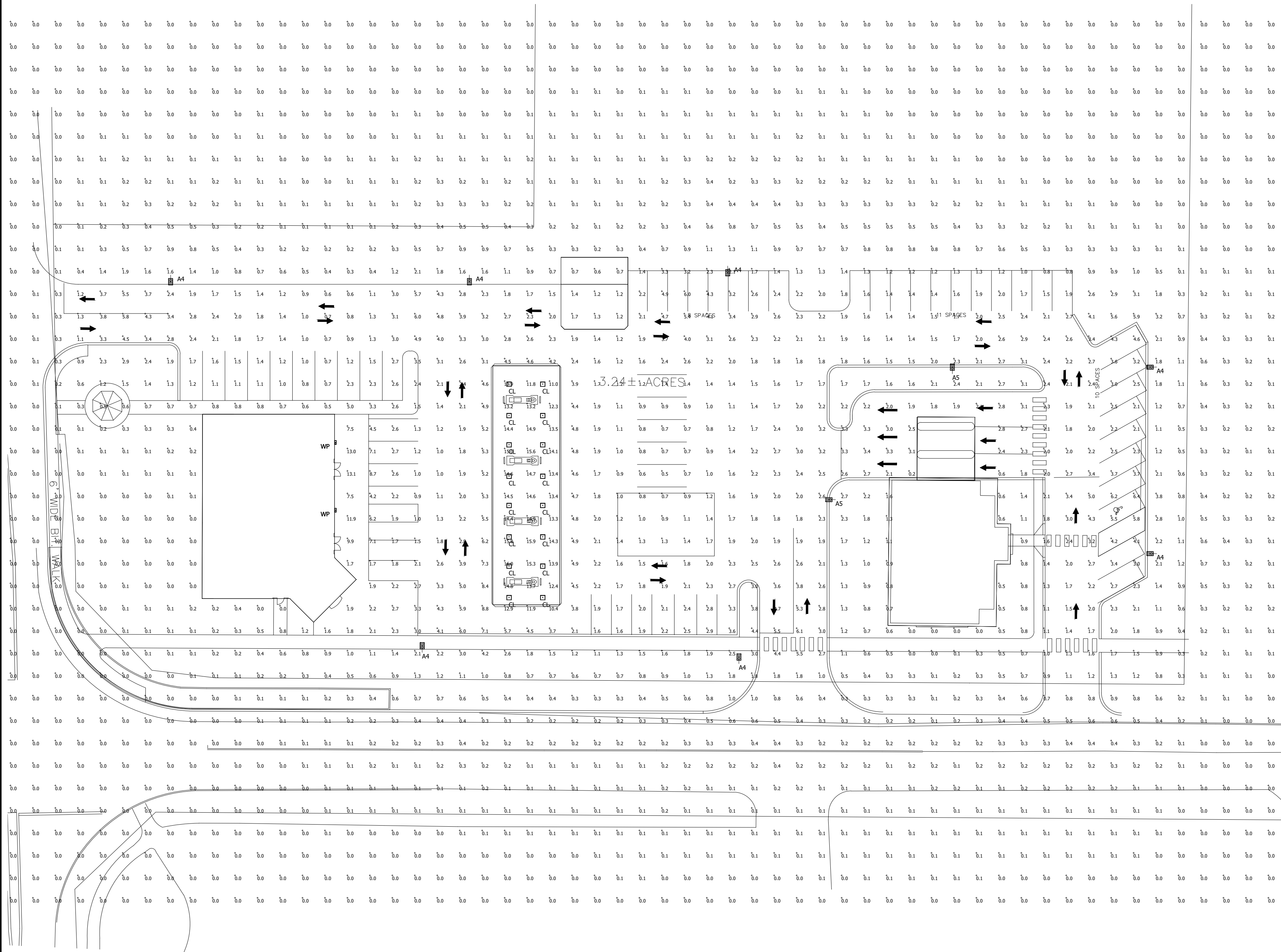
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


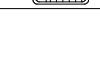
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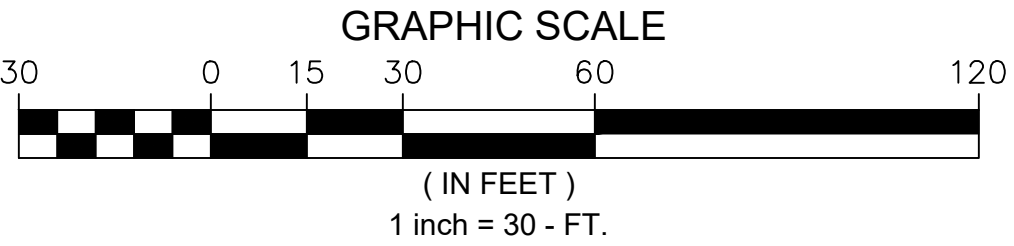
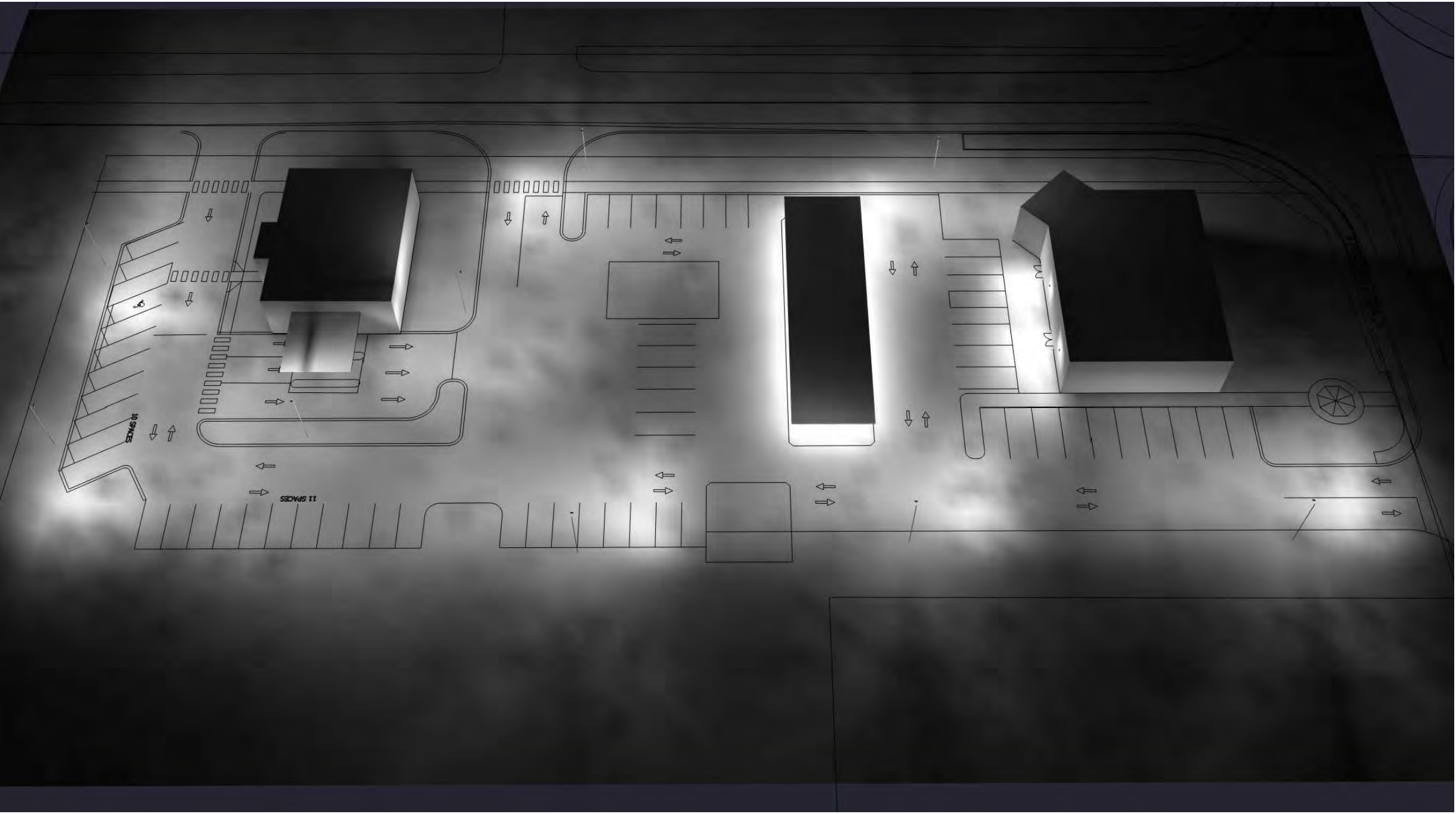
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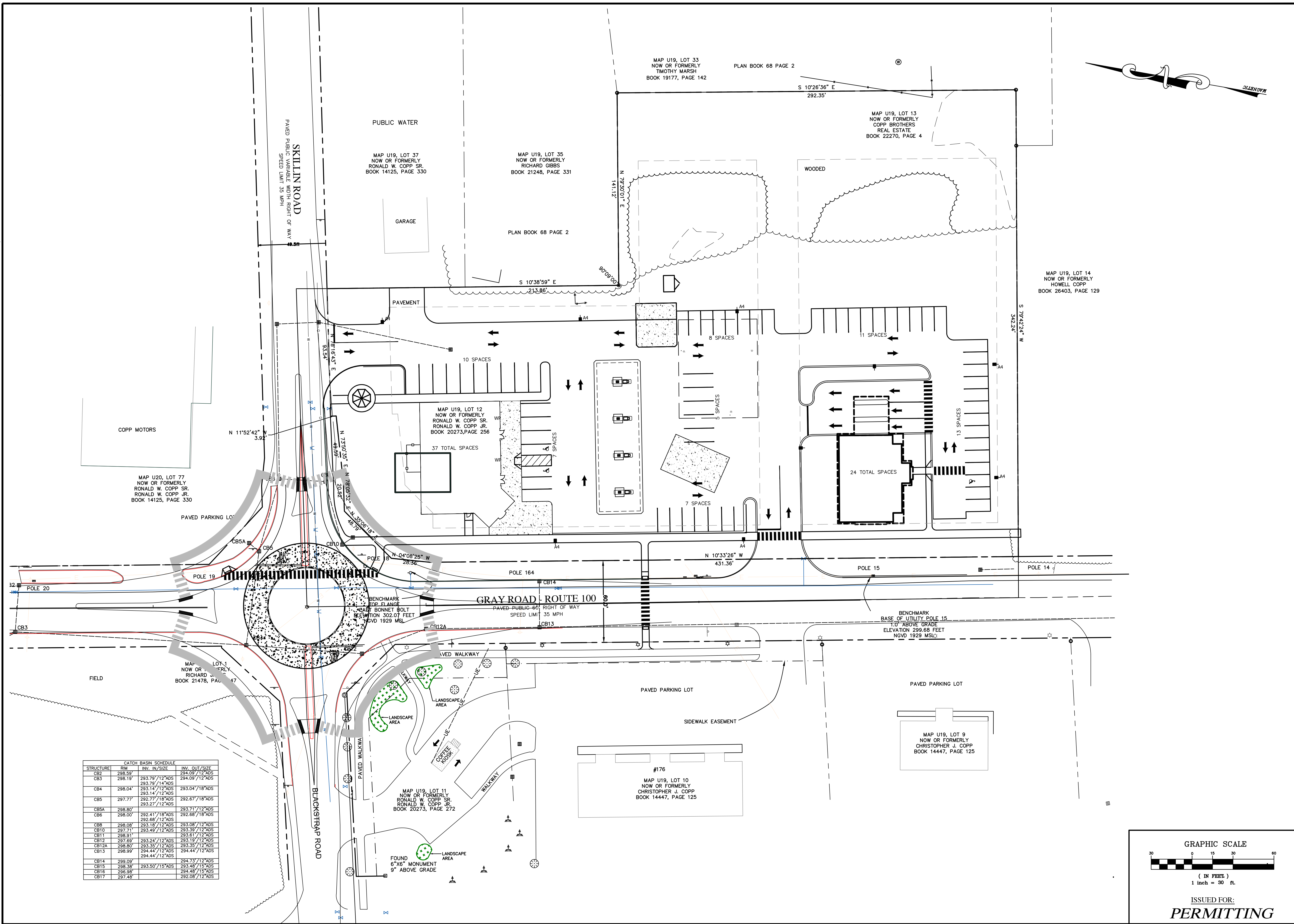


Luminaire Schedule							
Symbol	Qty	Label	Mounting Height	LLF	Lum. Lumens	Lum. Watts	Description
	4	WP	10' - 0" AFG	0.900	3882	35	LNC2-48L-35-3K7-4W-UNV-DBT
	16	CL	12' - 0" AFG	0.900	4450	30	VSH-30-4K7-UNV
	2	A5	25' - 0" AFG	0.900	20539	160	VP-1-160L-160-3K7-5QW
	7	A4	25' - 0" AFG	0.900	20060	160	VP-1-160L-160-3K7-4W

Calculation Summary							
Label	CalcType	Units	Avg	Max	Min	Avg/Min	Max/Min
Fuel Canopy	Illuminance	Fc	13.74	15.7	8.5	1.62	1.85
Overall Area	Illuminance	Fc	0.89	16.0	0.0	N.A.	N.A.
Parking Area	Illuminance	Fc	2.44	8.8	0.5	4.88	17.60



1. THIS LIGHTING DESIGN IS BASED ON LIMITED INFORMATION SUPPLIED BY OTHERS TO CURRENT. SITE DETAILS PROVIDED HEREON ARE REPRODUCED ONLY AS A VISUALIZATION AID. FIELD DEVIATIONS MAY SIGNIFICANTLY AFFECT PREDICTED PERFORMANCE. PRIOR TO INSTALLATION, CRITICAL SITE INFORMATION (POLE LOCATIONS, ORIENTATION, MOUNTING HEIGHT, ETC.) SHOULD BE COORDINATED WITH THE CONTRACTOR AND/OR SPECIFIER RESPONSIBLE FOR THE PROJECT.							
2. LUMINAIRE DATA IS TESTED TO INDUSTRY STANDARDS UNDER LABORATORY CONDITIONS. OPERATING VOLTAGE AND NORMAL MANUFACTURING TOLERANCES OF LAMP, BALLAST, AND LUMINAIRE MAY AFFECT FIELD RESULTS.							
3. CONFORMANCE TO FACILITY CODE AND OTHER LOCAL REQUIREMENTS IS THE RESPONSIBILITY OF THE OWNER AND/OR THE OWNER'S REPRESENTATIVE.							
TITLE: RUSTY LANTERN CUMBERLAND, ME SITE PHOTOMETRIC PLAN		REVISED FROM DRAWING NUMBER(S):		Current®	DN BY: DHK	DATE: 08/15/23	CHK BY: N/A
					REV. BY:	DATE:	SCALE: AS NOTED
				QUOTE: N/A	DRAWING / DESIGN NO.: A231508		



CATCH BAY SCHEDULE				
STRUCTURE	RM	IN	SV/ SZ	IN
	IN	IN	IN	IN
C82	298.59'			294.09 / 12' ADS
C83	298.19'	293.79 / 12' ADS		294.09 / 12' ADS
C84	298.04'	293.79 / 12' ADS		294.09 / 12' ADS
C85	298.04'	293.74 / 12' ADS		293.64 / 18' ADS
C86	298.00'	293.77 / 12' ADS		293.67 / 18' ADS
C87	298.00'	293.77 / 12' ADS		293.71 / 12' ADS
C88	298.00'	292.41 / 18' ADS		292.68 / 18' ADS
C89	298.00'	292.68 / 12' ADS		293.08 / 12' ADS
C90	297.71'	292.68 / 12' ADS		293.39 / 12' ADS
C91	298.61'			293.61 / 12' ADS
C92	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C93	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C94	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C95	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C96	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C97	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C98	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C99	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C100	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C101	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C102	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C103	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C104	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C105	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C106	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C107	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C108	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C109	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C110	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C111	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C112	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C113	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C114	298.61'	293.24 / 12' ADS		293.61 / 12' ADS
C115	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C116	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C117	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C118	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C119	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C120	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C121	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C122	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C123	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C124	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C125	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C126	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C127	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C128	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C129	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C130	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C131	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C132	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C133	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C134	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C135	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C136	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C137	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C138	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C139	298.61'	293.50 / 15' ADS		293.48 / 15' ADS
C140	298.61'	293.50 / 15' ADS		293.48 / 15' ADS

**PRIORITY
REAL ESTATE
GROUP LLC**

SITE PLAN WITH PROPOSED ROUNDABOUT

RUSTY LANTERN CONVENIENCE STORE

181 GRAY ROAD, CUMBER; LAND, ME 04021

FOR: CUMBERLAND REAL ESTATE GROUP, LLC

2 MAIN STREET, TOPSHAM, ME 04086

STATE OF MAINE
★
CURTIS
Y.
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PROFESSIONAL ENGINEER
01-29-24

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NOT FOR CONSTRUCTION

THIS PLAN IS ISSUED FOR REVIEW AND INFORMATION PURPOSES ONLY. THIS PLAN WILL CHANGE AND IS NOT INTENDED FOR PRICING OR CONSTRUCTION.

PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.



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SIDEWALK CONCEPT PLAN

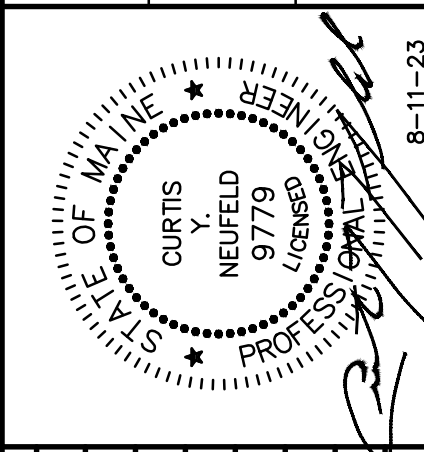
PROJECT: RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME 04021

PREPARED FOR: CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

PRIORITY
2 MAIN STREET
TOPSHAM, MAINE 04086
(207) 837-6198

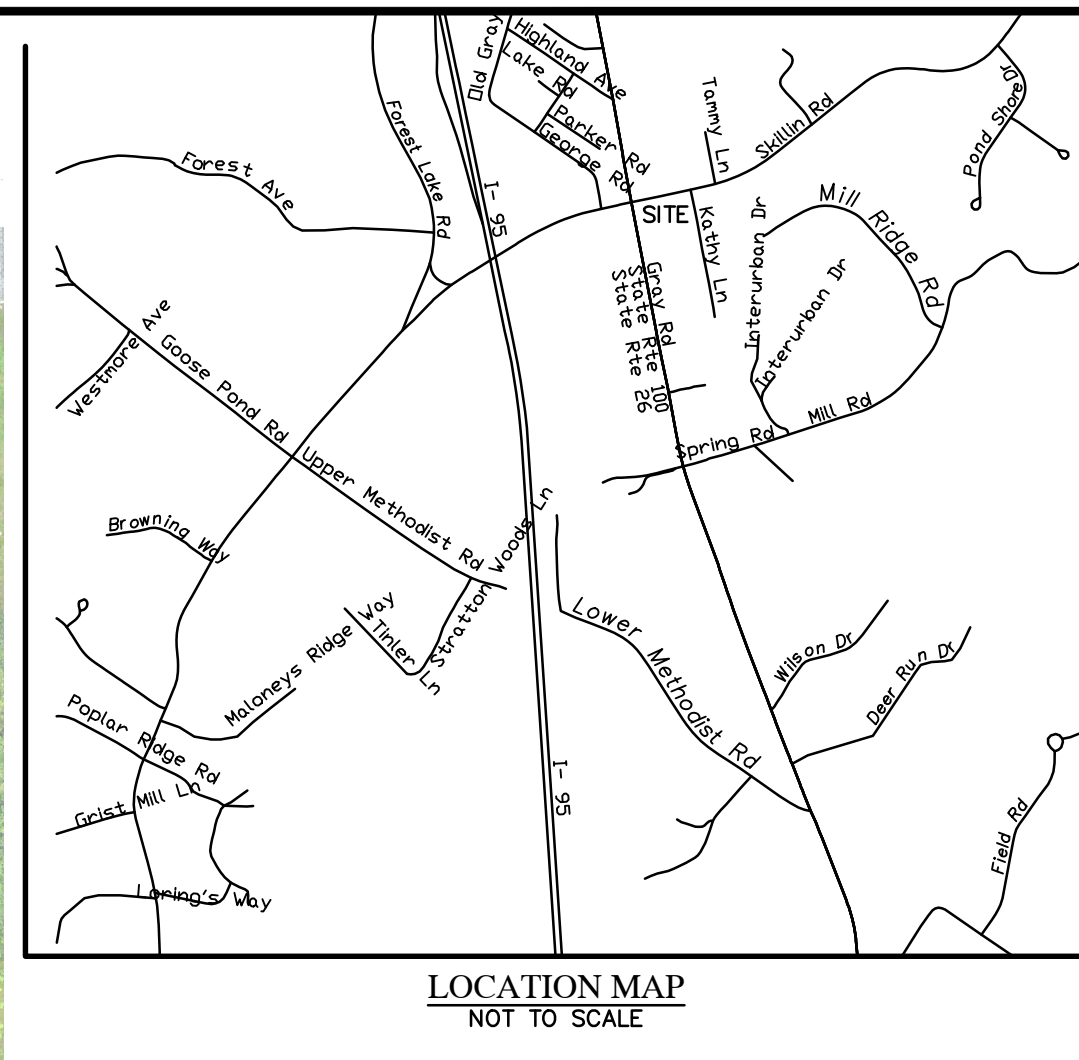
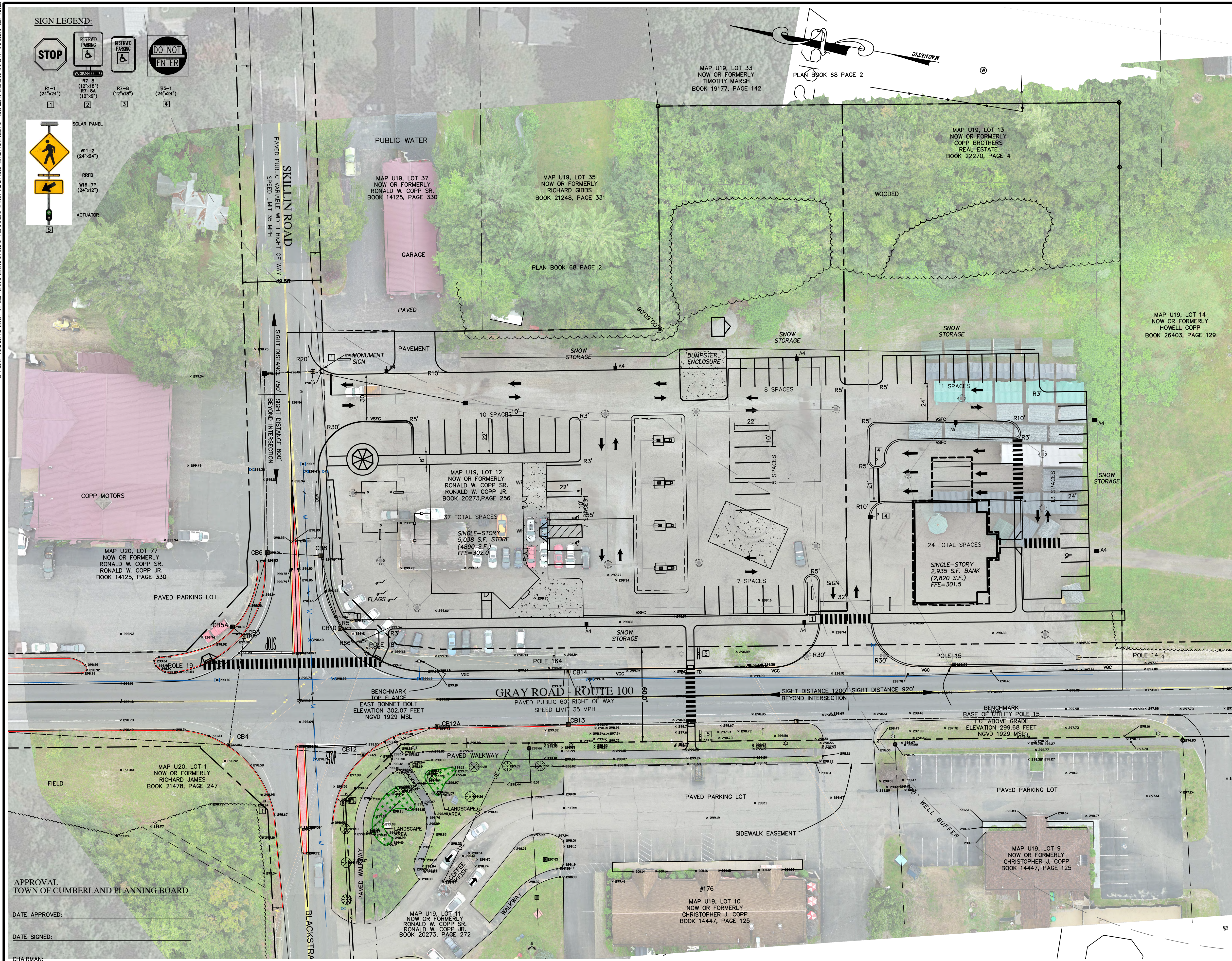
FIELD WK:	SCALE: 1"=30'	
DRN BY: CYN	JOB #: 22-RLM-004	
CHD BY: CYN	MAP/LOT: U-19 12&13	
DATE: 11-22-23	FILE:	

TITLE:



2.	01-29-24	SUBMITTED TO TOWN OF CUMBERLAND FOR SITE PLAN APPROVAL
1.	08-11-23	SUBMITTED FOR MAINEDOT REVIEW

1.	08-11-23	SUBMITTED FOR MAINTENANCE REVIEW
		SITE PLAN APPROVAL



GENERAL NOTES:

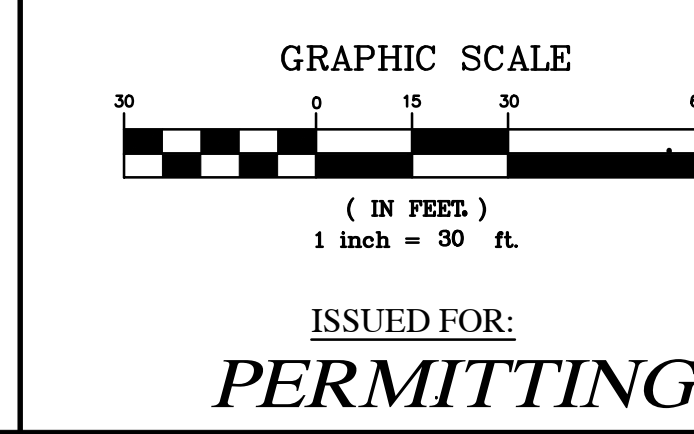
1. TITLE REFERENCE FOR SURVEYED PARCEL:
BK 20273, PG 256 (U19-12)
BK 34640, PG 209 (U19-13)
2. PLAN REFERENCE(S):
(1) EXISTING CONDITIONS SURVEY FOR PRIORITY REAL ESTATE GROUP OF 181 GRAY ROAD, CUMBERLAND, MAINE 04021, PREPARED BY BOUNDARY POINTS, NOT RECORDED.
3. AREA INFORMATION:
LOT AREA: 141,116 S.F. (3.24 ACRES)
4. TAX MAP REFERENCE:
TAX MAP U19, LOT 12 & 13.
5. BASIS OF BEARINGS:
BEARINGS ARE MAINE STATE PLANE, WEST ZONE, NAD 83.
6. ELEVATION DATUM:
NGVD 1929 MSL
7. FLOOD_ZONE INFORMATION:
PARCEL IS LOCATED WITHIN ZONE C (AREAS OF MINIMAL FLOODING) OF THE FLOOD INSURANCE RATE MAPS FOR CUMBERLAND COUNTY, MAINE. THE PROJECT IS LOCATED ON PANEL 15 OF 25 (COMMUNITY PANEL 230162 0015 B, EFF. DATE MAY 19, 1981)
8. IMPERVIOUS AREA:
EXISTING IMPERVIOUS AREA: 94,773 S.F. (2.18 AC)
PROPOSED IMPERVIOUS AREA: 68,232 S.F. (1.57 AC)
NET CHANGE IN IMPERVIOUS AREA: -26,541 S.F. (0.61 AC)

UTILITY NOTES:

1. INFORMATION REGARDING THE LOCATION OF EXISTING UNDERGROUND UTILITIES IS A PART OF THE RECORDS OF THE CITY OF PORTLAND, MAINE. CONTRACTOR SHALL BE RESPONSIBLE FOR FIELD VERIFYING UTILITY LOCATIONS PRIOR TO COMMENCING WORK. NOTING ANY DISCREPANCY BETWEEN UTILITIES AS SHOWN AND AS FOUND. CONTRACTOR SHALL NOTIFY DIG-SAFE PRIOR TO EXCAVATION.
1-888-344-7233

LAYOUT NOTES:

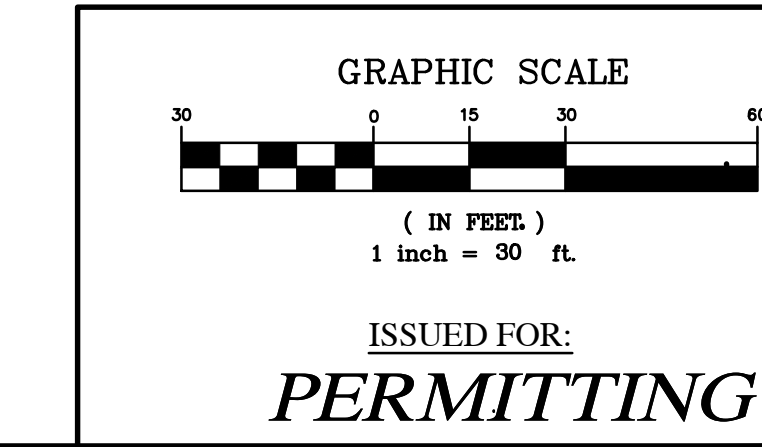
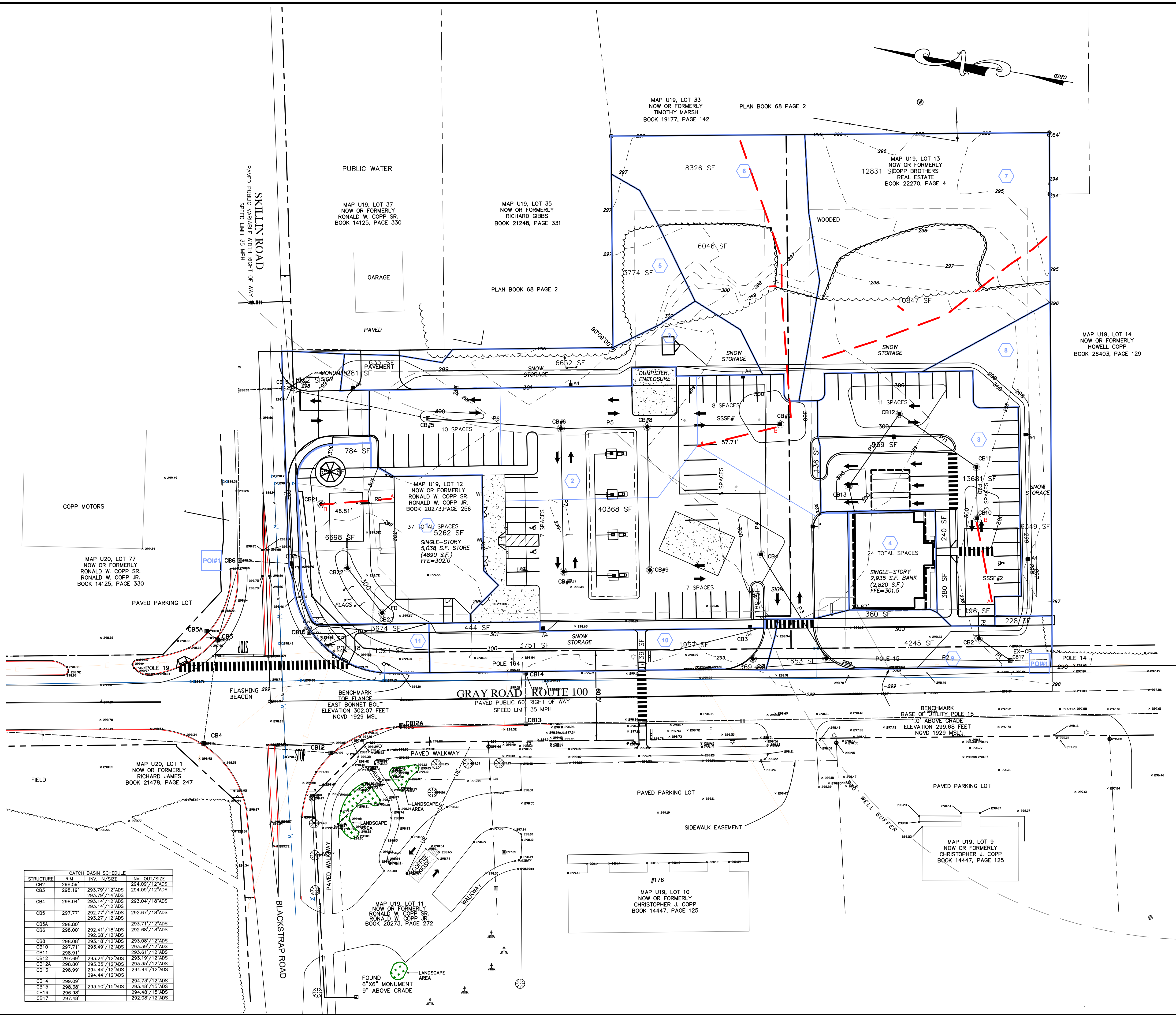
1. ALL DIMENSIONING, UNLESS NOTED OTHERWISE, IS TO THE FACE OF CURB OR FOUNDATION.
2. BOUNDARY INFORMATION ON LAYOUT PLAN IS FOR REFERENCE ONLY. REFER TO CERTIFIED BOUNDARY PLANS FOR BOUNDARY INFORMATION.
3. ALL HANDICAP ACCESSIBLE PARKING SPACES, RAMPS AND SIDEWALKS SHALL BE CONSTRUCTED IN CONFORMANCE WITH THE AMERICANS WITH DISABILITIES ACT (ADA).
4. ALL SITE SIGNAGE AND PAVEMENT MARKINGS SHALL CONFORM TO THE MANUAL OF UNIFORM TRAFFIC CONTROL DEVICES. (MUTCD)
5. BUILDING FOUNDATION SHOWN IS NOT FOR FOUNDATION LAYOUT. COORDINATE SITE WORK WITH ARCHITECTURAL DRAWINGS INCLUDING BUILDING FEATURES AND FOUNDATION PLAN.
6. REFER TO SHEET C4 FOR GRADING AND DRAINAGE INFORMATION.
7. REFER TO SHEET L1 FOR LANDSCAPE INFORMATION.
8. REFER TO SHEET L2 FOR LIGHTING INFORMATION.

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THIS DRAWING IS THE PROPERTY AND INSTRUMENT OF PRIORITY REAL ESTATE GROUP, LLC. NO REPRODUCTION OR CHANGES MAY BE MADE TO THIS DRAWING WITHOUT THE EXPRESS WRITTEN PERMISSION OF PRIORITY REAL ESTATE GROUP, LLC. ANY MODIFICATION, CHANGE OR USE OF THIS DRAWING WITHOUT THE EXPRESS WRITTEN PERMISSION OF PRIORITY REAL ESTATE GROUP, LLC IS PROHIBITED. DATE: 01-29-24

C:\USERS\CURT NEUFELD\ONE\DRIVE\PROJECTS\22-RLM-004 CUMBERLAND\DWG\22-004 SITE.DWG, DR2 POST, 1/30/2024 9:41 AM, CURT NEUFELD

STRUCTURE	CATCH BASIN SCHEDULE	INV. IN/OUT	INV. OUT/IN
CB2	298.59'	293.79'/12"ADS	294.09'/12"ADS
CB3	298.19'	293.79'/12"ADS	294.09'/12"ADS
CB4	298.04'	293.14'/12"ADS	293.04'/18"ADS
CB5	297.77'	292.77'/18"ADS	292.67'/18"ADS
CB5A	298.80'	292.41'/18"ADS	293.71'/12"ADS
CB6	298.00'	292.41'/18"ADS	292.68'/18"ADS
CB8	298.08'	293.18'/12"ADS	293.08'/12"ADS
CB10	297.71'	293.49'/12"ADS	293.39'/12"ADS
CB11	298.91'	293.49'/12"ADS	293.61'/12"ADS
CB12	297.69'	293.24'/12"ADS	293.19'/12"ADS
CB12A	298.60'	293.35'/12"ADS	293.35'/12"ADS
CB13	298.99'	294.44'/12"ADS	294.44'/12"ADS
CB14	299.09'	294.44'/12"ADS	294.73'/12"ADS
CB15	298.38'	293.50'/15"ADS	293.48'/15"ADS
CB16	298.98'	294.48'/15"ADS	294.48'/15"ADS
CB17	297.48'	292.08'/12"ADS	292.08'/12"ADS



LEGEND:

- SUBCATCHMENT AREA
- POINT OF INTEREST
- TIME OF CONCENTRATION

PRIORITY REAL ESTATE GROUP

PRIORITY

2 MAIN STREET
TOPSHAM, MAINE 04086
(207) 837-6198

SCALE: 1"=30'

DR2

FIELD WK: CYN

DRN BY: CYN

MAP/LOT: U-19 12&13

DATE: 11-22-23

FILE:

POST-DEVELOPMENT DRAINAGE PLAN

PROJECT: RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME 04021

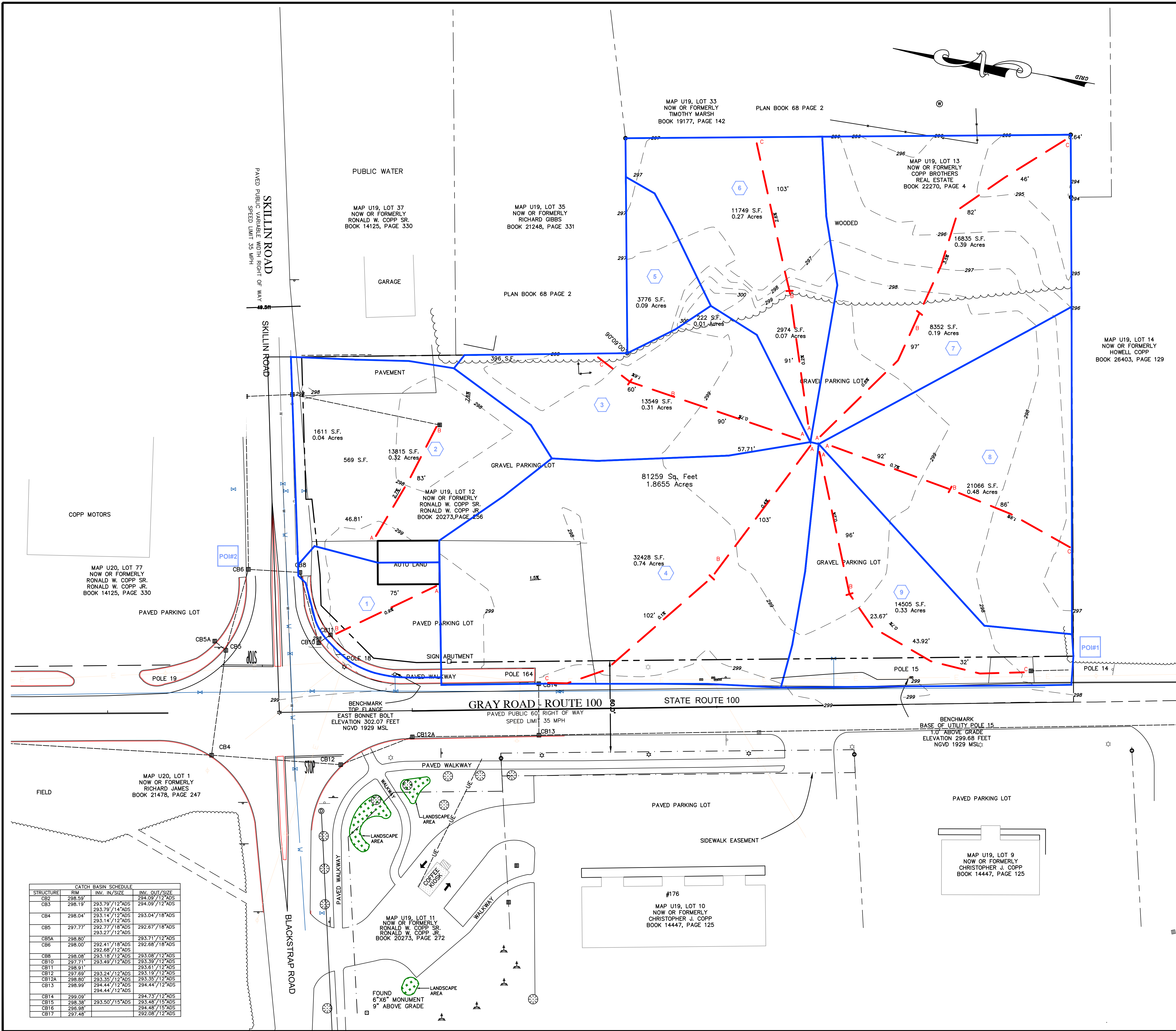
PREPARED FOR: CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET, TOPSHAM, ME 04086

01-29-24

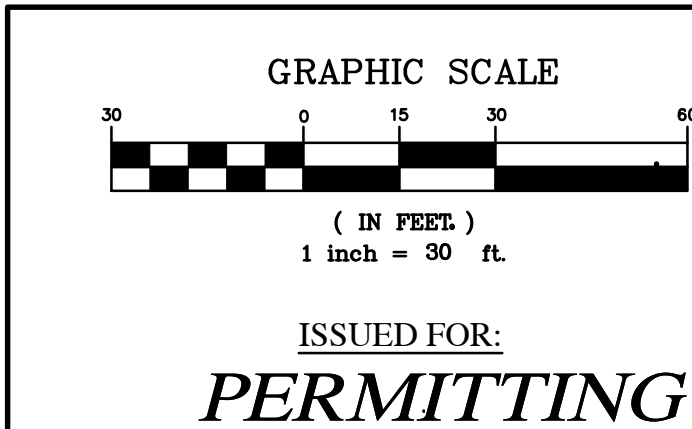
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PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.




CATCH BASIN SCHEDULE				
STRUCTURE	RM	IN	IN/ SIZE	OUT/ SIZE
CB1	298'19"	293'79"	12" AD	294.09' / 12" AD
CB3	298'19"	293'79"	12" AD	294.09' / 12" AD
CB4	298'04"	293'14"	12" AD	293.04' / 18" AD
CB5	297'77"	293'77"	18" AD	292.67' / 18" AD
CB5A	298'80"	293'27"	12" AD	293.71' / 12" AD
CB6	298'80"	292'41"	18" AD	292.68' / 18" AD
CB8	298'08"	293'18"	12" AD	293.08' / 12" AD
CB10	297'71"	293'49"	12" AD	293.39' / 12" AD
CB11	298'91"	293'35"	12" AD	293.61' / 12" AD
CB12	298'69"	293'25"	12" AD	293.59' / 12" AD
CB12A	298'80"	293'24"	12" AD	293.35' / 12" AD
CB13	298'99"	294'44"	12" AD	294.44' / 12" AD
CB14	299'09"			294.73' / 12" AD
CB15	298'36"	293'50"	15" AD	294.48' / 15" AD
CB16	298'91"	293'48"	12" AD	294.48' / 12" AD
CB17	297'48"			292.08' / 12" AD



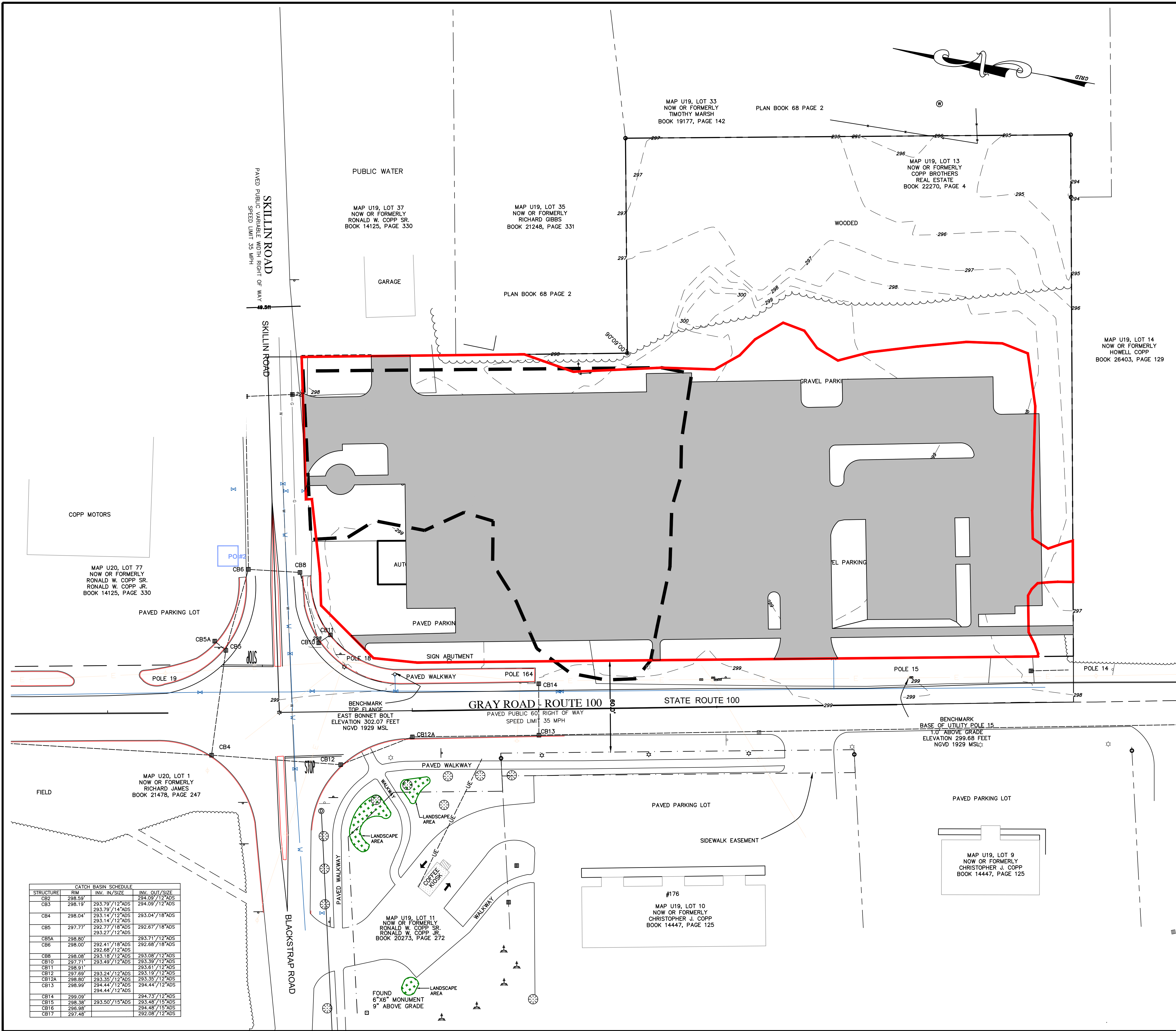
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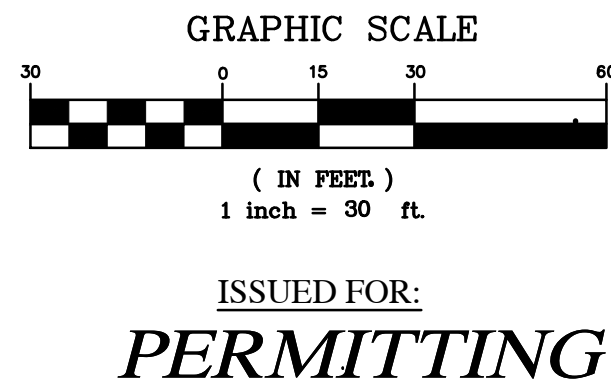
PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND MUST BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.

TITLE: <i>PRE-DEVELOPMENT DRAINAGE PLAN</i>				PRIORITY	
PROJECT: <i>RUSTY LANTERN CONVENIENCE STORE 181 GRAY ROAD, CUMBERLAND, ME 04021</i>		FIELD WK:		SCALE: 1"=30'	SHEET:
PREPARED FOR: <i>CUMBERLAND REAL ESTATE GROUP, LLC 2 MAIN STREET, TOPSHAM, ME 04086</i>		DRN BY: CYN		JOB #: 22-RLM-004	DR1
		CHD BY: CYN		MAP/LOT: U-19 12&13	
		DATE: 11-23-23		FILE:	

[illegible]



CATCH BASIN SCHEDULE				
STRUCTURE	RM	IN	IN/ SIZE	OUT/ SIZE
CB1	298'19"	293'79"	12" AD	294.09' / 12" AD
CB3	298'19"	293'79"	12" AD	294.09' / 12" AD
CB4	298'04"	293'14"	12" AD	293.04' / 18" AD
CB5	297'77"	293'77"	18" AD	292.67' / 18" AD
CB5A	298'80"	293'27"	12" AD	293.71' / 12" AD
CB6	298'80"	292'41"	18" AD	292.68' / 18" AD
CB8	298'08"	293'18"	12" AD	293.08' / 12" AD
CB10	297'71"	293'49"	12" AD	293.39' / 12" AD
CB11	298'91"	293'35"	12" AD	293.61' / 12" AD
CB12	298'69"	293'24"	12" AD	293.54' / 12" AD
CB12A	298'80"	293'25"	12" AD	293.35' / 12" AD
CB13	298'99"	294'44"	12" AD	294.44' / 12" AD
CB14	299'09"			294.73' / 12" AD
CB15	298'36"	293'50"	15" AD	294.48' / 15" AD
CB16	298'91"	293'48"	12" AD	294.48' / 12" AD
CB17	297'48"			292.08' / 12" AD



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PRICING BASED ON THIS PLAN SHALL BE CONSIDERED PRELIMINARY AND SHOULD BE UPDATED PRIOR TO FINAL CONSTRUCTION DRAWINGS.

TITLE: *PRE/POST DEVELOPMENT IMPERVIOUS AREA COMPARISON*

PROJECT: RUSTY LANTERN CONVENIENCE STORE
181 GRAY ROAD, CUMBERLAND, ME 04021

PREPARED FOR:
CUMBERLAND REAL ESTATE GROUP, LLC
2 MAIN STREET. TOPSHAM. ME 04086

PRIORITY
C MAIN STREET

2 MAIN STREET
TOPSHAM, MAINE 04086
(207) 837-6198

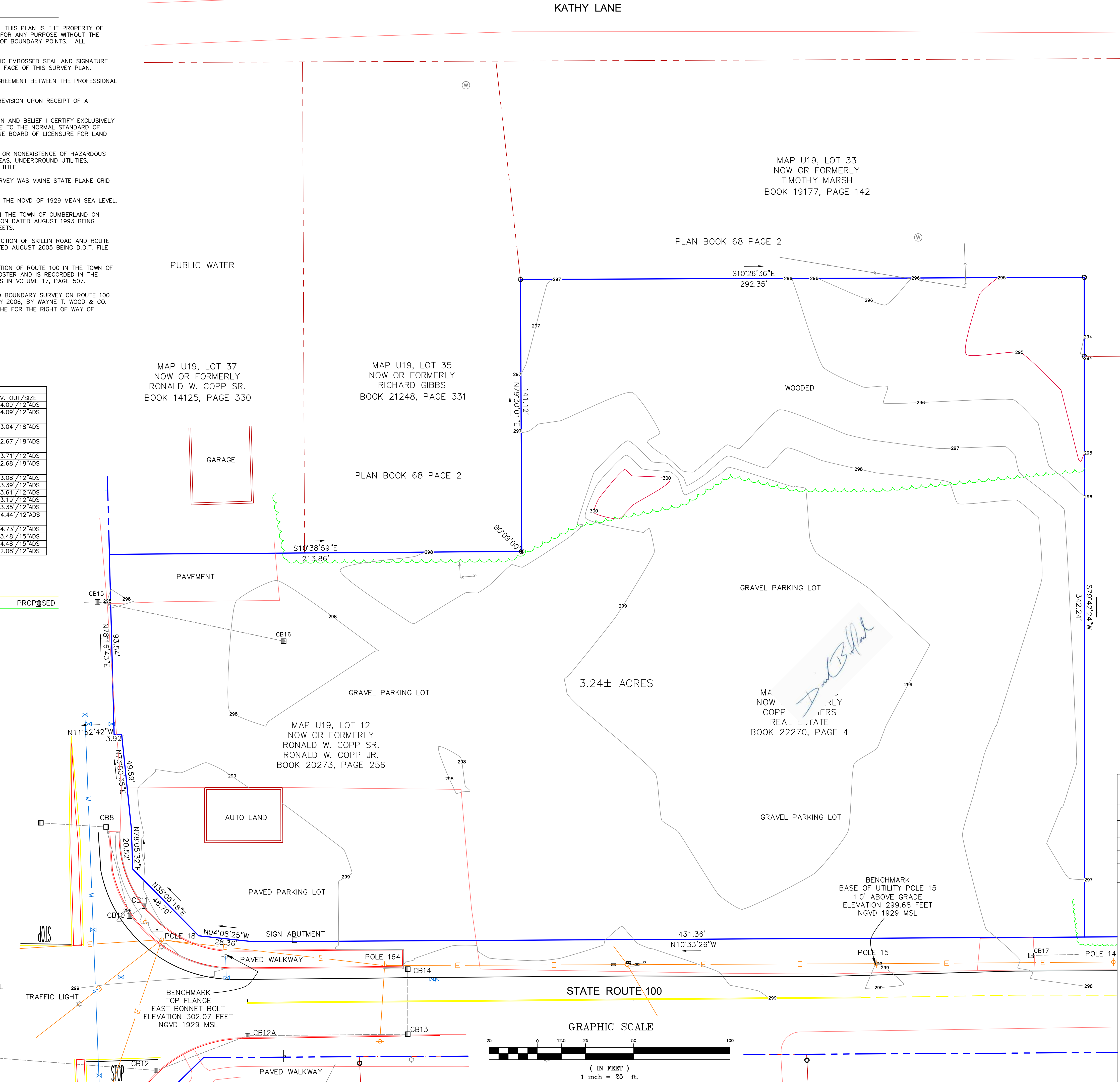
SURVEYOR'S NOTES

- 1 THIS SURVEY PLAN IS COPYRIGHT PROTECTED. THIS PLAN IS THE PROPERTY OF BOUNDARY POINTS, AND SHALL NOT BE USED FOR ANY PURPOSE WITHOUT THE WRITTEN CONSENT OF AN AUTHORIZED AGENT OF BOUNDARY POINTS. ALL RIGHTS RESERVED.
- 2 THIS SURVEY PLAN IS ONLY VALID IF AUTHENTIC EMBOSSED SEAL AND SIGNATURE OF CERTIFYING PROFESSIONAL APPEAR ON THE FACE OF THIS SURVEY PLAN.
- 3 REFERENCE IS MADE TO THE CONTRACTUAL AGREEMENT BETWEEN THE PROFESSIONAL LAND SURVEYOR AND THE CLIENT.
- 4 THIS SURVEY PLAN IS SUBJECT TO POSSIBLE REVISION UPON RECEIPT OF A CERTIFIED TITLE OPINION.
- 5 ON THE BASIS OF MY KNOWLEDGE, INFORMATION AND BELIEF I CERTIFY EXCLUSIVELY TO THE CLIENT THAT THIS SURVEY PLAN, MADE TO THE NORMAL STANDARD OF CARE, SUBSTANTIALLY CONFORMS TO THE MAINE BOARD OF LICENSURE FOR LAND SURVEYOR STANDARDS.
- 6 NO CERTIFICATION IS MADE TO THE EXISTENCE OR NONEXISTENCE OF HAZARDOUS SUBSTANCES, ENVIRONMENTALLY SENSITIVE AREAS, UNDERGROUND UTILITIES, UNDERGROUND STRUCTURES, OR REAL ESTATE TITLE.
- 7 THE SOURCE OF BEARINGS FOR THIS LAND SURVEY WAS MAINE STATE PLANE GRID WEST ZONE, N.A.D. 1983.
- 8 ELEVATIONS AND CONTOURS ARE BASED UPON THE NGVD OF 1929 MEAN SEA LEVEL.
- 9 REFERENCE IS MADE TO RIGHT OF WAY MAP IN THE TOWN OF CUMBERLAND ON ROUTE 100 BY DEPARTMENT OF TRANSPORTATION DATED AUGUST 1993 BEING D.O.T. FILE NUMBER 3-405 AND HAVING 2 SHEETS.
- 10 REFERENCE IS MADE TO PLAN OF THE INTERSECTION OF SKILLIN ROAD AND ROUTE 100 BY DEPARTMENT OF TRANSPORTATION DATED AUGUST 2005 BEING D.O.T. FILE NUMBER 3-517.
- 11 REFERENCE IS MADE TO PLAN OF THE RELOCATION OF ROUTE 100 IN THE TOWN OF CUMBERLAND DATED AUGUST 1906, BY H.W. FOSTER AND IS RECORDED IN THE CUMBERLAND COUNTY COMMISSIONERS RECORDS IN VOLUME 17, PAGE 507.
- 12 REFERENCE IS MADE TO PLAN OF A STANDARD BOUNDARY SURVEY ON ROUTE 100 IN THE TOWN OF CUMBERLAND DATED JANUARY 2006, BY WAYNE T. WOOD & CO. FOR ELVIN COPP. THIS PLAN WAS USED FOR THE FOR THE RIGHT OF WAY OF BLACKSTRAP ROAD.

CATCH BASIN SCHEDULE			
STRUCTURE	RIM	INV. IN/SIZE	INV. OUT/SIZE
CB2	298.59'	293.79'/12"ADS	294.09'/12"ADS
CB3	298.19'	293.79'/14"ADS	294.09'/12"ADS
CB4	298.04'	293.14'/12"ADS	293.04'/18"ADS
CB5	297.77'	292.77'/18"ADS	292.67'/18"ADS
CB5A	298.80'	293.27'/12"ADS	293.71'/12"ADS
CB6	298.00'	292.41'/18"ADS	292.68'/18"ADS
CB8	298.08'	293.18'/12"ADS	293.08'/12"ADS
CB10	297.71'	293.49'/12"ADS	293.39'/12"ADS
CB11	298.91'	293.61'/12"ADS	293.61'/12"ADS
CB12	297.69'	293.24'/12"ADS	293.19'/12"ADS
CB12A	298.80'	293.35'/12"ADS	293.35'/12"ADS
CB13	298.99'	294.44'/12"ADS	294.44'/12"ADS
CB14	299.09'	294.44'/12"ADS	294.73'/12"ADS
CB15	298.38'	293.50'/15"ADS	293.48'/15"ADS
CB16	296.98'		294.48'/15"ADS
CB17	297.48'		292.08'/12"ADS

LEGEND

EXISTING	DESCRIPTION	PROPOSED
	PROPERTY/ROW	
	EASEMENT	
	CENTERLINE	
	MONUMENT	
	IRON PIPE/ROD	
	5/8" IRON REBAR	
	DRILLHOLE	
	CURVE/LINE NO.	
	BUILDING	
	WETLANDS	
	EDGE WETLAND	
	SIGN	
	STREAM	
	ROCK OUTCROP	
	EDGE PAVEMENT	
	GRAVEL ROAD	
	GRANITE CURBLINE	
	EDGE WATER	
	TREELINE	
	MW-8	
	MONITORING WELL	
	124	
	WATER	
	STORM DRAIN	
	OVERHEAD	
	PAVED PARKING LOT	
	GATE VALVE	
	LIGHT	
	UTILITY POLE	
	HYDRANT	
	CATCH BASIN	
	MANHOLE	
	POTABLE WELL	
	CULVERT	
	SPOT GRADE	
	FENCE AS NOTED	
	WOODED GUARDRAIL	
	RIP RAP AREA	
	DECIDUOUS TREE	
	CONIFEROUS TREE	
	MAIL BOX	



Scale: 1" = 25'

Project No: 23-128F

AutoCAD Release: 2023

Drawn By: DB

Date: 5-30-2023

THIS PLAN IS PROVIDED EXCLUSIVELY FOR THE CLIENT STATED HEREON. ANY USE OR ALTERATION OF THIS PLAN BY OTHERS SHALL BE AT THE USER'S SOLE RISK AND WITHOUT LIABILITY TO BOUNDARY POINTS, LLC.

EXISTING CONDITIONS SURVEY FOR PRIORITY REAL ESTATE GROUP OF 181 GRAY ROAD CUMBERLAND MAINE 04021

Boundary Points

A DIVISION OF MAIN-LAND

69 MAIN ST. LIVERMORE FALLS, MAINE
367 US ROUTE 1 FALMOUTH, MAINE
PH: (207) 897-6752 FAX: (207) 897-5404
WWW.MAIN-LANDDCI.COM

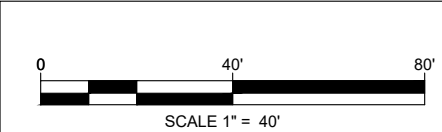
1

STATE OF MAINE
DAVID BOUFFARD
2282
PROFESSIONAL LAND SURVEYOR



SUBSURFACE SAND FILTER 3
168 UNITS

SUBSURFACE SAND FILTER 1
1192 UNITS





ENGINEER OF RECORD TO REVIEW, APPROVE AND ENDORSE FINAL SITE SPECIFIC DESIGN.



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1-800-448-3636, www.ferguson.com

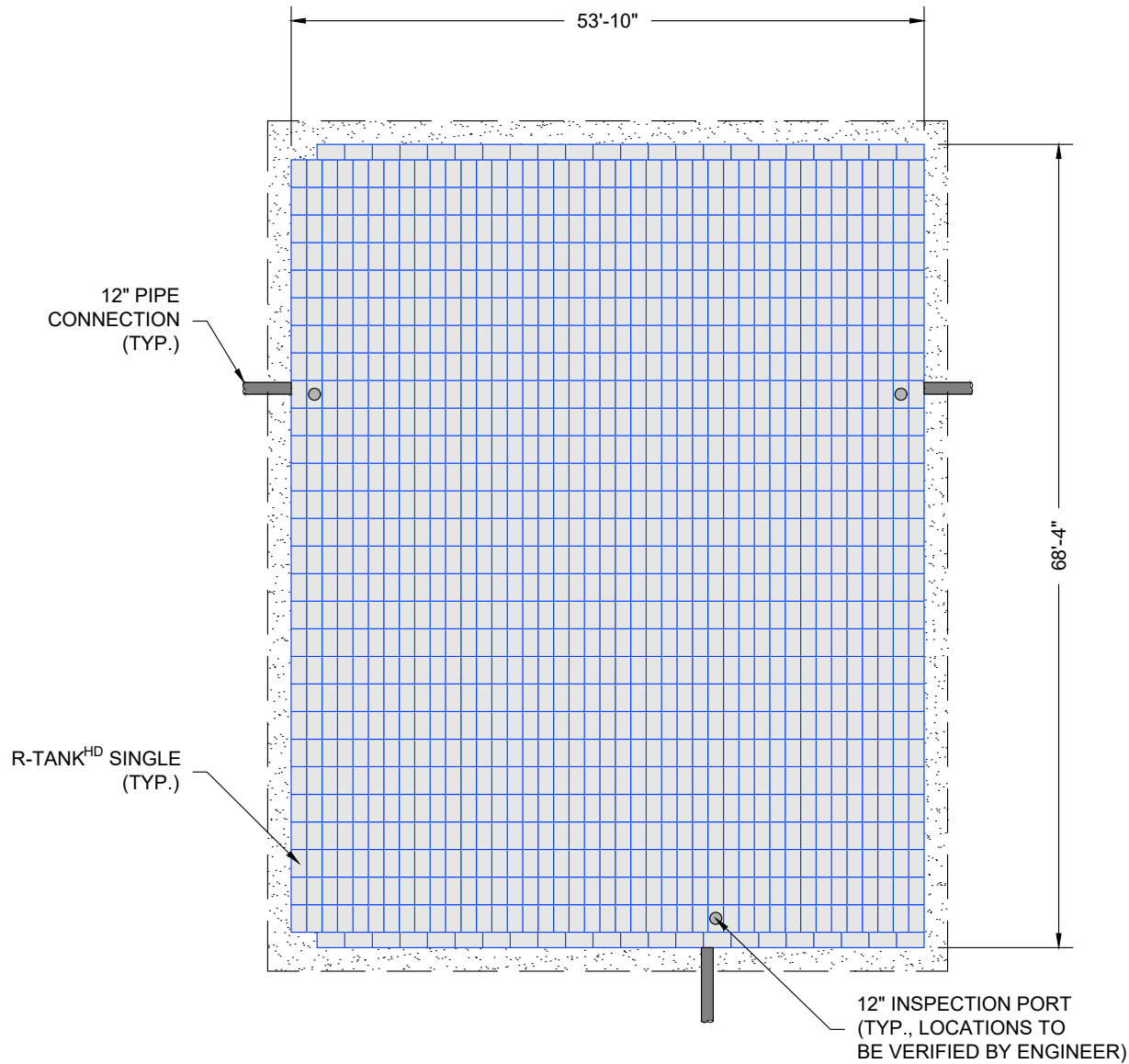
R-TANK^{HD} SYSTEM OVERLAY
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

SCALE
1" = 40'

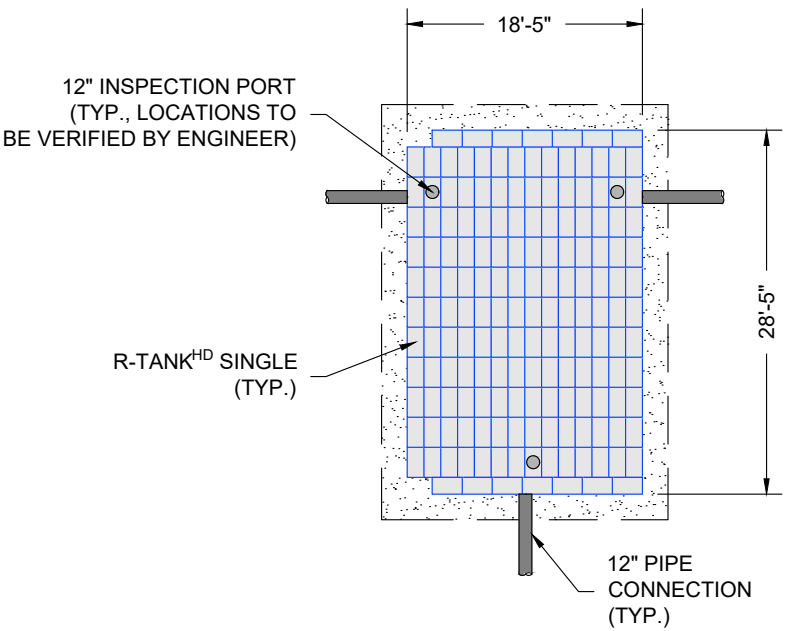
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BMK

DATE
01/29/2024

SHEET NO.
1 of **6**



SUBSURFACE SAND FILTER 1



SUBSURFACE SAND FILTER 3

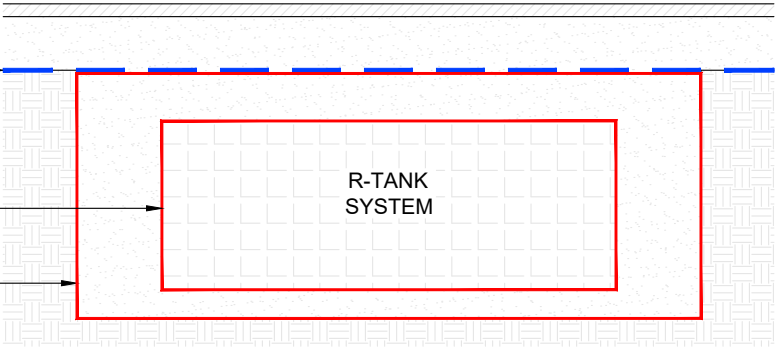
R-TANK QUANTITIES		
SYSTEM DESIGNATION	FILTER 1	FILTER 3
R-TANK ^{HD} MODULE TYPE	SINGLE	SINGLE
TRAFFIC LOAD	HS-20	HS-20
# OF SINGLE R-TANKS	1192	168
TOTAL SYSTEM STORAGE	7,417 CF	1,192 CF
R-TANK STORAGE VOLUME	5,032 CF	709 CF
STONE STORAGE VOLUME (40% VOID RATIO)	2,385 CF	483 CF
STONE BED FOOTPRINT	4,180 SF	726 SF
STONE QUANTITY	221 CY	45 CY
N080 NON-WOVEN GEOTEXTILE TANK WRAP	983 SY	150 SY
N080 NON-WOVEN GEOTEXTILE EXCAVATION WRAP	1,158 SY	223 SY
ACF BX-12 GEOGRID	639 SY	139 SY
12" INSPECTION PORTS	3	3
GEOTEXTILE PIPE BOOTS (12")	3	3
STORMRING CPS (12")	3	2
NOTE: STONE QUANTITY INCLUDES 12" OF COVER AND 3" OF BASE.		
NOTE: GEOTEXTILE / LINER QUANTITIES INCLUDE A 15% WASTE FACTOR.		
SEE SHEETS 3 - 6 FOR DETAILS AND ADDITIONAL INFORMATION		

GRAPHIC SCALE		
R-TANK ELEVATIONS		
SYSTEM DESIGNATION	FILTER 1	FILTER 3
BASE INV.	293.53	295.00
TANK INV.	293.78	295.25
TOP OF TANK	295.22	296.69
GEOGRID	296.22	297.69
MIN. ALLOW. FINAL GRADE	296.89	298.36
MAX. ALLOW. FINAL GRADE	302.21	303.68

GEOGRID (ACF BX-12) PLACED 12" ABOVE THE R-TANK^{HD} SYSTEM. OVERLAP ADJACENT PANELS BY 18" MIN. GEOGRID SHOULD EXTEND 3' BEYOND THE EXCAVATION FOOTPRINT.

R-TANK^{HD} UNITS WRAPPED WITH N080 NON-WOVEN GEOTEXTILE (OR EQUAL)

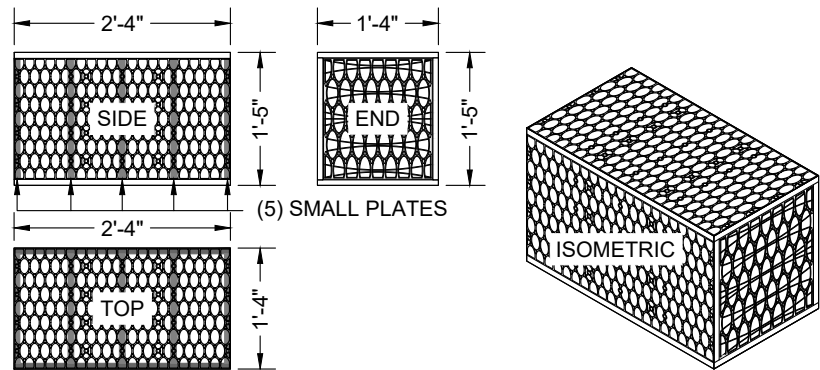
EXCAVATION WRAPPED WITH N080 NON-WOVEN GEOTEXTILE (OR EQUAL)



R-TANK^{HD} TANK WRAP & EXCAVATION ENVELOPE DETAIL

R-TANK^{HD} SYSTEM LAYOUT
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

SCALE
1" = 15'
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DATE
01/29/2024
SHEET NO.



MODULE DATA

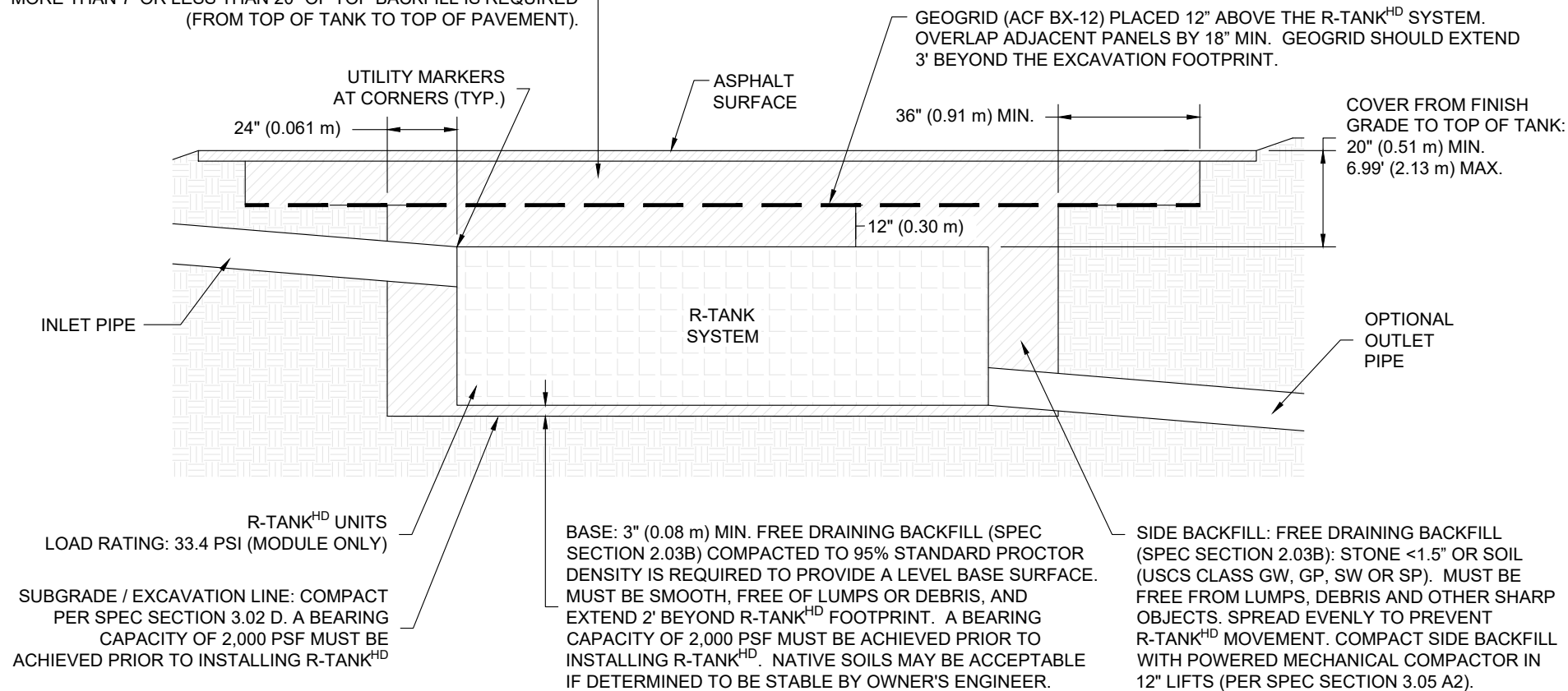
GEOMETRY:	LOAD RATING:
LENGTH = 28.15 IN. (715 MM)	33.4 PSI, (MODULE ONLY)
WIDTH = 15.75 IN. (400 MM)	HS20/HS25 - SEE SPEC FOR COVER REQUIREMENTS
HEIGHT = 17.32 IN. (440 MM)	MATERIAL:
TANK VOLUME = 4.44 CF	100% RECYCLED POLYPROPYLENE
STORAGE VOLUME = 4.22 CF	SMALL PLATES REQUIRED:
VOID INTERNAL VOLUME: 95%	5/SEGMENT, 5/MODULE
VOID SURFACE AREA: 90%	

SINGLE R-TANK^{HD} - MODULE DETAIL

TOTAL COVER: 20" MINIMUM AND 84" MAXIMUM. FIRST 12" MUST BE FREE DRAINING BACKFILL (SPEC SECTION 2.03B): STONE <1.5" OR SOIL (USCS CLASS GW, GP, SW OR SP). ADDITIONAL FILL MAY BE STRUCTURAL FILL (SPEC SECTION 2.03C): STONE OR SOIL (USCS CLASS SM, SP, SW, GM, GP OR GW) WITH MAX CLAY CONTENT <10%, MAX 25% PASSING NO. 200 SIEVE, AND MAX PLASTICITY INDEX OF 4. A MIN. 12" COVER MUST BE MAINTAINED BETWEEN BACKFILL EQUIPMENT AND THE TOP OF THE R-TANKTM SYSTEM AT ALL TIMES. TOTAL HEIGHT OF TOP BACKFILL SHOULD NOT EXCEED 7'. CONTACT FERGUSON WATERWORKS IF MORE THAN 7' OR LESS THAN 20" OF TOP BACKFILL IS REQUIRED (FROM TOP OF TANK TO TOP OF PAVEMENT).

NOTES:

- FOR COMPLETE MODULE DATA, SEE APPROPRIATE R-TANK^{HD} MODULE SHEET.
- INSTALLATIONS PER THIS DETAIL MEET GUIDELINES OF HL-93 LOADING PER THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, CUSTOMARY U.S. UNITS, 7TH EDITION, 2014 WITH 2015 AND 2016 INTERIM REVISIONS.
- PRE-TREATMENT STRUCTURES NOT SHOWN.
- FOR INFILTRATION APPLICATIONS, GEOTEXTILE ENVELOPING R-TANK SHALL BE ACF M200 (PER SPEC SECTION 2.02A) AND BASE SHALL BE 4" MIN. UNCOMPACTED FREE DRAINING BACKFILL (SPEC SECTION 2.03A) TO PROVIDE A LEVEL BASE. SURFACE MUST BE SMOOTH, FREE OF LUMPS OR DEBRIS, AND EXTEND 2' BEYOND R-TANK^{HD} FOOTPRINT.

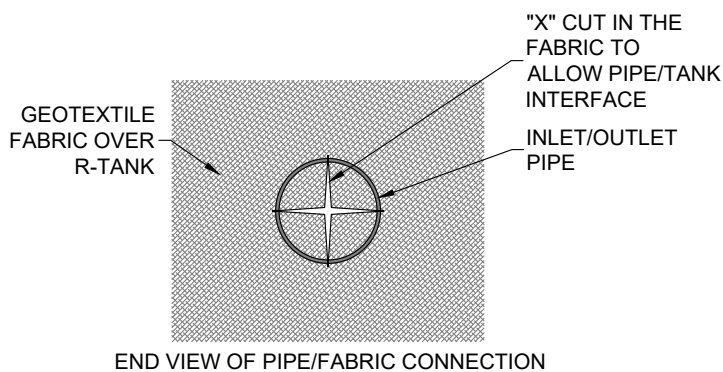


R-TANK^{HD} & HS-20 LOADS - SECTION VIEW

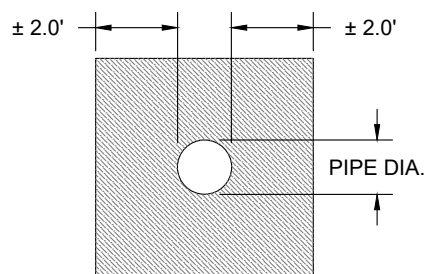
NOTE:

- PIPE BOOTS ARE AVAILABLE IN THE FOLLOWING STANDARD SIZES: 8" | 12" | 15" | 18" | 24".
- LARGER SPECIAL ORDER, CUSTOM SIZES ARE AVAILABLE.

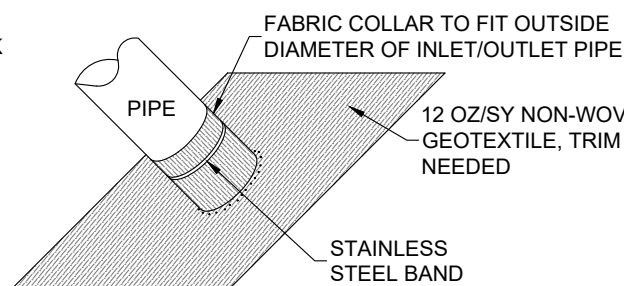
CUT AN "X" IN THE FABRIC ENVELOPE THAT IS SLIGHTLY LARGER THAN THE PIPE. PULL THE FABRIC FLAPS AROUND THE PIPE, AND SEAL WITH A STAINLESS STEEL BAND.



END VIEW OF PIPE/FABRIC CONNECTION

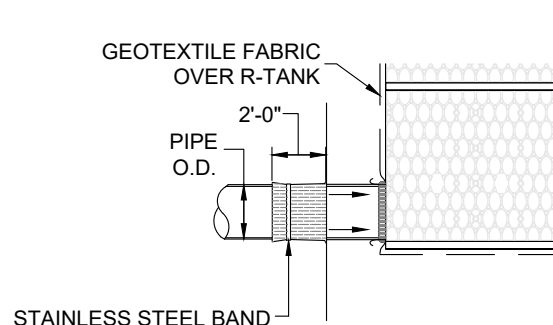


FRONT VIEW OF GEOTEXTILE BOOT

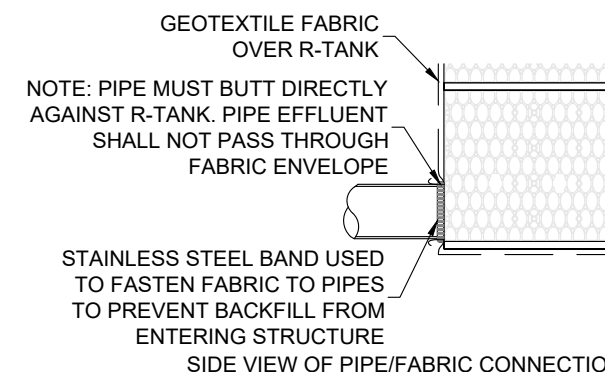


GEOTEXTILE BOOT

AFTER TANK WRAP IS SECURED TO PIPE, SLIDE BOOT AGAINST R-TANK AND SECURE WITH SECOND STAINLESS STEEL BAND, THEN ATTACH BOOT FLAP TO TANK ENVELOPE FABRIC WITH DUCT TAPE OR OTHER ADHESIVE.



SIDE VIEW OF GEOTEXTILE BOOT



SIDE VIEW OF PIPE/FABRIC CONNECTION

R-TANK TYPICAL TANK INLET/OUTLET W/ GEOTEXTILE PIPE BOOT DETAIL



FOR ADDITIONAL INFORMATION PLEASE CONTACT:
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1-800-448-3636, www.ferguson.com

R-TANK^{HD} SYSTEM DETAILS
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

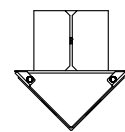
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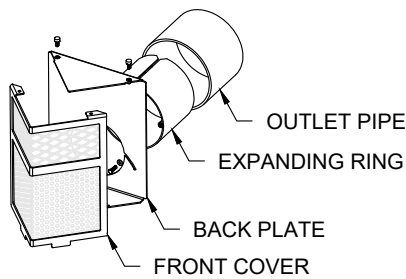
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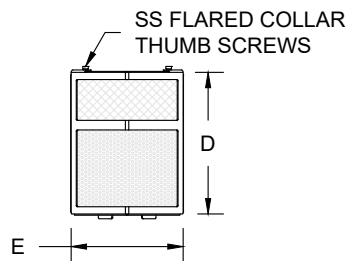
3 of 6



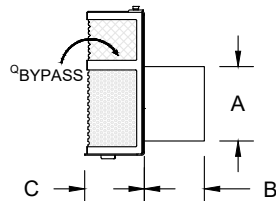
PLAN VIEW



REFERENCE VIEW



FRONT VIEW



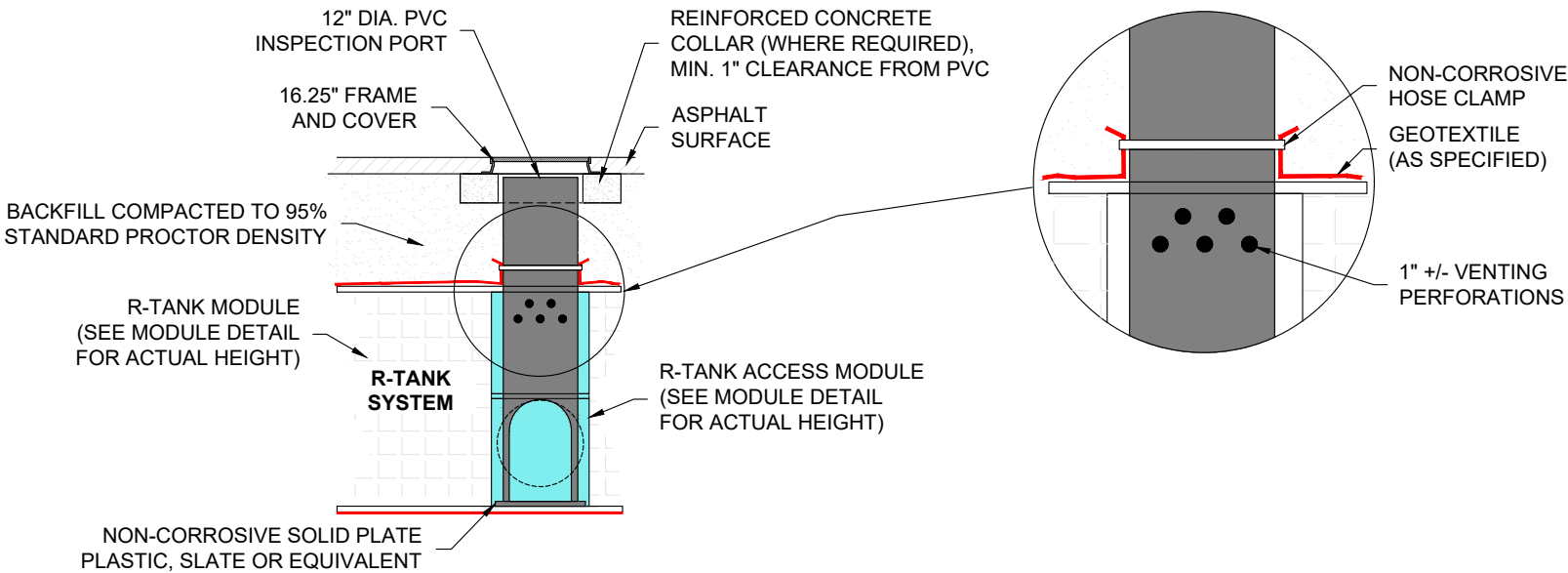
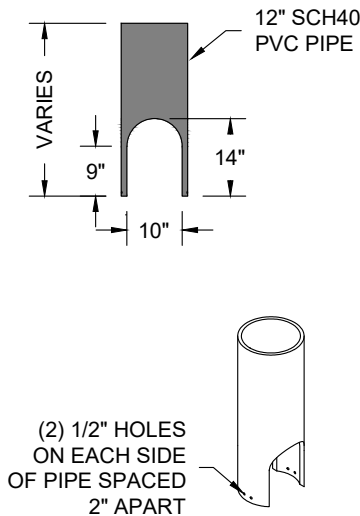
SIDE VIEW

PIPE DIA. (A)	STUB LENGTH (B)	CPS DEPTH (C)	CPS HEIGHT (D)	CPS WIDTH (E)
6"	4.00"	8.50"	10.00"	10.00"
8"	6.00"	11.00"	12.25"	11.50"
10"	8.00"	16.00"	13.50"	13.50"
12"	8.00"	16.00"	15.50"	15.50"
15"	8.00"	16.00"	21.50"	18.50"
18"	8.00"	16.00"	28.00"	21.50"
24"	10.00"	18.00"	40.00"	28.00"

STORMRING CPS PRETREATMENT DETAIL

NOTES

1. THE INSPECTION PORT IS USED IN THE ACCESS MODULE TO INSPECT THE LEVEL OF SEDIMENT ACCUMULATION.
2. MINIMUM REQUIRED MAINTENANCE INCLUDES A QUARTERLY INSPECTION DURING THE FIRST YEAR OF OPERATION AND A YEARLY INSPECTION THEREAFTER. FLUSH AS NEEDED.
3. R-TANK^{HD}, R-TANK^{SD}, R-TANK^{UD} AND R-TANK^{XD} MAY BE USED IN TRAFFIC APPLICATIONS.
4. SEE TRAFFIC LOADING DETAIL FOR MINIMUM & MAXIMUM COVER REQUIREMENTS.
5. IF INSPECTION PORT IS LOCATED IN A NON-TRAFFIC AREA, A PLASTIC CAP CAN BE USED IN LIEU OF A FRAME AND COVER WITH CONCRETE COLLAR.



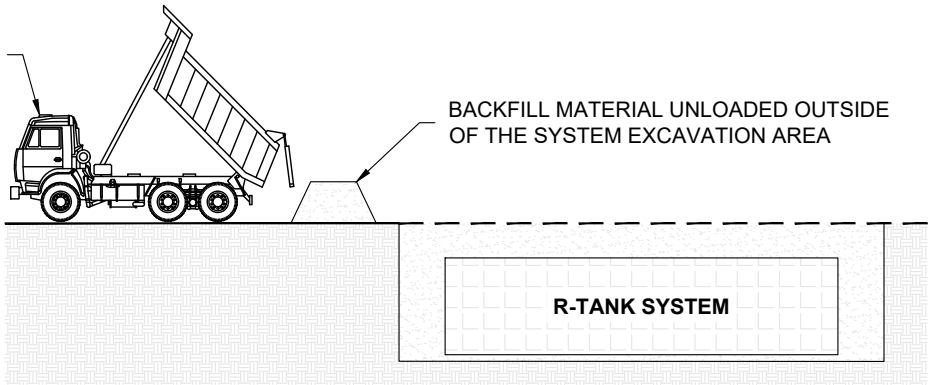
R-TANK TYPICAL VEHICULAR LOAD RATED INSPECTION PORT



R-TANK^{HD} SYSTEM DETAILS
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

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DUMP TRUCKS AND PANS SHALL NOT OPERATE OVER THE SYSTEM EXCAVATION AREA



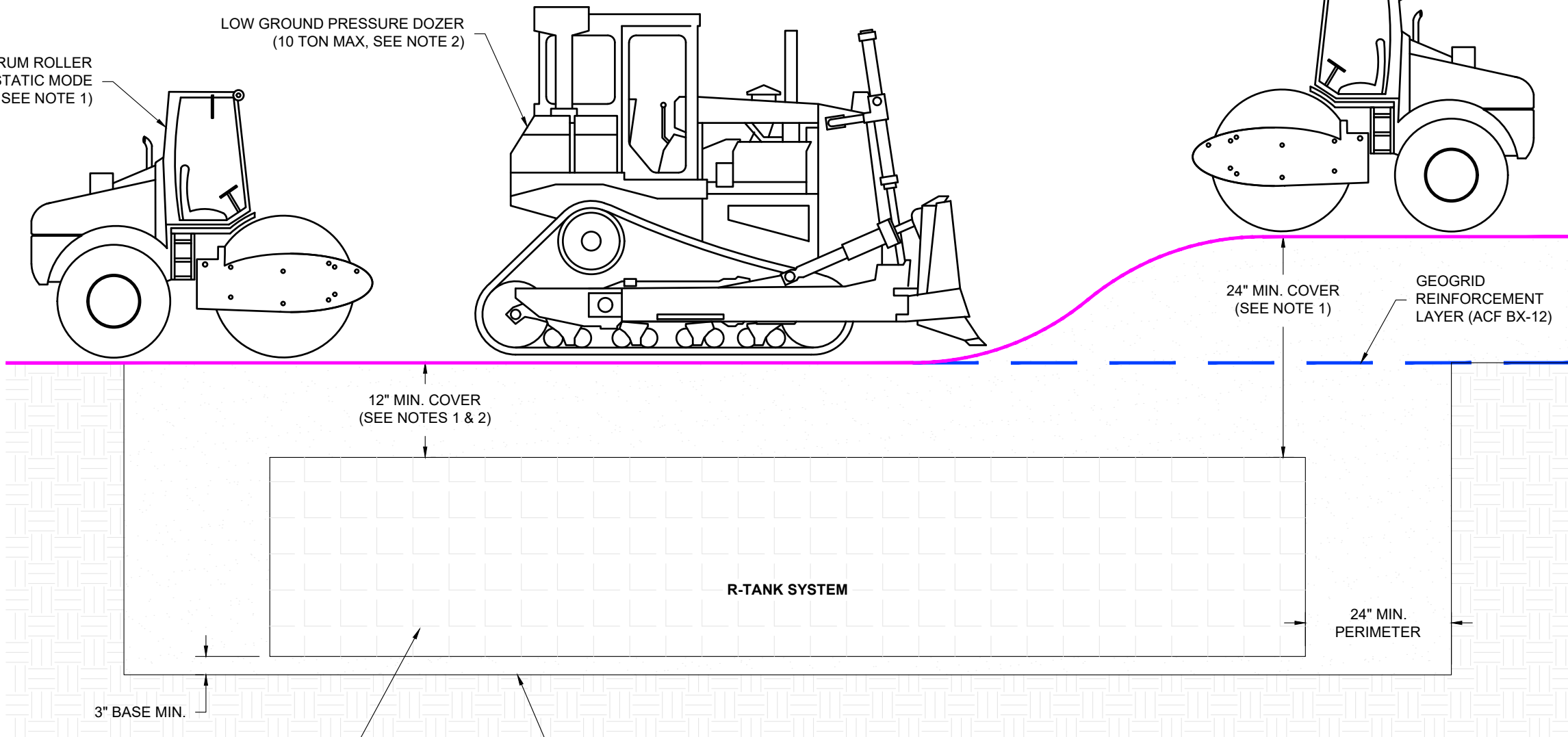
DUMP TRUCK DETAIL (SEE NOTE 3)

- NOTES:
1. FOLLOWING PLACEMENT OF SIDE BACKFILL, A UNIFORM 12" LIFT OF THE FREELY DRAINING MATERIAL (SPEC SECTION 2.03 B2) SHALL BE PLACED OVER THE R-TANK AND LIGHTLY COMPACTED USING A WALK-BEHIND TRENCH ROLLER. ALTERNATELY, A ROLLER (MAXIMUM GROSS VEHICLE WEIGHT OF 6 TONS) MAY BE USED. ROLLER MUST REMAIN IN STATIC MODE UNTIL A MINIMUM OF 24" OF COVER HAS BEEN PLACED OVER THE MODULES. SHEEP FOOT ROLLERS SHOULD NOT BE USED. **SPEC SECTION 3.05 A5**
 2. ONLY LOW PRESSURE TIRE OR TRACK VEHICLES (LESS THAN 7 PSI AND OPERATING WEIGHT OF LESS THAN 20,000 LBS) SHALL BE OPERATED OVER THE R-TANK SYSTEM DURING CONSTRUCTION. **SPEC SECTION 3.05 A5**
 3. DUMP TRUCKS AND PANS SHALL NOT BE OPERATED WITHIN THE R-TANK SYSTEM AT ANY TIME. WHERE NECESSARY, THE HEAVY EQUIPMENT SHOULD UNLOAD IN AN AREA ADJACENT TO THE R-TANK SYSTEM AND THE MATERIAL SHOULD BE MOVED OVER THE SYSTEM WITH TRACKED EQUIPMENT. **SPEC SECTION 3.05 A5**
 4. ENSURE THAT ALL UNRELATED CONSTRUCTION TRAFFIC IS KEPT AWAY FROM THE LIMITS OF EXCAVATION UNTIL THE PROJECT IS COMPLETE AND FINAL SURFACE MATERIALS ARE IN PLACE. NO NON-INSTALLATION RELATED LOADING SHOULD BE ALLOWED OVER THE R-TANK SYSTEM UNTIL THE FINAL DESIGN SECTION HAS BEEN CONSTRUCTED (INCLUDING PAVEMENT). **SPEC SECTION 3.05 B**
 5. SEE R-TANK INSTALLATION GUIDE OR CONTACT YOUR LOCAL FERGUSON REPRESENTATIVE FOR ADDITIONAL INFORMATION.

SMOOTH DRUM ROLLER
STATIC MODE
(6 TON MAX, SEE NOTE 1)

LOW GROUND PRESSURE DOZER
(10 TON MAX, SEE NOTE 2)

SMOOTH DRUM ROLLER
VIBRATORY MODE
(6 TON MAX, SEE NOTE 1)



R-TANK^{HD} UNITS
HD: LOAD RATING: 33.4 PSI (MODULE ONLY)

SUBGRADE / EXCAVATION LINE: COMPACT PER SPEC SECTION 3.02 D. A BEARING CAPACITY OF 2,000 PSF MUST BE ACHIEVED PRIOR TO INSTALLING R-TANK^{HD} OR R-TANK^{SD}

CONSTRUCTION EQUIPMENT COVER DETAIL - VEHICULAR TRAFFIC



ENGINEER OF RECORD TO REVIEW, APPROVE AND ENDORSE FINAL SITE SPECIFIC DESIGN.



FOR ADDITIONAL INFORMATION PLEASE CONTACT:
FERGUSON WATERWORKS,
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R-TANK^{HD} CONSTRUCTION EQUIPMENT
COVER DETAIL
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

SCALE
NTS

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BMK

DATE
01/29/2024

SHEET NO.

R-TANK SPECIFICATION

PART 1 - GENERAL

1.01 RELATED DOCUMENTS

- A. Drawings, technical specification and general provisions of the Contract as modified herein apply to this section.

1.02 DESCRIPTION OF WORK INCLUDED

- A. Provide excavation and base preparation per geotechnical engineer's recommendations and/or as shown on the design drawings, to provide adequate support for project design loads and safety from excavation sidewall collapse. Excavations shall be in accordance with the owner's and OSHA requirements.
- B. Provide and install R-TankHD/, R-TankHD/, R-TankSD/, or R-TankU/D/ system (hereafter called R-Tank) and all related products including fill materials, geotextiles, geogrids, inlet and outlet pipe with connections per the manufacturer's installation guidelines provided in this section.
- C. Provide and construct the cover of the R-Tank system including; stone backfill, structural fill cover, and pavement section as specified.
- D. Protect R-Tank system from construction traffic after installation until completion of all construction activity in the installation area.

1.03 QUALITY CONTROL

- A. All materials shall be manufactured in ISO certified facilities.
- B. Installation Contractor shall demonstrate the following experience:
1. A minimum of three R-Tank or equivalent projects completed within 2 years; and,
2. A minimum of 25,000 cubic feet of storage volume completed within 2 years.
3. Contractor experience requirement may be waived if the manufacturer's representative provides on-site training and review during construction.
- C. Installation Personnel: Performed only by skilled workers with satisfactory record of performance on bulk earthworks, pipe, chamber, or pond/landfill construction projects of comparable size and quality.
- D. Contractor must have manufacturer's representative available for site review if requested by Owner.

1.04 SUBMITTALS

- A. Submit proposed R-Tank layout drawings. Drawings shall include typical section details as well as the required base elevation of stone and tanks, minimum cover requirements and tank configuration.
- B. Submit manufacturer's product data, including compressive strength and unit weight.
- C. Submit manufacturer's installation instructions.
- D. Submit R-Tank sample for review. Reviewed and accepted samples will be returned to the Contractor.
- E. Submit material certificates for geotextile, geogrid, base course and backfill materials.
- F. Submit required experience and personnel requirements as specified in Section 1.03.
- G. Any proposed equal alternative product substitution to this specification must be submitted for review and approved prior to bid opening. Review package should include third party reviewed performance data that meets or exceeds criteria in Table 2.01 B.

1.05 DELIVERY, STORAGE, AND HANDLING

- A. Protect R-Tank and other materials from damage during delivery, and store UV sensitive materials under tarp to protect from sunlight when time from delivery to installation exceeds two weeks. Storage of materials should be on smooth surfaces, free from dirt, mud and debris.
- B. Handling is to be performed with equipment appropriate to the materials and site conditions, and may include hand, handcart, forklifts, extension lifts, etc.
- C. Cold weather:
1. Care must be taken when handling plastics when air temperature is 40 degrees or below as plastic becomes brittle.
2. Do not use frozen materials or materials mixed or coated with ice or frost.
3. Do not build on frozen ground or wet, saturated or muddy subgrade.

1.06 PREINSTALLATION CONFERENCE.

- A. Prior to the start of the installation, a preinstallation conference shall occur with the representatives from the design team, the general contractor, the excavation contractor, the R-Tank installation contractor, and the manufacturer's representative.

1.07 PROJECT CONDITIONS

- A. Coordinate installation for the R-Tank system with other on-site activities to eliminate all non-installation related construction traffic over the completed R-Tank system. No loads heavier than the design loads shall be allowed over the system, and in no case shall loads higher than a standard AASHTO HS20 (or HS25, depending on design criteria) load be allowed on the system at any time.
- B. Protect adjacent work from damage during R-Tank system installation.
- C. All pre-treatment systems to remove debris and heavy sediments must be in place and functional prior to operation of the R-Tank system. Additional pretreatment measures may be needed if unit is operational during construction due to increased sediment loads.
- D. Contractor is responsible for any damage to the system during construction.

PART 2 - PRODUCTS

2.01 R-TANK UNITS

- A. R-Tank - Injection molded plastic tank plates assembled to form a 95% void modular structure of predesigned height (custom for each project).
- B. R-Tank units shall meet the following Physical & Chemical Characteristics:

PROPERTY	DESCRIPTION	R-Tank ^{HD} VALUE	R-Tank ^{HD} VALUE	R-Tank ^{SD} VALUE	R-Tank ^{UD} VALUE
Void Area	Volume available for water storage	95%	95%	95%	95%
Surface Void Area	Percentage of exterior available for infiltration	90%	90%	90%	90%
Vertical Compressive Strength	ASTM D 2412 / ASTM F 2418	30.0 psi	33.4 psi	42.9 psi	134.2 psi
Lateral Compressive Strength	ASTM D 2412 / ASTM F 2418	20.0 psi	22.4 psi	28.9 psi	N/A
HS-20 Minimum Cover	Cover required to support HS-20 loads	N/A	20"	18"	12" (STONE BACKFILL)
HS-25 Minimum Cover	Cover required to support HS-25 loads	N/A	24"	19"	15" (STONE BACKFILL)
Maximum Cover	Maximum allowable cover depth	3 feet	< 7 feet	< 10 feet	5 feet
Unit Weight	Weight of plastic per cubic foot of tank	3.29 lbs / cf	3.62 lbs/cf	3.96 lbs / cf	4.33 lbs / cf
Rib Thickness	Thickness of load-bearing members	0.18 inches	0.18 inches	0.18 inches	N/A
Service Temperature	Safe temperature range for use	-14 – 167° F	-14 – 167° F	-14 – 167° F	-14 – 167° F

- C. Supplier: Ferguson Waterworks 2831 Cardwell Road Richmond, VA 23234 (T): 800-448-3636; (F): 804-743-7779 www.ferguson.com

2.02 GEOSYNTHETICS

- A. Geotextile. A geotextile envelope is required to prevent backfill material from entering the R-Tank modules.
1. Standard Application: The standard geotextile shall be an 8 oz per square yard nonwoven geotextile (ACF N080 or equivalent).
2. Infiltration Applications: When water must infiltrate/exfiltrate through the geotextile as a function of the system design, a woven monofilament (ACF M200 or equivalent) shall be used.
- B. Geogrid. For installations subject to traffic loads and/or when required by project plans, install geogrid (ACF BX12 or equivalent) to reinforce backfill above the R-Tank system. Geogrid is not always required for R-TankUD/ installations, and is often not required for non-traffic load applications.

2.03 BACKFILL & COVER MATERIALS

- A. Bedding Materials: Stone (angular and smaller than 1.5" in diameter) or soil (GW, GP, SW, or SP as classified by the Unified Soil Classification System) shall be used below the R-Tank system (3" minimum). Material must be free from lumps, debris, and any sharp objects that could cut the geotextile. Material shall be within 3 percent of the optimum moisture content as determined by ASTM D698 at the time of installation. For infiltration applications bedding material shall be free draining.
- B. Side and Top Backfill: Material must be free from lumps, debris and any sharp objects that could cut the geotextile. Material shall be within 3 percent of the optimum moisture content as determined by ASTM D698 at the time of installation.
1. Traffic Applications - Free draining material shall be used adjacent to (24" minimum) and above (for the first 12") the R-Tank system.
- a. For HD, and SD modules, backfill materials shall be free draining stone (angular and smaller than 1.5" in diameter) or soil (GW, GP, SW, or SP as classified by the Unified Soil Classification System).
- b. For UD modules with less than 14" of top cover, backfill materials shall be free draining stone (angular and smaller than 1.5" in diameter). The use of soil backfill on the sides and top of the UD module is not permitted unless the modules are installed outside of traffic areas or with cover depths of 14" or more. Top backfill material (from top of module to bottom of pavement base or 12" maximum) must be consistent with side backfill.
2. Non-Traffic / Green Space Applications - For all R-Tank modules installed in green spaces and not subjected to vehicular loads, backfill materials may either follow the guidelines for Traffic Applications above, or the top backfill layer (12" minimum) may consist of AASHTO #57 stone blended with 30-40% (by volume) topsoil to aid in establishing vegetation.
- C. Additional Cover Materials: Structural Fill shall consist of granular materials meeting the gradational requirements of SM, SP, SW, GM, GP or GW as classified by the Unified Soil Classification System. Structural fill shall have a maximum of 25 percent passing the No. 200 sieve, shall have a maximum clay content of 10 percent and a maximum Plasticity Index of 4. Material shall be within 3 percent of the optimum moisture content as determined by ASTM D698 at the time of installation.

2.04 OTHER MATERIALS

- A. Utility Marker: Install metallic tape at corners of R-Tank system to mark the area for future utility detection.

PART 3 - EXECUTION

3.01 ASSEMBLY OF R-TANK UNITS

- A. Assembly of modules shall be performed in accordance with the R-Tank Installation Manual, Section 2.

3.02 LAYOUT AND EXCAVATION

- A. Installer shall stake out, excavate, and prepare the subgrade area to the required plan grades and dimensions, ensuring that the excavation is at least 2 feet greater than R-Tank dimensions in each direction allowing for installation of geotextile filter fabric, R-Tank modules, and free draining backfill materials.
- B. All excavations must be prepared with OSHA approved excavated sides and sufficient working space.
- C. Protect partially completed installation against damage from other construction traffic by establishing a perimeter with high visibility construction tape, fencing, barricades, or other means until construction is complete.
- D. Base of the excavation shall be uniform, level, and free of lumps or debris and soft or yielding subgrade areas. A minimum 2,000 pounds per square foot bearing capacity is required.
1. Standard Applications: Compact subgrade to a minimum of 95% of Standard Proctor (ASTM D698) density or as required by the Owner's engineer.
2. Infiltration Applications: Subgrade shall be prepared in accordance with the contract documents. Compaction of subgrade should not be performed in infiltration applications.
- E. Unsuitable Soils or Conditions: All questions about the base of the excavation shall be directed to the owner's engineer, who will approve the subgrade conditions prior to placement of stone. The owner's engineer shall determine the required bearing capacity of the R-Tank subgrade; however in no case shall a bearing capacity of less than 2,000 pounds per square foot be provided.
1. If unsuitable soils are encountered at the subgrade, or if the subgrade is pumping or appears excessively soft, repair the area in accordance with contract documents and/or as directed by the owner's engineer.
2. If indications of the water table are observed during excavation, the engineer shall be contacted to provide recommendations.
3. Do not start installation of the R-Tank system until unsatisfactory subgrade conditions are corrected and the subgrade conditions are accepted by the owner's engineer.

3.03 PREPARATION OF BASE

- A. Place a thin layer (3" unless otherwise specified) of bedding material (Section 2.03 A), over the subgrade to establish a level working platform for the R-Tank modules. Level to within 1/8" (+/- 1/4") or as shown on the plans. Native subgrade soils or other materials may be used if determined to meet the requirements of 2.03 A and are accepted by the owner's engineer.
1. Standard Applications: Static roll or otherwise compact bedding materials until they are firm and unyielding.
2. Infiltration Applications: Bedding materials shall be prepared in accordance with the contract documents.
- B. Outline the footprint of the R-Tank system on the excavation floor using spray paint or chalk line to ensure a 2' perimeter is available around the R-Tank system for proper installation and compaction of backfill.

3.04 INSTALLATION OF THE R-TANKS

- A. Where a geotextile wrap is specified on the stone base, cut strips to length and install in excavation, removing wrinkles so material lays flat. Overlap geotextile a minimum 12" or as recommended by manufacturer. Use tape, special adhesives, sandbags or other ballast to secure overlaps. As geotextiles can be damaged by extreme heat, smoking is not permissible on/near the geotextile, and tools using a flame to tack the overlaps, such as propane torches, are prohibited.
- B. Where an impervious liner (for containment) is specified, install the liner per manufacturer's recommendations and the contract documents. The R-Tank units shall be separated from impervious liner by a non-woven geotextile fabric installed accordance with Section 3.04A.
- C. Install R-Tank modules by placing side by side, in accordance with the design drawings. No lateral connections are required. It is advisable to use a string line to form square corners and straight edges along the perimeter of the R-Tank system. The modules are to be oriented as per the design drawing with required depth as shown on plans.
1. For LD, HD, and SD installations, the large side plate of the tank should be placed on the perimeter of the system. This will typically require that the two ends of the tank area will have a row of tanks placed perpendicular to all other tanks. If this is not shown in the construction drawings, it is a simple field adjustment that will have minimal effect on the overall system footprint. Refer to R-Tank Installation Guide for more details
2. For UD installations, there is no perpendicular end row required.
- D. Wrap the R-Tank top and sides in specified geotextile. Cut strips of geotextile so that it will cover the sides and top, encapsulating the entire system to prevent backfill entry into the system. Overlap geotextile 12" or as recommended by manufacturer. Take great care to avoid damage to geotextile (and, if specified, impervious liner) during placement.
- E. Identify locations of inlet, outlet and any other penetrations of the geotextile (and optional liner). These connections should be installed flush (buted up to the R-Tank) and the geotextile fabric shall be cut to enable hydraulic continuity between the connections and the R-Tank units. These connections shall be secured using pipe boots with stainless steel pipe clamps. Support pipe in trenches during backfill operations to prevent pipe from settling and damaging the geotextile, impervious liner (if specified) or pipe. Connecting pipes at 90 degree angles facilitates construction, unless otherwise specified. Ensure end of pipe is installed snug against R-Tank system.
- F. Install Inspection and Maintenance Ports in locations noted on plans. At a minimum one maintenance port shall be installed within 10' of each inlet & outlet connection, and with a maximum spacing of one maintenance port for every 2,500 square feet. Install all ports as noted in the R-Tank Installation Guide.
- G. If required, install ventilation pipes and vents as specified on drawings to provide ventilation for proper hydraulic performance. The number of pipes and vents will depend on the size of the system. Vents are often installed using a 90 degree elbow with PVC pipe into a landscaped area with "U" bend or venting bollard to inhibit the ingress of debris. A ground level concrete or steel cover can be used.

3.05 BACKFILLING OF THE R-TANK UNITS

- A. Backfill and fill with recommended materials as follows:
1. Place freely draining backfill materials (Section 2.03 B) around the perimeter in lifts with a maximum thickness of 12". Each lift shall be placed around the entire perimeter such that each lift is no more than 24" higher than the side backfill along any other location on the perimeter of the R-Tank system. No fill shall be placed over top of tanks until the side backfill has been completed.
2. Each lift shall be compacted at the specified moisture content to a minimum of 95% of the Standard Proctor Density until no further densification is observed (for self-compacting stone materials). The side lifts must be compacted with walk behind compaction equipment. Even when "self-compacting" backfill materials are selected, a walk behind vibratory compactor must be used.
3. Take care to ensure that the compaction process does not allow the machinery to come into contact with the modules due to the potential for damage to the geotextile and R-Tank units.
4. No compaction equipment is permissible to operate directly on the R-Tank modules.
5. Top Backfill: Only low pressure track vehicles shall be operated over the R-Tank system during construction. Dump Trucks and Pans shall not be operated within the R-Tank system footprint at any time. Heavy equipment should unload in an area adjacent to the R-Tank system and the material should be moved over the system using tracked equipment with an operating weight of less than 10 tons.
- a. Typical Applications: Install a 12" (or as shown on plans) lift of freely draining material (Section 2.03 B) over the R-Tank Units, maintaining 12" between equipment tracks and R-Tank System. Lightly compacted using a walk-behind trench roller. Alternately, a roller (maximum gross vehicle weight of 6 tons) may be used. Roller must remain in static mode until a minimum of 24" of cover has been placed over the modules. Sheep foot rollers should not be used.
- b. Shallow Applications (< 18" total cover): Install top backfill in accordance with plans.
6. If required, install a geogrid as shown on plans. Geogrid shall extend a minimum of 3 feet beyond the limits of the excavation wall.
7. Following placement and compaction of the initial cover, subsequent lifts of structural fill (Section 2.03 C) shall be placed at the specified moisture content and compacted to a minimum of 95% of the Standard Proctor Density and shall cover the entire footprint of the R-Tank system. During placement of fill above the system, unless otherwise specified, a uniform elevation of fill shall be maintained to within 12" across the footprint of the R-Tank system. Do not exceed maximum cover depths listed in Table 2.01 B.
8. Place additional layers of geotextile and/or geogrid at elevations as specified in the design details. Each layer of geosynthetic reinforcement placed above the R-Tank system shall extend a minimum of 3 feet beyond the limits of the excavation wall.
- B. Ensure that all unrelated construction traffic is kept away from the limits of excavation until the project is complete and final surface materials are in place. No non-installation related loading should be allowed over the R-Tank system until the final design section has been constructed (including pavement).
- C. Place surfacing materials, such as groundcovers (no large trees), or paving materials over the structure with care to avoid displacement of cover fill and damage to surrounding areas.
- D. Backfill depth over R-Tank system must be within the limitations shown in the table in Section 2.01 B. If the total backfill depth does not comply with this table, contact engineer or manufacturer's representative for assistance.

3.06 MAINTENANCE REQUIREMENTS

- A. A routine maintenance effort is required to ensure proper performance of the R-Tank system. The Maintenance program should be focused on pretreatment systems. Ensuring these structures are clean and functioning properly will reduce the risk of contamination of the R-Tank system and stormwater released from the site. Pre-treatment systems shall be inspected yearly, or as directed by the regulatory agency and by the manufacturer (for proprietary systems). Maintain as needed using acceptable practices or following manufacturer's guidelines (for proprietary systems).
- B. All inlet pipes and Inspection and/or Maintenance Ports in the R-Tank system will need to be inspected for accumulation of sediments at least quarterly through the first year of operation and at least yearly thereafter.
- C. If sediment has accumulated to the level noted in the R-Tank Maintenance Guide or beyond a level acceptable to the Owner's engineer, the R-Tank system should be flushed.
- D. All inspection and maintenance activities should be performed in accordance with the R-Tank Operation, Inspection & Maintenance Manual.

HD

TANK



ENGINEER OF RECORD TO REVIEW, APPROVE AND ENDORSE FINAL SITE SPECIFIC DESIGN.

FERGUSON
WATERWORKS

FOR ADDITIONAL INFORMATION PLEASE CONTACT:

FERGUSON WATERWORKS,
1-800-448-3636, www.ferguson.com

R-TANK^{HD} SPECIFICATION
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

SCALE
NTS

DRAWN BY
BMK

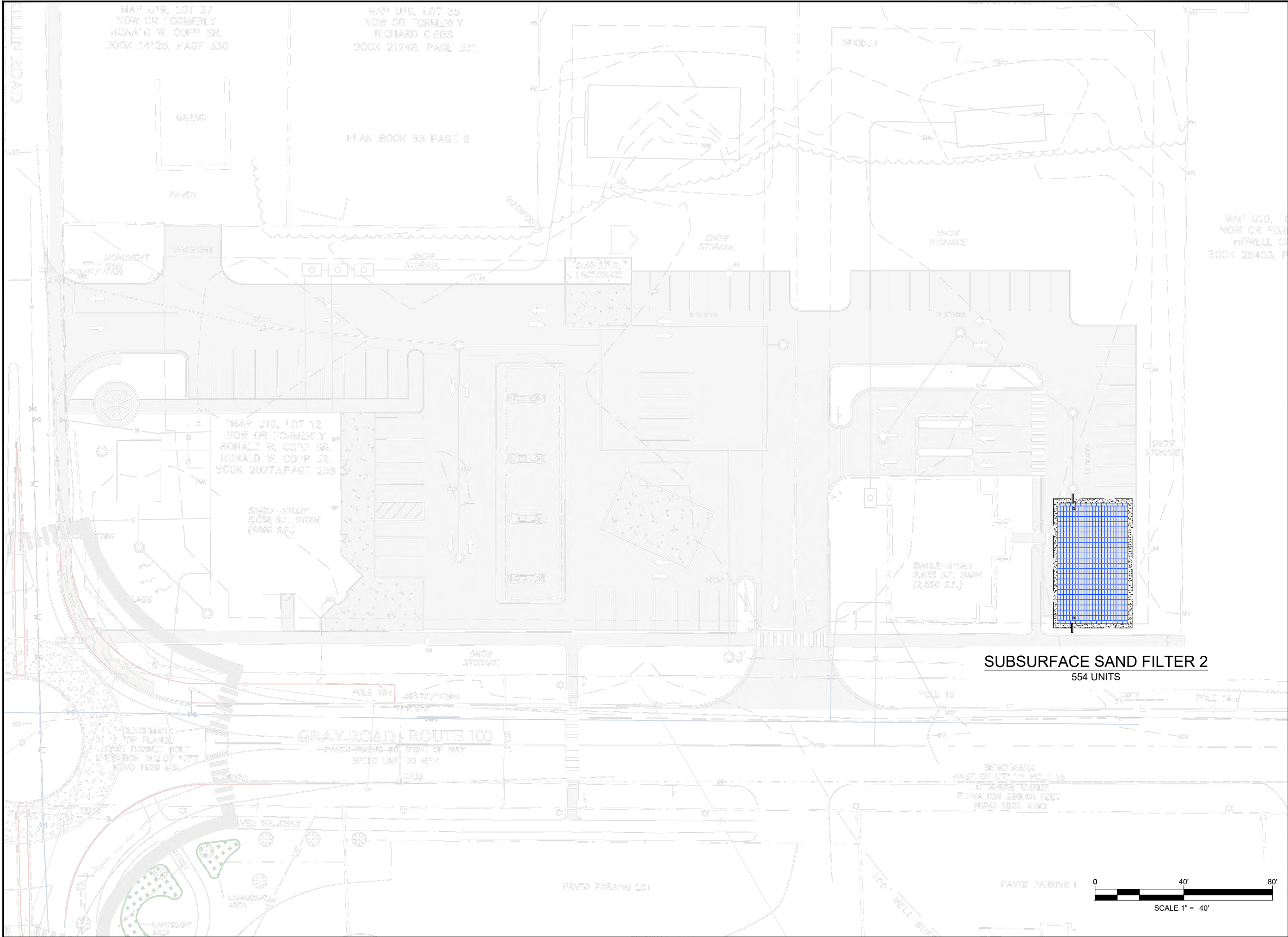
DATE
01/29/2024

SHEET NO.

6

of

6



MAP U19, LOT 37
NOW OR FORMERLY
RONALD W. COPP SR.
BOOK 14125, PAGE 330

MAP U19, LOT 35
NOW OR FORMERLY
RICHARD GIBBS
BOOK 21248, PAGE 331

PLAN BOOK 68 PAGE 2

GARAGE

PAVED

MONUMENT
SIGN

PAVEMENT

SNOW
STORAGE

SNOW
STORAGE

SNOW
STORAGE

MAP U19, LOT 14
NOW OR FORMERLY
HOWELL CO
BOOK 26403, PAGE 1

MAP U19, LOT 12
NOW OR FORMERLY
RONALD W. COPP SR.
RONALD W. COPP JR.
BOOK 20273, PAGE 256

SINGLE-STORY
5,038 S.F. STORE
(4,890 S.F.)

SINGLE-STORY
2,935 S.F. BANK
(2,820 S.F.)

SUBSURFACE SAND FILTER 2
554 UNITS

GRAY ROAD - ROUTE 100

PAVED PUBLIC 60' RIGHT OF WAY
SPEED LIMIT 35 MPH

BENCHMARK
BASE OF UTILITY POLE 15
1.0' ABOVE GRADE
ELEVATION 289.68 FEET
NGVD 1929 MSL

R-TANK^{SD} SYSTEM OVERLAY
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

SCALE
1" = 40'
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BMK
DATE
01/29/2024
SHEET NO.

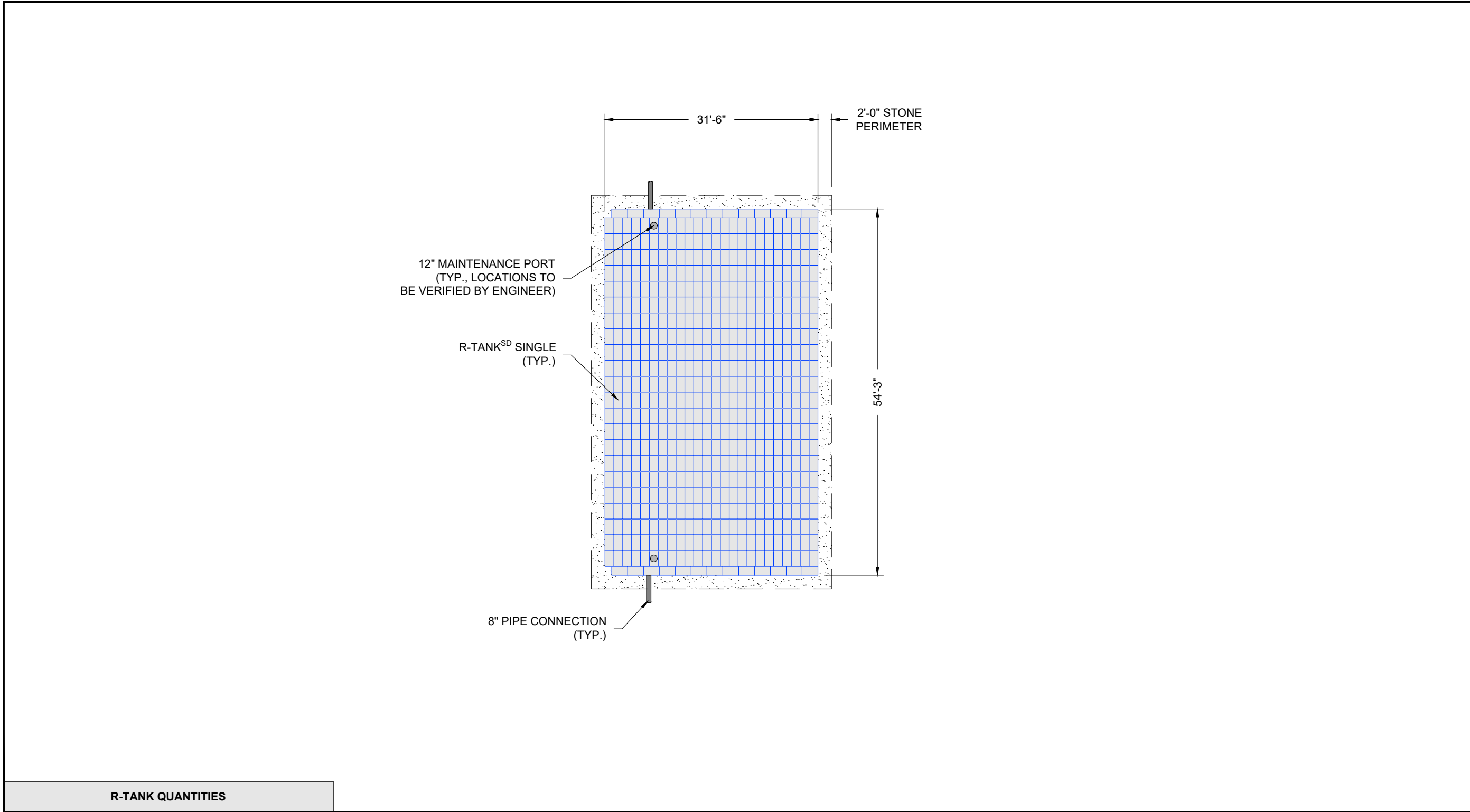
1 of 6

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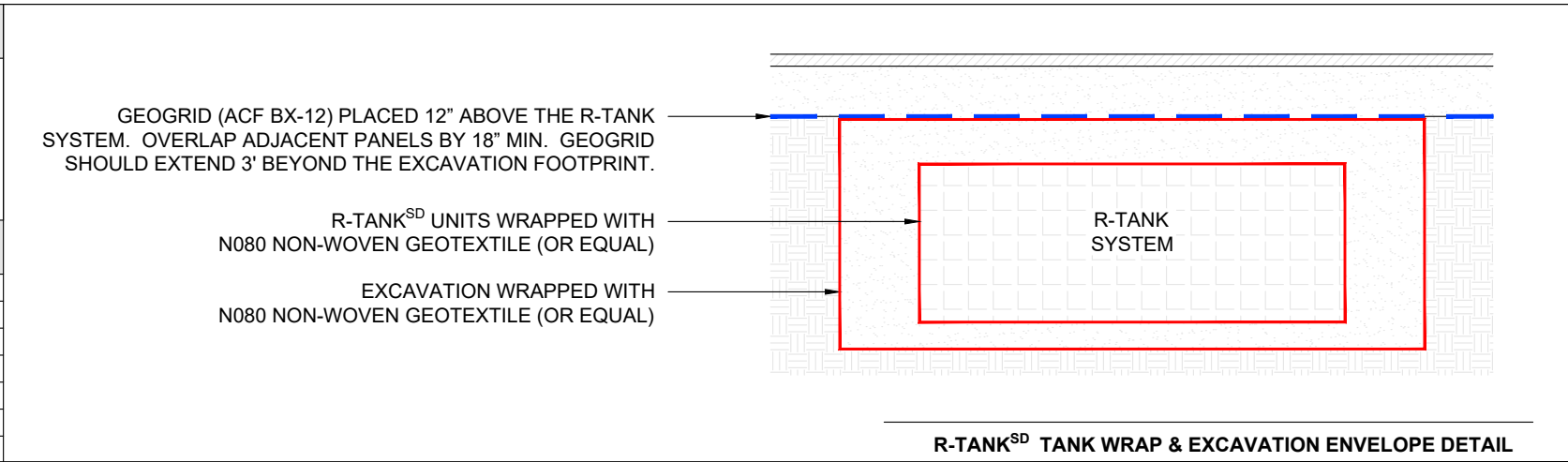


ENGINEER OF RECORD TO REVIEW, APPROVE AND
ENDORSE FINAL SITE SPECIFIC DESIGN.



R-TANK QUANTITIES	
R-TANK ^{SD} MODULE TYPE	SINGLE
TRAFFIC LOAD	HS-20
# OF SINGLE R-TANKS	554
TOTAL SYSTEM STORAGE	2,424 CF
R-TANK STORAGE VOLUME	1,276 CF
STONE STORAGE VOLUME (40% VOID RATIO)	1,148 CF
STONE BED FOOTPRINT	2,067 SF
STONE QUANTITY	106 CY
N080 NON-WOVEN GEOTEXTILE TANK WRAP	453 SY
N080 NON-WOVEN GEOTEXTILE EXCAVATION WRAP	577 SY
ACF BX-12 GEOGRID	341 SY
12" MAINTENANCE PORTS	2
GEOTEXTILE PIPE BOOTS (8")	2
STORMRING CPS (8")	1
NOTE: STONE QUANTITY INCLUDES 12" OF COVER AND 3" OF BASE.	
NOTE: GEOTEXTILE / LINER QUANTITIES INCLUDE A 15% WASTE FACTOR.	
SEE SHEETS 3 - 6 FOR DETAILS AND ADDITIONAL INFORMATION	

GRAPHIC SCALE	
R-TANK ELEVATIONS	
DESCRIPTION	ELEVATION
BASE INV.	292.47
TANK INV.	292.72
TOP OF TANK	293.51
GEOGRID	294.51
MIN. ALLOW. FINAL GRADE	295.01
MAX. ALLOW. FINAL GRADE	303.50



R-TANK^{SD} TANK WRAP & EXCAVATION ENVELOPE DETAIL



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ENDORSE FINAL SITE SPECIFIC DESIGN.



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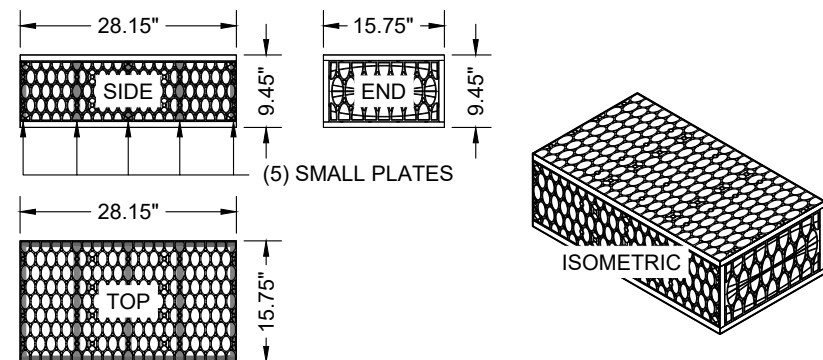
R-TANK^{SD} SYSTEM LAYOUT
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

SCALE
1" = 15'

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DATE
01/29/2024

SHEET NO.



MODULE DATA

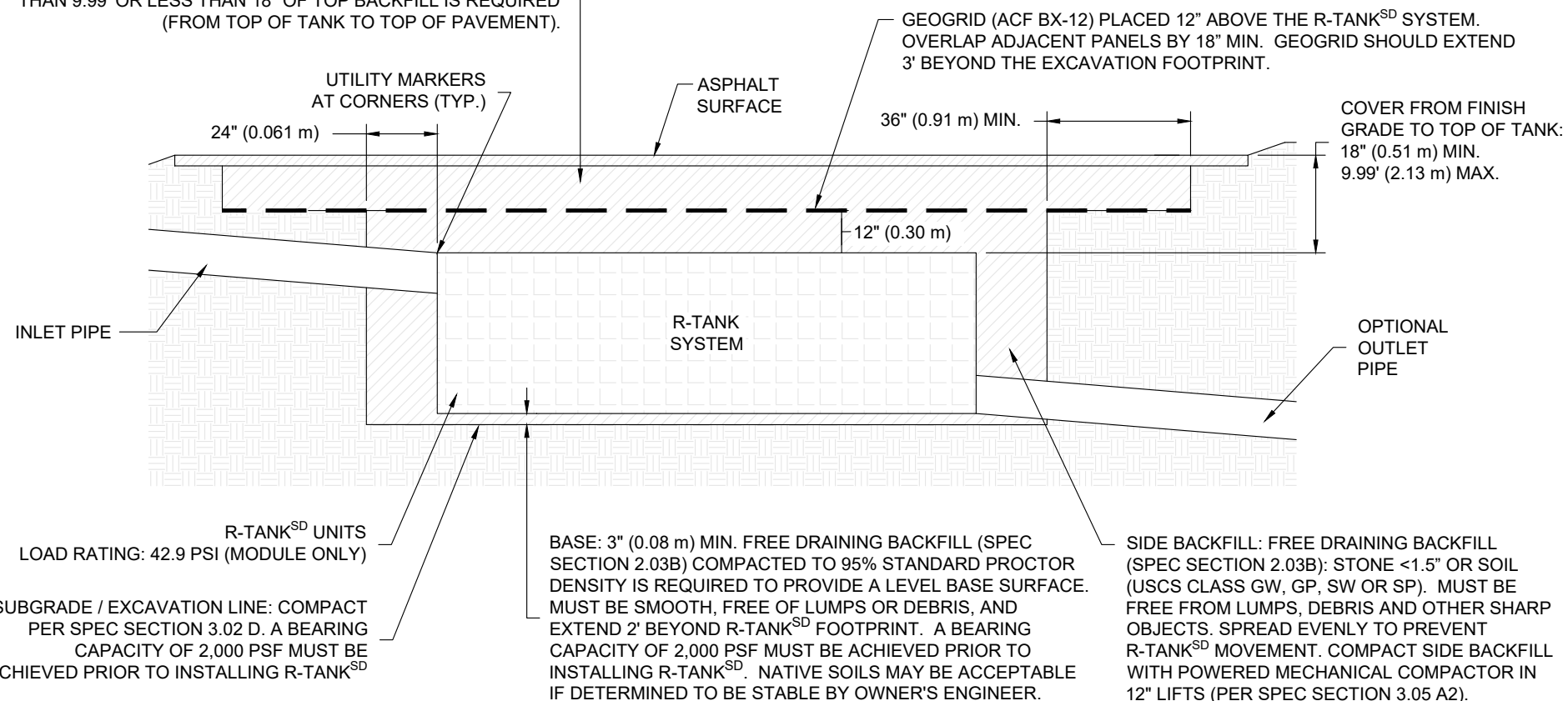
GEOMETRY:	LOAD RATING:
LENGTH = 28.15 IN. (715 MM)	42.9 PSI, (MODULE ONLY)
WIDTH = 15.75 IN. (400 MM)	HS20/HS25 - SEE SPEC FOR COVER REQUIREMENTS
HEIGHT = 9.45 IN. (240 MM)	MATERIAL:
TANK VOLUME = 2.42 CF	100% RECYCLED POLYPROPYLENE
STORAGE VOLUME = 2.30 CF	SMALL PLATES REQUIRED:
VOID INTERNAL VOLUME: 95%	5/SEGMENT, 5/MODULE
VOID SURFACE AREA: 90%	

SINGLE R-TANK^{SD} - MODULE DETAIL

TOTAL COVER: 18" MINIMUM AND 9.99' MAXIMUM. FIRST 12" MUST BE FREE DRAINING BACKFILL (SPEC SECTION 2.03B): STONE <1.5" OR SOIL (USCS CLASS GW, GP, SW OR SP). ADDITIONAL FILL MAY BE STRUCTURAL FILL (SPEC SECTION 2.03C): STONE OR SOIL (USCS CLASS SM, SP, SW, GM, GP OR GW) WITH MAX CLAY CONTENT<10%, MAX 25% PASSING NO. 200 SIEVE, AND MAX PLASTICITY INDEX OF 4. A MIN. 12" COVER MUST BE MAINTAINED BETWEEN BACKFILL EQUIPMENT AND THE TOP OF THE R-TANK™ SYSTEM AT ALL TIMES. TOTAL HEIGHT OF TOP BACKFILL SHOULD NOT EXCEED 9.99'. CONTACT FERGUSON WATERWORKS IF MORE THAN 9.99' OR LESS THAN 18" OF TOP BACKFILL IS REQUIRED (FROM TOP OF TANK TO TOP OF PAVEMENT).

NOTES:

- FOR COMPLETE MODULE DATA, SEE APPROPRIATE R-TANK^{SD} MODULE SHEET.
- INSTALLATIONS PER THIS DETAIL MEET GUIDELINES OF HL-93 LOADING PER THE AASHTO LRFD BRIDGE DESIGN SPECIFICATIONS, CUSTOMARY U.S. UNITS, 7TH EDITION, 2014 WITH 2015 AND 2016 INTERIM REVISIONS.
- PRE-TREATMENT STRUCTURES NOT SHOWN.
- FOR INFILTRATION APPLICATIONS, GEOTEXTILE ENVELOPING R-TANK SHALL BE ACF M200 (PER SPEC SECTION 2.02A) AND BASE SHALL BE 4" MIN. UNCOMPACTED FREE DRAINING BACKFILL (SPEC SECTION 2.03A) TO PROVIDE A LEVEL BASE. SURFACE MUST BE SMOOTH, FREE OF LUMPS OR DEBRIS, AND EXTEND 2' BEYOND R-TANK^{SD} FOOTPRINT.

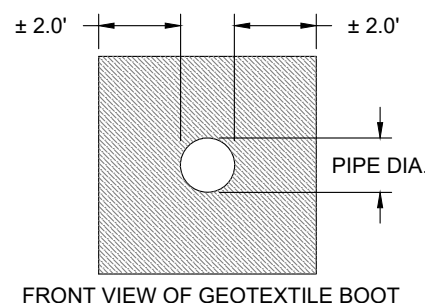


R-TANK^{SD} & HS-20 LOADS - SECTION VIEW

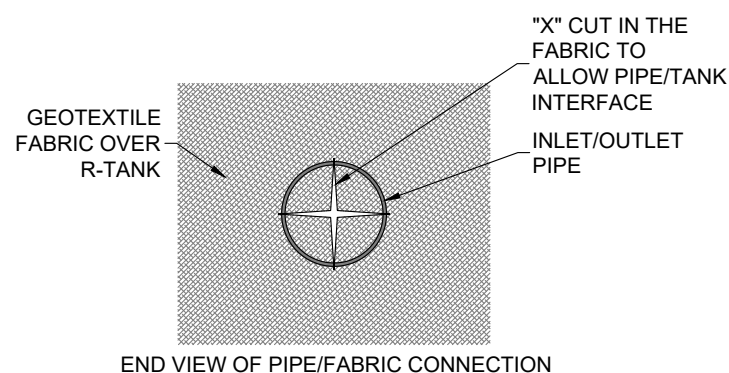
NOTE:

- PIPE BOOTS ARE AVAILABLE IN THE FOLLOWING STANDARD SIZES: 8" | 12" | 15" | 18" | 24".
- LARGER SPECIAL ORDER, CUSTOM SIZES ARE AVAILABLE.

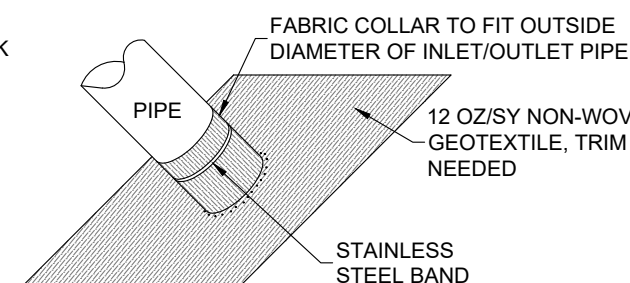
CUT AN "X" IN THE FABRIC ENVELOPE THAT IS SLIGHTLY LARGER THAN THE PIPE. PULL THE FABRIC FLAPS AROUND THE PIPE, AND SEAL WITH A STAINLESS STEEL BAND.



FRONT VIEW OF GEOTEXTILE BOOT

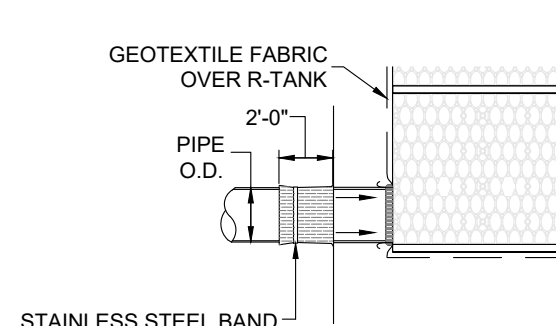


END VIEW OF PIPE/FABRIC CONNECTION

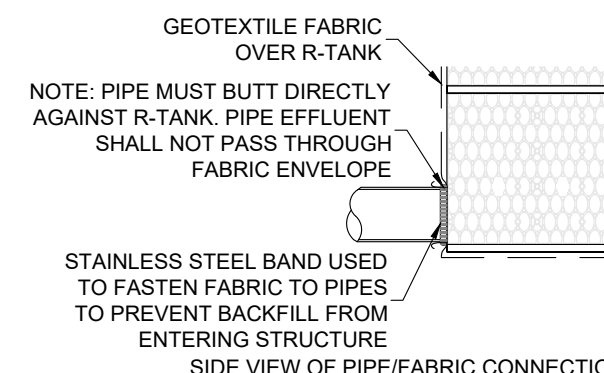


GEOTEXTILE BOOT

AFTER TANK WRAP IS SECURED TO PIPE, SLIDE BOOT AGAINST R-TANK AND SECURE WITH SECOND STAINLESS STEEL BAND, THEN ATTACH BOOT FLAP TO TANK ENVELOPE FABRIC WITH DUCT TAPE OR OTHER ADHESIVE.



SIDE VIEW OF GEOTEXTILE BOOT



SIDE VIEW OF PIPE/FABRIC CONNECTION

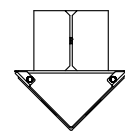
R-TANK TYPICAL TANK INLET/OUTLET W/ GEOTEXTILE PIPE BOOT DETAIL



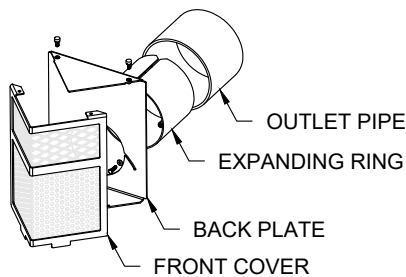
FERGUSON
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R-TANK^{SD} SYSTEM DETAILS
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

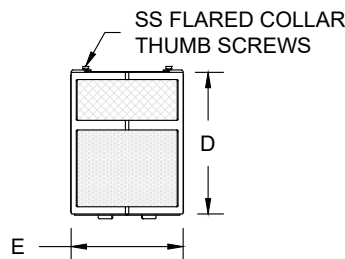
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DATE
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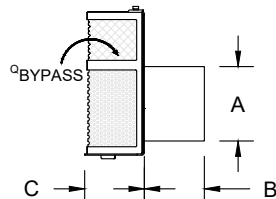
PLAN VIEW



REFERENCE VIEW



FRONT VIEW



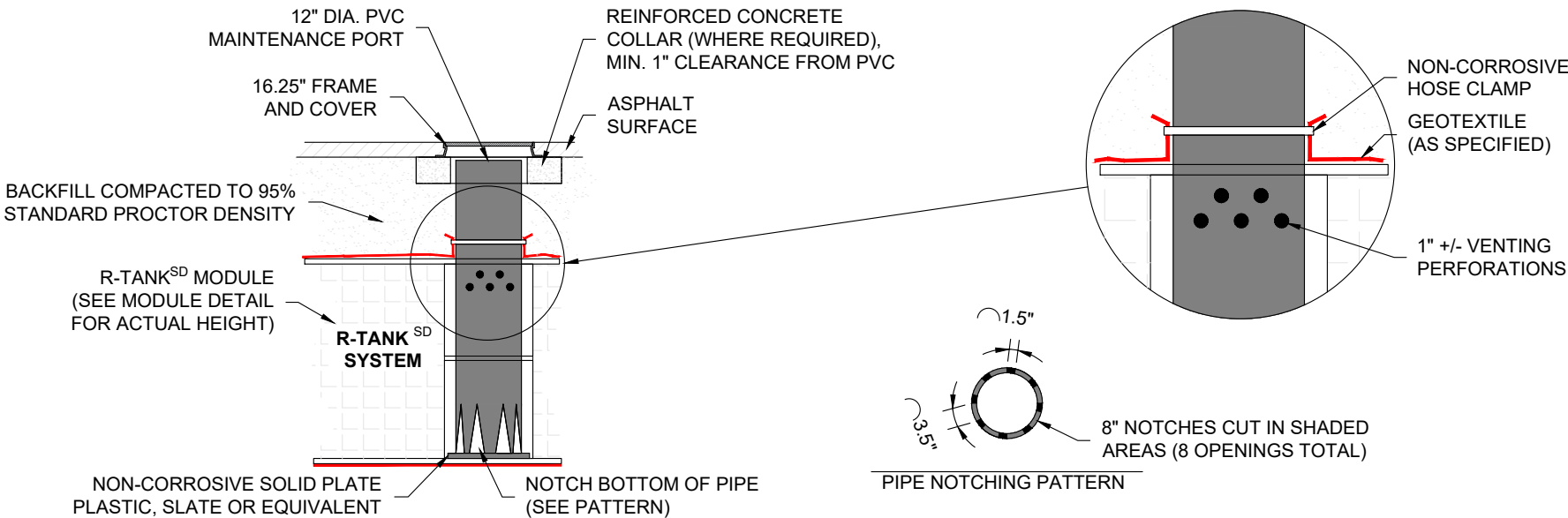
SIDE VIEW

PIPE DIA. (A)	STUB LENGTH (B)	CPS DEPTH (C)	CPS HEIGHT (D)	CPS WIDTH (E)
6"	4.00"	8.50"	10.00"	10.00"
8"	6.00"	11.00"	12.25"	11.50"
10"	8.00"	16.00"	13.50"	13.50"
12"	8.00"	16.00"	15.50"	15.50"
15"	8.00"	16.00"	21.50"	18.50"
18"	8.00"	16.00"	28.00"	21.50"
24"	10.00"	18.00"	40.00"	28.00"

STORMRING CPS PRETREATMENT DETAIL

NOTES

1. THIS PORT IS USED TO PUMP WATER INTO THE SYSTEM AND RE-SUSPEND ACCUMULATED SEDIMENT SO THAT IT MAY BE PUMPED OUT.
2. MINIMUM REQUIRED MAINTENANCE INCLUDES A QUARTERLY INSPECTION DURING THE FIRST YEAR OF OPERATION AND A YEARLY INSPECTION THEREAFTER. FLUSH AS NEEDED.
3. R-TANK^{HD}, R-TANK^{SD}, R-TANK^{UD} AND R-TANK^{XD} MAY BE USED IN TRAFFIC APPLICATIONS.
4. SEE TRAFFIC LOADING DETAIL FOR MINIMUM & MAXIMUM COVER REQUIREMENTS.
5. IF MAINTENANCE PORT IS LOCATED IN A NON-TRAFFIC AREA, A PLASTIC CAP CAN BE USED IN LIEU OF A FRAME AND COVER WITH CONCRETE COLLAR.



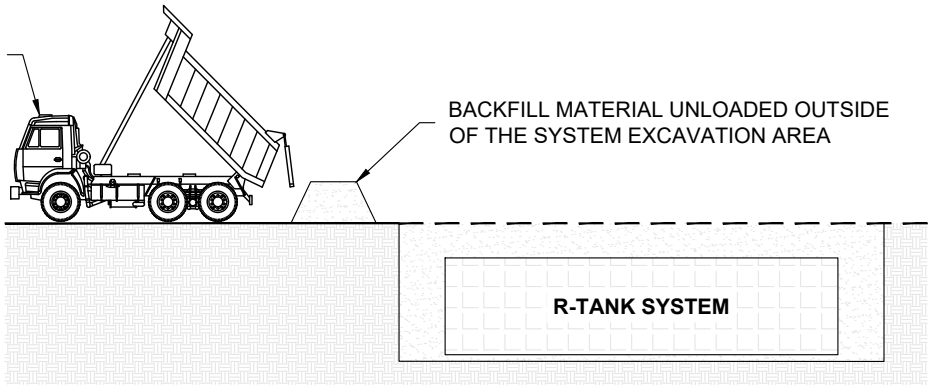
R-TANK^{SD} TYPICAL MAINTENANCE PORT



R-TANK^{SD} SYSTEM DETAILS
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

SCALE
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01/29/2024
SHEET NO.

DUMP TRUCKS AND PANS SHALL NOT OPERATE OVER THE SYSTEM EXCAVATION AREA



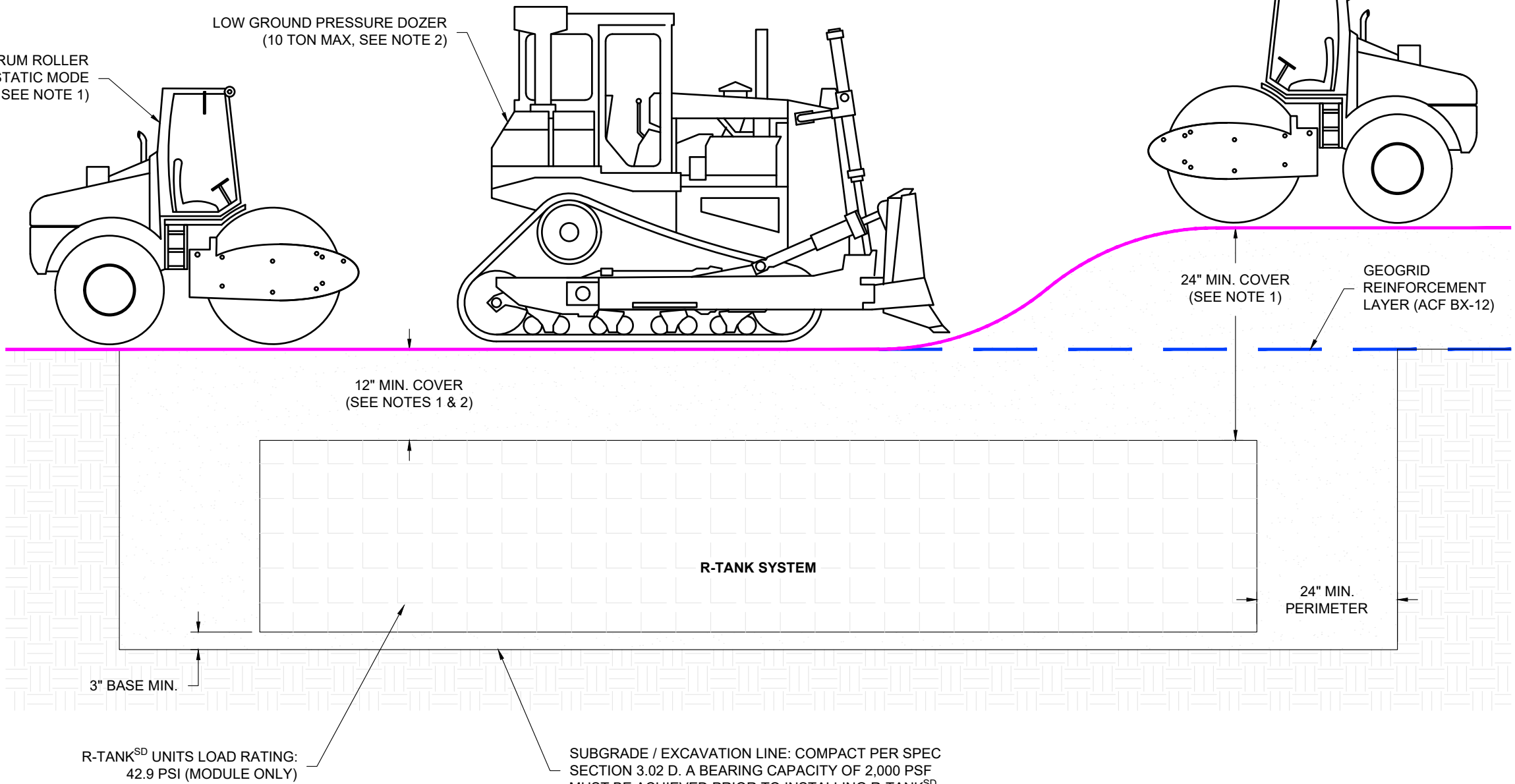
DUMP TRUCK DETAIL (SEE NOTE 3)

- NOTES:
1. FOLLOWING PLACEMENT OF SIDE BACKFILL, A UNIFORM 12" LIFT OF THE FREELY DRAINING MATERIAL (SPEC SECTION 2.03 B2) SHALL BE PLACED OVER THE R-TANK AND LIGHTLY COMPACTED USING A WALK-BEHIND TRENCH ROLLER. ALTERNATELY, A ROLLER (MAXIMUM GROSS VEHICLE WEIGHT OF 6 TONS) MAY BE USED. ROLLER MUST REMAIN IN STATIC MODE UNTIL A MINIMUM OF 24" OF COVER HAS BEEN PLACED OVER THE MODULES. SHEEP FOOT ROLLERS SHOULD NOT BE USED. **SPEC SECTION 3.05 A5**
 2. ONLY LOW PRESSURE TIRE OR TRACK VEHICLES (LESS THAN 7 PSI AND OPERATING WEIGHT OF LESS THAN 20,000 LBS) SHALL BE OPERATED OVER THE R-TANK SYSTEM DURING CONSTRUCTION. **SPEC SECTION 3.05 A5**
 3. DUMP TRUCKS AND PANS SHALL NOT BE OPERATED WITHIN THE R-TANK SYSTEM AT ANY TIME. WHERE NECESSARY, THE HEAVY EQUIPMENT SHOULD UNLOAD IN AN AREA ADJACENT TO THE R-TANK SYSTEM AND THE MATERIAL SHOULD BE MOVED OVER THE SYSTEM WITH TRACKED EQUIPMENT. **SPEC SECTION 3.05 A5**
 4. ENSURE THAT ALL UNRELATED CONSTRUCTION TRAFFIC IS KEPT AWAY FROM THE LIMITS OF EXCAVATION UNTIL THE PROJECT IS COMPLETE AND FINAL SURFACE MATERIALS ARE IN PLACE. NO NON-INSTALLATION RELATED LOADING SHOULD BE ALLOWED OVER THE R-TANK SYSTEM UNTIL THE FINAL DESIGN SECTION HAS BEEN CONSTRUCTED (INCLUDING PAVEMENT). **SPEC SECTION 3.05 B**
 5. SEE R-TANK INSTALLATION GUIDE OR CONTACT YOUR LOCAL FERGUSON REPRESENTATIVE FOR ADDITIONAL INFORMATION.

SMOOTH DRUM ROLLER
STATIC MODE
(6 TON MAX, SEE NOTE 1)

LOW GROUND PRESSURE DOZER
(10 TON MAX, SEE NOTE 2)

SMOOTH DRUM ROLLER
VIBRATORY MODE
(6 TON MAX, SEE NOTE 1)



CONSTRUCTION EQUIPMENT COVER DETAIL - VEHICULAR TRAFFIC



ENGINEER OF RECORD TO REVIEW, APPROVE AND
ENDORSE FINAL SITE SPECIFIC DESIGN.



FOR ADDITIONAL INFORMATION PLEASE CONTACT:
FERGUSON WATERWORKS,
1-800-448-3636, www.ferguson.com

R-TANK^{SD} CONSTRUCTION EQUIPMENT
COVER DETAIL
RUSTY LANTERN CONVENIENCE STORE
CUMBERLAND, ME

SCALE
NTS

DRAWN BY
BMK

DATE
01/29/2024

SHEET NO.

R-TANK SPECIFICATION

PART 1 - GENERAL

1.01 RELATED DOCUMENTS

- A. Drawings, technical specification and general provisions of the Contract as modified herein apply to this section.

1.02 DESCRIPTION OF WORK INCLUDED

- A. Provide excavation and base preparation per geotechnical engineer's recommendations and/or as shown on the design drawings, to provide adequate support for project design loads and safety from excavation sidewall collapse. Excavations shall be in accordance with the owner's and OSHA requirements.
- B. Provide and install R-TankLD/, R-TankHD/, R-TankSD/, or R-TankUD/ system (hereafter called R-Tank) and all related products including fill materials, geotextiles, geogrids, inlet and outlet pipe with connections per the manufacturer's installation guidelines provided in this section.
- C. Provide and construct the cover of the R-Tank system including; stone backfill, structural fill cover, and pavement section as specified.
- D. Protect R-Tank system from construction traffic after installation until completion of all construction activity in the installation area.

1.03 QUALITY CONTROL

- A. All materials shall be manufactured in ISO certified facilities.
- B. Installation Contractor shall demonstrate the following experience:
1. A minimum of three R-Tank or equivalent projects completed within 2 years; and,
2. A minimum of 25,000 cubic feet of storage volume completed within 2 years.
3. Contractor experience requirement may be waived if the manufacturer's representative provides on-site training and review during construction.
- C. Installation Personnel: Performed only by skilled workers with satisfactory record of performance on bulk earthworks, pipe, chamber, or pond/landfill construction projects of comparable size and quality.
- D. Contractor must have manufacturer's representative available for site review if requested by Owner.

1.04 SUBMITTALS

- A. Submit proposed R-Tank layout drawings. Drawings shall include typical section details as well as the required base elevation of stone and tanks, minimum cover requirements and tank configuration.
- B. Submit manufacturer's product data, including compressive strength and unit weight.
- C. Submit manufacturer's installation instructions.
- D. Submit R-Tank sample for review. Reviewed and accepted samples will be returned to the Contractor.
- E. Submit material certificates for geotextile, geogrid, base course and backfill materials.
- F. Submit required experience and personnel requirements as specified in Section 1.03.
- G. Any proposed equal alternative product substitution to this specification must be submitted for review and approved prior to bid opening. Review package should include third party reviewed performance data that meets or exceeds criteria in Table 2.01 B.

1.05 DELIVERY, STORAGE, AND HANDLING

- A. Protect R-Tank and other materials from damage during delivery, and store UV sensitive materials under tarp to protect from sunlight when time from delivery to installation exceeds two weeks. Storage of materials should be on smooth surfaces, free from dirt, mud and debris.
- B. Handling is to be performed with equipment appropriate to the materials and site conditions, and may include hand, handcart, forklifts, extension lifts, etc.
- C. Cold weather:
1. Care must be taken when handling plastics when air temperature is 40 degrees or below as plastic becomes brittle.
2. Do not use frozen materials or materials mixed or coated with ice or frost.
3. Do not build on frozen ground or wet, saturated or muddy subgrade.

1.06 PREINSTALLATION CONFERENCE.

- A. Prior to the start of the installation, a preinstallation conference shall occur with the representatives from the design team, the general contractor, the excavation contractor, the R-Tank installation contractor, and the manufacturer's representative.

1.07 PROJECT CONDITIONS

- A. Coordinate installation for the R-Tank system with other on-site activities to eliminate all non-installation related construction traffic over the completed R-Tank system. No loads heavier than the design loads shall be allowed over the system, and in no case shall loads higher than a standard AASHTO HS20 (or HS25, depending on design criteria) load be allowed on the system at any time.
- B. Protect adjacent work from damage during R-Tank system installation.
- C. All pre-treatment systems to remove debris and heavy sediments must be in place and functional prior to operation of the R-Tank system. Additional pretreatment measures may be needed if unit is operational during construction due to increased sediment loads.
- D. Contractor is responsible for any damage to the system during construction.

PART 2 - PRODUCTS

2.01 R-TANK UNITS

- A. R-Tank - Injection molded plastic tank plates assembled to form a 95% void modular structure of predesigned height (custom for each project).
- B. R-Tank units shall meet the following Physical & Chemical Characteristics:

PROPERTY	DESCRIPTION	R-Tank ^{LD} VALUE	R-Tank ^{HD} VALUE	R-Tank ^{SD} VALUE	R-Tank ^{UD} VALUE
Void Area	Volume available for water storage	95%	95%	95%	95%
Surface Void Area	Percentage of exterior available for infiltration	90%	90%	90%	90%
Vertical Compressive Strength	ASTM D 2412 / ASTM F 2418	30.0 psi	33.4 psi	42.9 psi	134.2 psi
Lateral Compressive Strength	ASTM D 2412 / ASTM F 2418	20.0 psi	22.4 psi	28.9 psi	N/A
HS-20 Minimum Cover	Cover required to support HS-20 loads	N/A	20"	18"	12" (STONE BACKFILL)
HS-25 Minimum Cover	Cover required to support HS-25 loads	N/A	24"	19"	15" (STONE BACKFILL)
Maximum Cover	Maximum allowable cover depth	3 feet	< 7 feet	< 10 feet	5 feet
Unit Weight	Weight of plastic per cubic foot of tank	3.29 lbs / cf	3.62 lbs/cf	3.96 lbs / cf	4.33 lbs / cf
Rib Thickness	Thickness of load-bearing members	0.18 inches	0.18 inches	0.18 inches	N/A
Service Temperature	Safe temperature range for use	-14 – 167° F	-14 – 167° F	-14 – 167° F	-14 – 167° F

- C. Supplier: Ferguson Waterworks 2831 Cardwell Road Richmond, VA 23234 (T): 800-448-3636; (F): 804-743-7779 www.ferguson.com

2.02 GEOSYNTHETICS

- A. Geotextile. A geotextile envelope is required to prevent backfill material from entering the R-Tank modules.
1. Standard Application: The standard geotextile shall be an 8 oz per square yard nonwoven geotextile (ACF N080 or equivalent).
2. Infiltration Applications: When water must infiltrate/exfiltrate through the geotextile as a function of the system design, a woven monofilament (ACF M200 or equivalent) shall be used.
- B. Geogrid. For installations subject to traffic loads and/or when required by project plans, install geogrid (ACF BX12 or equivalent) to reinforce backfill above the R-Tank system. Geogrid is not always required for R-TankUD/ installations, and is often not required for non-traffic load applications.

2.03 BACKFILL & COVER MATERIALS

- A. Bedding Materials: Stone (angular and smaller than 1.5" in diameter) or soil (GW, GP, SW, or SP as classified by the Unified Soil Classification System) shall be used below the R-Tank system (3" minimum). Material must be free from lumps, debris, and any sharp objects that could cut the geotextile. Material shall be within 3 percent of the optimum moisture content as determined by ASTM D698 at the time of installation. For infiltration applications bedding material shall be free draining.
- B. Side and Top Backfill: Material must be free from lumps, debris and any sharp objects that could cut the geotextile. Material shall be within 3 percent of the optimum moisture content as determined by ASTM D698 at the time of installation.
1. Traffic Applications - Free draining material shall be used adjacent to (24" minimum) and above (for the first 12") the R-Tank system.
- a. For HD, and SD modules, backfill materials shall be free draining stone (angular and smaller than 1.5" in diameter) or soil (GW, GP, SW, or SP as classified by the Unified Soil Classification System).
- b. For UD modules with less than 14" of top cover, backfill materials shall be free draining stone (angular and smaller than 1.5" in diameter). The use of soil backfill on the sides and top of the UD module is not permitted unless the modules are installed outside of traffic areas or with cover depths of 14" or more. Top backfill material (from top of module to bottom of pavement base or 12" maximum) must be consistent with side backfill.
2. Non-Traffic / Green Space Applications - For all R-Tank modules installed in green spaces and not subjected to vehicular loads, backfill materials may either follow the guidelines for Traffic Applications above, or the top backfill layer (12" minimum) may consist of AASHTO #57 stone blended with 30-40% (by volume) topsoil to aid in establishing vegetation.
- C. Additional Cover Materials: Structural Fill shall consist of granular materials meeting the gradational requirements of SM, SP, SW, GM, GP or GW as classified by the Unified Soil Classification System. Structural fill shall have a maximum of 25 percent passing the No. 200 sieve, shall have a maximum clay content of 10 percent and a maximum Plasticity Index of 4. Material shall be within 3 percent of the optimum moisture content as determined by ASTM D698 at the time of installation.

2.04 OTHER MATERIALS

- A. Utility Marker: Install metallic tape at corners of R-Tank system to mark the area for future utility detection.

PART 3 - EXECUTION

3.01 ASSEMBLY OF R-TANK UNITS

- A. Assembly of modules shall be performed in accordance with the R-Tank Installation Manual, Section 2.

3.02 LAYOUT AND EXCAVATION

- A. Installer shall stake out, excavate, and prepare the subgrade area to the required plan grades and dimensions, ensuring that the excavation is at least 2 feet greater than R-Tank dimensions in each direction allowing for installation of geotextile filter fabric, R-Tank modules, and free draining backfill materials.
- B. All excavations must be prepared with OSHA approved excavated sides and sufficient working space.
- C. Protect partially completed installation against damage from other construction traffic by establishing a perimeter with high visibility construction tape, fencing, barricades, or other means until construction is complete.
- D. Base of the excavation shall be uniform, level, and free of lumps or debris and soft or yielding subgrade areas. A minimum 2,000 pounds per square foot bearing capacity is required.
1. Standard Applications: Compact subgrade to a minimum of 95% of Standard Proctor (ASTM D698) density or as required by the Owner's engineer.
2. Infiltration Applications: Subgrade shall be prepared in accordance with the contract documents. Compaction of subgrade should not be performed in infiltration applications.
- E. Unsuitable Soils or Conditions: All questions about the base of the excavation shall be directed to the owner's engineer, who will approve the subgrade conditions prior to placement of stone. The owner's engineer shall determine the required bearing capacity of the R-Tank subgrade; however in no case shall a bearing capacity of less than 2,000 pounds per square foot be provided.
1. If unsuitable soils are encountered at the subgrade, or if the subgrade is pumping or appears excessively soft, repair the area in accordance with contract documents and/or as directed by the owner's engineer.
2. If indications of the water table are observed during excavation, the engineer shall be contacted to provide recommendations.
3. Do not start installation of the R-Tank system until unsatisfactory subgrade conditions are corrected and the subgrade conditions are accepted by the owner's engineer.

3.03 PREPARATION OF BASE

- A. Place a thin layer (3" unless otherwise specified) of bedding material (Section 2.03 A), over the subgrade to establish a level working platform for the R-Tank modules. Level to within 1/8" (+/- 1/4") or as shown on the plans. Native subgrade soils or other materials may be used if determined to meet the requirements of 2.03 A and are accepted by the owner's engineer.
1. Standard Applications: Static roll or otherwise compact bedding materials until they are firm and unyielding.
2. Infiltration Applications: Bedding materials shall be prepared in accordance with the contract documents.
- B. Outline the footprint of the R-Tank system on the excavation floor using spray paint or chalk line to ensure a 2' perimeter is available around the R-Tank system for proper installation and compaction of backfill.

3.04 INSTALLATION OF THE R-TANKS

- A. Where a geotextile wrap is specified on the stone base, cut strips to length and install in excavation, removing wrinkles so material lays flat. Overlap geotextile a minimum 12" or as recommended by manufacturer. Use tape, special adhesives, sandbags or other ballast to secure overlaps. As geotextiles can be damaged by extreme heat, smoking is not permissible on/near the geotextile, and tools using a flame to tack the overlaps, such as propane torches, are prohibited.
- B. Where an impervious liner (for containment) is specified, install the liner per manufacturer's recommendations and the contract documents. The R-Tank units shall be separated from impervious liner by a non-woven geotextile fabric installed accordance with Section 3.04A.
- C. Install R-Tank modules by placing side by side, in accordance with the design drawings. No lateral connections are required. It is advisable to use a string line to form square corners and straight edges along the perimeter of the R-Tank system. The modules are to be oriented as per the design drawing with required depth as shown on plans.
1. For LD, HD, and SD installations, the large side plate of the tank should be placed on the perimeter of the system. This will typically require that the two ends of the tank area will have a row of tanks placed perpendicular to all other tanks. If this is not shown in the construction drawings, it is a simple field adjustment that will have minimal effect on the overall system footprint. Refer to R-Tank Installation Guide for more details
2. For UD installations, there is no perpendicular end row required.
- D. Wrap the R-Tank top and sides in specified geotextile. Cut strips of geotextile so that it will cover the sides and top, encapsulating the entire system to prevent backfill entry into the system. Overlap geotextile 12" or as recommended by manufacturer. Take great care to avoid damage to geotextile (and, if specified, impervious liner) during placement.
- E. Identify locations of inlet, outlet and any other penetrations of the geotextile (and optional liner). These connections should be installed flush (buted up to the R-Tank) and the geotextile fabric shall be cut to enable hydraulic continuity between the connections and the R-Tank units. These connections shall be secured using pipe boots with stainless steel pipe clamps. Support pipe in trenches during backfill operations to prevent pipe from settling and damaging the geotextile, impervious liner (if specified) or pipe. Connecting pipes at 90 degree angles facilitates construction, unless otherwise specified. Ensure end of pipe is installed snug against R-Tank system.
- F. Install Inspection and Maintenance Ports in locations noted on plans. At a minimum one maintenance port shall be installed within 10' of each inlet & outlet connection, and with a maximum spacing of one maintenance port for every 2,500 square feet. Install all ports as noted in the R-Tank Installation Guide.
- G. If required, install ventilation pipes and vents as specified on drawings to provide ventilation for proper hydraulic performance. The number of pipes and vents will depend on the size of the system. Vents are often installed using a 90 degree elbow with PVC pipe into a landscaped area with "U" bend or venting bollard to inhibit the ingress of debris. A ground level concrete or steel cover can be used.

3.05 BACKFILLING OF THE R-TANK UNITS

- A. Backfill and fill with recommended materials as follows:
1. Place freely draining backfill materials (Section 2.03 B) around the perimeter in lifts with a maximum thickness of 12". Each lift shall be placed around the entire perimeter such that each lift is no more than 24" higher than the side backfill along any other location on the perimeter of the R-Tank system. No fill shall be placed over top of tanks until the side backfill has been completed.
2. Each lift shall be compacted at the specified moisture content to a minimum of 95% of the Standard Proctor Density until no further densification is observed (for self-compacting stone materials). The side lifts must be compacted with walk behind compaction equipment. Even when "self-compacting" backfill materials are selected, a walk behind vibratory compactor must be used.
3. Take care to ensure that the compaction process does not allow the machinery to come into contact with the modules due to the potential for damage to the geotextile and R-Tank units.
4. No compaction equipment is permissible to operate directly on the R-Tank modules.
5. Top Backfill: Only low pressure track vehicles shall be operated over the R-Tank system during construction. Dump Trucks and Pans shall not be operated within the R-Tank system footprint at any time. Heavy equipment should unload in an area adjacent to the R-Tank system and the material should be moved over the system using tracked equipment with an operating weight of less than 10 tons.
- a. Typical Applications: Install a 12" (or as shown on plans) lift of freely draining material (Section 2.03 B) over the R-Tank Units, maintaining 12" between equipment tracks and R-Tank System. Lightly compacted using a walk-behind trench roller. Alternately, a roller (maximum gross vehicle weight of 6 tons) may be used. Roller must remain in static mode until a minimum of 24" of cover has been placed over the modules. Sheep foot rollers should not be used.
- b. Shallow Applications (< 18" total cover): Install top backfill in accordance with plans.
6. If required, install a geogrid as shown on plans. Geogrid shall extend a minimum of 3 feet beyond the limits of the excavation wall.
7. Following placement and compaction of the initial cover, subsequent lifts of structural fill (Section 2.03 C) shall be placed at the specified moisture content and compacted to a minimum of 95% of the Standard Proctor Density and shall cover the entire footprint of the R-Tank system. During placement of fill above the system, unless otherwise specified, a uniform elevation of fill shall be maintained to within 12" across the footprint of the R-Tank system. Do not exceed maximum cover depths listed in Table 2.01 B.
8. Place additional layers of geotextile and/or geogrid at elevations as specified in the design details. Each layer of geosynthetic reinforcement placed above the R-Tank system shall extend a minimum of 3 feet beyond the limits of the excavation wall.
- B. Ensure that all unrelated construction traffic is kept away from the limits of excavation until the project is complete and final surface materials are in place. No non-installation related loading should be allowed over the R-Tank system until the final design section has been constructed (including pavement).
- C. Place surfacing materials, such as groundcovers (no large trees), or paving materials over the structure with care to avoid displacement of cover fill and damage to surrounding areas.
- D. Backfill depth over R-Tank system must be within the limitations shown in the table in Section 2.01 B. If the total backfill depth does not comply with this table, contact engineer or manufacturer's representative for assistance.

3.06 MAINTENANCE REQUIREMENTS

- A. A routine maintenance effort is required to ensure proper performance of the R-Tank system. The Maintenance program should be focused on pretreatment systems. Ensuring these structures are clean and functioning properly will reduce the risk of contamination of the R-Tank system and stormwater released from the site. Pre-treatment systems shall be inspected yearly, or as directed by the regulatory agency and by the manufacturer (for proprietary systems). Maintain as needed using acceptable practices or following manufacturer's guidelines (for proprietary systems).
- B. All inlet pipes and Inspection and/or Maintenance Ports in the R-Tank system will need to be inspected for accumulation of sediments at least quarterly through the first year of operation and at least yearly thereafter.
- C. If sediment has accumulated to the level noted in the R-Tank Maintenance Guide or beyond a level acceptable to the Owner's engineer, the R-Tank system should be flushed.
- D. All inspection and maintenance activities should be performed in accordance with the R-Tank Operation, Inspection & Maintenance Manual.



ENGINEER OF RECORD TO REVIEW, APPROVE AND ENDORSE FINAL SITE SPECIFIC DESIGN.



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